

**TWO-STAGE FAN
IV. PERFORMANCE DATA FOR STATOR SETTING ANGLE OPTIMIZATION**

by
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16. Abstract <p>Stator setting angle optimization tests were conducted on a two-stage fan to improve efficiency at overspeed, stall margin at design speed, and both efficiency and stall margin at partspeed. The fan has a design pressure ratio of 2.8, a flow rate of 184.2 lb/sec (83.55 kg/sec) and a 1st-stage rotor tip speed of 1450 ft/sec (441.96 in/sec). Performance was obtained at 70, 100, and 105 percent of design speed with different combinations of 1st-stage and 2nd-stage stator settings. One combination of settings, other than design, was common to all three speeds. At design speed, a 2.0 percentage point increase in stall margin was obtained at the expense of a 1.3 percentage point efficiency decrease. At 105 percent speed, efficiency was improved by 1.8 percentage points but stall margin decreased 4.7 percentage points. At 70 percent speed, no change in stall margin or operating line efficiency was obtained with stator resets although considerable speed-flow regulation occurred.</p>					
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FOREWORD

This report was prepared for the National Aeronautics and Space Administration, Lewis Research Center, under Contract NAS3-13494 to present data and performance of a two-stage fan tested to determine the optimum stator stagger angle. During this effort Mr. R. S. Ruggeri was the NASA Project Manager and Mr. H. V. Marman was the P&WA Program Manager. This report was prepared by G. Burger and M. J. Keenan, with contributions from B. Gray, T. Hodges, A. Merrow, J. Rawlins, A. Finke, and other Pratt & Whitney Aircraft personnel.

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TWO-STAGE FAN

IV. PERFORMANCE DATA FOR STATOR SETTING ANGLE OPTIMIZATION

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SUMMARY

Stator setting angle optimization tests were conducted on a two-stage fan designed for a tip speed of 1450 ft/sec [441.96 m/sec], an overall pressure ratio of 2.8, and a corrected flow of 184.2 lbm/sec [83.55 kg/sec]. The tests were conducted to determine the effects of changes in stator settings on fan performance in terms of overall fan efficiency and stall margin and to help define which blade elements were critical in setting the fan stall line. Detailed aerodynamic performance of the fan was obtained at 70 percent, 100 percent, and 105 percent of design speed with four to six different combinations of stator settings at each speed. Earlier tests had documented the performance of the fan with stators in their design positions. One combination of stator settings, besides design, was common to all three speeds to permit investigation of speed effects on performance.

At design speed the objective of the stator angle optimization was to improve stall margin with a minimum penalty in efficiency. Tests with design stator-settings showed that at design speed and pressure ratio all blade elements were sufficiently close to minimum loss to make gains in efficiency improbable. Stall margin was improved at the expense of operating line efficiency by closing the 2nd-stage stator (reset in a direction to reduce incidence). The optimum configuration tested at design speed was with the 1st-stage stator set at its design stagger angle and the 2nd-stage stator closed 5 degrees. This combination of stator settings gave an operating line overall fan efficiency of 83.7% with a corresponding 14.0% stall margin, representing a 2.0% increase in stall margin and a 1.3 percentage point decrease in operating line efficiency compared to design settings. Overall fan pressure ratio at stall with this stator setting combination was lower than with the design setting configuration, but the increased flow range provided an increase in stall margin.

The objective of the stator angle optimization at 105 percent speed was to increase efficiency with a minimum stall margin penalty. The optimum configuration tested at this speed was with the 1st-stage stator closed 2.5 degrees and the 2nd-stage stator opened 2.5 degrees. A gain of 1.8 percentage points in efficiency was obtained while stall margin decreased 4.7 percentage points. Most of the efficiency benefit was gained by the improved 2nd-stage stator recovery at the 2.5-degree open setting.

The objective of the stator angle optimization at 70 percent speed was to improve both efficiency and stall margin. During testing, overall fan pressure ratio was increased by opening the 1st-stage stator, due to increased work input from the 2nd-stage rotor; however, changes in stall margin and efficiency were small. Considerable flow regulation occurred with variations of both stator settings. The tip region of the first stage was the most highly loaded area regardless of stator setting and was probably the cause of stall at 70 percent speed.

The configuration with the 5-degree closed 1st-stage stator and the 2.5-degree opened 2nd-stage stator was common to all three speeds. The overall fan pressure ratio was reduced at all speeds due to the closed 1st-stage stator which reduced the work input from the 2nd-stage rotor. Operating line overall efficiency of the fan was unchanged at 70 percent and 100 percent speeds but was improved by 1.5 percentage points at 105 percent speed. The speed-flow modulation obtained at 70 percent speed was small at design speed and not evident at 105 percent speed. At 105 percent speed, the 1st-stage pressure ratios were higher along a very steep speedline with this stator reset, and efficiency was increased by two percentage points. First-stage pressure ratios and efficiencies were essentially unchanged at 70 percent and 100 percent speeds.

Studies were made of possible benefits of using a variable flap inlet-guide-vane in conjunction with the existing variable stators at 70 percent and 110 percent of design speed. These studies showed a probable benefit in stall margin of approximately nine percentage points at 70 percent speed with the inlet-guide-vane flap in a position to reduce the incidence and loadings of the 1st-stage rotor. A small reduction in overall fan efficiency could occur due to the inlet-guide-vane losses. No stall margin or efficiency benefit was predicted for 110 percent speed. With the inlet-guide-vane flap positioned to increase the work input and loading of the 1st-stage rotor, radial distributions of flow cause loading limits to be encountered at the hub of the 1st- and 2nd-stage rotors and the 2nd-stage stator at approximately the same flow where the loading limits of the 2nd-stage hub were predicted without an inlet-guide-vane.

INTRODUCTION

An extensive program has been conducted by NASA on high speed, high-loading, single-stage fans. Based on demonstrations of good performance at high speeds and loadings in single stages, a two-stage, highly-loaded, high speed fan was designed, fabricated, and tested. The objectives of the two-stage fan program were to evaluate the stage matching problems, distortion tolerance, response to stator adjustment, and effectiveness of casing treatment for such a fan. Design tip speed for the two-stage fan was 1450 ft/sec [441.96 m/sec]; design pressure ratio was 2.8; tip diameter was 31.0 inches [0.787 m] at the inlet of the 1st-stage rotor; design corrected flow was 184.2 lbm/sec [83.55 kg/sec]; and the hub-tip ratio was 0.4. Details of the aerodynamic and mechanical designs are given in Reference 1.

Good aerodynamic performance was documented during the first test of this two-stage fan. At design speed and pressure ratio, the measured flow closely matched the design value; the efficiency was 85.7%, exceeding the design goal of 83.9%; and the stall margin was 10%. Measured rotor losses were about equal to the design values, but stator losses were less than the design values. The first test was abbreviated due to flutter on the 2nd-stage rotor blades and cracking of the root leading edges of some stator vanes. Failure of one 1st-stage stator vane root leading edge has been attributed to a locally thin section, and failure of one 2nd-stage vane has been attributed to a stress concentration resulting from a brazed-on leading edge sensor. Results of the first test are reported in detail in Reference 2.

The blades for the 2nd-stage rotor were redesigned with partspan shrouds to eliminate flutter, and the fan was rebuilt with these redesigned rotor blades. In addition, a sufficient number of 1st-stage stator vanes were fabricated to insure that all vanes in the rebuild would meet design thickness specifications. Stator leading edge pressure sensors were not used in the rebuild in order to avoid stress concentrations and because the data from the first build showed that the stator discharge instrumentation provides the same information with good accuracy. Design details of the 2nd-stage rotor with the partspan shroud are given in Reference 3.

Tests of the modified two-stage fan were run with uniform inlet flow, tip-radial, hub-radial, and circumferential inlet distortion to document performance with stators in the design positions relative to the air stream. Results of these tests are reported in detail in Reference 3.

This report presents the results of a stator optimization program to obtain increased overall fan efficiency or stall margin. Each stator was capable of being reset in 2.5-degree increments. The 2nd-stage stator was capable of being reset from 10 degrees open to 10 degrees closed. The 1st-stage stator was capable of being reset 10 degrees closed, but axial spacing limited opening this stator to 5 degrees from the design position. Tests were conducted at 70, 100, and 105 percent of design speed with four to six different combinations of stator settings at each speed. Results of these tests are presented separately for each speed to clarify the effects of the stator positions. One stator reset configuration common to all three speeds (1st-stage stator closed 5 degrees, 2nd-stage stator open 2.5 degrees) is analyzed for speed effects on performance. The baseline performance data with design stator-settings presented in this report were taken during the uniform inlet flow test portion of the program reported in Reference 3. In addition to the test results, an analytical study of the effects of adding an inlet guide to the compressor is presented.

The symbols used in this report and performance parameters are defined in Appendix A.

APPARATUS

AERODYNAMIC DESIGN

The two-stage fan test arrangement is shown schematically in Figure 1, and a detailed description of the aerodynamic and mechanical design of the fan is given in Reference 1. A detailed description of the redesigned 2nd-stage rotor used in this test is given in Reference 3.

Design performance parameters at the design point are summarized in Table I.

TABLE I – DESIGN OVERALL PERFORMANCE PARAMETERS

Corrected Speed: $N/\sqrt{\sigma} = 10720$ rpm - Corrected Flow: $W\sqrt{\theta}/\delta = 184.20$ lbm/sec
 [83.55 kg/sec]

	PRESSURE RATIO		ADIABATIC EFFICIENCY (%)	
	Local	Cumulative	Local	Cumulative
Rotor 1	1.786	1.786	89.4	89.4
Stator 1	.976	1.742	–	85.3
Rotor 2	1.655	2.884	89.9	86.5
Stator 2	.971	2.80	–	83.7

The fan was designed without inlet-guide-vanes (IGV) but with the provision for adding a variable camber IGV at a later date. Stators were designed with the ability for resetting at different stagger angles without requiring removal of the fan from the test stand. Both stators were designed to turn the flow to the axial direction (design position). The tip diameter of the 1st-stage rotor inlet was selected as 31 inches [0.787 m] to permit use of existing hardware and to allow adequate horsepower margin for the drive engine. With a required 1st-stage rotor tip speed of 1450 ft/sec [441.96 m/sec], the design speed corrected to standard inlet conditions was 10,720 rpm. The inlet inner case diameter was held at a minimum of 10 inches [0.254 m] to provide clearance for the front bearing compartment. The specific flow at the inlet to the 1st-stage rotor was set at 42.0 lbm/sec-ft² [205 kg/sec-m²], consistent with advanced fan technology. This, with the specified hub-tip ratio of 0.4 and the chosen tip diameter, yielded a design inlet corrected flow of 184.2 lbm/sec [83.55 kg/sec].

The average Mach number at the fan exit was approximately 0.5, a practical value for thrust augmentation.

Flowpath convergence and wall curvature between inlet and exit were used to control velocity profiles and blade aerodynamic loadings (diffusion factors) near the walls. Design loadings were similar to those for which good single-stage performance has been obtained, as explained in Reference 1.

Blockages were included in the aerodynamic design to account for boundary layer growth on the casing walls and for presence of the rotor partspan shrouds. Boundary layer displacement thickness at the 1st-stage rotor inlet was assumed equal to that measured downstream of inlet bellmouths used in research programs at Pratt & Whitney Aircraft. Growth of the wall displacement thickness through the blade rows of the two-stage fan was estimated using a correlation developed by W. T. Hanley (ref. 4) wherein growth along the casing walls is chiefly a function of wall static pressure gradient. To account for the presence of partspan shrouds, a blockage equal to the percent of total annulus area occupied by the shroud was applied at the exit of each rotor and the inlet of the following stator, and half this amount was used at the inlet of each rotor. No allowance for shroud

blockage was applied at the 1st-stage or 2nd-stage stator exits. Total blockage inputs to the streamline analysis calculation at various axial locations were computed as the sum of end-wall blockages and shroud blockages and were applied equally to all stream tubes.

The axial spacings between rotor and stator of both the 1st-stage and 2nd-stage were held to a minimum, as shown in the flowpath drawing in Figure 2, which is in line with actual engine design practice. A spacing of slightly more than one inch [0.0254 m] was allowed between stages to provide room for radial and tangential traverse instrumentation at the exit of the 1st-stage stator.

Coordinates of blade edges at the hub and tip are given in Figure 2. The differences between the coordinates of the original and redesigned 2nd-stage rotor are due to changes in blade edge location. Flowpath walls were not changed.

Rotor and stator blade sections for both stages of the fan were multiple-circular-arc (MCA) airfoils designed on conical surfaces which approximate stream surfaces of revolution. Blade setting angles were determined from design flow angles and incidence and deviation angle criteria described in Reference 1. Blade chords were chosen to be consistent with moderate axial lengths, acceptable rotor loadings, and structural requirements. Airfoil leading and trailing edge radii and blade thicknesses were chosen to provide mechanical integrity while maintaining adequate flow area. A partspan shroud was located at 61 percent span on the 1st-stage rotor and at 60 percent span on the redesigned 2nd-stage rotor. A view of a rotor and stator for each blade row of the two-stage fan is shown in Figure 3.

Design details of the 1st-stage rotor, the 1st-stage stator, the original 2nd-stage rotor, and the 2nd-stage stator, including manufacturing sections defined on planes normal to the stacking line, are given in Reference 1. Details of the redesigned 2nd-stage rotor are given in Reference 3. A summary of important design parameters of blades and vanes is given in Table II. Stator velocity vectors calculated for the negatively sloped total pressure profile of the redesigned 2nd-stage rotor showed that both stators would be satisfactory for tests with the redesigned rotor.

TABLE II – BLADE AND VANE GEOMETRIC PARAMETERS

	FIRST-STAGE		SECOND-STAGE	
	Rotor	Stator	Rotor (Redesign)	Stator
Number of airfoils	28	46	60	59
Aspect ratio ¹	2.48	2.75	2.63	2.20
Hub chord, inch [meter]	3.62 [0.092]	2.75 [0.070]	2.10 [0.053]	2.22 [0.056]
Tip chord, inch [meter]	4.55 [0.116]	3.10 [0.079]	1.89 [0.048]	2.45 [0.062]
Hub solidity	2.38	2.52	2.24	2.25
Tip solidity	1.33	1.55	1.27	1.66

¹ Average length/axially-projected hub chord

MECHANICAL DESIGN

Predicted rotor and stator stresses due to static and dynamic loads are well within the capabilities of the materials selected. Rotor blades were fabricated from AMS 4928 (titanium alloy); stator vanes were fabricated from AMS 5613 (stainless steel); and disks, spacers, and hubs were fabricated from AMS 6415 (low alloy steel). The 1st-stage rotor blades have partspan shrouds at 61 percent span from the hub to avoid resonances, and the redesigned 2nd-stage rotor blades, used in the test described herein, have partspan shrouds at 60 percent span from the hub to avoid flutter. An oil damped front bearing was incorporated as a result of the initial tests which revealed incipient critical speed problems. Mechanical design of the original fan configuration is described in detail in Reference 1, and details of the rotor redesign and oil damped bearing design are given in Reference 3.

TEST FACILITY

The test program was carried out in a sea-level compressor test stand (Figure 4) that was equipped with a gas turbine drive engine with a 2.1:1 gearbox to provide speed-range capability. Airflow entered the rig through a calibrated nozzle. A 72 ft [21.9 m] straight section of 42 in. [1.07 m] diameter pipe ran from the nozzle to a 90 in. [2.29 m] diameter inlet plenum. A wire mesh screen and an "egg crate" structure located in the plenum provided a uniform total pressure profile to the compressor. The airflow was exhausted from the compressor into a toroidal collector and then into a 6 ft [1.83 m] diameter discharge stack. The stack contained a 6 ft [1.83 m] diameter valve to provide back pressure, or throttling, for the test compressor. Two smaller valves, a 24 in. [0.61 m] and a 12 in. [0.305 m], located in the bypass lines provided fine adjustment of back pressure.

Rotor strain-gage and inlet hub static pressure instrumentation leads were routed through the nonrotating nose fairing. Ten struts, 14 inches [0.356 meters] upstream of the rotor leading edge, supported the forward bearing and the assembly for the strain-gage slip-ring. Eight struts located 11 inches [0.28 meters] downstream of the stator trailing edge supported the rear bearing.

INSTRUMENTATION AND CALIBRATION

Airflow to the compressor was measured by means of a calibrated nozzle designed to the standards of the ISO (International Organization for Standards). Airflow measurements were within one percent accuracy.

The compressor speed was measured by means of an impulse type pickup. The pickup was an electromagnetic device which counted the number of gear teeth that passed within an interval of time and converted the count to RPM. Between 4,000 rpm and 12,000 rpm, accuracy was within 0.2%.

All temperatures were measured using chromel-alumel, type K thermocouples and were recorded in millivolts by means of an automatic data acquisition system. Temperature elements were calibrated for Mach numbers over their full operating range. Effects of total pressure level on temperature recovery were accounted for by using the corrections found in Reference 5. The thermocouple leads were calibrated for each temperature element. Overall rms temperature accuracy was estimated to be $\pm 1.0^\circ\text{F}$ [$\pm 0.56^\circ\text{K}$].

Wedge probes which measured total pressure, static pressure, and air angle and combination probes which measured total pressure, total temperature, static pressure, and air angle were calibrated for Mach number as a function of indicated static-to-total pressure ratio, with pitch angle as a parameter. Total pressure recovery and yaw angle deviation were calibrated as functions of Mach number and pitch angle. Accuracy of the measured air angles was within 1.0 degree.

All pressures from probes, fixed rakes, and static taps were measured with transducers and recorded in millivolts by an automatic data acquisition system. The accuracy of the pressure was ± 0.1 of the full scale value. All pressures from instrument locations upstream of the 1st-stage rotor trailing edge were measured using 15 lbf/in.^2 [$1.033 \times 10^5 \text{ N/m}^2$] full-scale transducers. Pressures from the trailing edge of the 1st-stage rotor and from all downstream locations were measured using 50 lbf/in.^2 [$3.445 \times 10^5 \text{ N/m}^2$] full-scale transducers. Two proximity detectors, located over the tips of each rotor blade at midchord, were used to monitor blade tip clearance.

Photographs of typical instrumentation are shown in Figure 5, and the axial and circumferential positions of the instrumentation are shown in Figures 6 and 7, respectively. Instrumentation for measuring overall and blade element performance data is listed in Table III.

The eleven radial positions at each axial station were defined by the intersection of the axial station and the redesign streamlines that pass through 5, 10, 15, 30, 50, 60, 65, 70, 85, 90, and 95 percent of the passage height at the 1st-stage rotor trailing edge. The radial locations at which these streamlines passed the leading and trailing edges of each blade row are given in Appendix C, Table XII.

The parameters that were recorded continually during excursions into stall or surge are listed in Table IV.

TABLE III – PERFORMANCE AND BLADE ELEMENT INSTRUMENTATION

Instrument Plane Location	Parameter	Type and Quantity
Sta. 0 -- Inlet Plenum Chamber	1) P	6 pressure taps on plenum wall
	2) T	6 bare wire chromel-alumel thermocouples
Sta. 6 -- Rotor 1 Inlet (approx. $\frac{1}{2}$ rotor-chord upstream of rotor 1)	1) p	6 O.D. and I.D. wall static taps
	2) ⁽¹⁾ P, p, & air angle	2 wedge radial traverse probe spaced 180° apart circumferentially.
Sta. 8 -- Rotor 1 Exit (approx. halfway between rotor 1 T. E. and stator 1 L.E.)	1) ⁽²⁾ p	4 O.D. wall static taps approximately equally spaced circumferentially.
Sta. 11 -- Stator 1 Exit half-way between T. E. of stator 1 and L. E. of rotor 2)	1) ⁽²⁾ p	4 O. D. and 4 I. D. wall static taps, approximately equally spaced circumferentially.
	2) ⁽¹⁾ T, P, p, & air angle	Two NASA combination probes - one with circumferential traverse of one vane gap, plus radial traverse. Second probe with radial traverse at midgap.
Sta. 14 -- Rotor 2 Exit	1) ⁽²⁾ p	4 O. D. and I. D. wall static taps, approximately equally spaced circumferentially.
Sta. 16 -- Fan Discharge (within $\frac{1}{2}$	1) ⁽²⁾ p	4 O. D. and 4 I. D. wall static taps approximately equally spaced circumferentially.
	2) ⁽¹⁾ P, p, &	2 wedge probes, radial traversed. Approximately 180° apart and located at vane midchannel.
	3) ⁽¹⁾ T	2 wake rakes located approximately 180° apart, radially traversed. 10 elements across gap.
	4) ⁽¹⁾ p	2 wake rakes located approximately 180° apart, radially traversed, 13 elements across gap.
Sta. 17 -- Rig Exit	1) P	One circumferential P rake, 5 sensors located at 50% span (used for setting points).

⁽¹⁾ 11 radial locations for uniform inlet flow tests (5, 10, 15, 30, 50, 60, 65, 70, 85, 90, and 95% of passage blade height); 5 radial locations for distorted inlet flow tests (10, 30, 50, 70, and 90% of passage height)

⁽²⁾ Static pressure taps ahead of and behind stators are located on approximate extensions of mean channel streamlines.

TABLE IV – STALL TRANSIENT INSTRUMENTATION

Instrument Plane Location	Parameter	
Inlet Nozzle	p	1 static tap downstream and 1 static tap upstream of inlet nozzle.
	p	A Δ_p transducer sensing the differential pressure between the upstream and downstream nozzle static pressures.
	T	One nozzle temperature
Sta. 0 - Plenum	P	One plenum static tap
	T	One plenum temperature
Sta. 8, 11 - Rotor 1, Stator 1, and Sta. 14 Rotor 2 Exit	P	One O. D. static tap
Sta. 16 - Fan Discharge	P	One O. D. static tap
Sta. 17 - Fan Discharge	P	One circumferential pressure rake at 50 percent span
Gearbox	N	Impulse pickup

PROCEDURES

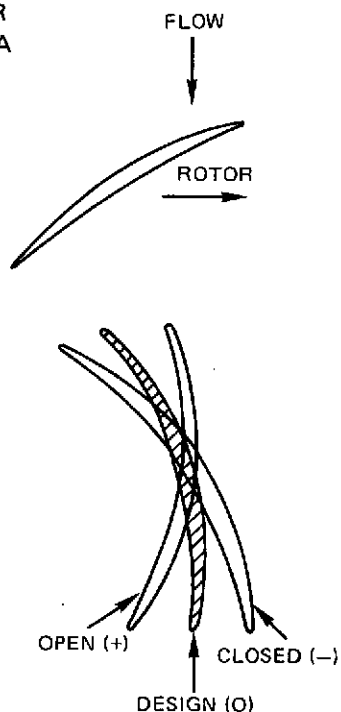
TEST PROCEDURE

The mechanical integrity of the compressor had been established during the shakedown tests of Reference 3 where no flutter limits or vibration problems were encountered. As a result, no detailed surveys were conducted with hot-film probes or with strain gages during the stator optimization tests.

Stator setting optimization tests were conducted at 70 percent, 100 percent, and 105 percent of design speed with uniform inlet flow to examine the effects of various stator stagger angles on first-stage and fan overall performance. At design speed, six different combinations of 1st-stage and 2nd-stage stator stagger angles were tested for comparison with the design configuration tested previously (ref. 3). At 70 percent and 105 percent of design speed, four different configurations were tested for comparison with the design setting. These configurations are listed in Table V.

TABLE V – STATOR OPTIMIZATION CONFIGURATIONS

Speed	SETTING ANGLE FROM DESIGN		NUMBER OF DATA POINTS
	Stator 1	Stator 2	
100%	0	0	6 ¹
	-5	+2.5	4
	+2.5	0	4
	0	+5	3
	0	-5	4
	0	-10	2
	+2.5	-5.0	4
105%	0	0	3 ¹
	-5	+2.5	4
	-7.5	+2.5	4
	-2.5	+2.5	4
70%	+2.5	-2.5	4
	0	0	4 ¹
	-5	+2.5	4
	+5	0	4
	+5	+7.5	4
	+5	-5	1



¹Data Obtained in a Previous Test (ref. 3)

The stators could be reset on the test stand but could not be remotely controlled from the test stand control room. Each subsequent stator setting was determined by observing the effects on overall performance of the settings tested up to that point. For each configuration tested, stall flow and stall pressure ratio were determined with the stall transient instrumentation shown in Table IV. Stall flow was assumed to be the value measured by the flow nozzle at the instant when wall statics and the ΔP transducer showed abrupt changes as the rig was throttled continuously towards stall. The pressure ratio at stall flow was determined from the measurement made with the total pressure rake at the fan discharge, 50 percent span location which had been correlated to the fullspan average total pressure during performance testing. Steady-state performance was recorded for at least three points distributed along a speedline from wide open to near stall throttle settings.

Optimum stator settings for each operating condition were determined in two steps. First-stage stator variations were investigated first with adjustments to the 2nd-stage stator made only to avoid high losses. These 2nd-stage adjustments were made using an analytical prediction of optimum 2nd-stage stator inlet angles as a result of 1st-stage stator setting. This schedule of 2nd-stage stator setting as a function of 1st-stage stator setting is plotted in Figure 8. In the second step, after the 1st-stage stator optimization testing, the 1st-stage stator was set at its optimum angle, and the 2nd-stage stator optimization tests were run. If at the end of the 2nd-stage stator optimization testing, it appeared that some untested combination of stator settings would give further improvements, this combination was also tested. Overall performance data were obtained for a total of 55 stator optimization data

points. First-stage data were obtained for 50 of these points. All complete data points were reduced by the streamline analysis program to obtain overall and blade element performance. These data points were in addition to the 13 design stator-setting data points taken at 70 percent, 100 percent, and 105 percent speeds during the uniform inlet flow portion of the Reference 3 test.

DATA REDUCTION TECHNIQUES

All steady-state performance data were automatically recorded in millivolts on computer cards and then converted to engineering units, corrected, and used to calculate overall and blade element parameters as described in the following sections.

Data Correction and Averaging

The data obtained from impact tube type total pressure probes (fixed radial rakes and traversing wake rakes) located in supersonic flow were corrected for shock loss.

Wedge probes were used to measure total pressure, air angle, and static pressure. Mach number was determined from calibrations of measured total and static pressure. The measured total pressure and flow angle from these probes were corrected using Mach number calibration curves for individual probes. The resulting calibrated Mach number and corrected total pressure were then used in conjunction with standard air-property tables to calculate static pressure.

Combination probes were used to measure total pressure, air angle, static pressure, and total temperature. Corrections were based on probe calibrations similar to those previously described for wedge probes but with an additional calibration of total temperature recovery versus Mach number. The temperature calibration was consistent with the general method for temperature correction described as follows.

Thermocouple signals were converted to temperature measurements using wire calibrations for individual sensors. These temperature measurements were converted into total temperature using Mach number calibrations for individual sensors and the pressure level correction given in Reference 5.

The circumferential total pressure distributions obtained at the exits of the 1st-stage and 2nd-stage stators were each mass-flow averaged at each radial position, using the measured distribution of total temperature and a constant circumferential static pressure determined by linearly interpolating the wall or wedge probe static pressure data. The arithmetic average of the three highest values from the circumferential total pressure distribution measured across the passage between adjacent stator vanes at each stator exit was chosen to represent the free-stream or stator inlet pressure at the appropriate percent of span. A circumferential mass-flow average total temperature was also calculated at each radial position using measured circumferential distributions of total temperature and pressure and static pressures linearly interpolated between wedge probe or inner and outer wall static tap measurements. Circumferentially mass-flow averaged temperatures from both wake rakes at the 2nd-stage stator exit were arithmetically averaged at each radial location. During tests with the nominal

(design) stator settings, one pressure rake did not traverse properly for some data points. Comparisons of measurements made when both rakes were properly functioning showed excellent agreement. As a result, only the data from the pressure rake which worked consistently were used in the data analysis of all stator optimization points.

Air angles measured by circumferential traverses at the 1st-stage stator exit were mass-flow averaged at each radial location. Air angles measured by the two wedge-probes at the 2nd-stage stator exit were arithmetically averaged at each radial location.

Performance Parameter Calculations

Overall and blade element performance parameters were calculated by means of a flowfield analysis computer program. All parameters were corrected to standard day conditions. Inputs to the flowfield program are listed in Table VI.

TABLE VI – INPUT PARAMETERS TO FLOWFIELD PROGRAM

LOCATION	PARAMETER
Compressor Inlet (Station 0, Figure 6)	1) Corrected mass flow
	2) Corrected rotor speed
Rotor 1 Inlet Instrument Plane (Station 6)	1) Constant radial blockage factor (to account for estimated wall boundary layer)
Stator 1 Inlet (Station 9)	1) Total pressure ratio versus radius
	2) Constant radial blockage factor
Stator 1 Exit Instrument Plane (Station 11)	1) Total temperature ratio versus radius
	2) Total pressure ratio versus radius
	3) Constant radial blockage factor
	4) Absolute air angle versus radius
Stator 2 Inlet (Station 14)	1) Total pressure ratio versus radius
	2) Constant radial blockage factor
Stator 2 Exit Instrument Plane (Station 16)	1) Total temperature ratio versus radius
	2) Total pressure ratio versus radius
	3) Constant radial blockage factor
	4) Absolute air angle versus radius

Total pressures and temperatures were ratioed to compressor inlet values. Compressor inlet total pressure was assumed equal to the inlet plenum pressure. Temperatures were ratioed to the inlet plenum temperature.

A blockage factor was used at each axial location to improve the accuracy of the static pressure and velocity calculations of the flowfield program. Blockages were applied equally to all stream-tubes at each of the axial locations. Axial distributions of flow blockage factors

were selected so that the hub and tip static pressures obtained from the flowfield calculations gave the best agreement with the wall average pressure for a representative midthrottle operating point at design speed. As shown in Table VII, the flow blockage factors used in the data reduction flowfield calculation were the same as those blockages used in the redesign of the 2nd-stage rotor except at the trailing edge of the 2nd-stage stator where three percent blockage was added to the calculation for data reduction. These values were the same as those that had been used to reduce the data from the design stator-setting test reported in Reference 3 – details of the blockage selection and static pressure comparisons are given in that reference.

TABLE VII – ANNULUS BLOCKAGES

STATION	DATA REDUCTION (%)	REDESIGN (%)
Rotor 1 Leading Edge	2.4	2.4
Rotor 1 Trailing Edge	4.1	4.1
Stator 1 Leading Edge	4.1	4.1
Stator 1 Trailing Edge	2.8	2.8
Rotor 2 Leading Edge	2.8	2.8
Rotor 2 Trailing Edge	5.3	5.3
Stator 2 Leading Edge	5.3	5.3
Stator 2 Trailing Edge and Downstream	6.5	3.5

All static pressure distributions and air angles behind the rotor were calculated by assuming axisymmetric flow and using mass flow continuity, radial equilibrium, and energy equations. Curvature, enthalpy, and entropy gradient terms were included in the equilibrium calculations. Aerodynamic conditions at the blade edges were calculated by translating the measured data from the instrument plane along streamlines to blade edges. Blade-edge stations were input to the flowfield calculation as slanted straight lines that closely approximated the meridional profiles of the manufactured blade edges. Blade-element parameters were calculated for airfoil sections lying on conical surfaces defined by the intersections of design streamlines and the blade edges. Calculations were made on streamlines passing through the trailing edge of the 1st-stage rotor at 5, 10, 15, 30, 50, 60, 65, 70, 85, 90, and 95 percent of the passage height. Percentage of passage height for other blade edges are given in Appendix C, Table XII. In addition to the blade element parameters, the output of the flowfield analysis program also includes overall performance of the 1st-stage rotor blade row, the first stage, the first stage plus the 2nd-stage rotor, the 2nd-stage rotor, and the complete two stage fan. Blade element performance is tabulated in Appendixes C, D, and E. Accumulated overall performance to the exit of each blade row is tabulated at the bottom of the blade element data sheet for that blade row.

DISASSEMBLY INSPECTION

The 1st-stage blade-tip rubstrip (composite material) failed while a post-test check point was being taken following completion of the stator optimization program. Disassembly of the test rig revealed minor damage (nicks) to the leading edge of the 1st- and 2nd-stage vanes

with slightly more damage to the leading edge of the 2nd-stage vanes; one of the 2nd-stage blades had a piece approximately ½ in. by 1 in. [0.013m by 0.025m] broken off at the tip leading edge. As a result of this damage, there was a sudden drop in flow, pressure ratio, and efficiency. No deterioration in performance had been observed prior to the final check point nor had routine inspections revealed any indication of rubstrip or blade damage prior to this failure. Zygo inspection of the 1st-stage and 2nd-stage vanes showed some minute cracks on the stator vanes which progressed from the vane stem and airfoil corners toward the center of the vane. The first stage had seven vanes with crack indications, and the second stage had nine vanes with crack indications. All crack indications were at the hub except on one 2nd-stage vane on which the indication was at the outer casing.

RESULTS AND DISCUSSION

STATOR OPTIMIZATION AT DESIGN SPEED

The purpose of the stator optimization studies at design speed was to gain fan stall margin with a minimum penalty in operating line efficiency. Analysis of the blade element data from the design stator-setting test showed that all elements were sufficiently close to the minimum loss to preclude improving maximum efficiency by changing stator settings.

The following discussion presents the results of these stator optimization studies in terms of overall and blade element performance comparisons. Stator settings are given in degrees from the nominal stagger angle setting (design setting). Negative angles indicate that the stator was closed (set in a direction to reduce incidence). Where the stator settings are given in parenthesis, the first number denotes the 1st-stage stator setting in degrees and the second number denotes the 2nd-stage stator setting. As an example: (-5,0) indicates that the 1st-stage stator was closed 5 degrees and that the 2nd-stage stator was set at nominal. For convenience, the 1st-stage stator is referred to as stator 1 and the 2nd-stage stator as stator 2. A similar abbreviation is used for the first and second stage rotors.

Fan, First-Stage, and Second-Stage Overall Performance

The following seven combinations of stator setting were tested at design speed (see Table V): (0,0); (-5, +2.5); (+2.5, 0); (0, +5); (0, -5); (0, +10); and (+2.5, -5).

Fan Overall Performance

Fan overall pressure ratio is presented in Figure 9 as a function of inlet corrected flow and adiabatic efficiency with different combinations of stator settings. Four configurations had design stator 1 settings with stator 2 settings varying in 5-degree increments from +5 to -10 degrees. These four speedlines gave a consistent trend with stator 2 closing of increasing stall margin at the expense of operating line efficiency, as shown in Figure 10 (stall margin is defined in Appendix A). Stall margin values were calculated for all speeds using the constant throttle operating line shown in Figure 9. This operating line passes through the design point and corresponds to a fixed area fan nozzle. Nozzle Mach numbers were determined

by a ratio of static pressure to total pressure equal to the reciprocal of the fan overall total pressure ratio. The nozzle flow was corrected to inlet conditions based on the selected pressure ratio and a temperature ratio derived from test efficiencies.

Stator 2 settings changed fan performance by shifting the region of lowest stator 2 loss towards stall as the setting was closed and away from stall as it was opened. This effect is illustrated in Figure 11 which shows stator 2 total pressure recovery versus fan overall pressure ratio for the different stagger angle settings. Other effects on performance of stator 2 setting were caused by radial flow shifts, as discussed under Blade Element Performance.

When stator 1 was opened with the nominal stator 2 setting, stall margin increased and efficiency decreased, similar to the trend obtained when stator 2 was closed while stator 1 was held in its nominal position. Opening of stator 1 was limited to 2.5 degrees because further opening caused rotor 2 blade flutter. With stator 1 at +2.5 degrees, closing stator 2 from 0 to -5 degrees reduced the stall flow but also reduced pressure ratio near stall so that no increase in stall margin occurred. Operating line efficiency decreased when stator 2 was closed as it did in tests with stator 1 at its nominal setting.

The major effects of opening the 1st-stage stator 2.5 degrees can be seen by comparing the overall performance of the (0, 0) and (+2.5, 0) configurations or the (0, -5) and (+2.5, -5) combinations plotted in Figure 9. Opening stator 1 caused the 2nd-stage rotor to do more work and increased the overall fan pressure ratio, but peak efficiency decreased approximately 0.5 percentage points with the (+2.5, 0) setting and 1.0 percentage point with the (+2.5, -5) setting. Stall margin increased by 0.5 percentage points to 12.5 percent for the (+2.5, 0) configuration due to the increased pressure ratio at stall. Stall margin decreased 1.1 percentage points for the (+2.5, -5) configuration compared to (0, -5) due to the higher stall flow although the pressure ratio was higher.

Maximum flow appears to have been limited by rotor 1 with stators at nominal or opened settings. Maximum flow did increase by 0.25% when stator 1 was opened 2.5 degrees, but this change is within measurement accuracy and much smaller than the 4.5% throat area increase of the opened stator 1. When stator 2 was opened 5 degrees, a 0.25% increase in flow also occurred, again within measurement accuracy. Closing stator 1 to -5 degrees decreased the throat area by approximately 10% and gave a maximum flow reduction of about 1.3%. Efficiency remained high at high flow and low pressure ratio, indicating that flow capacity was not set by stator choke which is usually accompanied by high loss. Examination of incidence data, as discussed subsequently under Blade Element Performance, shows that rotor 2 probably limited flow capacity with stator 1 closed to -5 degrees.

Closing stator 2 to -10 degrees decreased its throat area approximately 21% and reduced maximum flow by about 4.5%. This flow decrease appears to have been the result of stator 2 choke, consistent with the low total pressure recovery for stator 2 at this setting (Figure 11).

The optimum configuration seems to have been the (0, -5) combination which improved stall margin by two percentage points with a decrease in overall fan efficiency of 1.3 percentage points from the nominal setting.

Stall margin and overall fan efficiency results are summarized in Table VIII.

TABLE VIII – EFFICIENCY AND STALL MARGIN VALUES FOR STATOR OPTIMIZATION TESTS AT DESIGN SPEED

SPEED	SETTING ANGLE FROM NOMINAL (deg)		STALL MARGIN (%)	EFFICIENCY ON OPERATING LINE (%)
	Stator 1	Stator 2		
100%	0	0	12.0	85.0
	-5	+2.5	8.5	85.2
	+2.5	0	12.5	84.3
	0	+5	7.5	84.8
	0	-5	14.0	83.7
	0	-10	16.2	77.0
	+2.5	-5	12.9	82.1

First-Stage Performance

The 1st-stage rotor pressure ratio is shown in Figure 12 as a function of inlet corrected flow and adiabatic efficiency. The corresponding first-stage performance is presented in Figure 13, showing that with stator 1 nominal settings the various stator 2 settings had a negligible effect on first-stage pressure ratio. Efficiency was relatively unchanged by stator settings. The increased efficiencies shown for the (0, +5) and (0, -5) configurations appear inconsistent with results of the other stator settings although no errors were found in the data. Comparison of data from stator 2 reset tests in which stator 1 was set at +2.5 degrees shows no change in pressure ratio or efficiency with stator 2 variation. Stator 1 total pressure recovery was affected very little by any stagger angle changes. Pressure coefficient and adiabatic efficiency versus flow coefficient for the 1st-stage rotor and first-stage are presented in Figures 14 and 15.

Second-Stage Performance

Performance of the 2nd-stage rotor and the second stage is represented by the pressure coefficient and adiabatic efficiency versus flow coefficient curves of Figures 16 and 17. Figure 16 shows that stator 1 stagger angle variations had a significant influence on the performance characteristics of rotor 2. With stator 2 at a nominal setting, opening stator 1 by 2.5 degrees did not change the flow or pressure coefficients but reduced rotor efficiency. With stator 2 closed 5 degrees, the same 2.5 degree opening of stator 1 (+2.5,-5), increased pressure and flow coefficients but did not affect efficiency, compared to the (0,-5) combination. Stator 2 stagger angle settings had minor effects on rotor 2 performance except for the 10-degree closed stator 2 setting. In this position, stator 2 choking reduced the flow capacity of the second stage approximately 10% and decreased the rotor 2 pressure coefficient at the choke point.

Stator 2 losses had a strong effect on performance of the second stage. At open throttle points, where stator 2 was choked, the adiabatic efficiency average of the second stage was about 13 percentage points lower than the efficiency of rotor 2. At points where stator 2 operated with low loss (near peak efficiency), the efficiency of the second stage was approximately four percentage points lower than rotor 2 efficiency.

Blade Element Performance

Spanwise Comparison of Performance Parameters

Spanwise profiles of performance parameters from near stall data points for each configuration were compared in an attempt to determine which blade row stalled first. Figure 18 shows near stall diffusion factors versus span for each blade row for the various stator 2 settings with nominal stator 1 settings. At the nominal stator 2 setting, the rotor 2 hub was highly loaded and probably caused stall (Figure 18a). Closing stator 2 to -5° (Figure 18b) evened the radial loading distributions for all blade rows, and the improved balance reduced the local rotor 2 hub value. Closing stator 2 by 10 degrees once again caused the rotor 2 hub loading to increase to a critical level (Figure 18c). Opening stator 2 by five degrees caused stator 2 hub diffusion factors to approach critical values while rotor 2 values were relatively low (Figure 18d). The only effect of opening stator 1 was to increase rotor 2 hub loadings slightly as shown in Figure 18e.

Spanwise profiles of exit meridional velocity (Figure 19) indicate that closing stator 2 from -5 to -10 degrees caused blockage which forced flow away from the hub of rotor 2 and stator 2. These calculated flow velocities were caused by the radial profiles of total pressure ratio shown in Figure 20. Calculations also showed that a large increase in rotor 2 hub loss caused the reduced pressure ratio (Figure 21). One explanation for the high loss is that the free-stream pressures used to calculate rotor loss were lower than the actual rotor exit total pressures. Figure 22 shows total pressures measured by the stator 2 exit wake rake at 10 percent span for points near operating line conditions with stator 2 at 0, -5 , and -10 degrees. As can be seen, the wake covers the entire span for the -10 -degree stator setting so that no free-stream region is apparent. The value of rotor exit pressure, calculated in the manner described under Data Reduction Techniques, was probably lower than the true rotor exit pressure. This resulted in values of rotor 2 loss and loading that are probably higher than the true values, in which case the total pressure recovery of stator 2 for the (0, -10) stator setting is even lower than that shown in Figure 11. Another probable result would be that the corresponding rotor 2 pressure coefficient and efficiency values shown in Figure 16 are too low.

Variations with Incidence Angle

Blade element performance in terms of loss coefficient, diffusion factor, and deviation angle versus incidence angle is presented in Figure 23 through 26 for rotor 1, stator 1, rotor 2, and stator 2, at five of the 11 radial positions where performance parameters were calculated. Tabulations of the data at all eleven radial positions are given in Appendix C.

Rotor 1

Design speed blade element data for rotor 1 (Figure 23) shows that for any given stator setting the rotor operates within a small range of incidence angles, due to the flow regulation of the stators. Loss levels are relatively constant for all configurations except at the hub region and are insensitive to incidence changes at all spans. The losses for the open 5-degree and closed 5-degree stator 2 settings with nominal stator 1 seem to be lower than the rest, especially in the lower portion of the span.

Negative hub losses, noted from 5 percent to 30 percent of span (Appendix C and Figures 23a and 23b), can be attributed to incorrect matching of temperatures and pressures in regions of steep radial gradients since the pressure and temperature probe elements were offset radially by approximately one percent of span. Distributions of losses between rotors and stators are not believed to be the source of the problem since stator losses appear reasonable for these points. These low losses gave the questionably high level of rotor 1 efficiency shown in the performance map of Figure 12. Diffusion factors followed the same increasing trend with incidence for all stator configurations, reaching a maximum value of 0.63 from 15 percent to 60 percent of span for the closed 10-degree stator 2 setting (Appendix C). The flow limit imposed by this setting caused rotor 1 to operate at 1.5 to 2.0 degrees higher incidence than nominal, with the increased back pressure causing the high loadings and probable stall initiation.

Stator 1

Blade element data for stator 1 (Figure 24) indicate that the losses were low for the entire range of incidences encountered due to stagger angle or flow regulations. A unique curve of diffusion factor versus incidence was obtained for each stator 2 setting. Each curve showed loading increasing with incidence at approximately the same rate but each having a different loading level for a given incidence angle. The curves shifted to higher incidence for opened stator 1 settings. Diffusion factors between 0.62 and 0.64 were attained near stall for the stator 1 nominal position with stator 2 closed 10 degrees. Apparently, the flow reduction caused by stator 2 is the reason stator 1 operated at higher incidence and loading.

Rotor 2

Rotor 2 loss coefficients versus incidence angle (Figure 25) for all stator configurations show a rotor 2 choking tendency characterized by sharp increases in loss with decreasing incidence, particularly in the wake region caused by the partspan shroud (45 percent to 66 percent of span). Very low incidence angles are evident for tests with stator 1 closed to -5 degrees. These angles probably reached the minimum possible incidence (ref. 6) for the portion of the blade having relative supersonic flow (from 37 percent to 100 percent of span), limiting fan flow capacity for this stator setting. Diffusion factors are quite high near the hub, reaching 0.72 at eight percent of span due to high back pressure with stator 2 closed to -10 degrees.

Rotor 2 deviations are low for points where stage 1 efficiency appears to be unusually high (Figure 13), indicating that the temperature rise attributed to rotor 2 was greater than

for similar data points with other stator settings.

The high value of rotor 2 loss shown at eight percent span for the (0, -10) data point at 4.5 degrees incidence is questionable since it was difficult to determine the free-stream pressure corresponding to rotor 2 pressure.

Stator 2

Blade element data for stator 2 (Figure 26) show evidence of hub choking, as indicated by the rapid increase in losses with decreasing incidence. From 42 percent span to the tip there is little variation of loss with incidence for any stagger angle setting. Each stator 2 stagger angle setting increased loading (diffusion factor) with incidence, each shifted in incidence according to the stagger angle. Maximum diffusion factor was 0.62 at the hub for the 10-degree closed stator 2.

Deviation angles are not considered reliable at very low incidence angles where the stator was near choke and stator wakes became large enough to influence angle measurements.

STATOR OPTIMIZATION AT 105 PERCENT OF DESIGN SPEED

The purpose of the stator optimization tests at 105 percent speed was to increase overall fan efficiency with a minimum stall margin penalty. The following five combinations of stator settings were tested (see Table V): (0, 0); (-5, +2.5); (-7.5, +2.5); (-2.5, +2.5); and (+2.5, -2.5). Overall and blade element performance comparisons are discussed in the following sections.

Fan, First-Stage, and Second-Stage Overall Performance

Fan Overall Performance

The fan overall pressure ratio with different combinations of stator settings is presented in Figure 27 as a function of inlet corrected flow and adiabatic efficiency. The three configurations with stator 2 opened 2.5 degrees all had improved operating line efficiencies of about 1.5 percentage points compared to that with nominal settings. This seems to have been due to a significant improvement in stator 2 recovery near the operating line pressure ratio (Figure 28). Closing stator 1 with this open stator 2 setting decreased overall fan pressure ratio due to the decreased rotor 2 work input. This reduced the stall margin from 15.7% with the nominal settings to 11% and 7.4% for stator 1 positions of -2.5 and -7.5 degrees, respectively. Opening stator 1 to +2.5 degrees caused a slight decrease in rotor 2 pressure coefficient near stall which resulted in a decreased overall fan pressure ratio. The one percentage point decrease in operating line efficiency with the 2.5 degree open stator 1 (Figure 27) was due to the decrease in stator 2 recovery in its 2.5 degree closed position, as shown in Figure 28.

The optimum configuration tested was, therefore, the closed 2.5 degree stator 1 with the opened 2.5 degree stator 2 which obtained an adiabatic efficiency of 82.5% on the operating

line, an improvement of 1.5 percentage points relative to the efficiency obtained with nominal settings. Simultaneously, stall margin dropped 4.7 percentage points to a value of 11%. However, the data indicate that most of the improvement in efficiency could have been obtained without a loss in stall margin by setting stator 1 at nominal and stator 2 at +2.5 degrees. At the operating line pressure ratio of 2.88, the change in stator 2 total pressure recovery was 0.01 (Figure 28). This change in recovery is equivalent to an efficiency change of 1.1 percentage points. In its nominal setting, stator 1 would have maintained the high level of rotor 2 work input and the stator 2 opened setting would have given stator 2 lower loss on the operating line. The relationship between the improvement in efficiency and stator 2 setting was not obvious during testing because of a time lag between testing and blade element analysis. Time was allotted at the end of the main test program to test the optimum configurations at each speed after detailed analysis of the data, but the rotor rub strip failure prevented these tests (see Disassembly Inspection).

Fan flow capacity was not affected significantly by opening either stator, indicating that rotor 1 determined the maximum flow capacity of the fan. Closing stator 1 to -7.5 degrees reduced maximum flow by approximately 1.2%. This lower flow is believed to have resulted from the minimum possible incidence limit on the supersonic portion of rotor 2 similar to the flow limit observed at design speed; however stator 1 losses indicate that this stator was near choke which may have contributed to the flow decrease. Stall margin and efficiency results for 105 percent speed test points are summarized in Table IX.

TABLE IX – EFFICIENCY AND STALL MARGIN VALUES
FOR STATOR OPTIMIZATION TESTS AT 105% SPEED

SPEED	SETTING ANGLE FROM NOMINAL (deg)		STALL MARGIN (%)	EFFICIENCY ON OPERATING LINE (%)
	Stator 1	Stator 2		
	105%	0		
	-5	+2.5	8.5	82.5
	-7.5	+2.5	7.4	82.8
	-2.5	+2.5	11.0	82.5
	+2.5	-2.5	14.7	80.0

First-Stage Performance

The 1st-stage rotor pressure ratio is shown in Figure 29 as a function of inlet corrected flow and adiabatic efficiency. The corresponding first-stage performance is shown in Figure 30. The first-stage and rotor 1 pressure ratios did not change significantly with any stator variation. The first-stage and rotor 1 efficiencies seem to have varied inconsistently with stator setting with both the opened and closed configurations yielding efficiencies higher than those for the nominal settings. At wide open throttle, stator 1 recovery did not fall off as it did for stator 2 (Figure 28), indicating that stator 1 was not choked at any setting tested. Pressure coefficient and adiabatic efficiency versus flow coefficient curves for rotor 1 and the first-stage are presented in Figures 31 and 32.

Second-Stage Performance

The performance of rotor 2 and the second stage is shown in Figures 33 and 34 as pressure coefficient and efficiency versus flow coefficient. Closing stator 1 decreased flow capacity and pressure coefficient, and opening stator 1 increased flow but decreased the peak pressure coefficient slightly. Actual work input increased when stator 1 was opened, but a large drop in efficiency of approximately five percentage points reduced the ideal work (used to calculate pressure coefficient) below the level obtained at the design stator setting.

Blade Element Performance

Spanwise Comparisons of Performance Parameters

Diffusion factor is presented versus span in Figure 35 for each blade row for the near stall data points of each stator configuration. These points are also close to peak efficiency. The nominal and closed 2.5-degree stator 1 configurations had high loadings on the tip of rotor 2 which could have caused stall. Closing stator 1 to -7.5 degrees reduced the rotor 2 loading so that the 2.5-degree open stator 2 hub became critical. Stator 1 loadings changed very little with stagger angle changes.

Variations with Incidence Angle

Blade element performance in terms of loss coefficient, diffusion factor, and deviation angle versus incidence angle is presented in Figures 36 through 39 for rotor 1, stator 1, rotor 2, and stator 2, at five of the eleven radial positions where performance parameters were calculated. Tabulations of the data at all eleven radial locations are given in Appendix D.

Rotor 1

The rotor 1 blade element data (Figure 36) show that the small range of incidence angle near the hub was extended somewhat by closing stator 1 which reduced maximum flow and permitted lower flow before stall. These lower flows somewhat relieved the rotor 1 choking, as shown by the lower losses at higher incidences for the blade elements, particularly in the regions affected by the partspan shroud and the tip. The lower rotor 1 losses account for the remainder of the overall fan efficiency gained with stator 2 opened 2.5 degrees. Levels and trends in loss data are consistent with those found in the nominal position stator tests. For all closed stator 1 configurations, diffusion factors leveled out to a maximum of about 0.55 to 0.60 in the lower 50 percent of span for incidence angles corresponding to near-stall data points (Figure 35).

Stator 1

Blade element data (Figure 37) for stator 1 closed to -7.5 degrees from nominal indicate choking at the hub with sharp increases in loss with decreasing incidence angle. Opening the stator 2.5 degrees defined the stall side of the loss curve from 85 percent to 95 percents of span (tabulated in Appendix D, also shown in Figure 37e). For each stator setting, diffusion factors

increased with incidence at the same slope but each curve shifted to higher incidence as the stator was opened. The maximum value of diffusion factor was 0.61 at the hub for the 2.5-degree open stator. Deviation levels increased with the closing of the stator.

Rotor 2

Loss versus incidence angle curves from rotor 2 blade element data (Figure 38) shifted to higher incidence with the closing of stator 1 out to 25 percent span and then shifted to lower incidence, suggesting a flow shift from hub to tip. Without a flow shift at the same flow and wheel speed, the rotor would be expected to operate at a lower incidence with the closed stator 1 due to increased preswirl. Meridional velocity profiles (Figure 40) show a reduction in hub flow with no change in tip flow. The negative incidence angles for the outboard portion of the blade, where relative Mach numbers exceeded 1.0, probably define the minimum possible incidence angle for the relative flow. High hub diffusion factors were gradually reduced with closing stator 1. At 82 percent and 88 percent spans, the rotor deviations were negative for the 7.5 degree closed stator 1. These negative deviations occurred for data points that had unusually high efficiency on the first stage, indicating that the portion of the fan temperature rise attributed to rotor 2 was greater than for other data points.

Stator 2

Stator 2 blade element data (Figure 39) indicate choking near the hub and tip for the nominal and closed 2.5 degree positions as shown by the rapid increase of loss with decreasing incidence angle. Opening stator 2 by 2.5 degrees relieved this choke trend somewhat and showed the beginning of stall loss increase at positive incidence from the hub to 23 percent span. The reduced losses near the hub for the +2.5-degree settings resulted in the improved stator 2 average total pressure recovery responsible for the increase in overall fan efficiency.

The rise in loss levels at low incidence angles (high flows) was accompanied by a sharp decrease in deviation angles, which may be the result of large stator wakes influencing the angle measurement of the probe at its gapwise location for a given stagger angle. Hub diffusion factors increased rapidly with increasing incidence angles, reaching levels of about 0.65 when stator 2 was open 2.5 degrees. These high values of loading in the hub region are the probable cause of stall for this stator 2 setting. Loading levels remained above 0.6 out to 11 percent span and also approached these values near the area of the partspan shroud wakes.

STATOR OPTIMIZATION AT 70 PERCENT OF DESIGN SPEED

The objective of the stator optimization at 70 percent of design speed was to improve both stall margin and efficiency. The following five combinations of stator settings were tested (see Table V): (0,0); (-5, +2.5); (+5, 0); (+5, +7.5); and (+5, -5). Overall and blade element performance are discussed in detail in the following sections.

Fan, First-Stage, and Second-Stage Overall Performance

Fan Overall Performance

Overall fan pressure ratio and adiabatic efficiency as functions of corrected inlet flow are presented in Figure 41. Pressure ratio of the fan was increased by opening stator 1 due primarily to increased rotor 2 work input. Higher fan pressure ratio characteristic curves crossed the operating line at higher flows. In this way, flow could be regulated between 113.6 lbm/sec [51.53 kg/sec] and 119.6 lbm/sec [54.18 kg/sec] at 70 percent speed. Similarly, opening stator 2 increased its recovery at open throttle points, raising fan pressure ratio to overcome system resistance at higher flows. Peak efficiency occurred near the operating line for all of the configurations tested with peak values falling between 84% and 84.5%. Stall margins also were nearly the same for all configurations, varying between 16.7% and 17.7%. Closing stator 1 allowed the fan to run at a lower flow before stall; nominal and opened stator 1 settings gave approximately the same flow at stall. Stator 2 total pressure recovery versus flow curves show that recovery varied slightly with setting angle changes except near wide open throttle (Figure 42). Stall flow was not affected by changes in stator 2 setting when stator 1 was fixed. Stall flows and operating line efficiencies for 70 percent speed are summarized in Table X.

TABLE X – EFFICIENCY AND STALL MARGIN VALUES
FOR STATOR OPTIMIZATION TESTS AT 70% SPEED

SPEED	SETTING ANGLE FROM NOMINAL (deg)		STALL MARGIN (%)	EFFICIENCY ON OPERATING LINE (%)
	Stator 1	Stator 2		
	70%	0		
	-5	+2.5	17.7	84.0
	+5	0	16.7	84.4
	+5	+7.5	17.7	84.2
	+5	-5	—	—

First-Stage Performance

Pressure ratio and adiabatic efficiency as functions of corrected inlet flow for rotor 1 and the first stage are shown in Figures 43 and 44, respectively. Rotor 1 pressure ratio was essentially unchanged by stator variations. Stator 1 recovery stayed highest over the operating range for nominal and closed settings while losing recovery near stall for opened settings. These changes (Figure 42) did not affect stage pressure ratios to any great extent, as shown by Figure 44. Efficiencies show a lot of scatter due to the sensitivity of pressure and temperature measurements at low speeds and show no consistent trends with stator setting. The shape of the efficiency versus flow curves for all configurations suggests that rotor 1 was operating on the stall side of optimum incidence as expected for this speed. Plots of pressure coefficient and adiabatic efficiency versus flow coefficient for rotor 1 and the first stage are presented in

Figures 45 and 46. Pressure coefficient increased with decreasing flow coefficient for the rotor and for the stage, but increasing stator loss near stall reduced the rate of rise for the stage.

Second-Stage Performance

Plots of pressure coefficient and adiabatic efficiency versus flow coefficient for rotor 2 and the second stage are presented in Figures 47 and 48. These data show that opening stator 1 increased the flow capacity and work input of rotor 2. Stator 2 setting had a strong effect on flow and stage 2 efficiency at open throttle operation with stator 1 fixed at 5 degrees open but had practically no effect near stall. Efficiency was higher for closed stator 1 settings, but this was offset by lower first-stage efficiency at the low flow rates obtained with stator 1 closed.

Blade Element Performance

Spanwise Comparison of Performance Parameters

Spanwise variations of diffusion factors at near-stall conditions for each blade row are compared in Figure 49 for each 1st-stage stator setting. The near-stall points for the various combinations of stator 2 setting with stator 1 fixed at 5 degrees open were nearly the same and, therefore, are not presented. The tip region of the first stage was apparently the most highly loaded area regardless of stator setting and was the probable cause of stall. Both rotor 1 and stator 1 loadings were sufficiently high to cause stall. Closing stator 1 reduced its loadings, and a lower stall flow was obtained, indicating the possibility of stator 1 controlling stall. Opening stator 1 increased its loadings; however, stall flow was the same as for the nominal settings. The blade row which actually initiated stall was not determined. Rotor 2 loadings increased significantly with stator 1 opened 5 degrees, but the loadings were still much lower than the rotor 1 values. Closing stator 2 lowered its loading distributions, as was expected.

Variations with Incidence Angle

Loss coefficient, diffusion factor, and deviation angle are presented versus incidence angle in Figures 50 through 53 for each blade row at five of the eleven radial positions where performance parameters were calculated. Tabulations of the data at all eleven radial locations are given in Appendix E.

Rotor 1

Blade element data for rotor 1 (Figure 50) indicate the probability of a tip stall as evidenced by increasing diffusion factors and loss coefficients with increasing (stall) incidence angles. Values of diffusion factor between 0.62 and 0.63 occurred at the highest incidence at 90 percent of span and reached 0.65 at 95 percent span. Deviations angles also increased rapidly with incidence angle at 90 percent and 95 percent of span.

Stator 1

Stator 1 blade element data (Figure 51) show that the losses were relatively constant over a wide incidence range and increased slightly at the higher incidence angles. The diffusion factor versus incidence curves for each stator setting angle have the same positive slope but shift with respect to incidence according to stator setting. Levels of diffusion factor reached 0.62 near the tip for the 5-degree open stator setting, about the same as for the rotor 1 tip.

Rotor 2

Blade element data for rotor 2 (Figure 52) show that the rotor was operating at higher incidence angles with stator 1 opened to +5 degrees, consistent with less preswirl at the stator 1 exit. Mach numbers increased approximately 9% for the same wheel speed and meridional velocity when stator 1 was opened from nominal to +5 degrees. At higher incidence angles, losses tended to be higher for the +5 degree stator 1 setting than for the nominal setting at all spans. Loading levels (diffusion factors) never exceeded 0.55 at any spanwise location.

Stator 2

Curves of loss versus incidence angles for stator 2 (Figure 53) indicate choking at both the hub and tip with a rapid increase in loss with decreasing incidence. Opening the stator 7.5 degrees relieved this choking and allowed the stator to operate near the minimum loss region across the span. Wide open throttle data points show this choking trend at all spans, but the majority of data is near minimum loss, resulting in little overall recovery difference in the operating range. Loading levels were quite low for all setting angles, never exceeding a diffusion factor of 0.5. The shifting of the diffusion factor versus incidence curves with stagger angle setting is similar to that which occurred for stator 1.

SPEED EFFECTS ON STATOR OPTIMIZATION

Fan Overall Performance

The only combination of reset stators common to all three speeds was the (-5, +2.5) configuration. Fan overall pressure ratio and efficiency versus corrected inlet flow is presented in Figure 54 for the (-5, +2.5) and nominal configurations. As can be seen, closing stator 1 reduced the pressure ratio due to less rotor 2 work input.

Operating line efficiency of the fan was unchanged at 70 percent and at 100 percent of design speed but improved by 1.5 percentage points at 105 percent speed. Flow regulation due to changes in stator settings was less at design speed than at 70 percent speed in terms of percent change in flow. The flow change at 105 percent speed was within the accuracy of flow measurement.

First-Stage Performance

Pressure ratio and efficiency versus corrected inlet flow are shown in Figure 55 for rotor 1 and in Figure 56 for the first stage. First-stage pressure ratios and efficiencies were essentially the same for both stator settings at 70 percent and 100 percent speeds. At 105 percent speed with the stator reset, the first-stage pressure ratios were higher along a very steep speedline and efficiency was increased by 2%. Curves of pressure coefficient versus flow coefficient (Figure 57) show that little change in first-stage performance occurred when the stator was reset.

Second-Stage Performance

Plots of pressure coefficient and adiabatic efficiency versus flow coefficient for the second stage are presented in Figure 58 for the nominal and reset stator positions. Closing stator 1 caused a drop in pressure coefficient at all speeds due to reduced rotor 2 work input. Flow coefficient was reduced at 100 percent and 105 percent speeds due to minimum incidence being reached on the supersonic relative flow portion of rotor 2. At 70 percent speed, the flow was less with the closed setting because of the reduction in stator 1 throat area.

ESTIMATE OF INLET GUIDE VANE BENEFITS FOR OFF-DESIGN OPERATION

Studies were made of the possible benefits in stall margin or overall fan efficiency at 70 percent and 110 percent of design speed with the addition of a variable flap IGV (inlet-guide-vane) used in conjunction with the existing variable stator vanes. Estimates of efficiency and loading at operating conditions other than design were made with the streamline analysis program incorporating an off-design cascade system for rotors. Stator loss coefficients and deviation angles were held constant. The cascade system calculated incremental changes from the input design values of rotor loss and deviation angles due to incidence and Mach number effects. At each speed, baseline performance was calculated for several flows without an IGV and with nominal stator positions. The system gave somewhat different pressure ratio versus corrected flow characteristics from the actual test data. Comparisons of calculated efficiency and loading distributions with various combinations of IGV and stator 1 stagger angles were made with the baseline values rather than test data to obtain incremental differences in stall margin or efficiency. Results of the study at 70 percent and 110 percent of design speed are presented separately in the following sections.

70 PERCENT SPEED IGV STUDY

Test results at 70 percent speed showed that rotor 1 was highly loaded and probably instigated stall, with stator 1 hub loadings almost as high as those for rotor 1. Second-stage blade rows were lightly loaded. The baseline prediction with the off-design system gave the same general loading trends as the test data for operating line conditions although the spanwise distribution was somewhat different at the same fan pressure ratio, as shown in Figure 59. Adding an IGV to reduce the incidence to the 1st-stage rotor (closing the IGV flap) reduced the rotor work input and loading. In order to obtain the same overall fan pressure ratio as the baseline

configuration at the operating line, it was necessary to run at slightly higher speeds or to open stator 1 to provide more rotor 2 work input. Figure 60 shows overall fan pressure ratio and efficiency versus corrected inlet flow at 70 percent speed for the test data and baseline prediction. Two other speedlines with an IGV closed 15 degrees are shown at slightly higher speeds, one with the nominal stator 1 and the other with stator 1 opened 5 degrees. Probable stall flows are shown for each case based on a plot of maximum diffusion factor (maximum occurring between 10 percent and 90 percent spans) versus corrected inlet flow for each blade row (Figure 61). Diffusion factor values of 0.65 were considered the limit for any blade row based on past experience. Closing the IGV by 15 degrees resulted in an increase in stall margin of approximately 9.5 percentage points (19.0% compared to 9.5%) for either the nominal or opened stator 1 settings. Peak overall fan efficiency decreased slightly with the addition of the IGV but was within one percentage point of the baseline and test data peak efficiency of 84.8%. Both configurations with the 15-degree closed IGV showed significant reductions in rotor 1 loadings so that rotor 2 and stator 1 loadings became the dominant factors. Stator 1 in its nominal position (IGV at -15°) reached the 0.65 diffusion factor limit before any other blade row. When stator 1 was opened 5 degrees (IGV at -15°), fan speed was reduced to obtain the proper operating line pressure ratio. Rotor 2 reached the 0.65 limit first, but incidences reached 6.5 degrees at the outer portion of stator 1 which may produce large losses. For this reason it appears as if the 15 degree closed IGV with stator 1 in its nominal position will give the most stall margin benefit with the least loss penalty. Spanwise loading distributions for each blade row are shown in Figure 62 for this configuration at a flow close to the predicted stall value. Reducing the rotor 1 loadings with the IGV may improve the tolerance to tip radial distortion (ref. 7) which should gain stall margin with the distortion, especially at 85 percent speed where a large penalty occurred (ref. 3).

110 PERCENT SPEED IGV STUDY

Test results at 110 percent speed showed the 2nd-stage blade rows to be highly loaded with rotor 2 probably initiating stall. The baseline prediction with the off-design loss system (no IGV and nominal stator 1) gave the same general trend of blade loadings as the test data although the spanwise distribution was different. Two configurations were examined with an IGV opened 5 degrees to increase the incidence angle and resulting work input and loading of the 1st-stage rotor. One configuration had stator 1 in its nominal position and the other had stator 1 closed 5 degrees to reduce the work input from the second stage. In both cases a slight reduction in speed was necessary to obtain the operating line pressure ratio of the baseline case. Figure 63 shows maximum diffusion factors (maximum occurring between 10 percent and 90 percent of span) for each blade row versus percent operating line flow for the test data, including results of the baseline prediction and the two inlet configurations with the IGV opened. Both test data and the baseline prediction showed rotor 2 and stator 2 maximum loadings increasing at a steeper rate with flow than the 1st-stage blade rows. Opening the IGV 5 degrees increased rotor 1 maximum loadings significantly. Rotor 2 loadings were generally lower across the span for the opened IGV configurations with both stator 1 settings, but each configuration reached the stall diffusion factor value of 0.65 on the rotor 2 hub at approximately the same flow as the baseline case. In fact, rotor 1, rotor 2, and stator 2 reached the stall limit at the same flow for the open IGV setting with

nominal stator 1. Closing stator 1 by 5 degrees with the opened IGV increased rotor 1 loadings even higher than with the nominal stator 1 so that the stall limiting diffusion factor of 0.65 was encountered at a higher flow than with the baseline configuration.

A spanwise comparison of blade row loadings for the baseline prediction and the five-degree open IGV with closed stator 1 is presented in Figure 64 for a predicted stall flow. This figure shows that rotor 2 loadings were generally lower across the span but peaked to the same value as the baseline prediction at 10 percent of span.

A plot of overall fan pressure ratio and adiabatic efficiency versus percent of operating line flow for the test data, baseline prediction, and the two configurations with the IGV opened (Figure 65) shows little change in efficiency or stall margin due to the addition of an IGV. The indicated stall points are based on the diffusion factor limits (0.65) shown in Figure 63. It was concluded that the addition of an inlet guide vane would give no significant benefit at 110 percent of design speed.

SUMMARY OF RESULTS

Stator optimization at design speed resulted in stall margin improvement at the expense of operating line efficiency by closing the 2nd-stage stator (resetting in a direction to reduce incidence). Improved blade loading distribution, especially on the 2nd-stage rotor, is the probable reason for the improvement in stall margin. However, closing the 2nd-stage stator decreased the pressure ratio and increased the hub losses of the 2nd-stage rotors. The optimum configuration tested gave a 2.0 percentage point increase in stall margin (14.0% compared to 12.0%) and 1.3 percentage point decrease in adiabatic efficiency (from 85% to 83.7%) compared to the operating line point with nominal stator settings.

At 105 percent speed, operating line adiabatic efficiency was improved by 1.5 percentage points (from 81% to 82.5%) with a 4.7 percentage point drop in stall margin (from 15.7% to 11.0%) with the 1st-stage stator closed 2.5 degrees and the 2nd-stage stator opened 2.5 degrees. The efficiency benefit came from the improved 2nd-stage stator recovery at a 2.5-degree open setting. Stall margin was reduced because of the decrease in 2nd-stage rotor work input with the closed 1st-stage stator setting. The increase in efficiency could probably have been obtained without a stall margin penalty if the 1st-stage stator had been left in its design position.

At 70 percent speed, stator setting variations had no effect on stall margin or overall fan operating line efficiency. The tip region of the first stage was the most highly loaded area and the probable cause of stall. Considerable speed-flow regulation occurred with variations of both stators but maximum recoveries changed very little.

The inlet-guide-vane study concluded that a significant stall margin benefit is probable at 70 percent speed with little or no efficiency penalty with the inlet-guide-vane in a position to reduce incidence to the 1st-stage rotor. No benefit was predicted for 110 percent speed.

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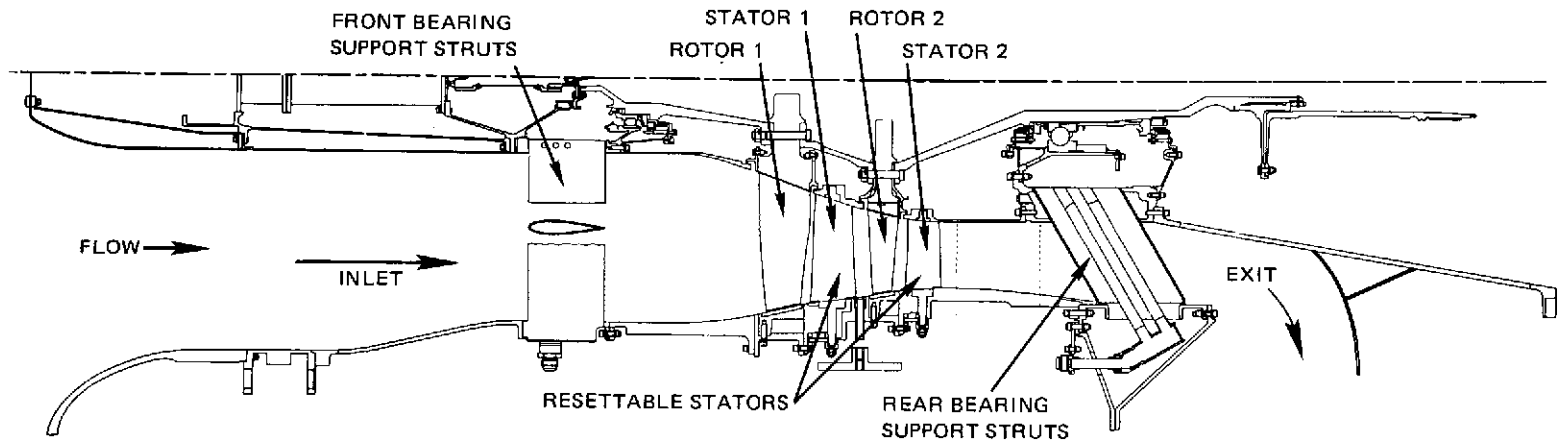


Figure 1 Schematic of Two-Stage Fan Test Arrangement

STA	DIAMETER		AXIAL DISTANCE FROM ROTOR 1 LEADING EDGE	
	I.D.	O.D.	z - I.D.	z - O.D.
4	10.00 (0.254)	32.48 (0.825)	-5.20 (-0.132)	-5.20 (-0.132)
5	10.26 (0.261)	32.33 (0.821)	-3.70 (-0.094)	-3.70 (-0.094)
6	10.94 (0.278)	31.96 (0.811)	-2.245 (-0.057)	-2.245 (-0.057)
7	12.40 (0.315)	31.00 (0.787)	0.0 (0.0)	0.42 (0.011)
8	14.84 (0.377)	29.93 (0.760)	3.30 (0.084)	2.75 (0.070)
9	15.22 (0.387)	29.67 (0.754)	3.80 (0.097)	3.45 (0.088)
10	16.85 (0.428)	28.96 (0.736)	6.15 (0.156)	6.33 (0.161)
11	17.18 (0.436)	28.82 (0.752)	6.75 (0.172)	6.75 (0.172)
*12	17.39 (0.442)	28.58 (0.726)	7.23 (0.184)	7.57 (0.192)
** 12	17.39 (0.442)	28.55 (0.725)	7.23 (0.184)	7.65 (0.194)
*13	18.35 (0.467)	28.12 (0.714)	9.20 (0.234)	8.82 (0.224)
** 13	18.37 (0.467)	28.14 (0.715)	9.27 (0.236)	8.76 (0.223)
14	18.58 (0.472)	27.90 (0.709)	9.80 (0.249)	9.59 (0.244)
15	18.90 (0.480)	27.60 (0.701)	11.85 (0.301)	11.93 (0.303)
16	18.90 (0.480)	27.60 (0.701)	13.50 (0.343)	13.50 (0.343)

DIMENSION IN INCHES
(METERS)

*ORIGINAL } DENOTES CHANGES IN
**REDESIGN } AXIAL POSITION DUE TO REDESIGN

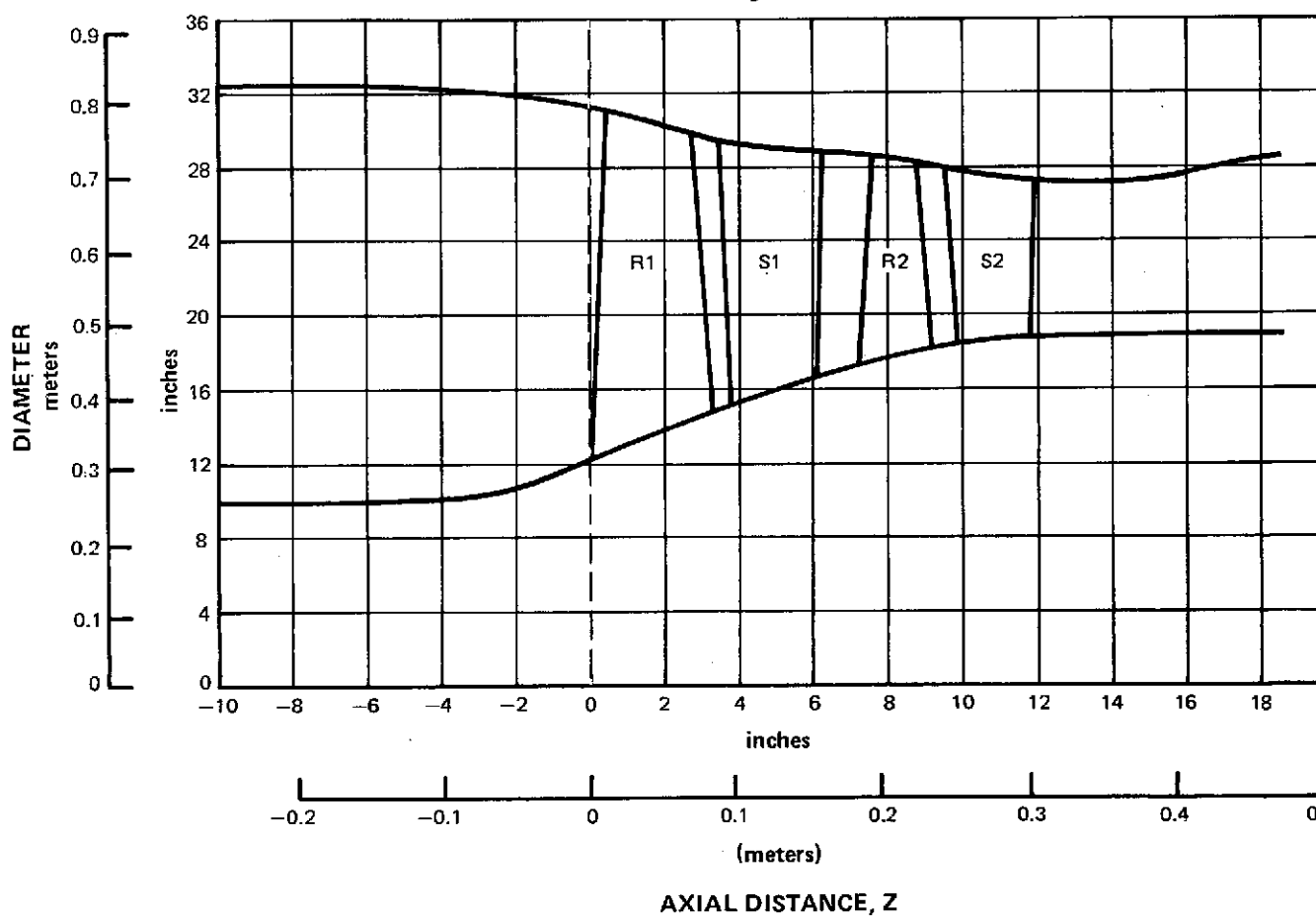
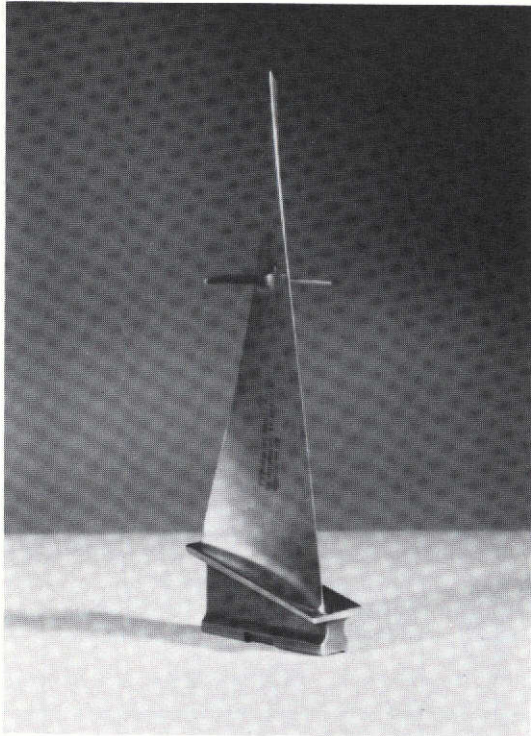
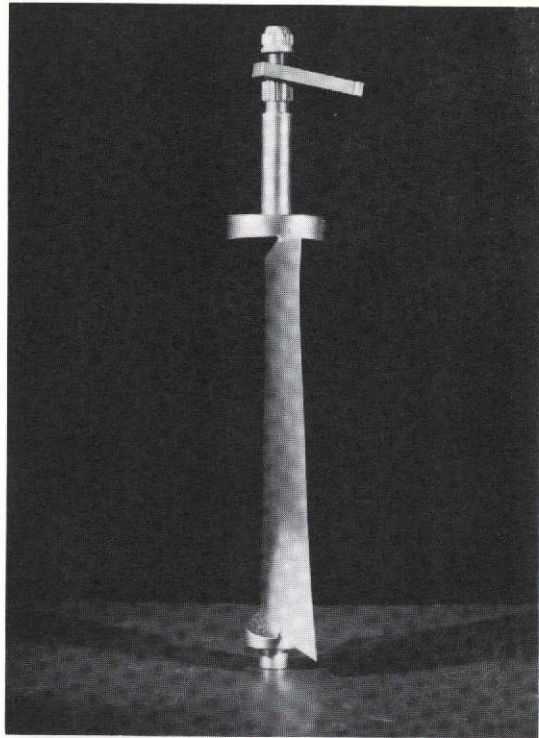


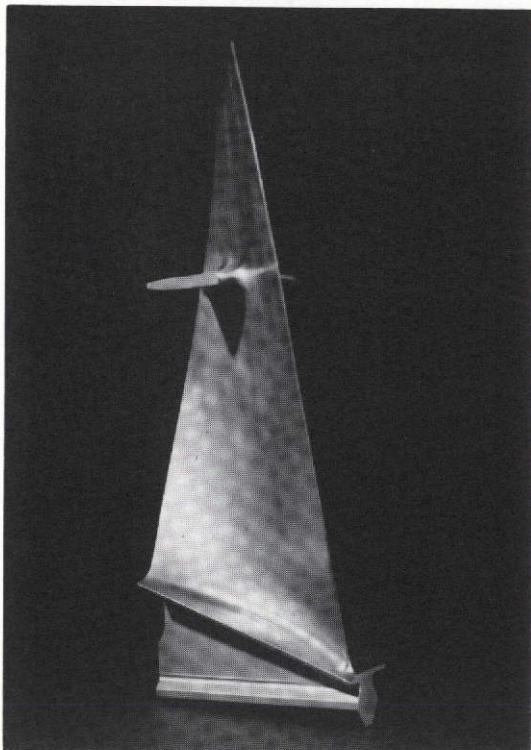
Figure 2 Fan Flowpath



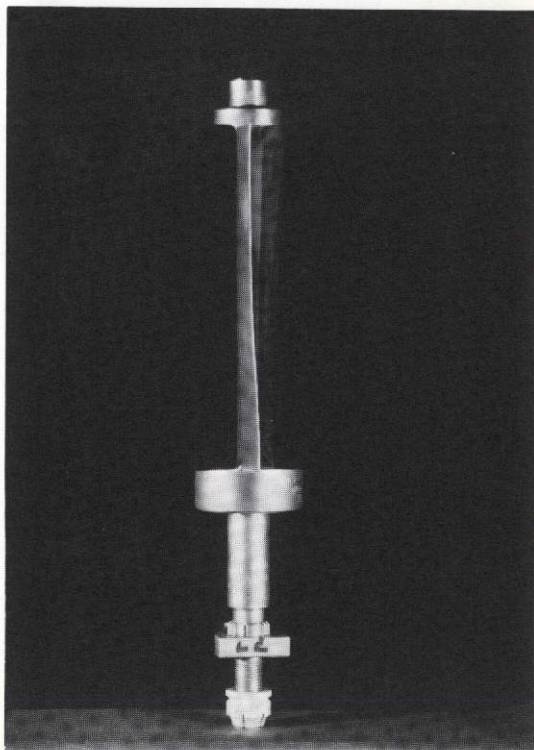
First-Stage Blade



First-Stage Vane



Second-Stage Redesigned Blade



Second-Stage Vane

Figure 3 Blades and Vanes Employed in Two-Stage Fan

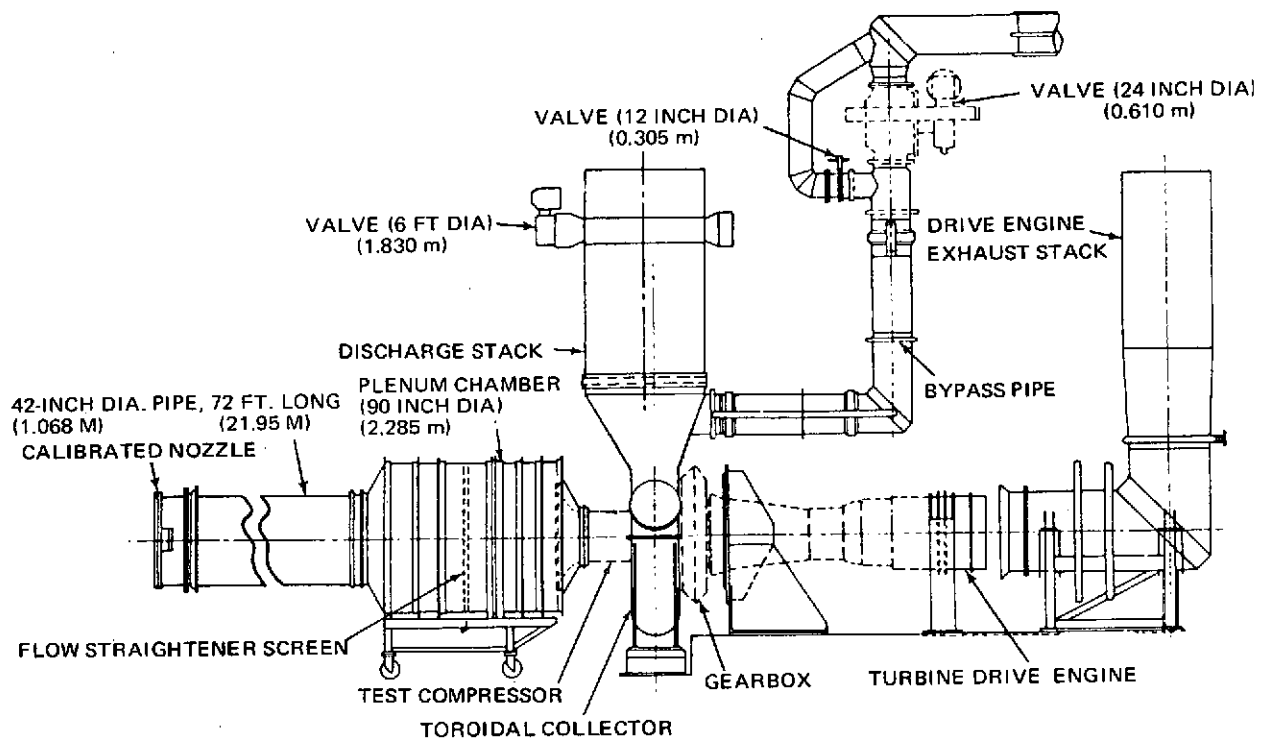
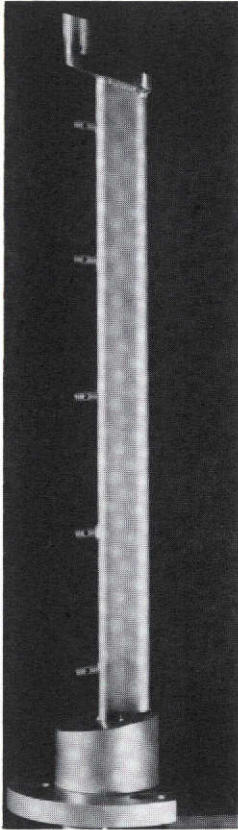
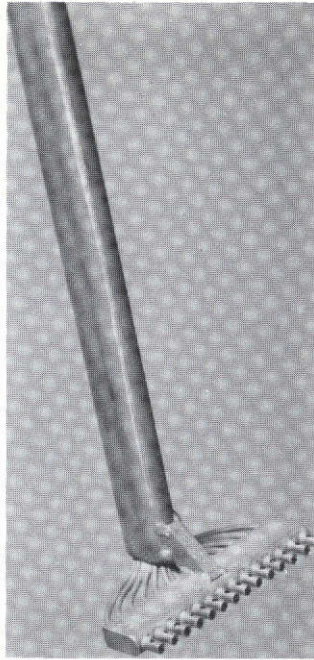


Figure 4 Schematic of Compressor Test Facility



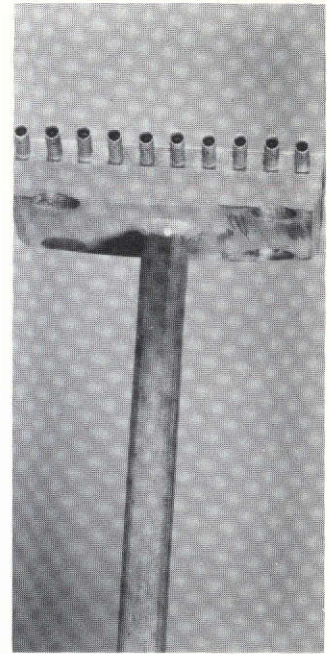
A. Fan Inlet
Total Pressure
Rake Probe



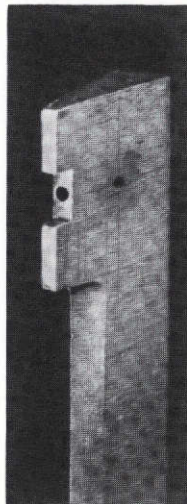
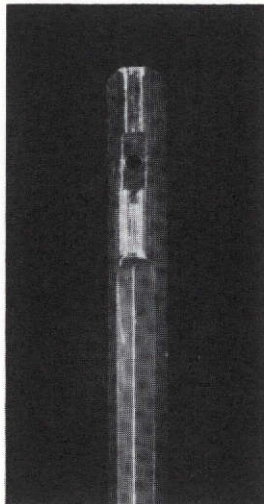
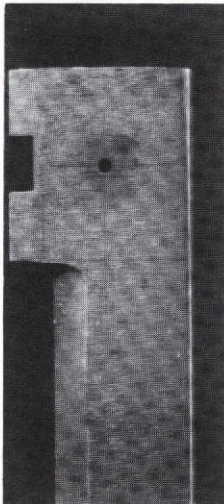
B. Stator 2 Exit Total Pressure
Wake Probe



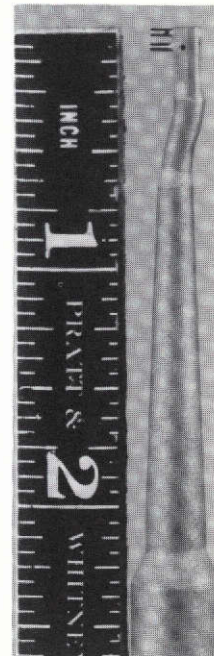
C. Fan Inlet
Hot Film
Probe



D. Stator 2 Exit Total Tempera-
ture Wake Rake



E. Fan Inlet & Static Exit Traverse Wedge Probes



F. Stator 1 Exit
NASA Combination Probe

Figure 5 Typical Instrumentation Employed in Two-Stage Fan

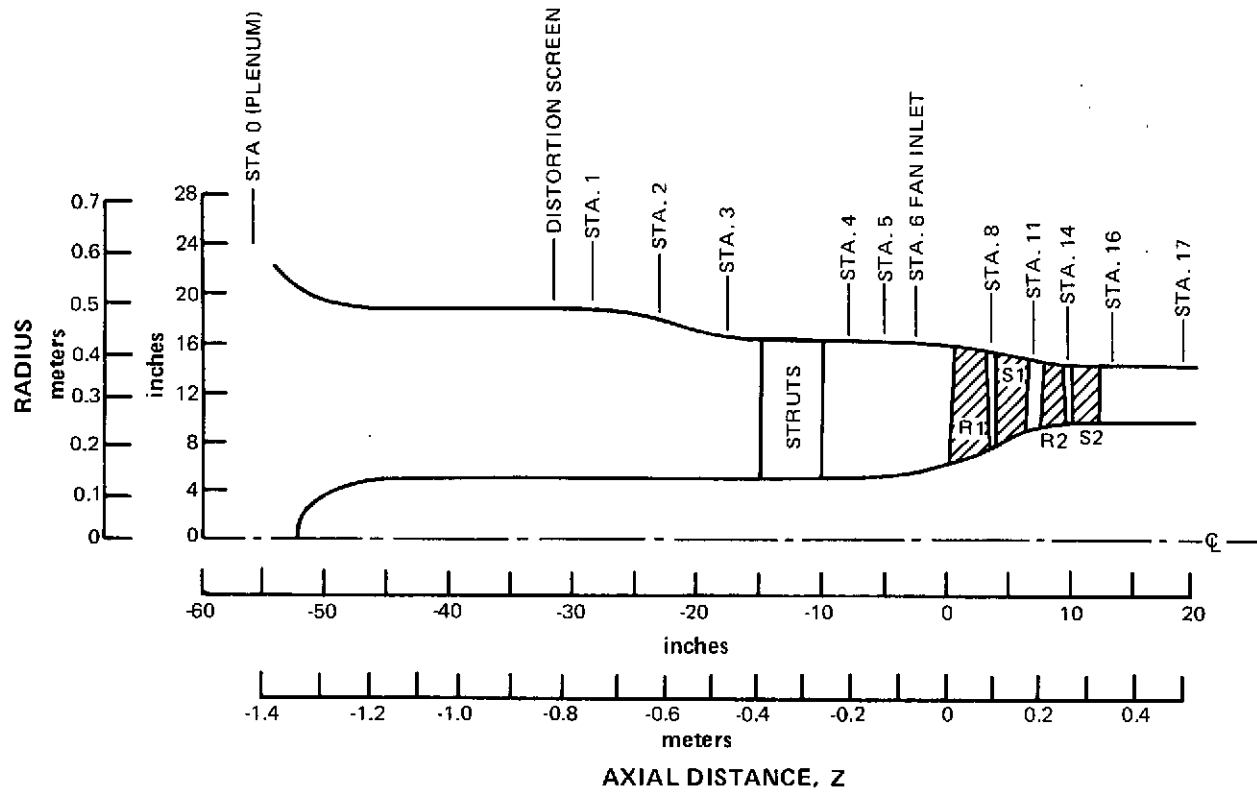


Figure 6 Axial Locations of Instrumentation

VIEW LOOKING DOWNSTREAM

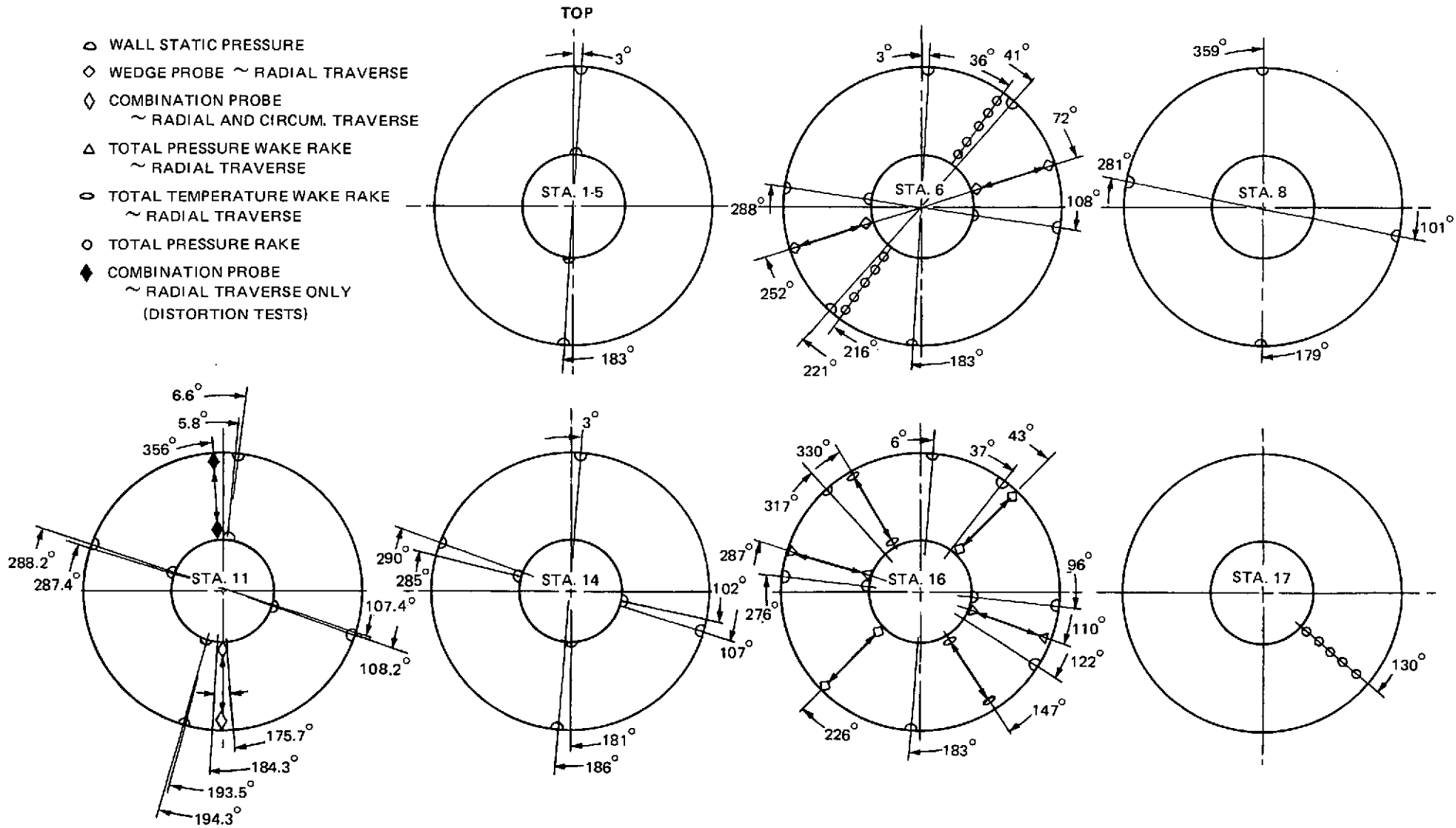


Figure 7 Circumferential Locations of Instrumentation

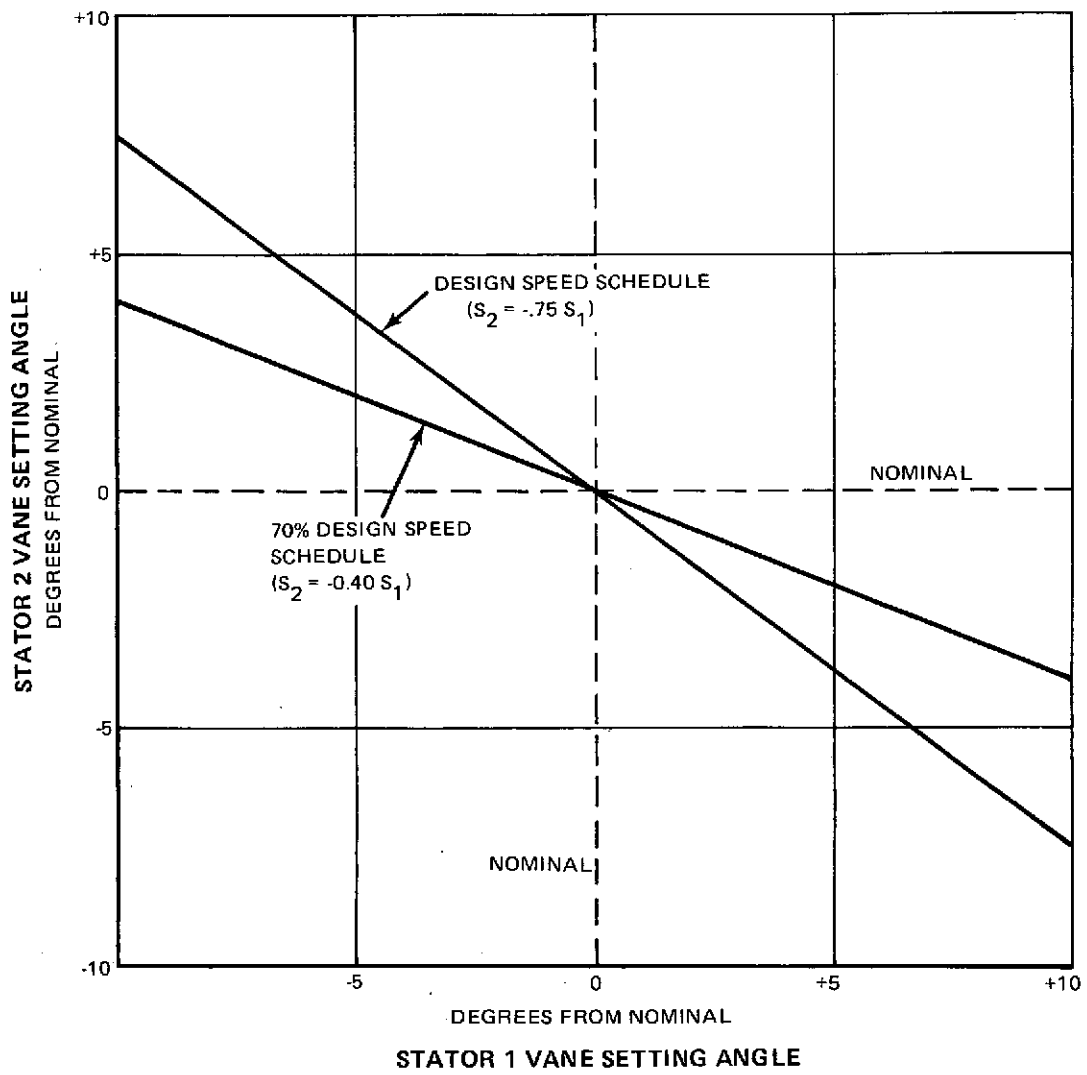


Figure 8 Analytical Schedule of Stator 2 Setting Versus Stator 1 Setting Angle

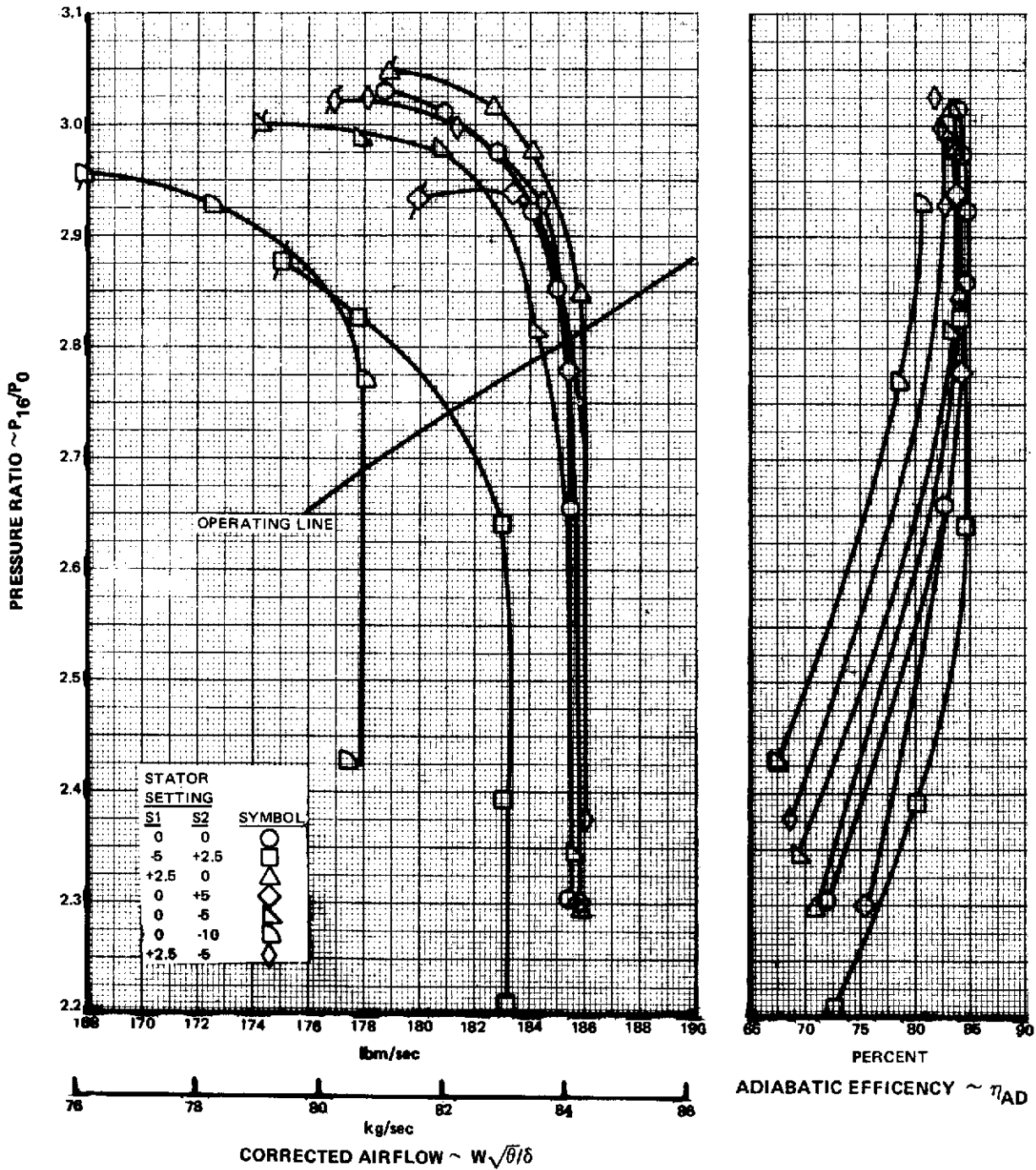


Figure 9 Fan Overall Performance at Design Speed

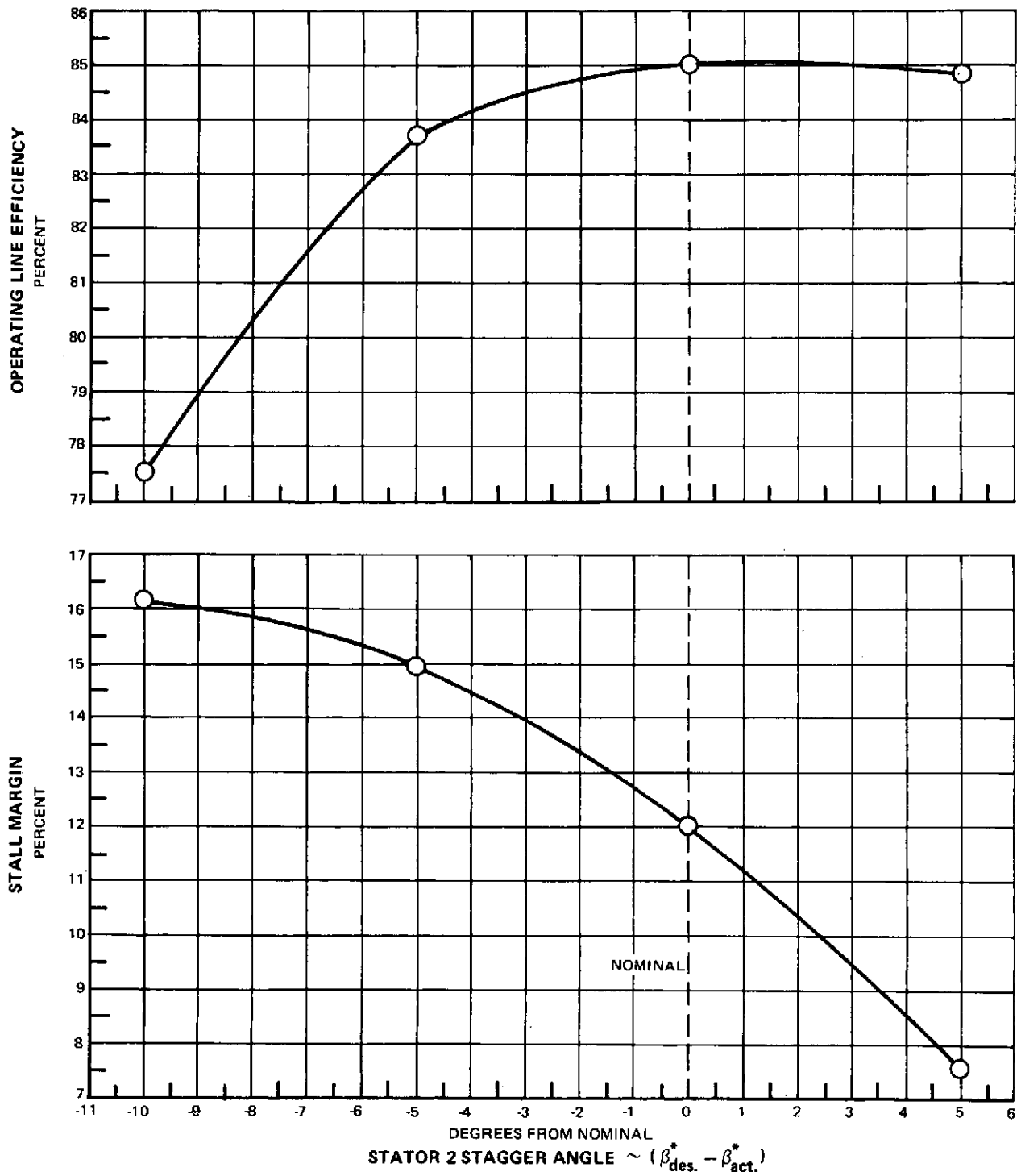


Figure 10 Stall Margin and Operating Line Efficiency Versus Stator 2 Stagger Angle at Design Speed, Nominal Stator 1 Setting

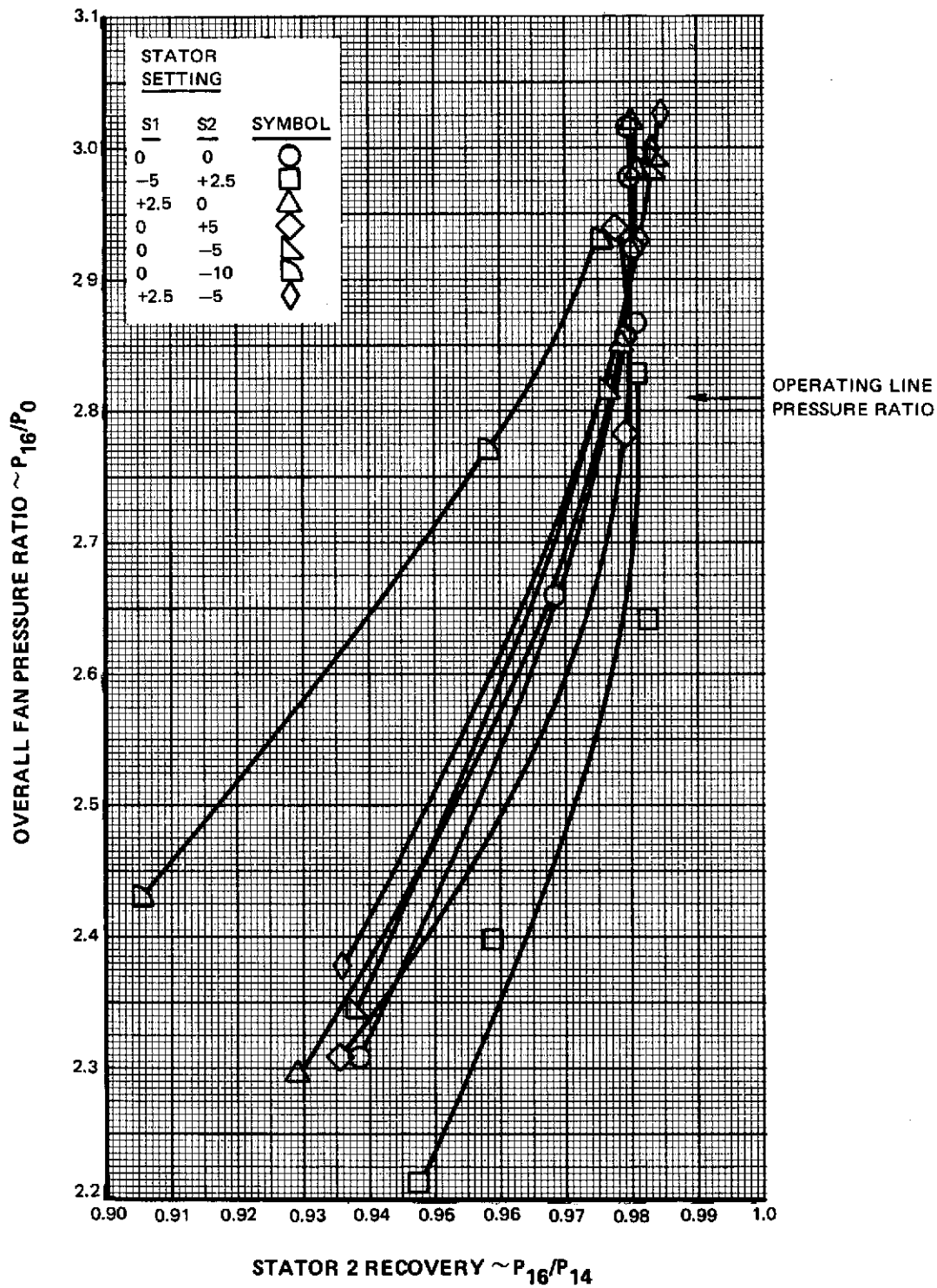


Figure 11 Stator 2 Total Pressure Recovery Versus Overall Fan Pressure Ratio at Design Speed

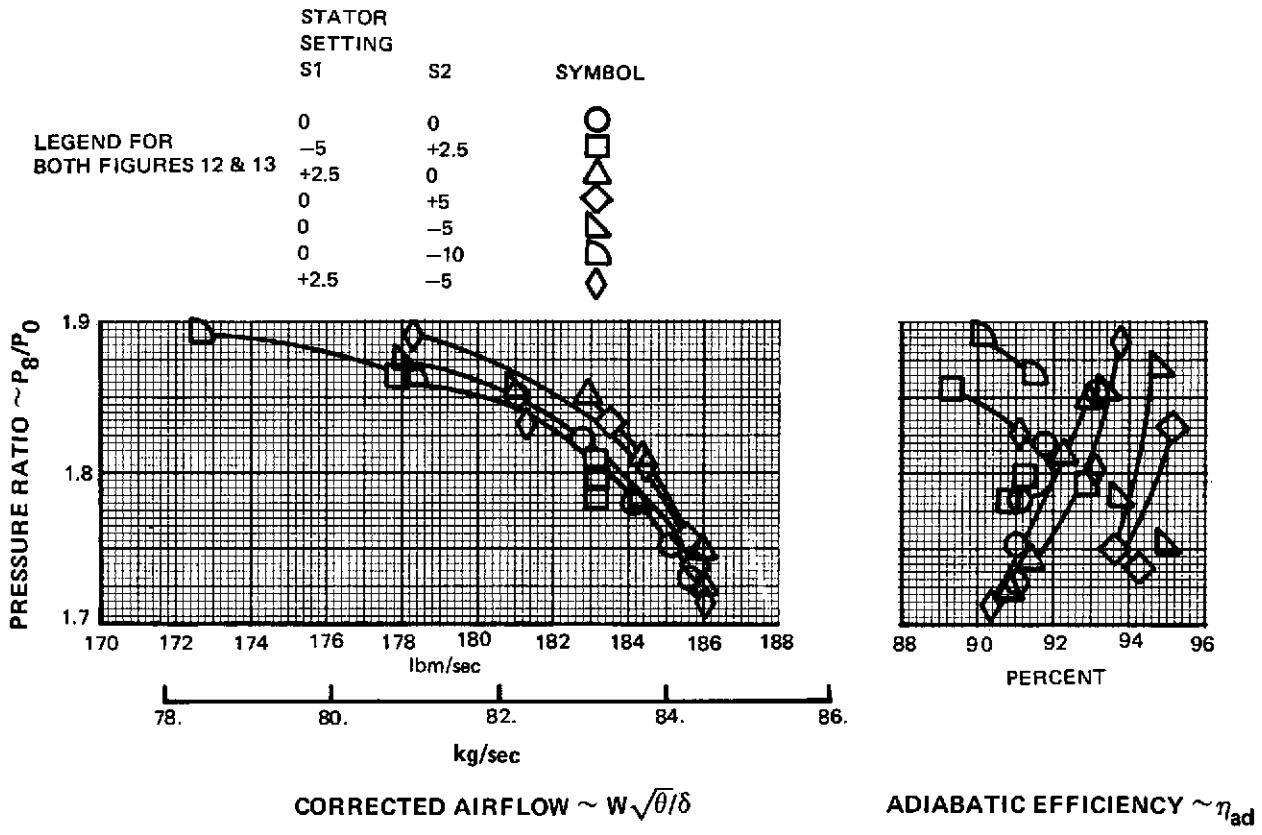


Figure 12 Rotor 1 Performance at Design Speed

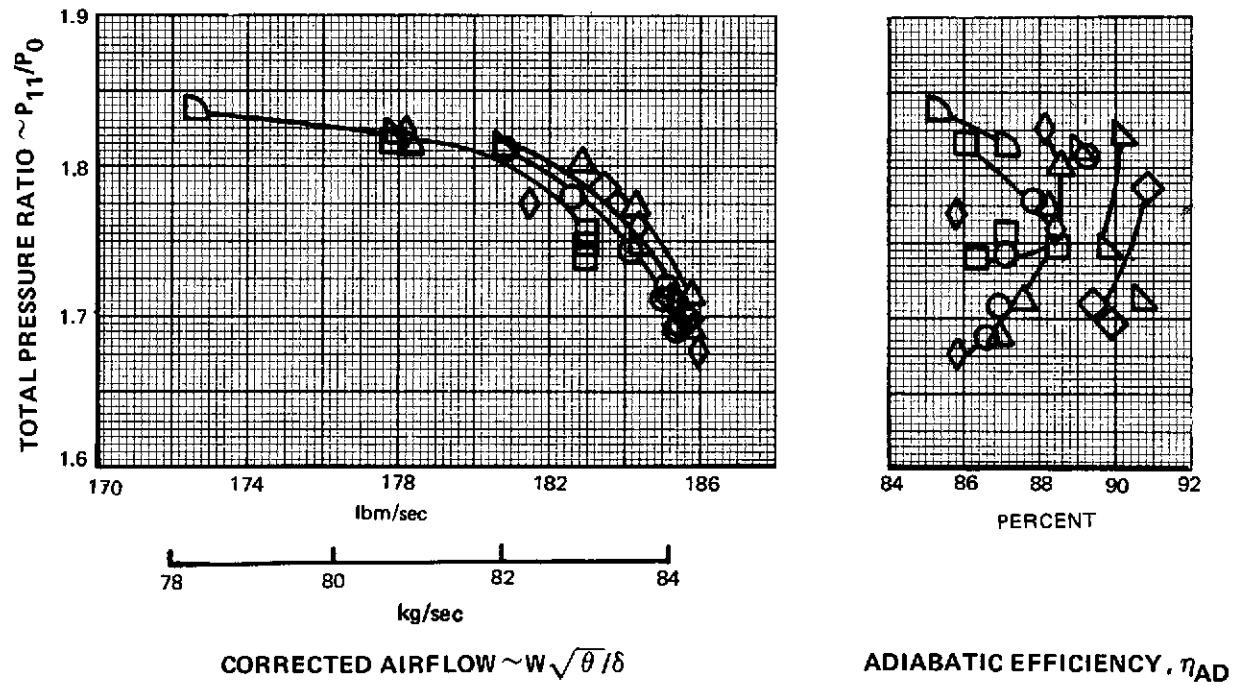


Figure 13 First-Stage Performance at Design Speed

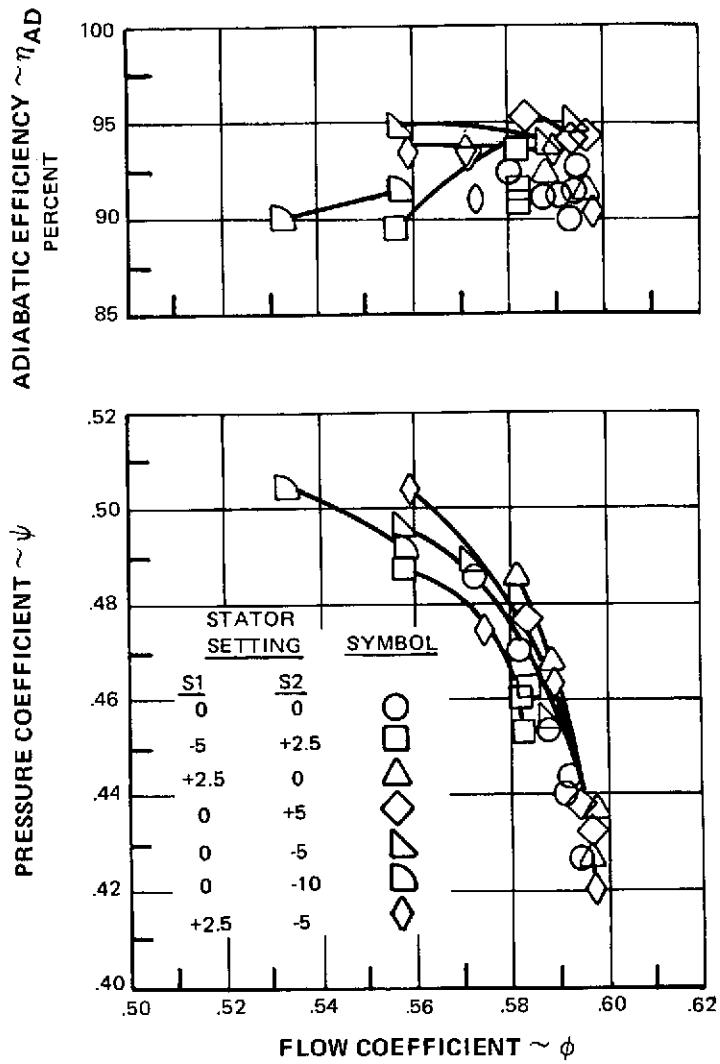


Figure 14 Pressure Coefficient and Adiabatic Efficiency Versus Flow Coefficient for Rotor 1 at Design Speed

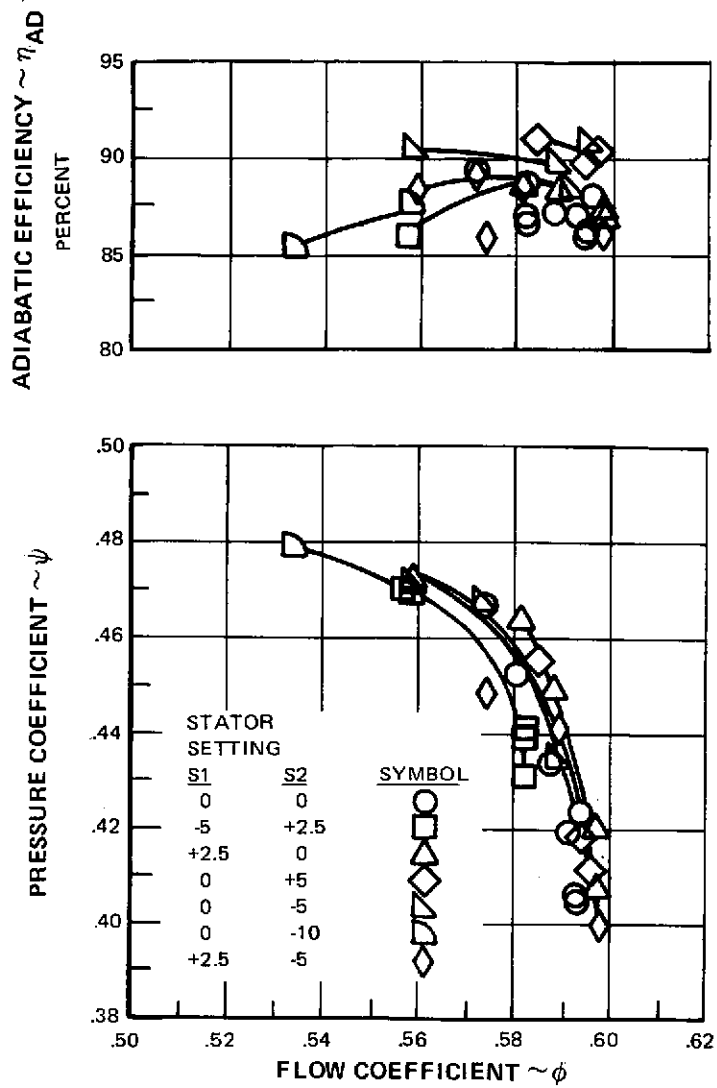


Figure 15 Pressure Coefficient and Adiabatic Efficiency Versus Flow Coefficient for First Stage at Design Speed

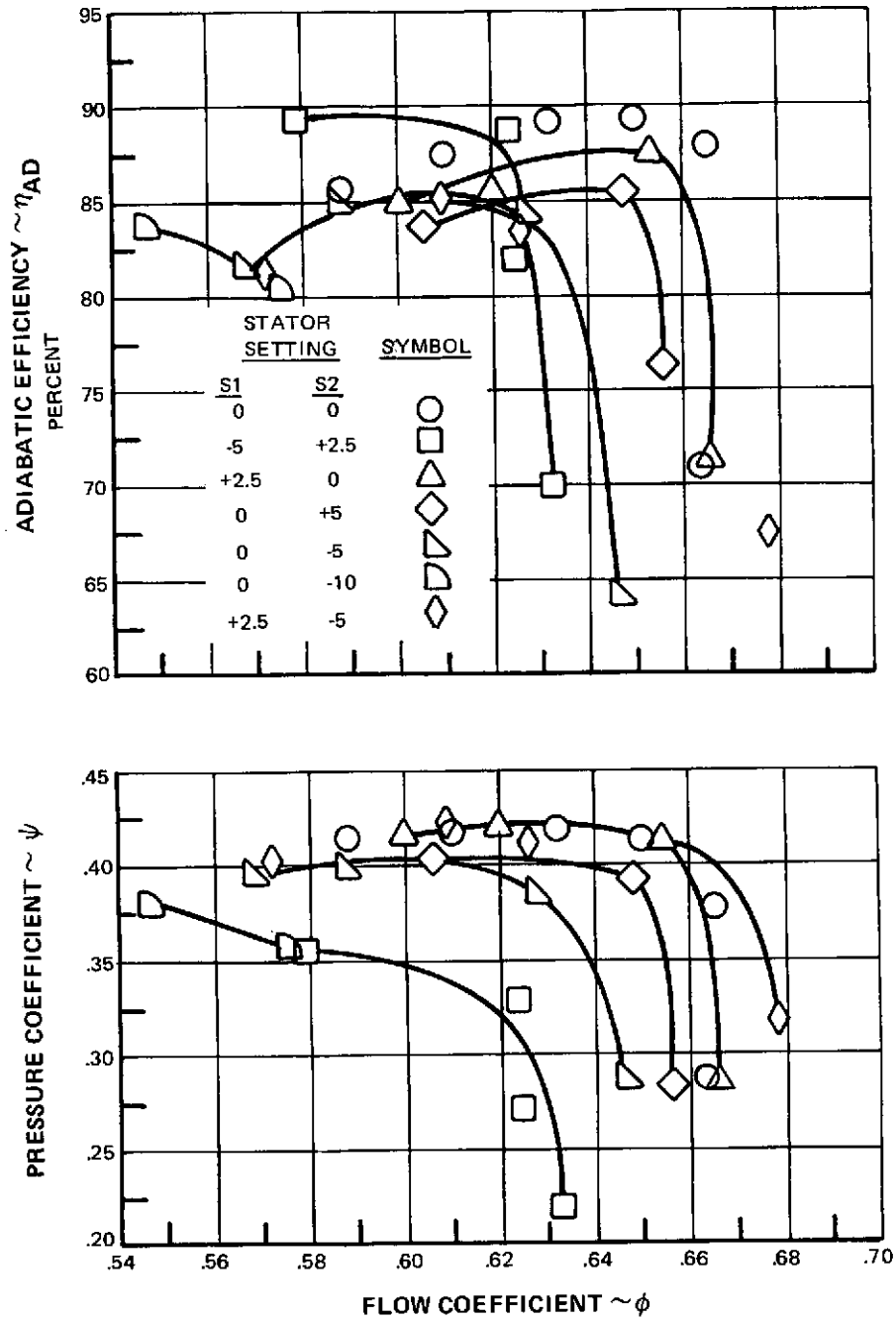


Figure 16 Pressure Coefficient and Adiabatic Efficiency Versus Flow Coefficient for Second-Rotor at Design Speed

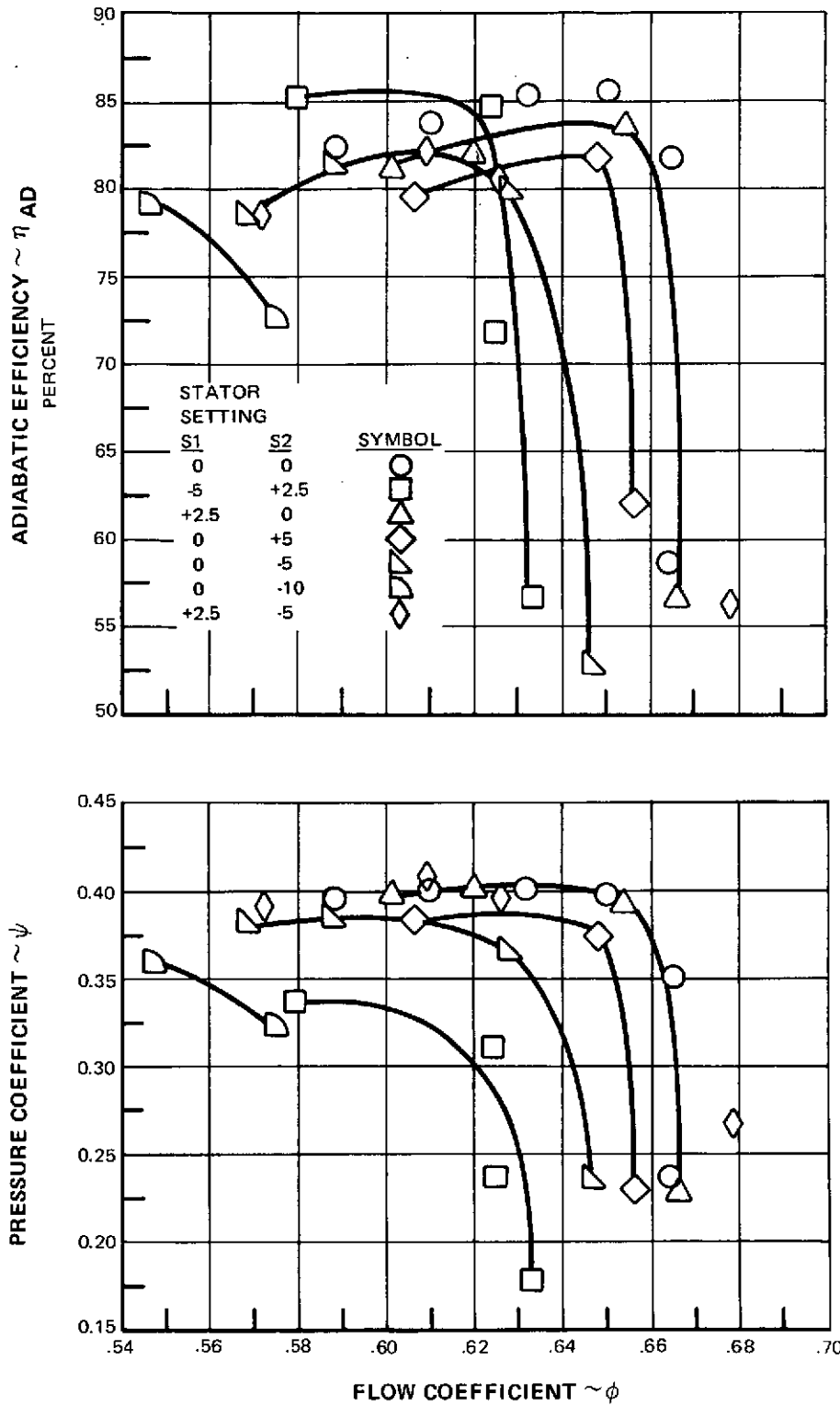


Figure 17 Pressure Coefficient and Adiabatic Efficiency Versus Flow Coefficient for Stage 2 at Design Speed

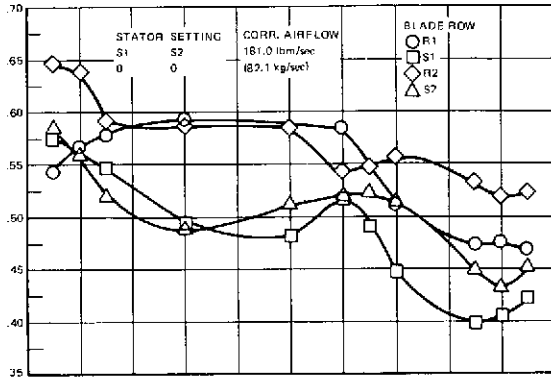


Figure 18A

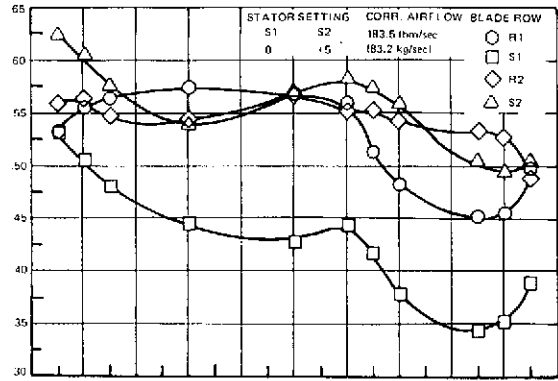


Figure 18D

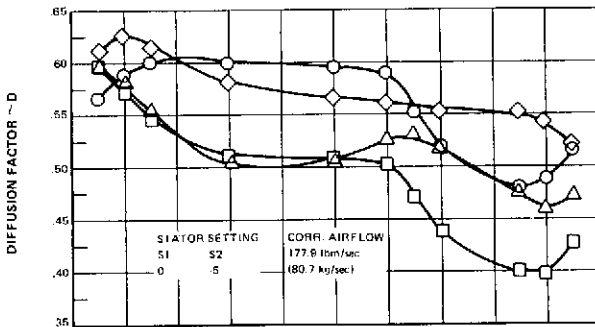


Figure 18B

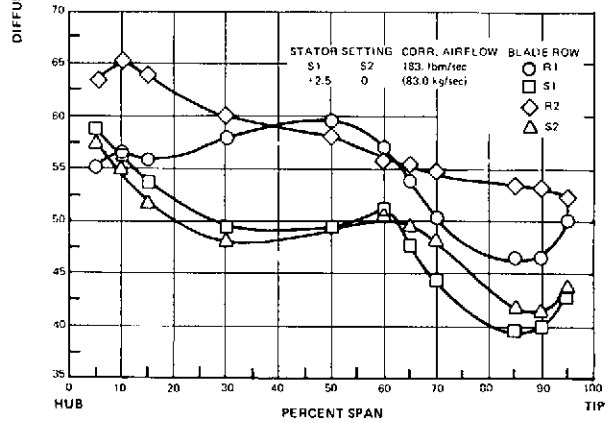


Figure 18E

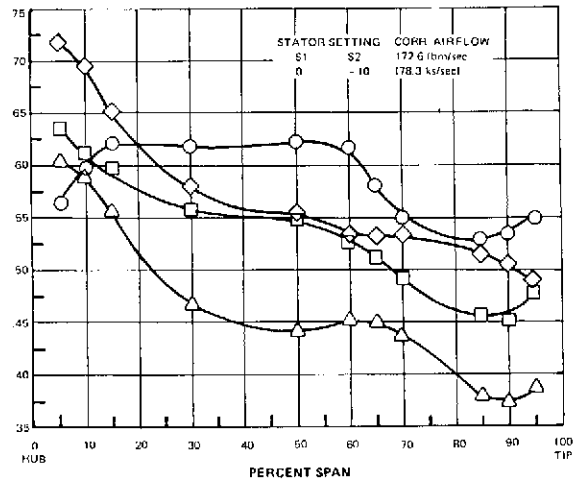


Figure 18C

Figure 18 Diffusion Factor Versus Span for Each Blade Row, Showing Effects of Varying Stator 2 Setting — Near-Stall Data at Design Speed

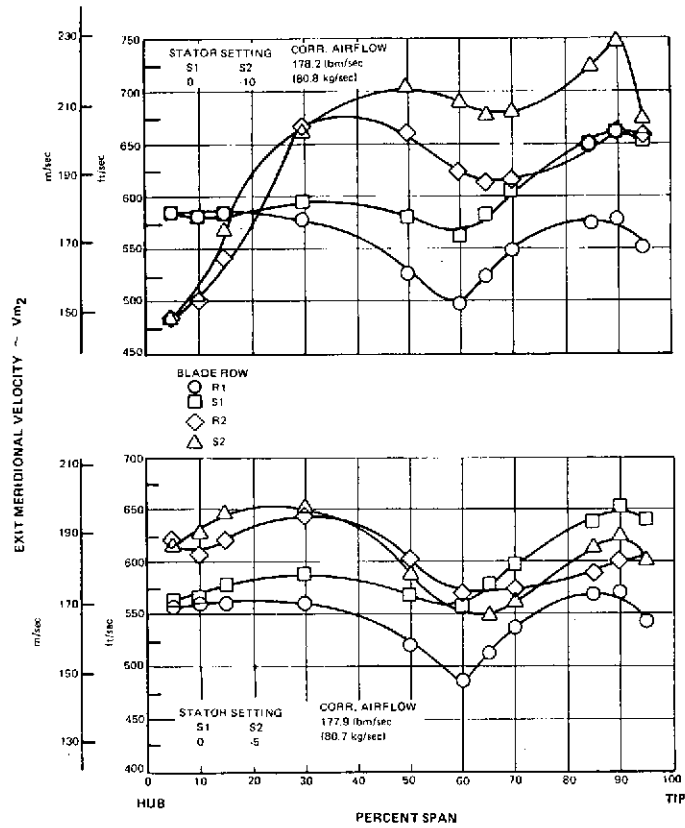


Figure 19 Exit Meridional Velocity Versus Span for All Blade Rows at Design Speed Showing Effects of Varying Stator 2 Setting – Design Speed

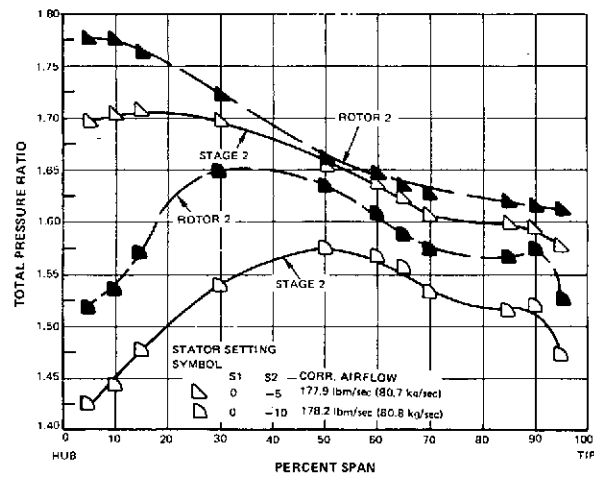


Figure 20 Second-Stage and Rotor 2 Pressure Ratio Versus Span Showing Effects of Varying Stator 2 Setting – Design Speed

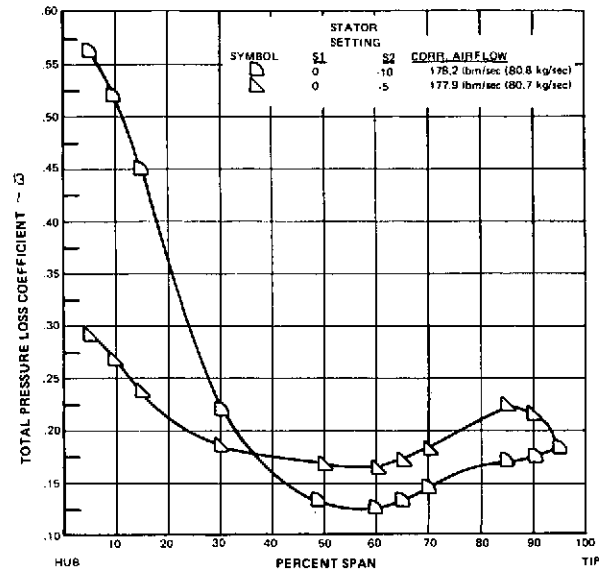


Figure 21 Rotor 2 Total Pressure Loss Coefficient Versus Span at Design Speed for Stator Settings (0, -5) and (0, -10)

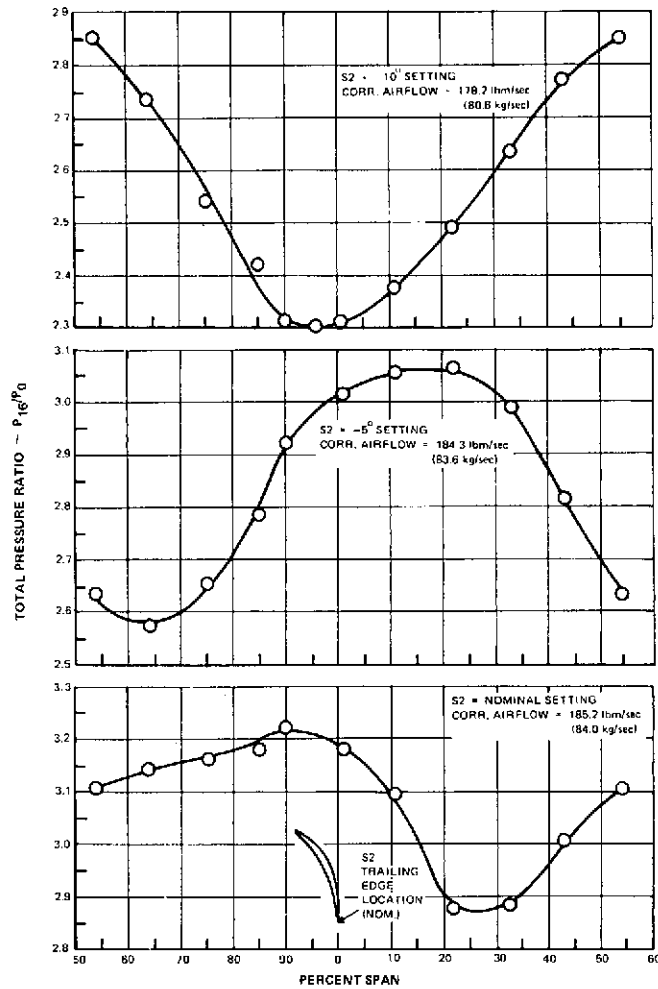


Figure 22 Stator 2 Exit Total Pressure Wakes for 10 Percent Span From the Hub at Design Speed

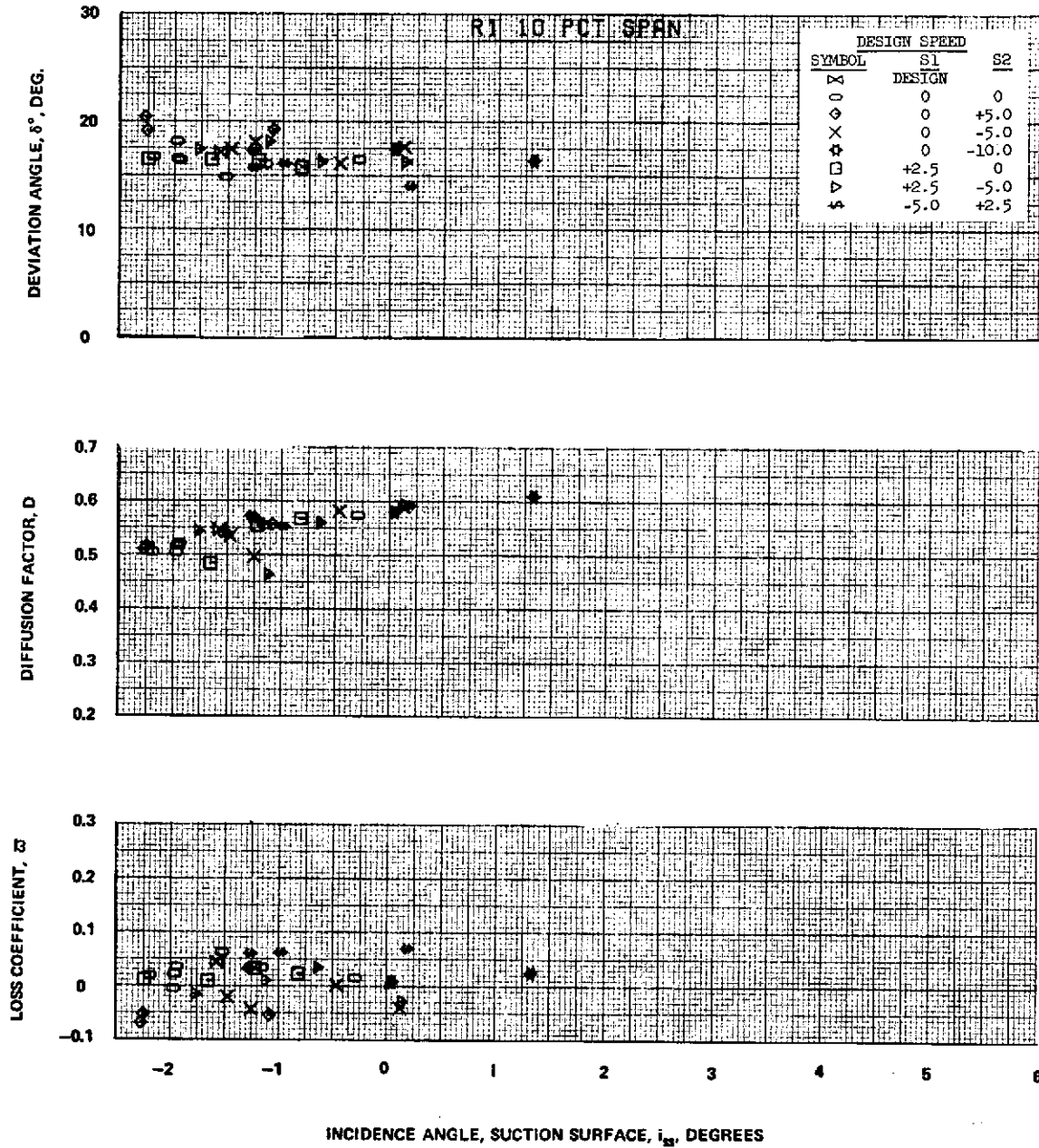


Figure 23A

Figure 23 Blade-Element Performance for Rotor 1 at Design Speed

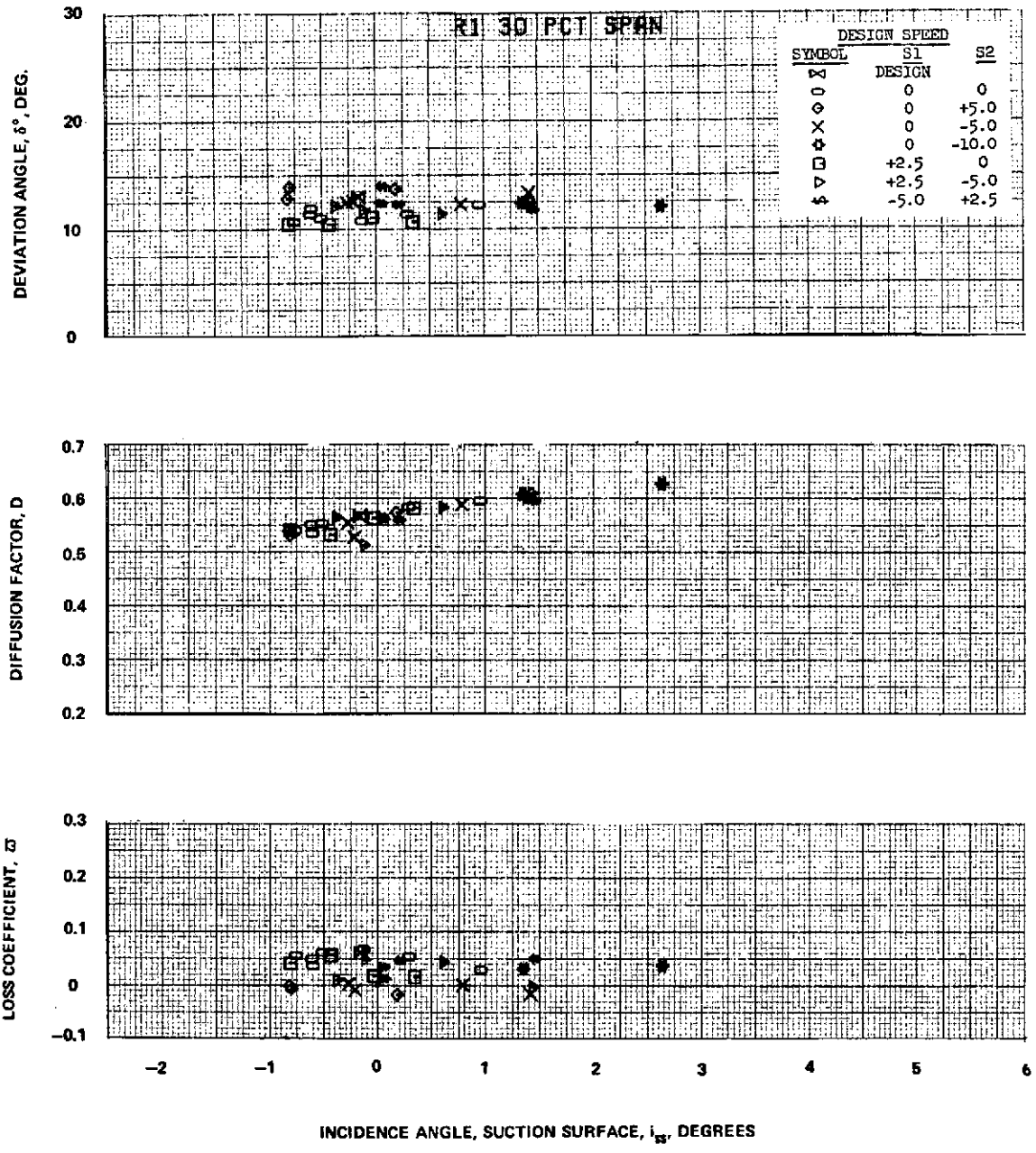


Figure 23B

Figure 23 (Cont'd) Blade-Element Performance for Rotor 1 at Design Speed

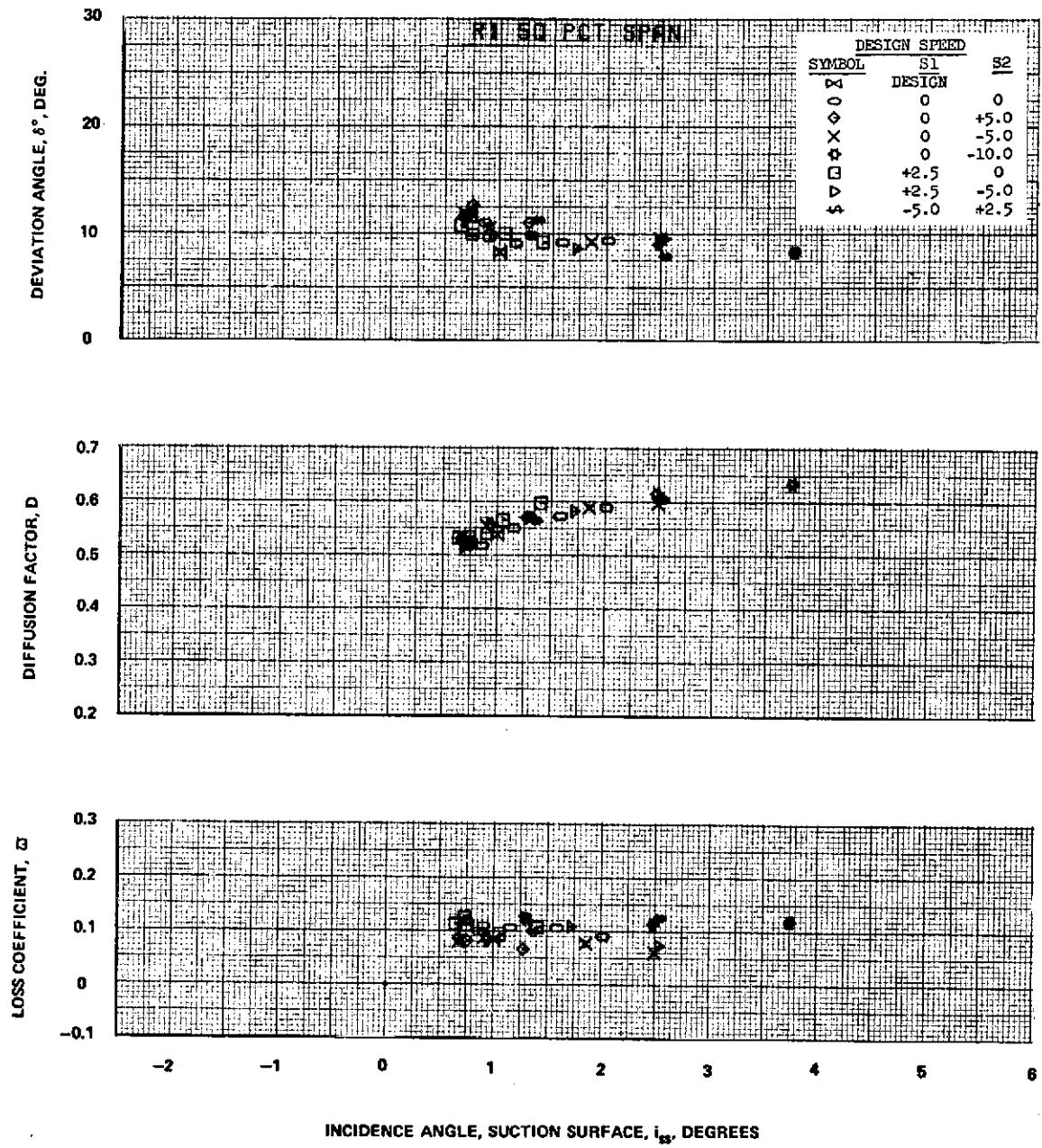


Figure 23C

Figure 23 (Cont'd) Blade-Element Performance for Rotor 1 at Design Speed

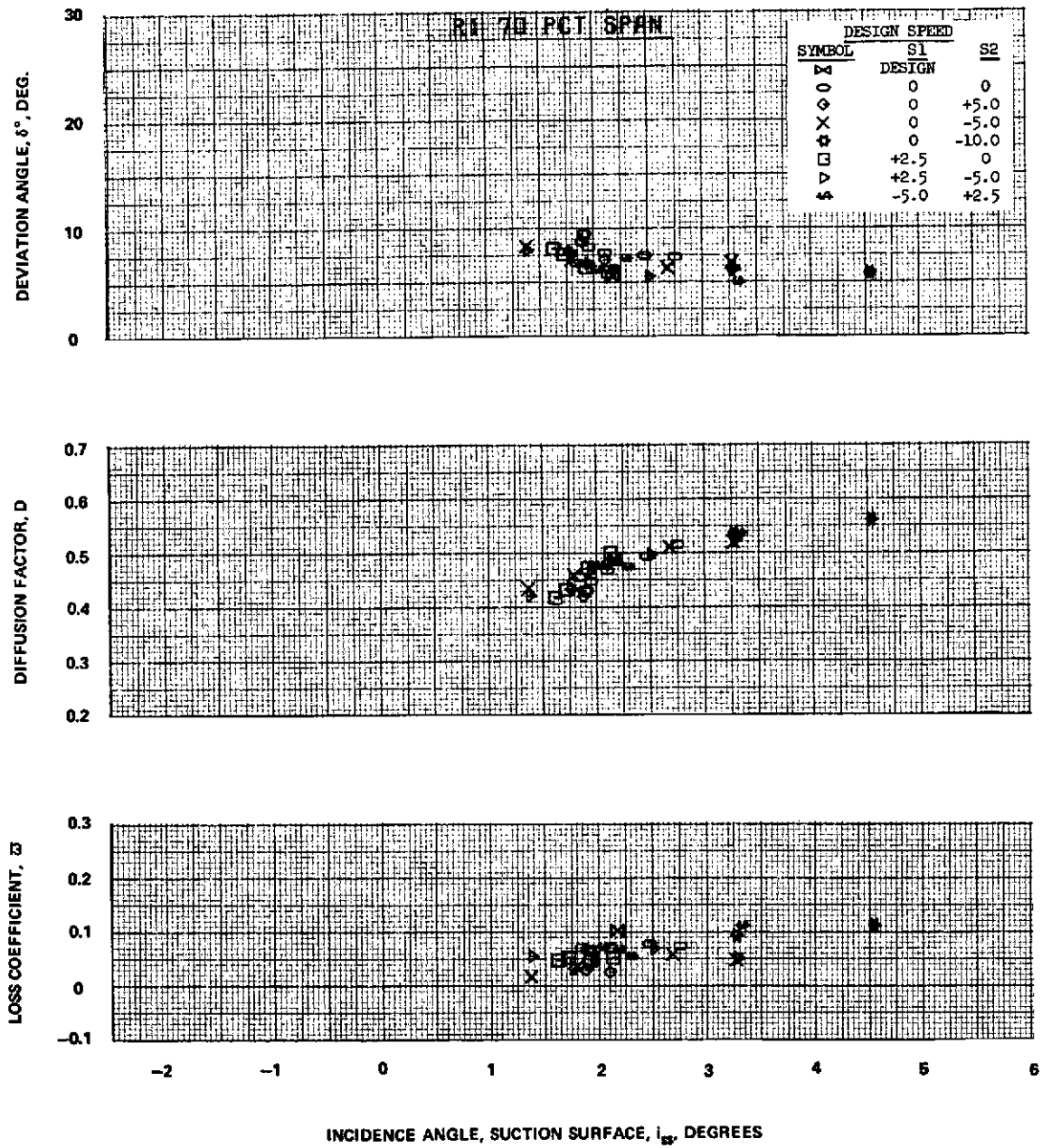


Figure 23D

Figure 23 (Cont'd) Blade-Element Performance for Rotor 1 at Design Speed

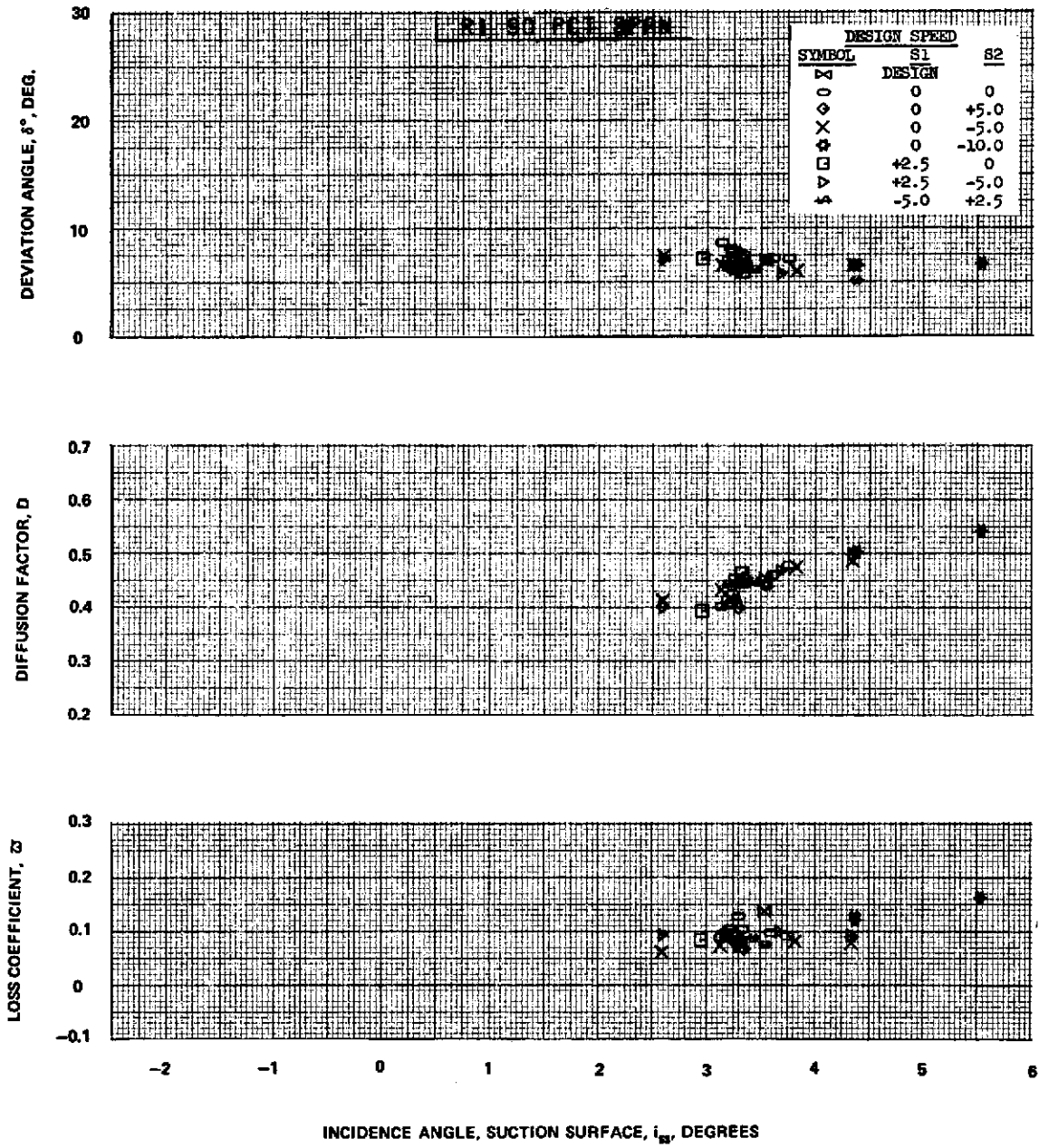


Figure 23E

Figure 23 (Cont'd) Blade-Element Performance for Rotor 1 at Design Speed

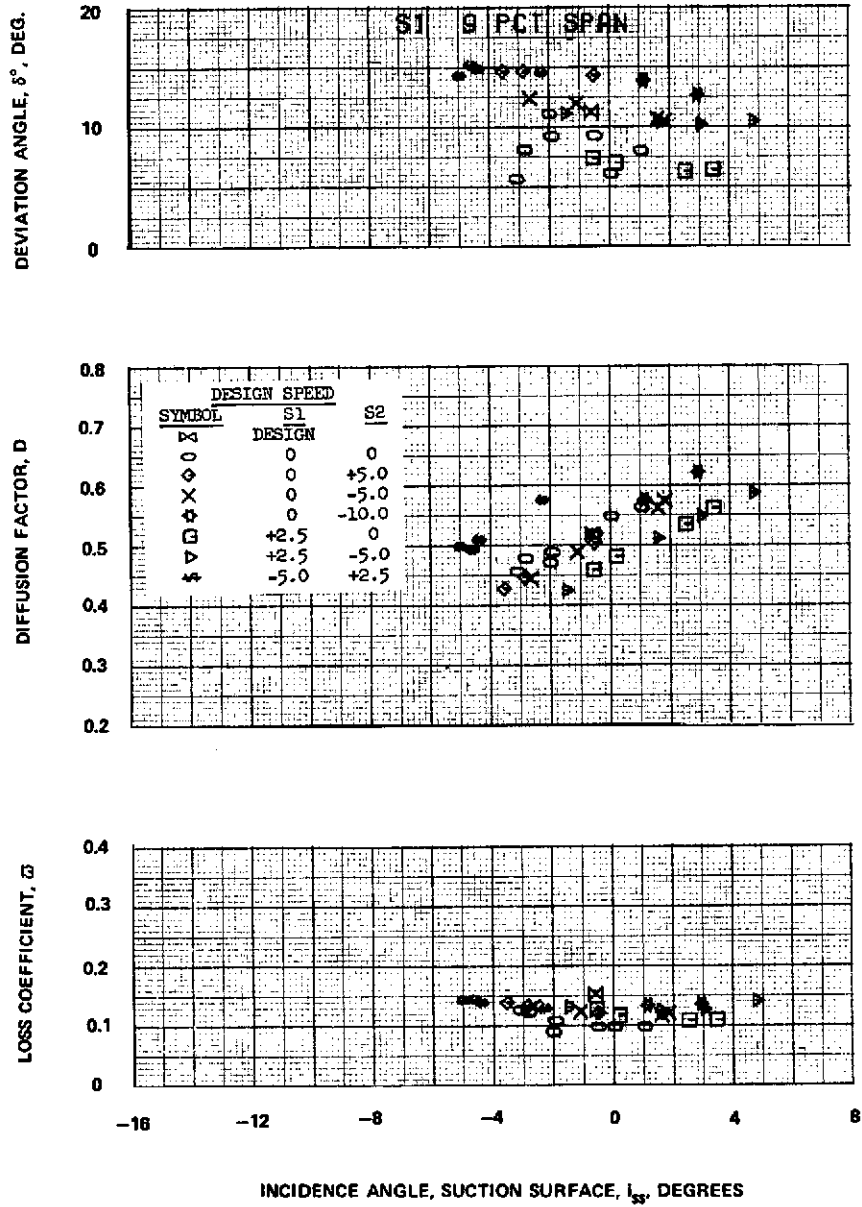


Figure 24A

Figure 24 Blade-Element Performance for Stator 1 at Design Speed

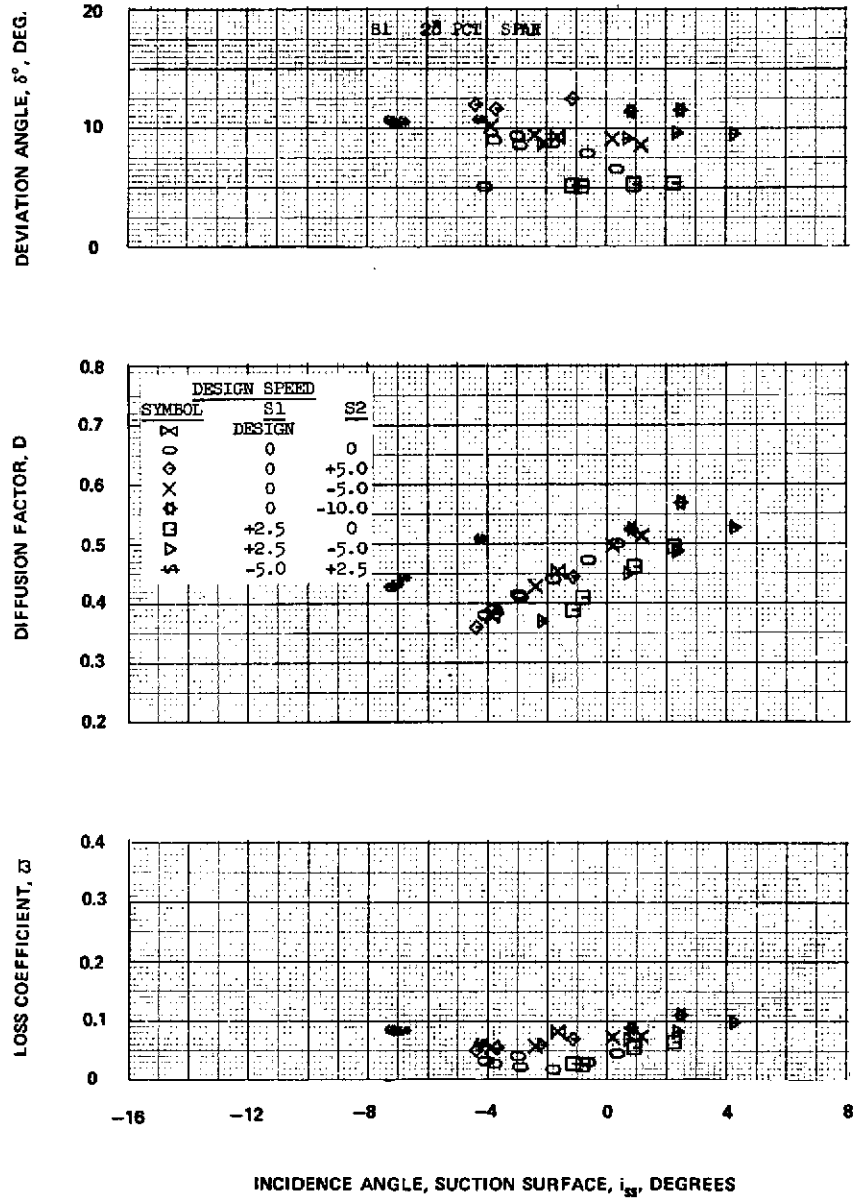


Figure 24B

Figure 24 (Cont'd) Blade-Element Performance for Stator 1 at Design Speed

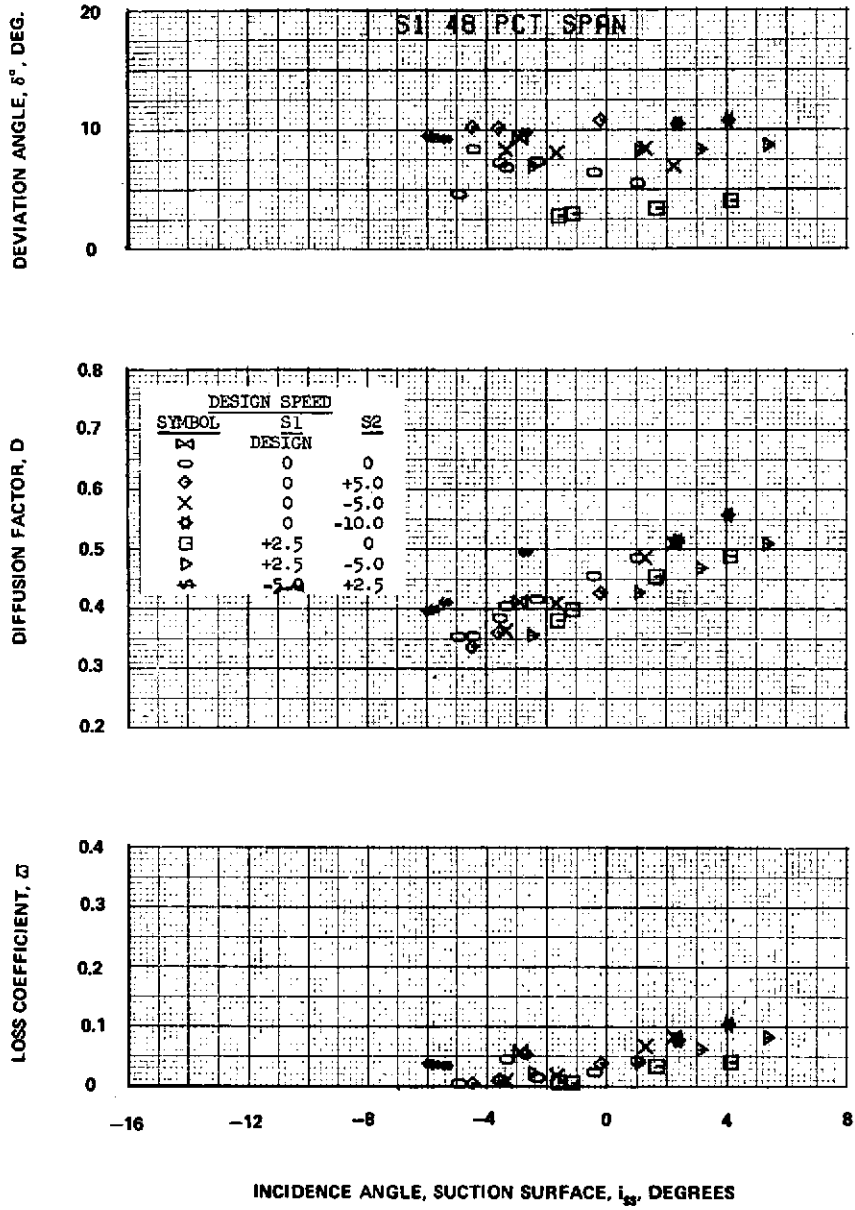


Figure 24C

Figure 24 (Cont'd) Blade-Element Performance for Stator 1 at Design Speed

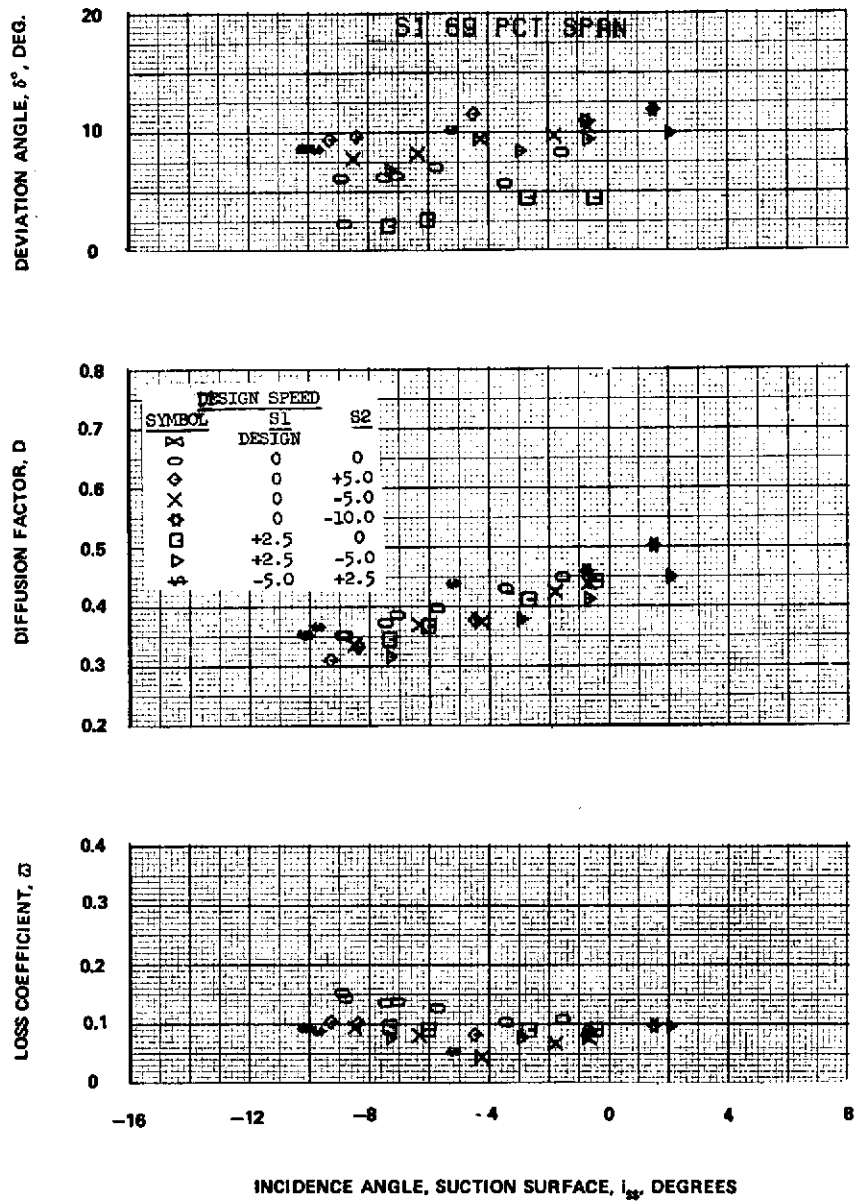


Figure 24D

Figure 24 (Cont'd) Blade-Element Performance for Stator 1 at Design Speed

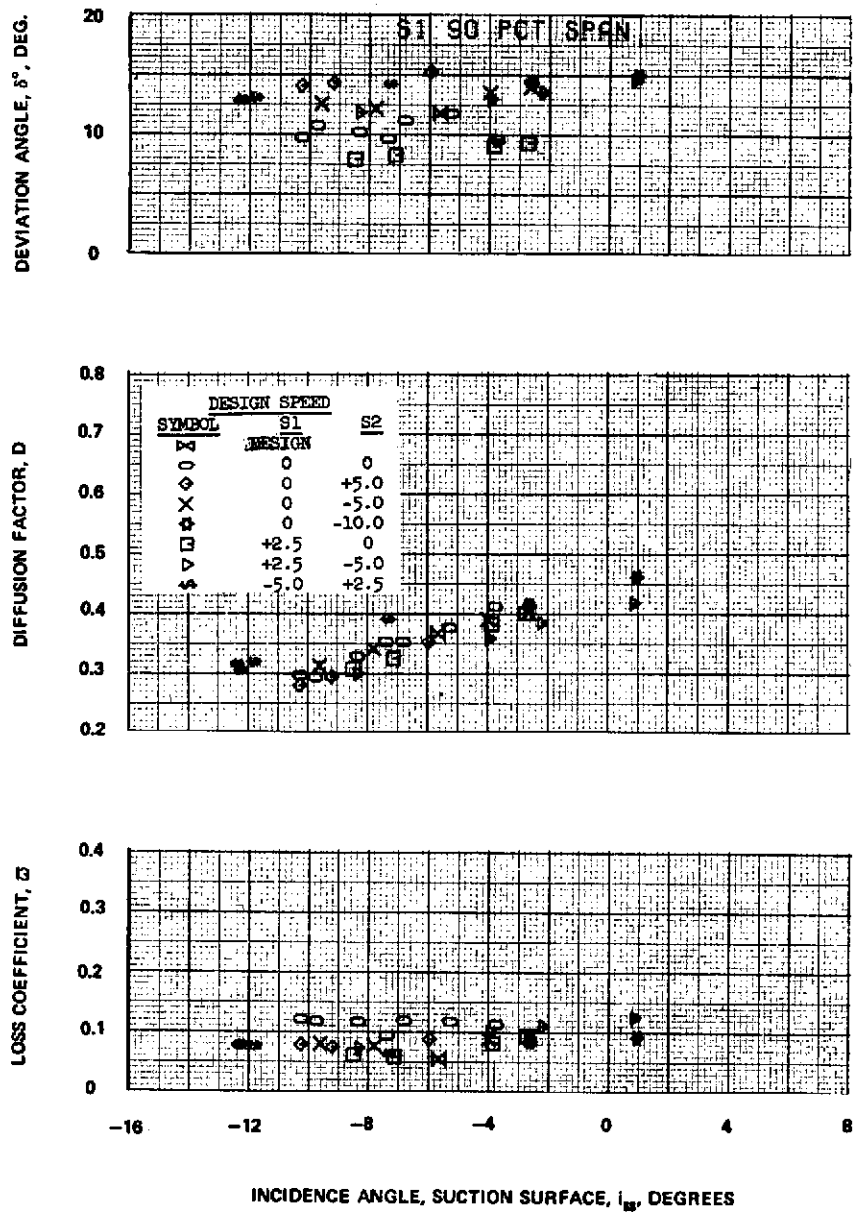


Figure 24E

Figure 24 (Cont'd) Blade-Element Performance for Stator 1 at Design Speed

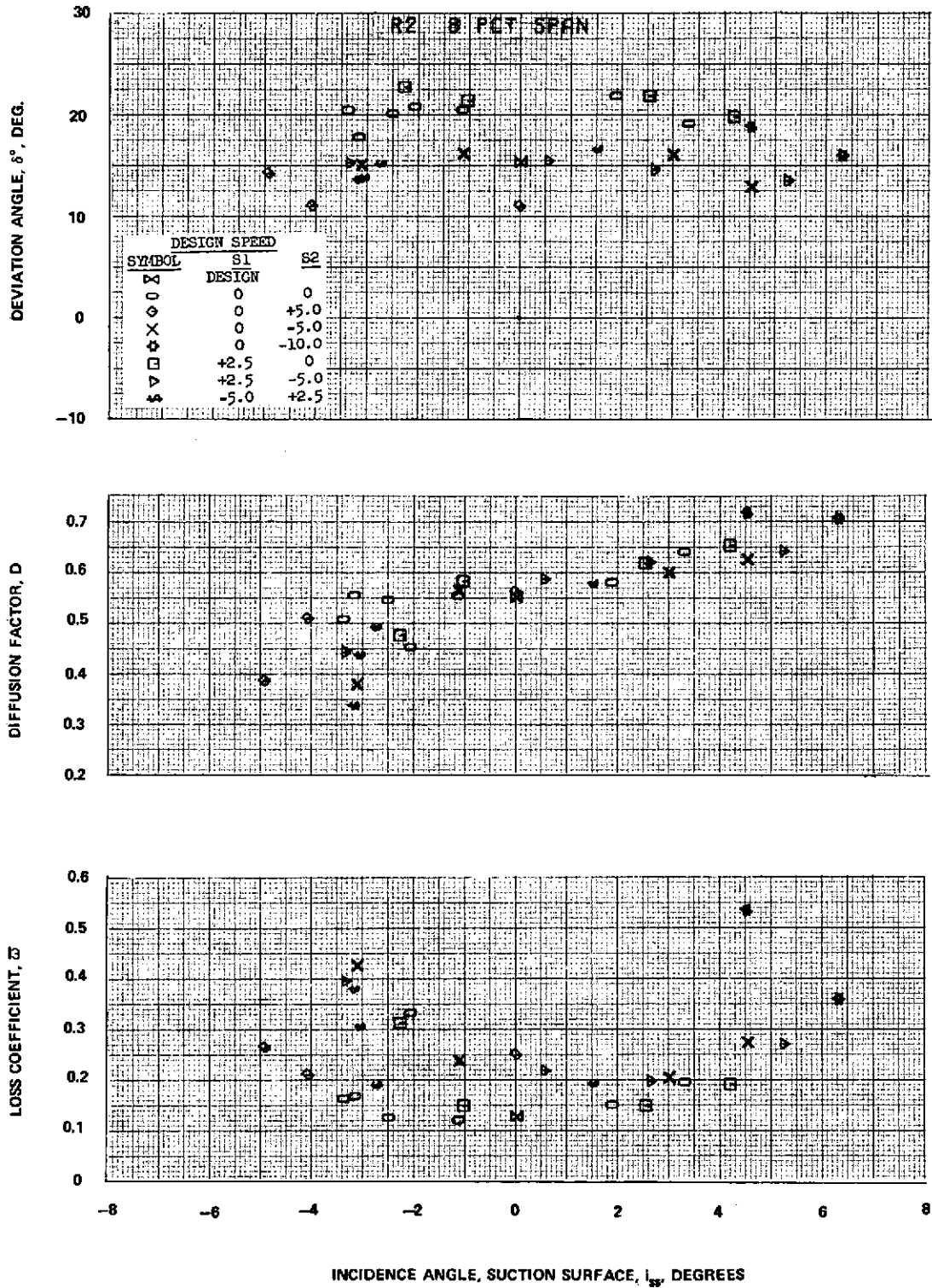
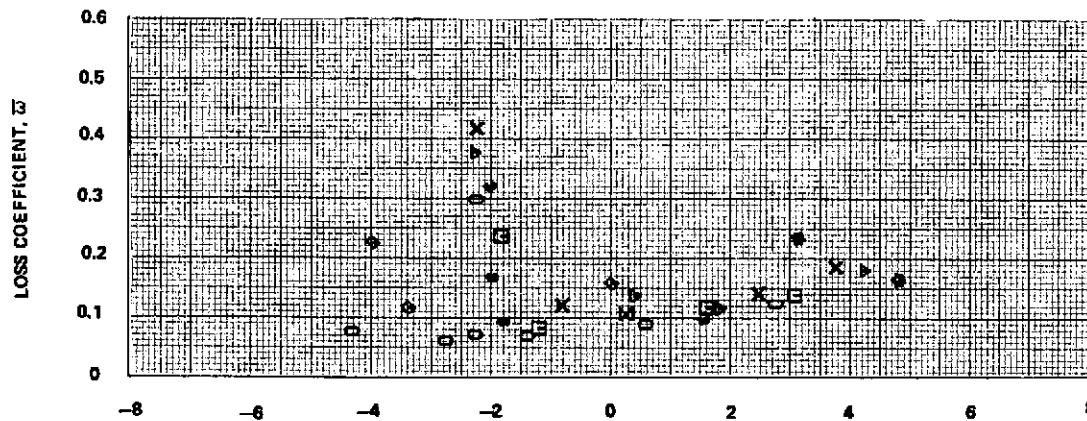
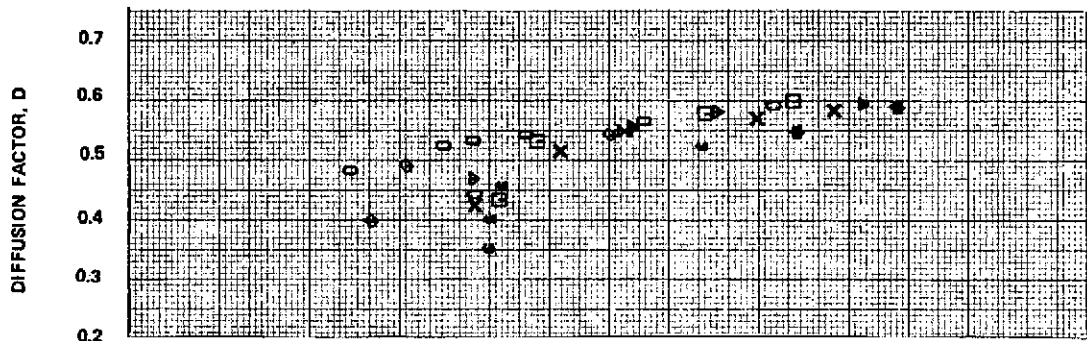
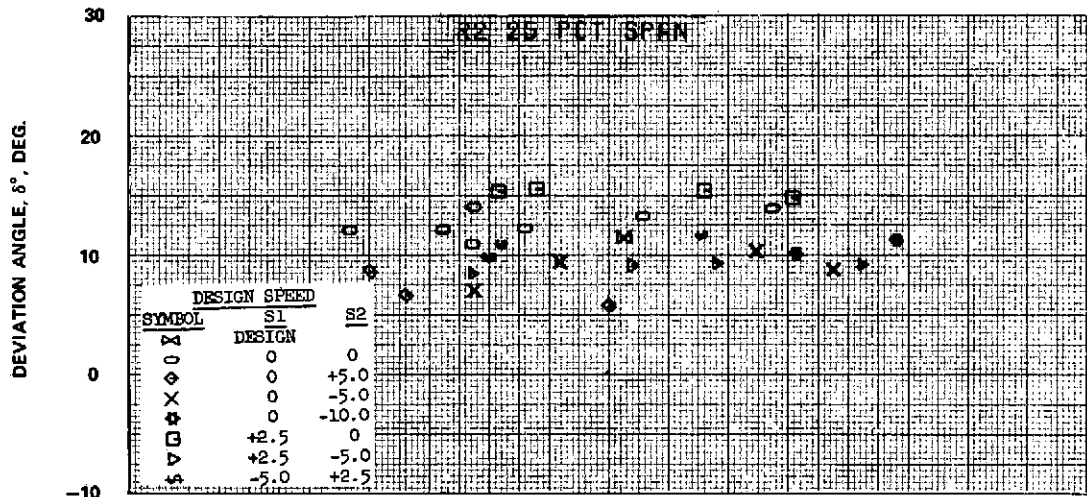


Figure 25A

Figure 25 Blade-Element Performance for Rotor 2 at Design Speed



INCIDENCE ANGLE, SUCTION SURFACE, i_{ss} , DEGREES

Figure 25B

Figure 25 (Cont'd) Blade-Element Performance for Rotor 2 at Design Speed

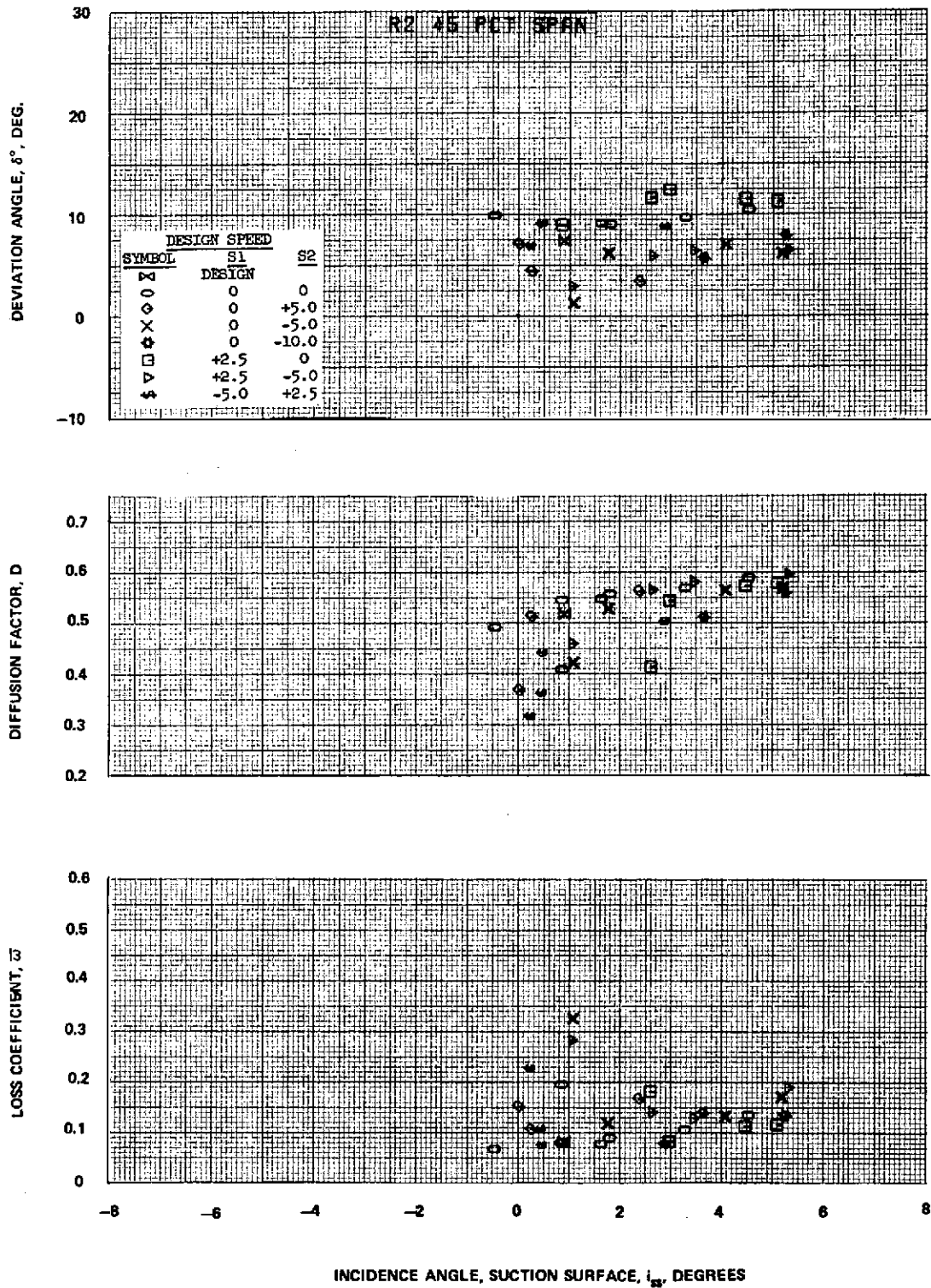


Figure 25C

Figure 25 (Cont'd) Blade-Element Performance for Rotor 2 at Design Speed

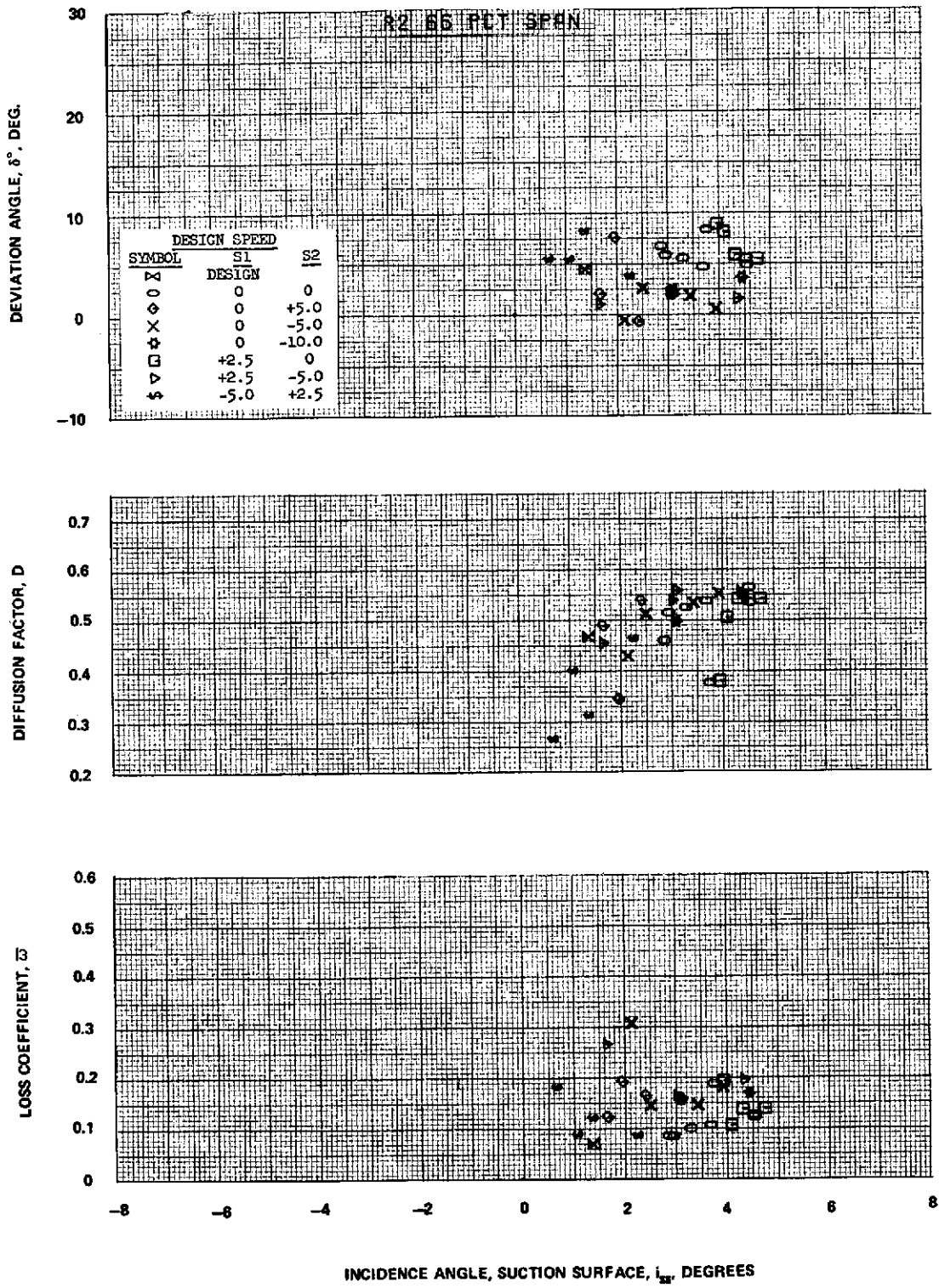


Figure 25D

Figure 25 (Cont'd) Blade-Element Performance for Rotor 2 at Design Speed

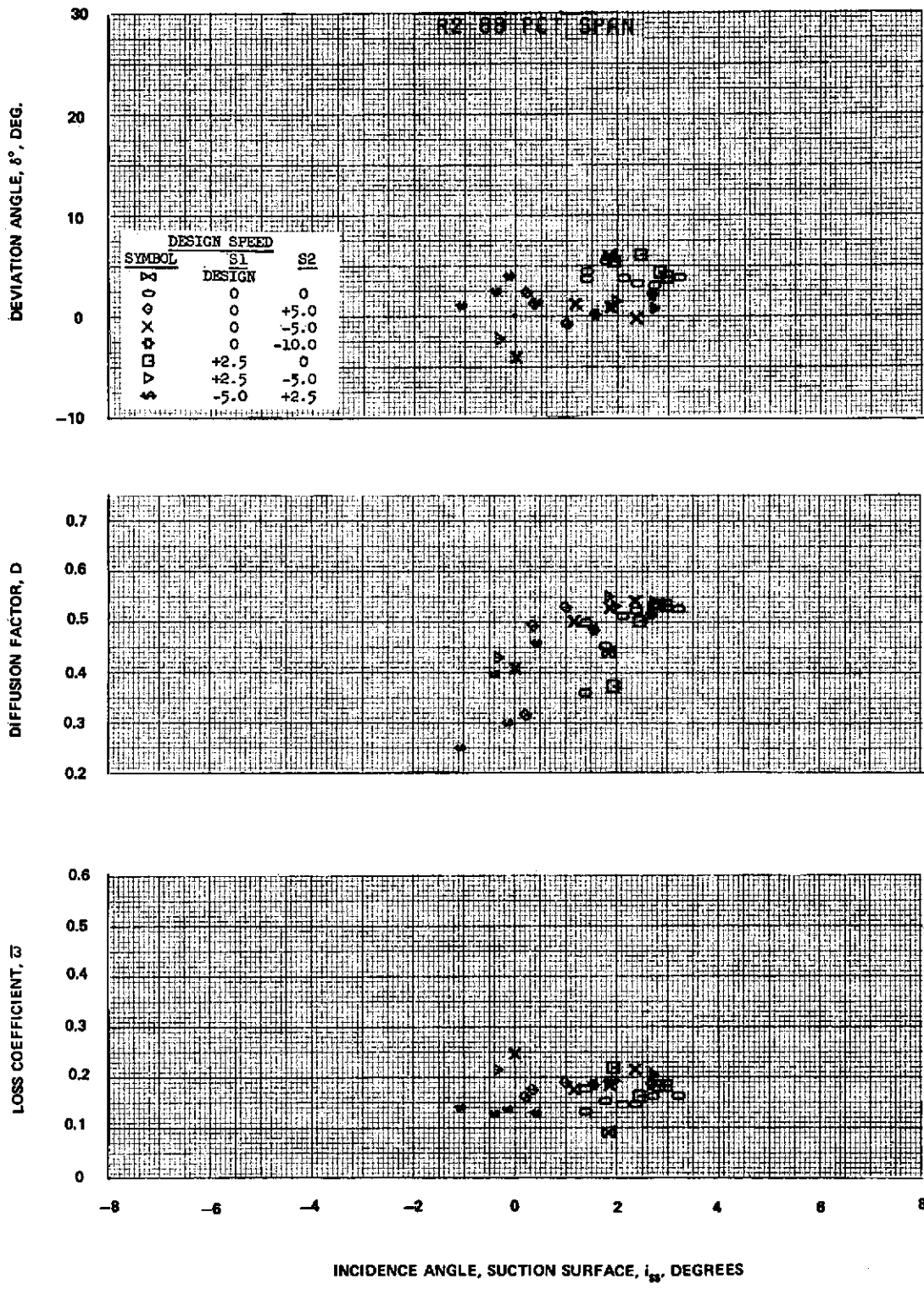


Figure 25E

Figure 25 (Cont'd) Blade-Element Performance for Rotor 2 at Design Speed

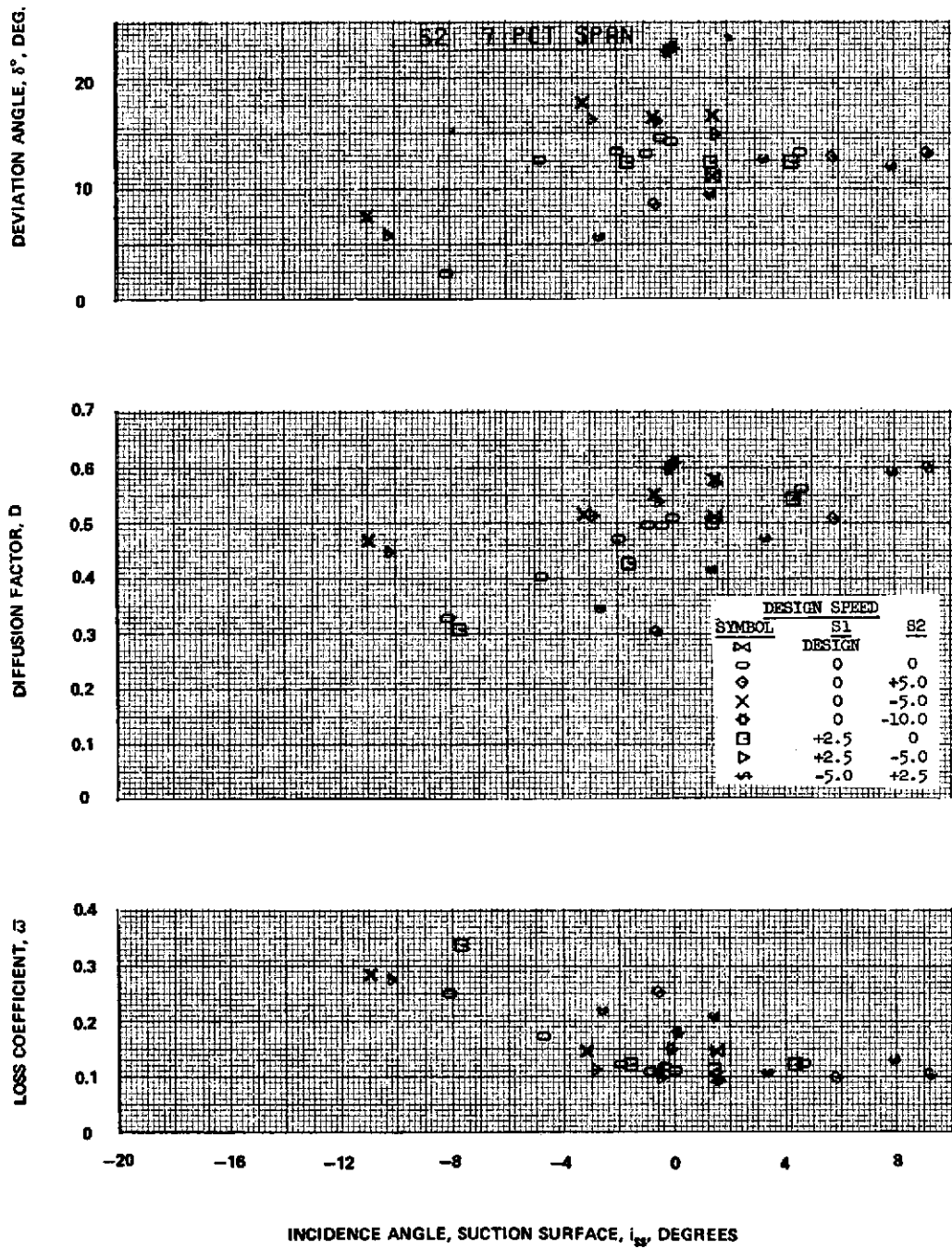


Figure 26A

Figure 26 Blade-Element Performance for Stator 2 at Design Speed

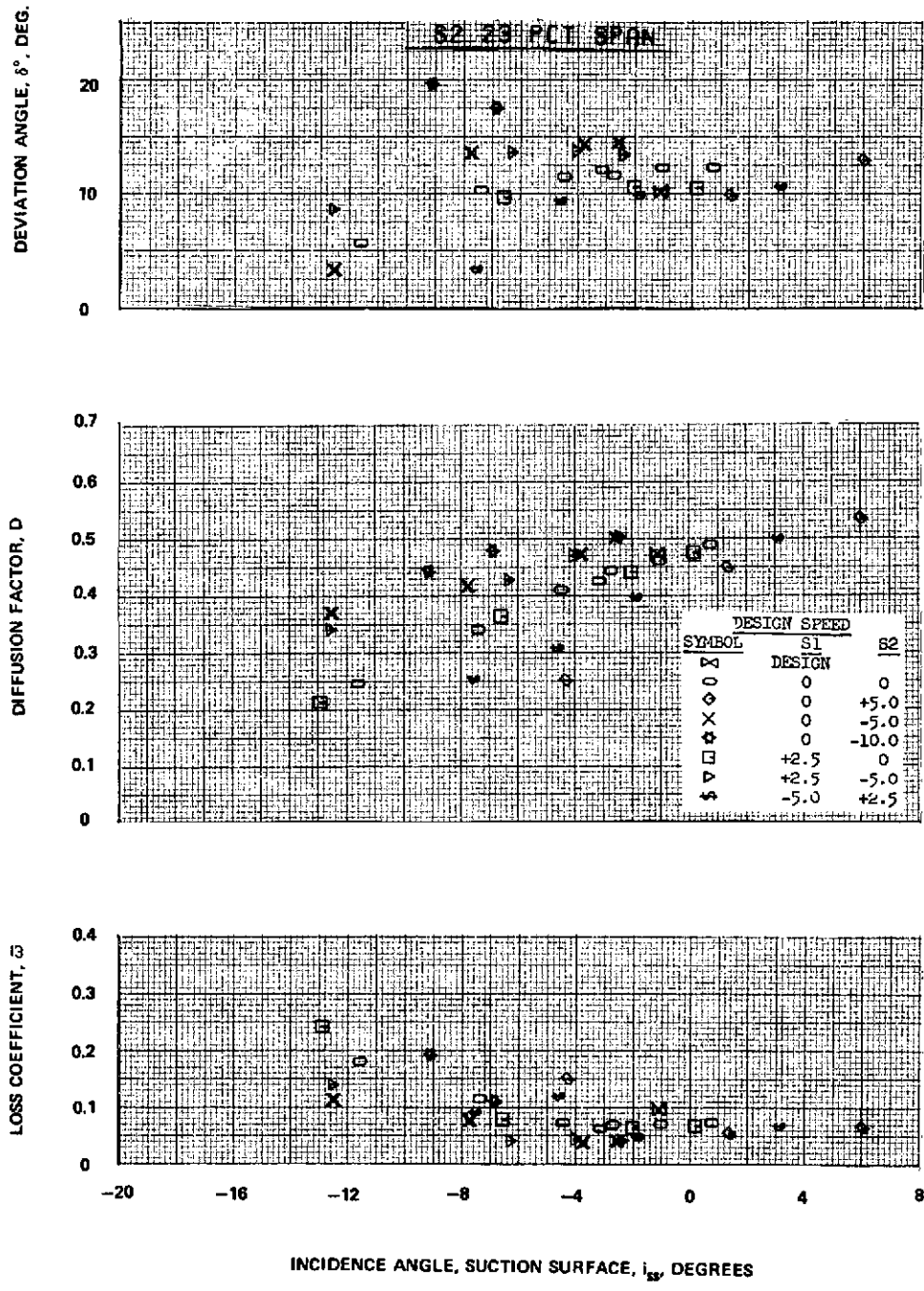


Figure 26B

Figure 26 (Cont'd) Blade-Element Performance for Stator 2 at Design Speed

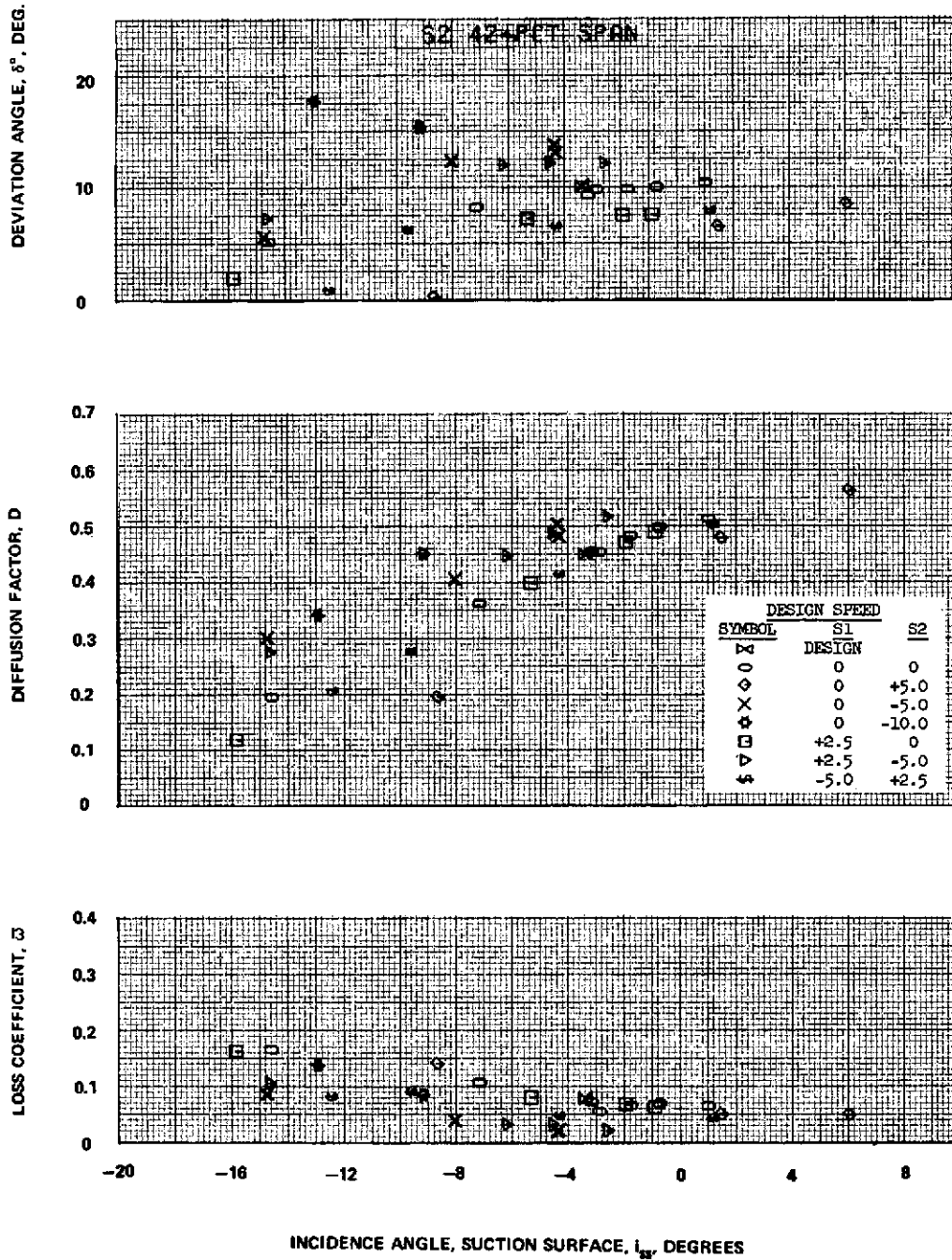


Figure 26C

Figure 26 (Cont'd) Blade-Element Performance for Stator 2 at Design Speed

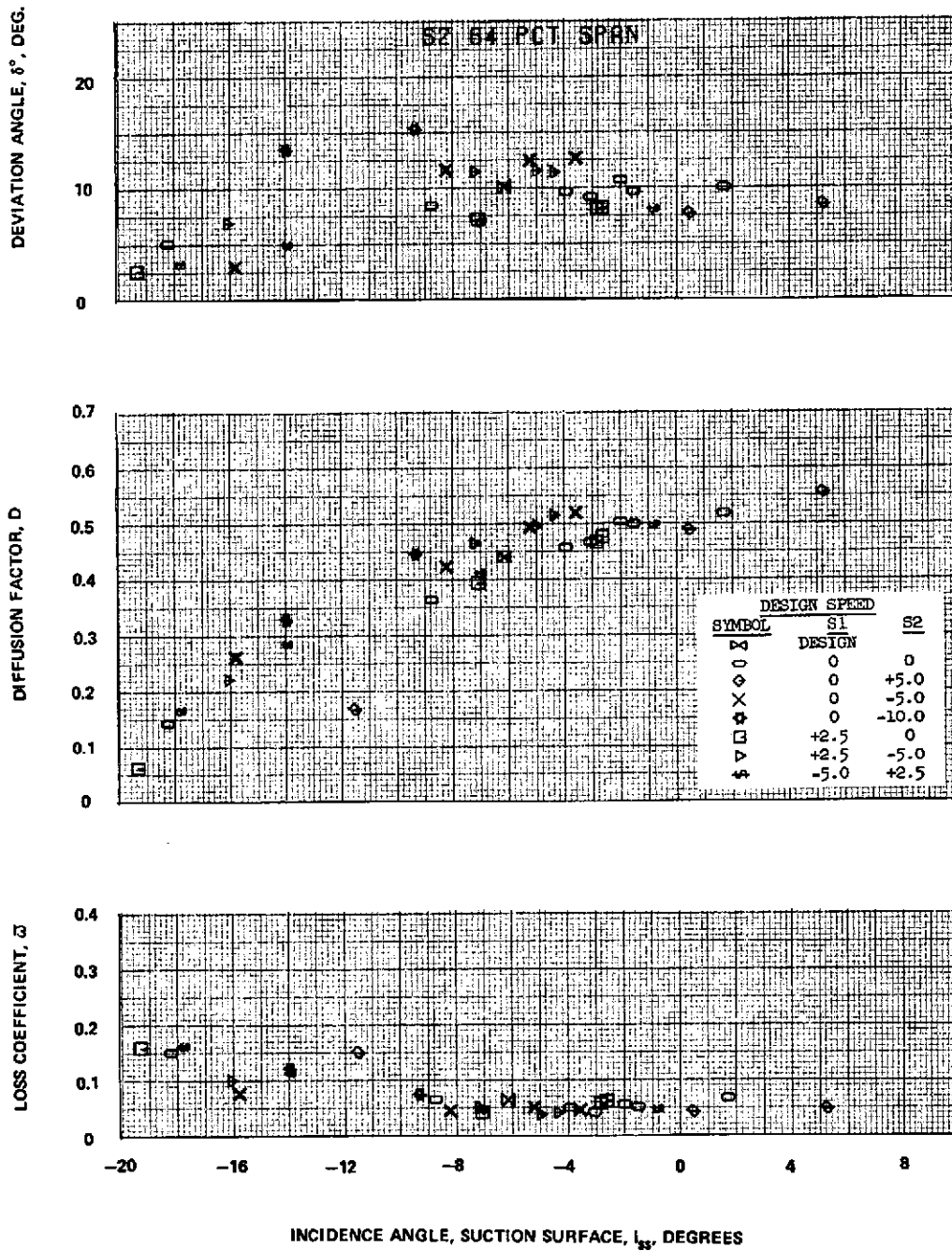


Figure 26D

Figure 26 (Cont'd) Blade-Element Performance for Stator 2 at Design Speed

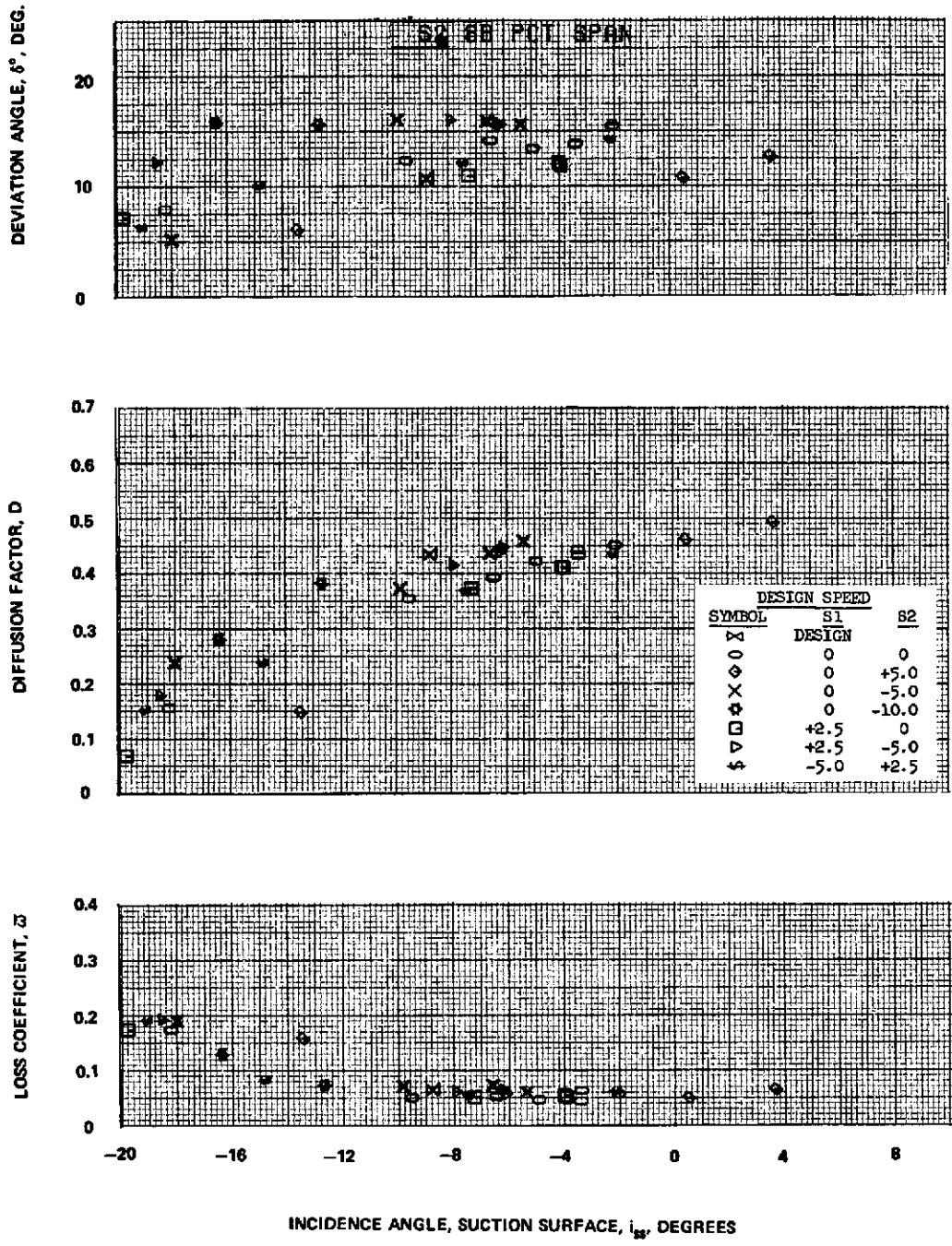


Figure 26E

Figure 26 (Cont'd) Blade-Element Performance for Stator 2 at Design Speed

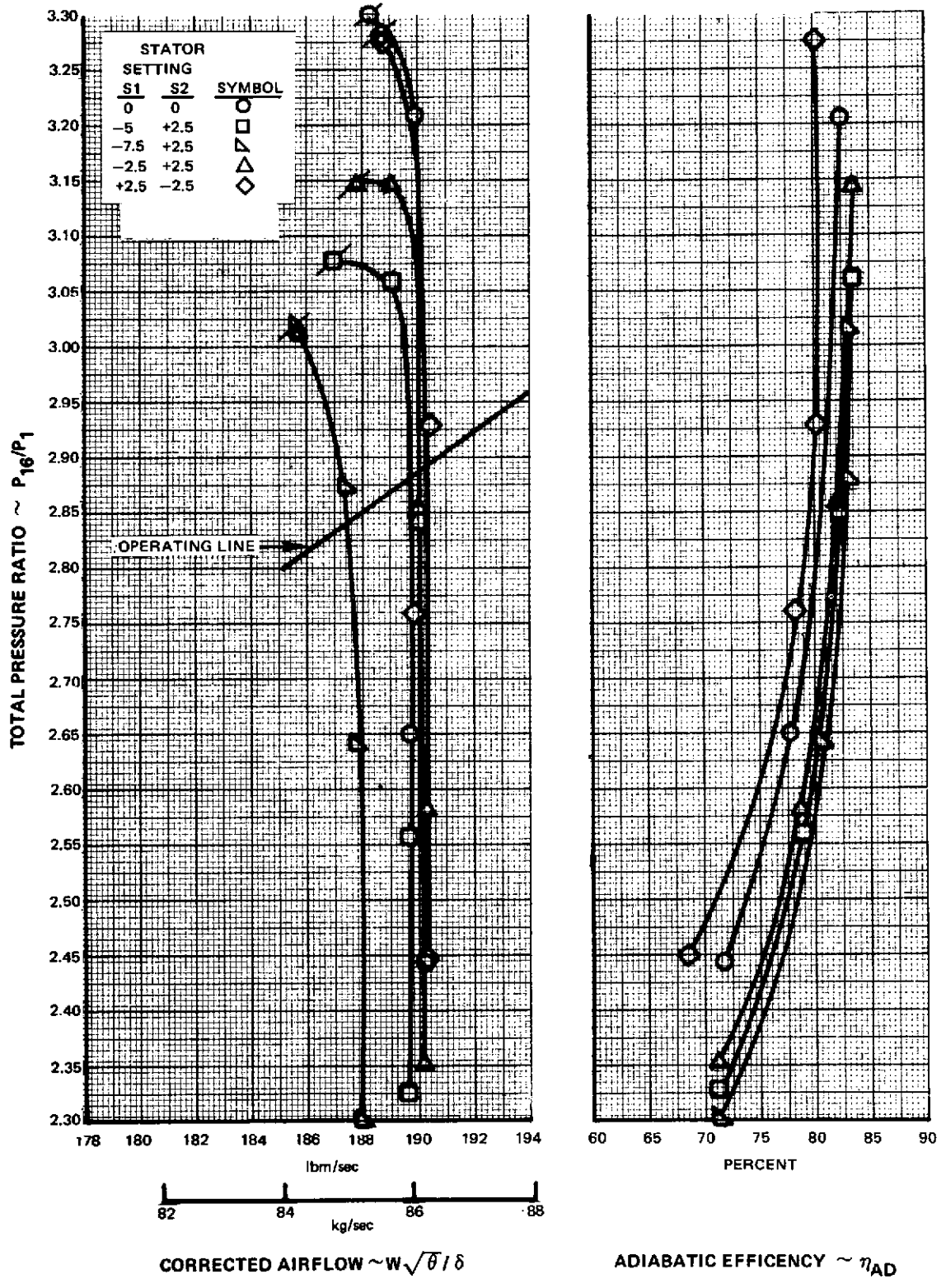


Figure 27 Fan Overall Performance at 105 Percent of Design Speed

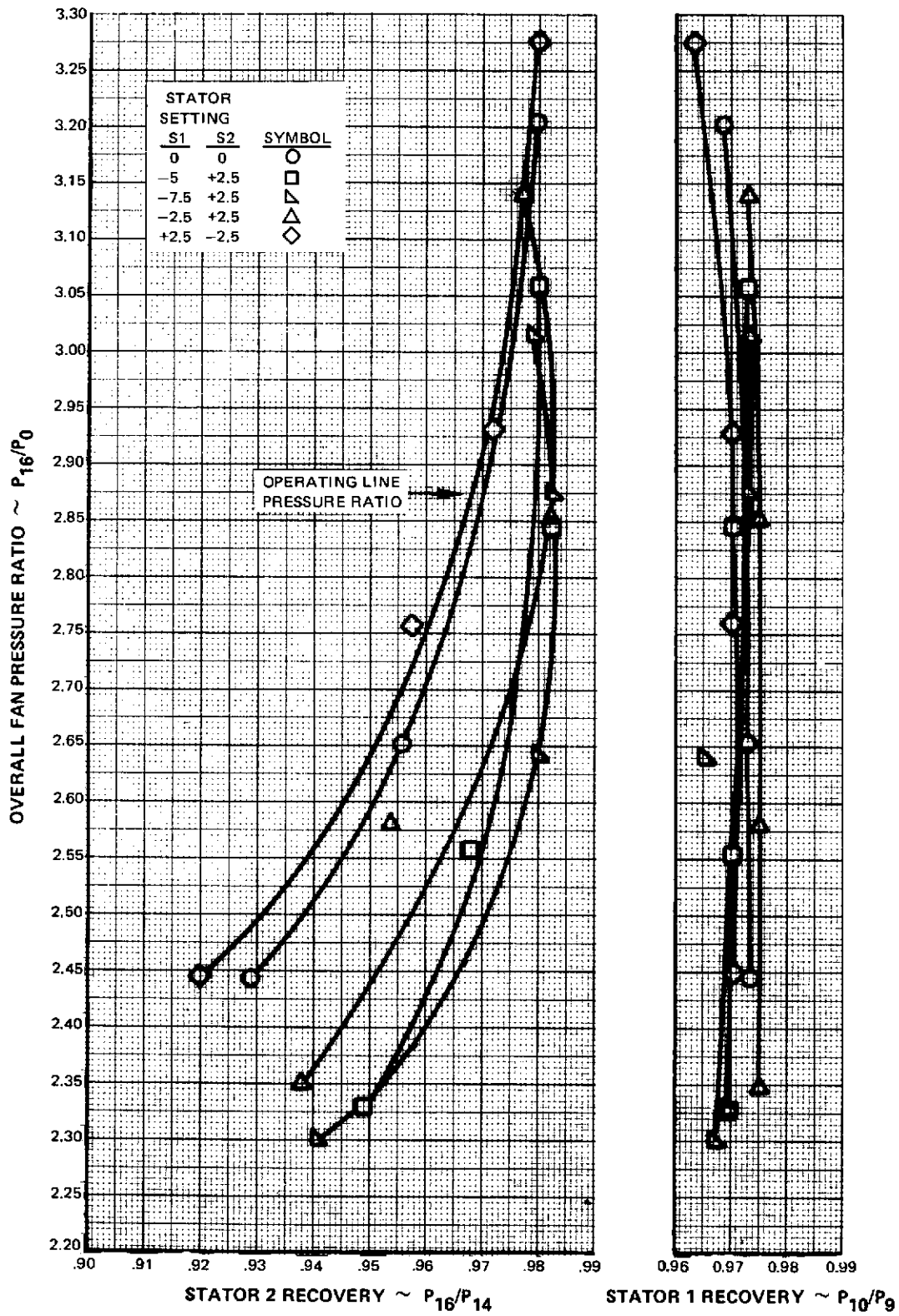


Figure 28 Stator Total Pressure Recovery Versus Fan Pressure Ratio at 105 Percent of Design Speed

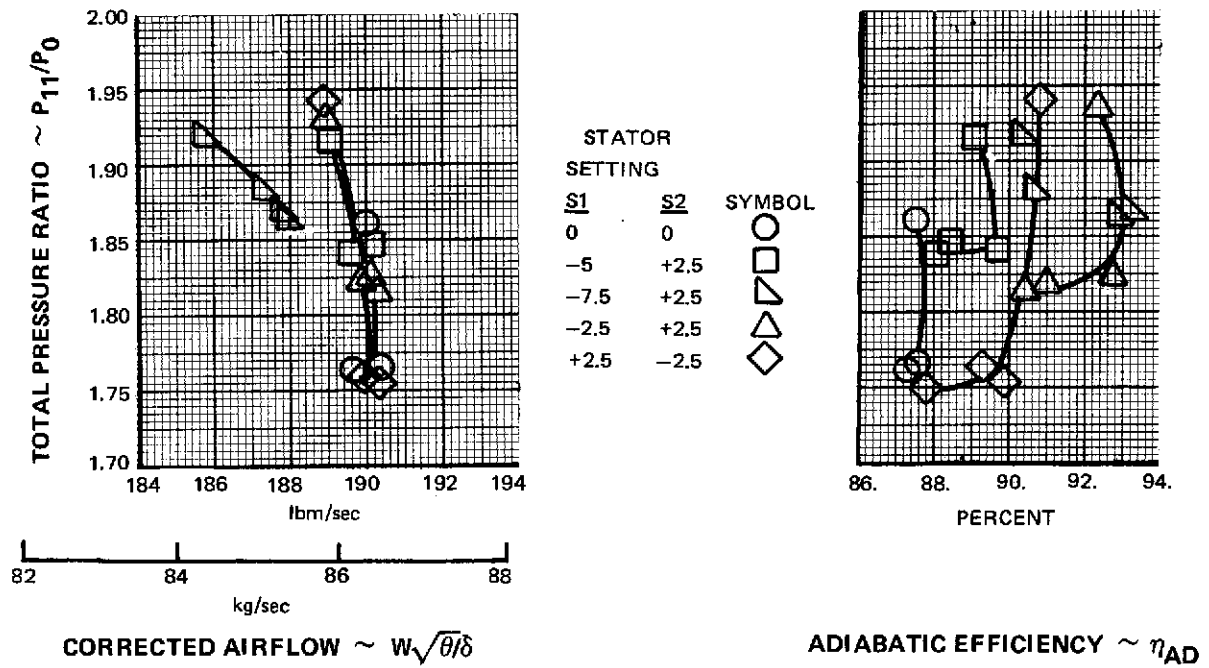


Figure 29 Rotor 1 Performance at 105 Percent of Design Speed

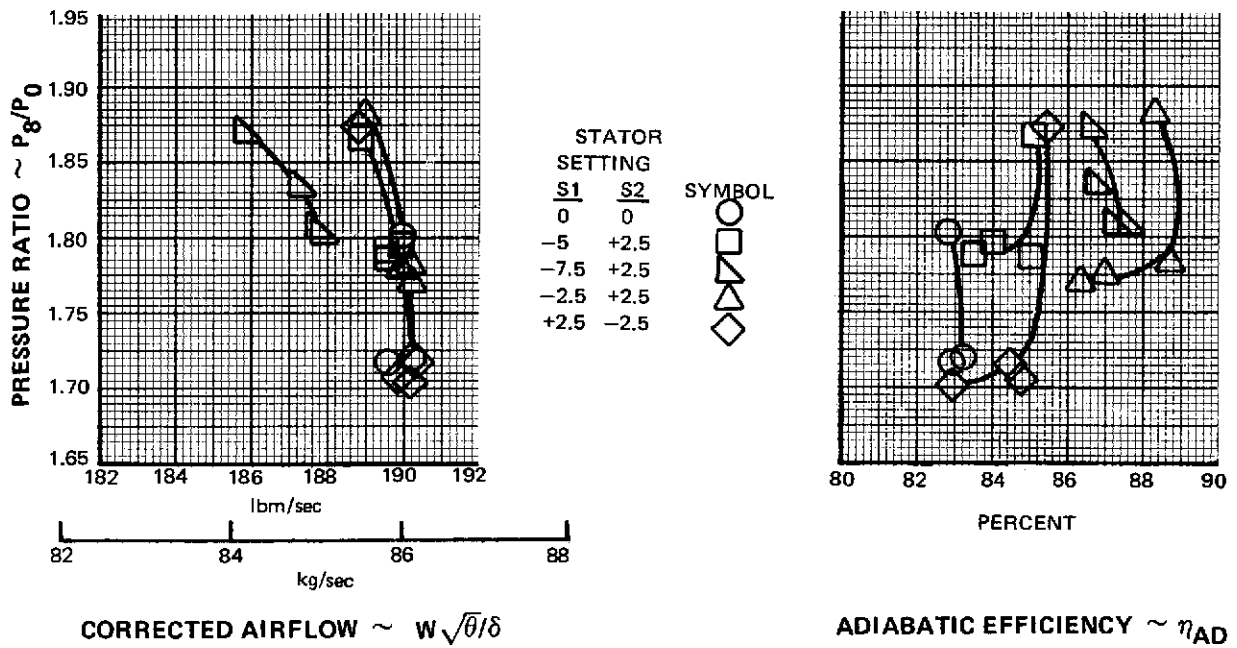


Figure 30 First-Stage Performance at 105 Percent of Design Speed

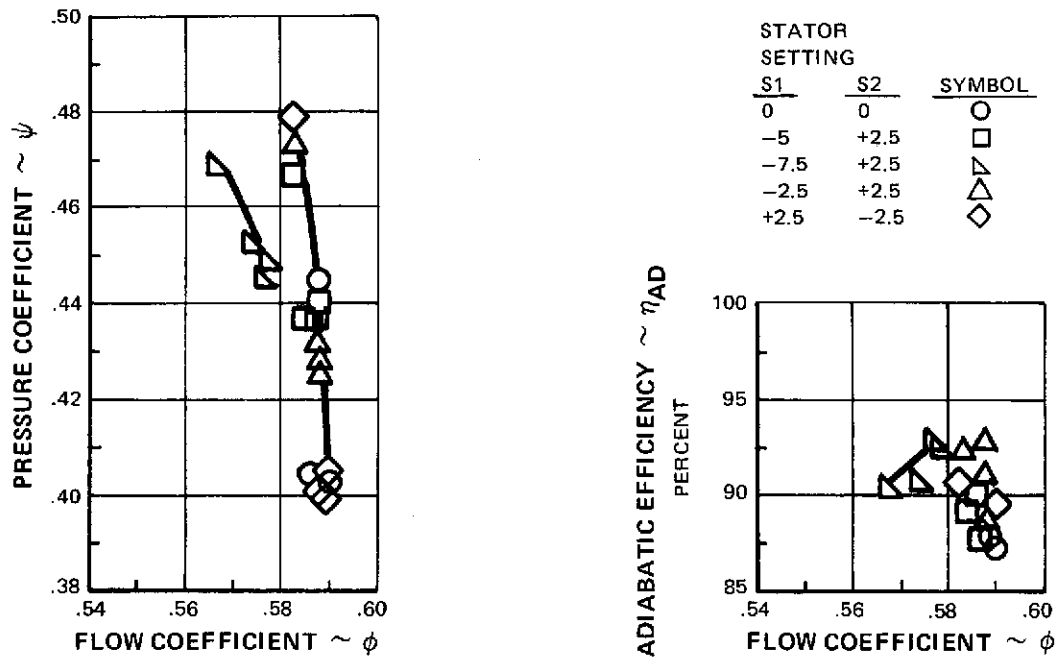


Figure 31 Pressure Coefficient and Adiabatic Efficiency Versus Flow Coefficient for Rotor 1 at 105 Percent of Design Speed

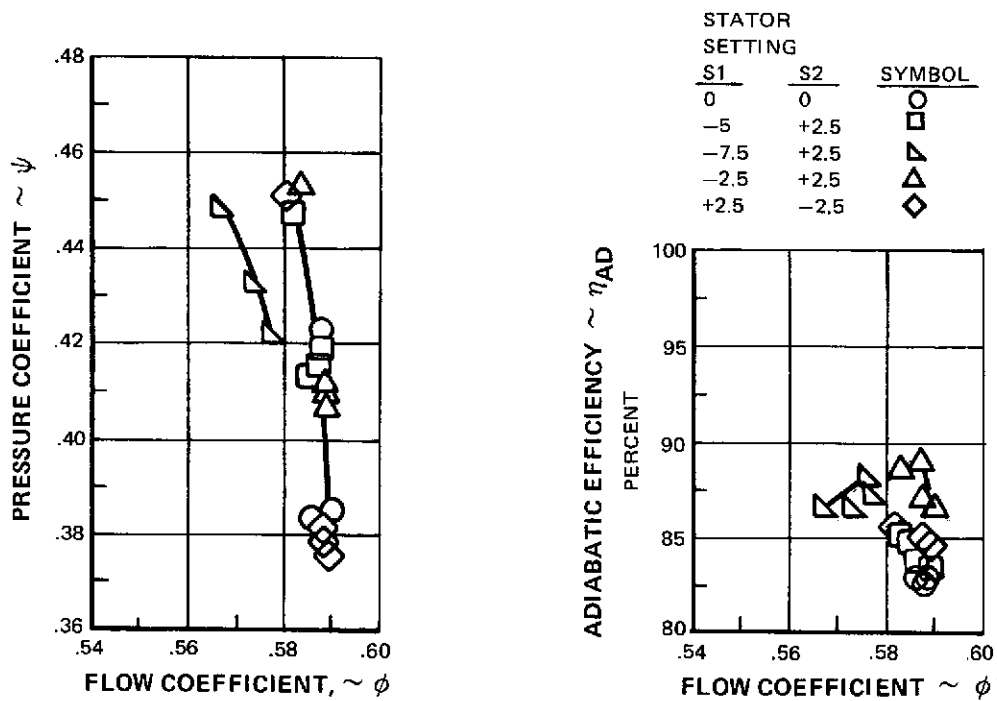


Figure 32 Pressure Coefficient and Adiabatic Efficiency Versus Flow Coefficient for the First Stage at 105 Percent of Design Speed

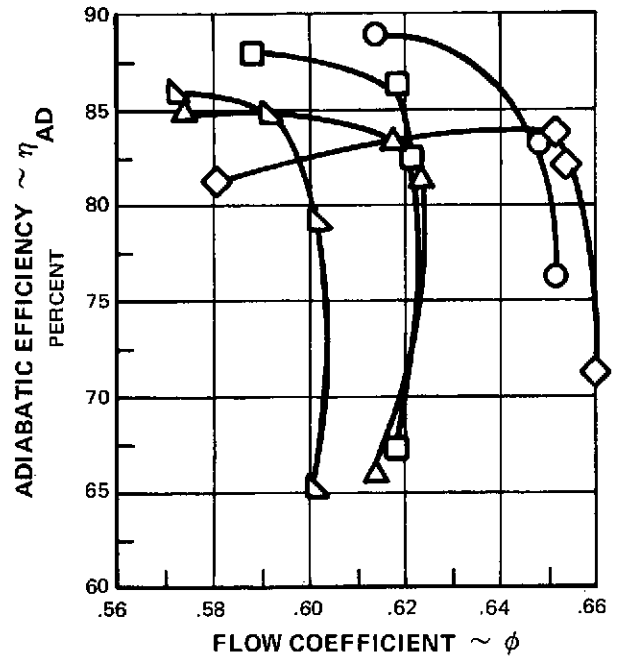
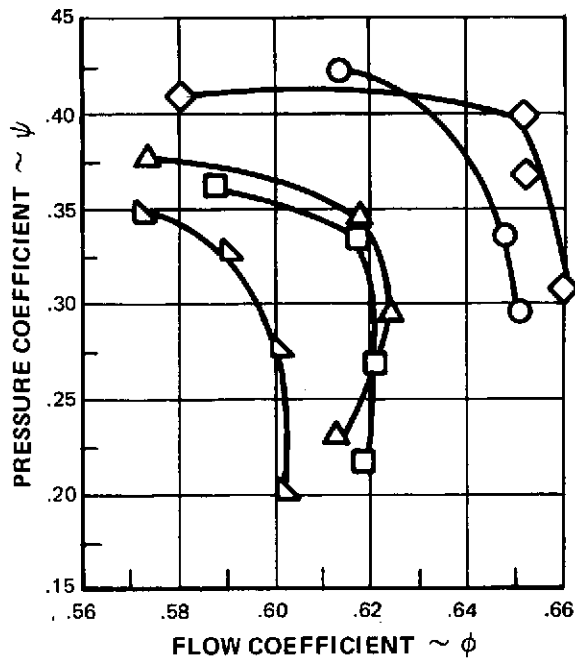


Figure 33 Pressure Coefficient and Adiabatic Efficiency Versus Flow Coefficient for Rotor 2 at 105 Percent of Design Speed

STATOR SETTING		SYMBOL
S1	S2	
0	0	○
-5	+2.5	□
-7.5	+2.5	▽
-2.5	+2.5	△
+2.5	-2.5	◇

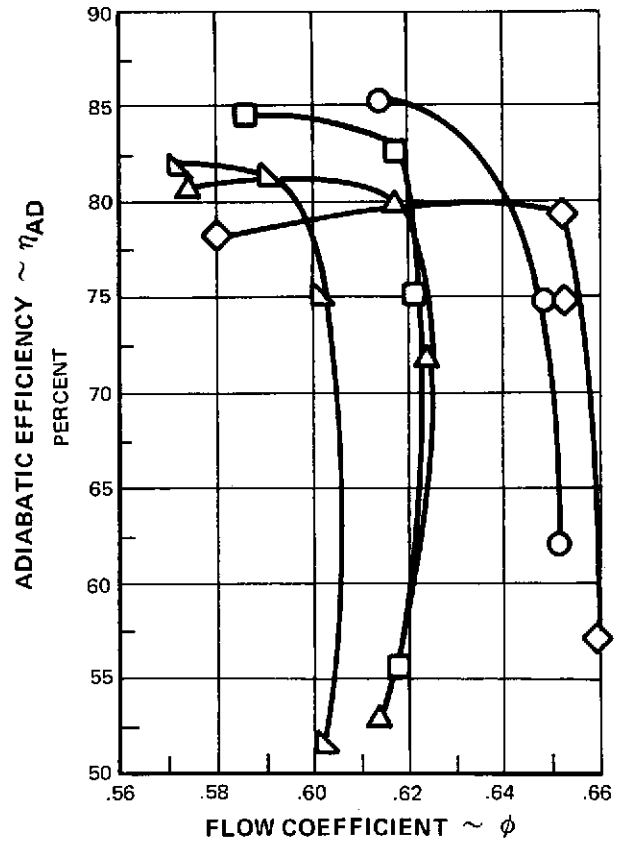
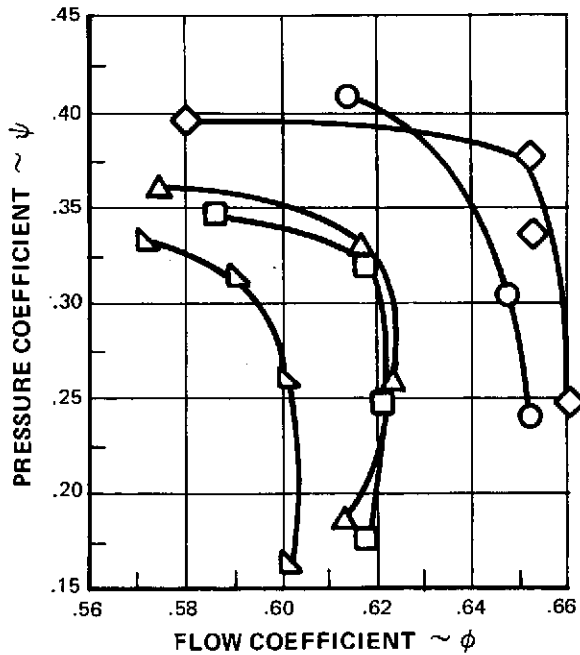


Figure 34 Pressure Coefficient and Adiabatic Efficiency Versus Flow Coefficient for the Second Stage at 105 Percent of Design Speed

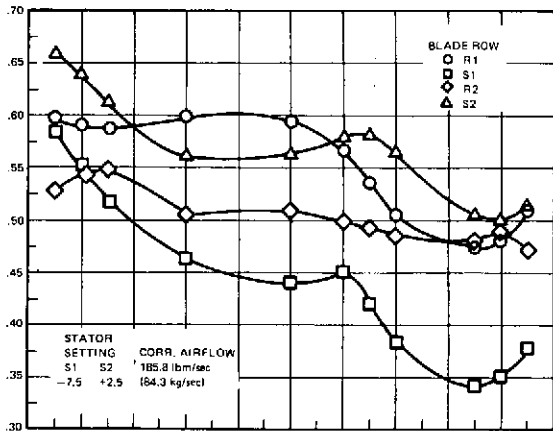


Figure 35A

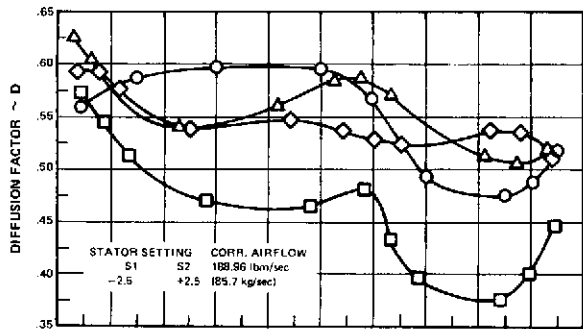


Figure 35B

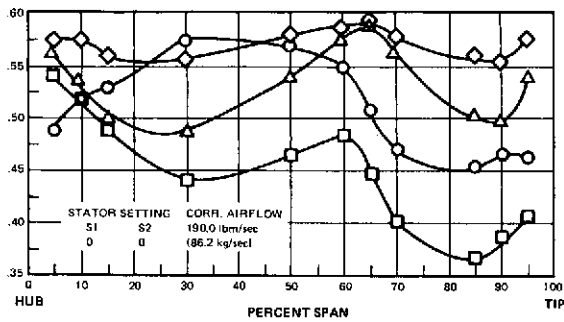


Figure 35C

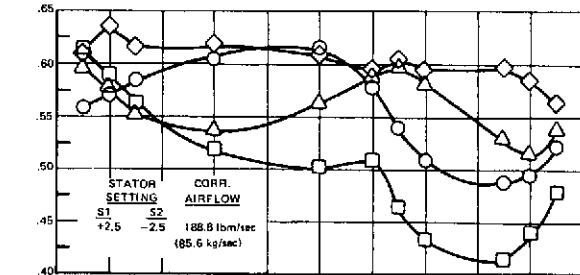


Figure 35D

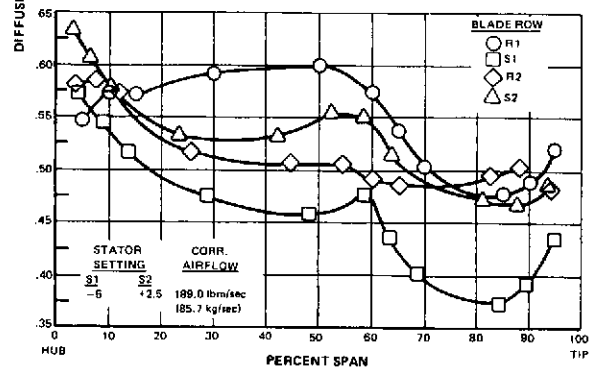


Figure 35E

Figure 35 Near-Stall Diffusion Factors Versus Span for Each Blade Row, Showing Effects of Varying Stator Settings at 105 Percent of Design Speed

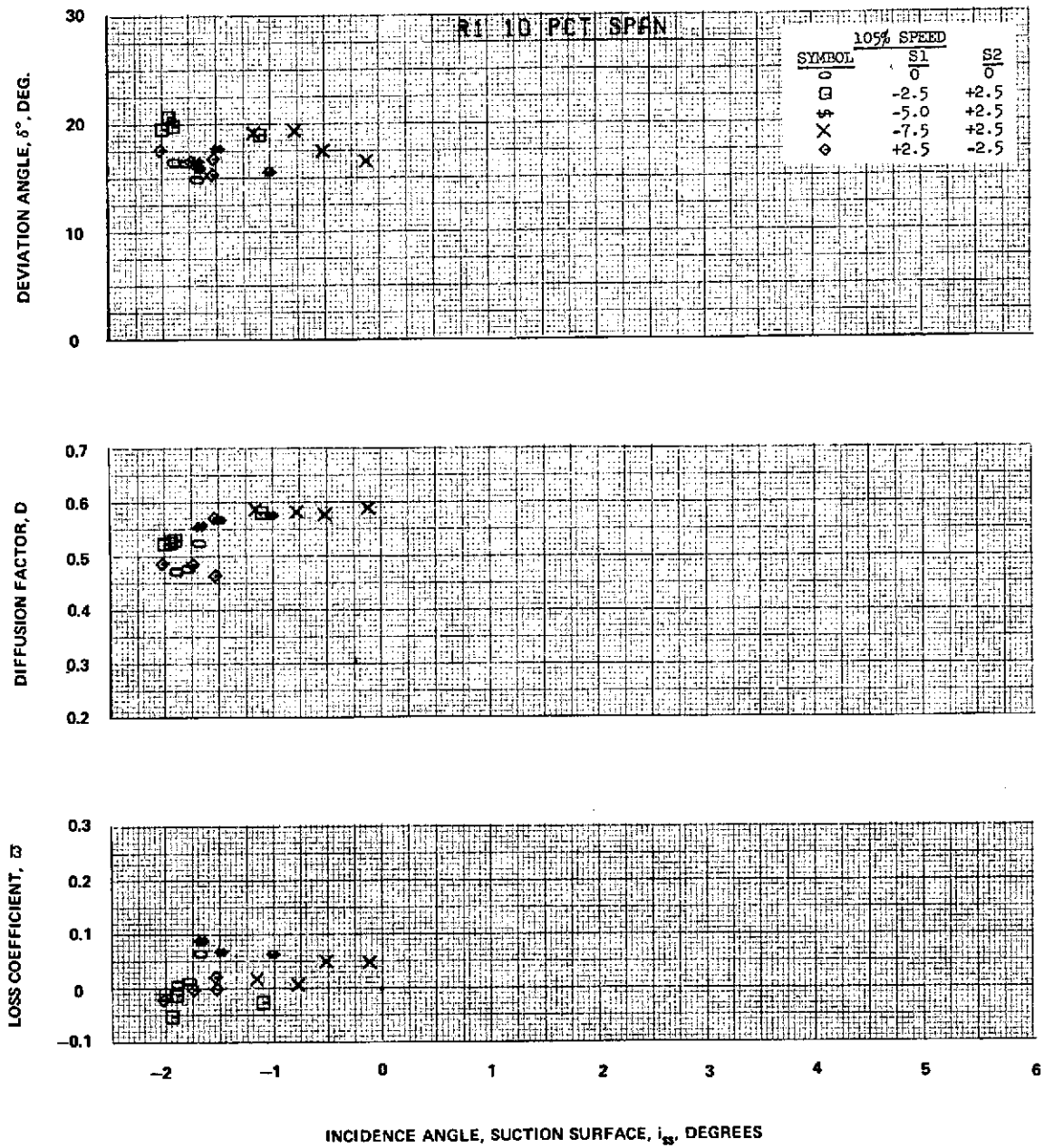


Figure 36A

Figure 36 Blade-Element Performance for Rotor 1 at 105 Percent of Design Speed

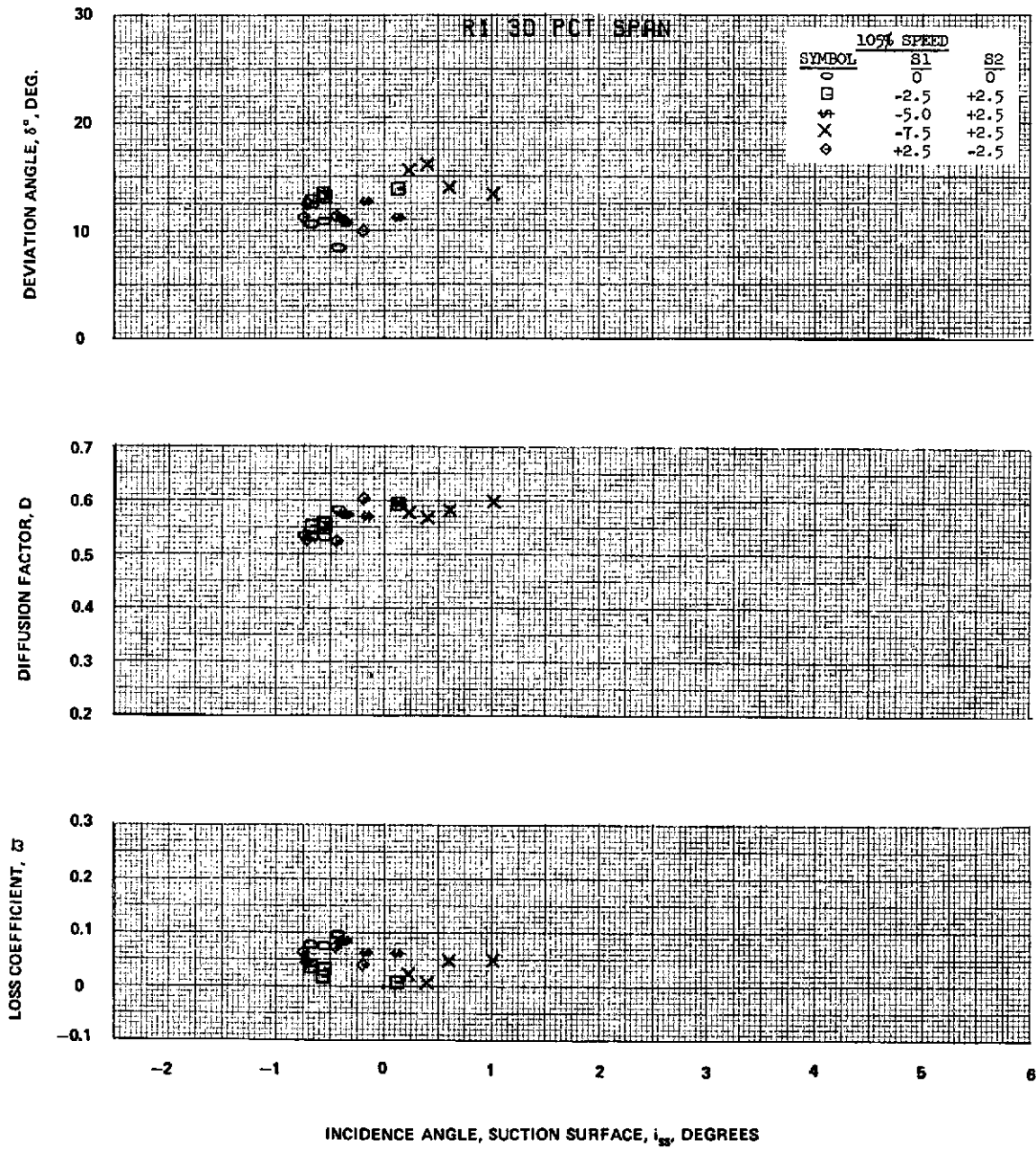


Figure 36B

Figure 36 (Cont'd) Blade-Element Performance for Rotor 1 at 105 Percent of Design Speed

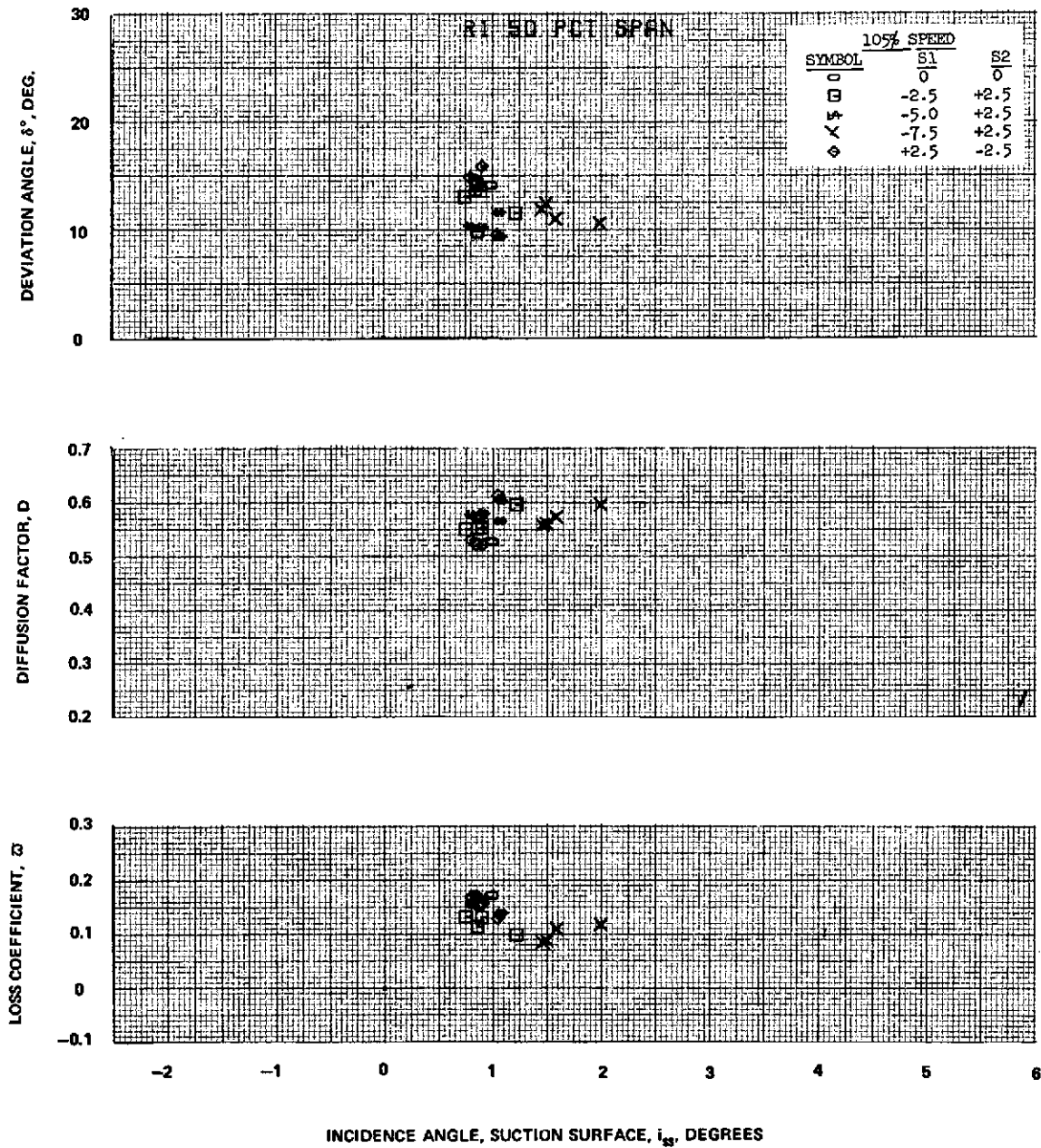


Figure 36C

Figure 36 (Cont'd) Blade-Element Performance for Rotor 1 at 105 Percent of Design Speed

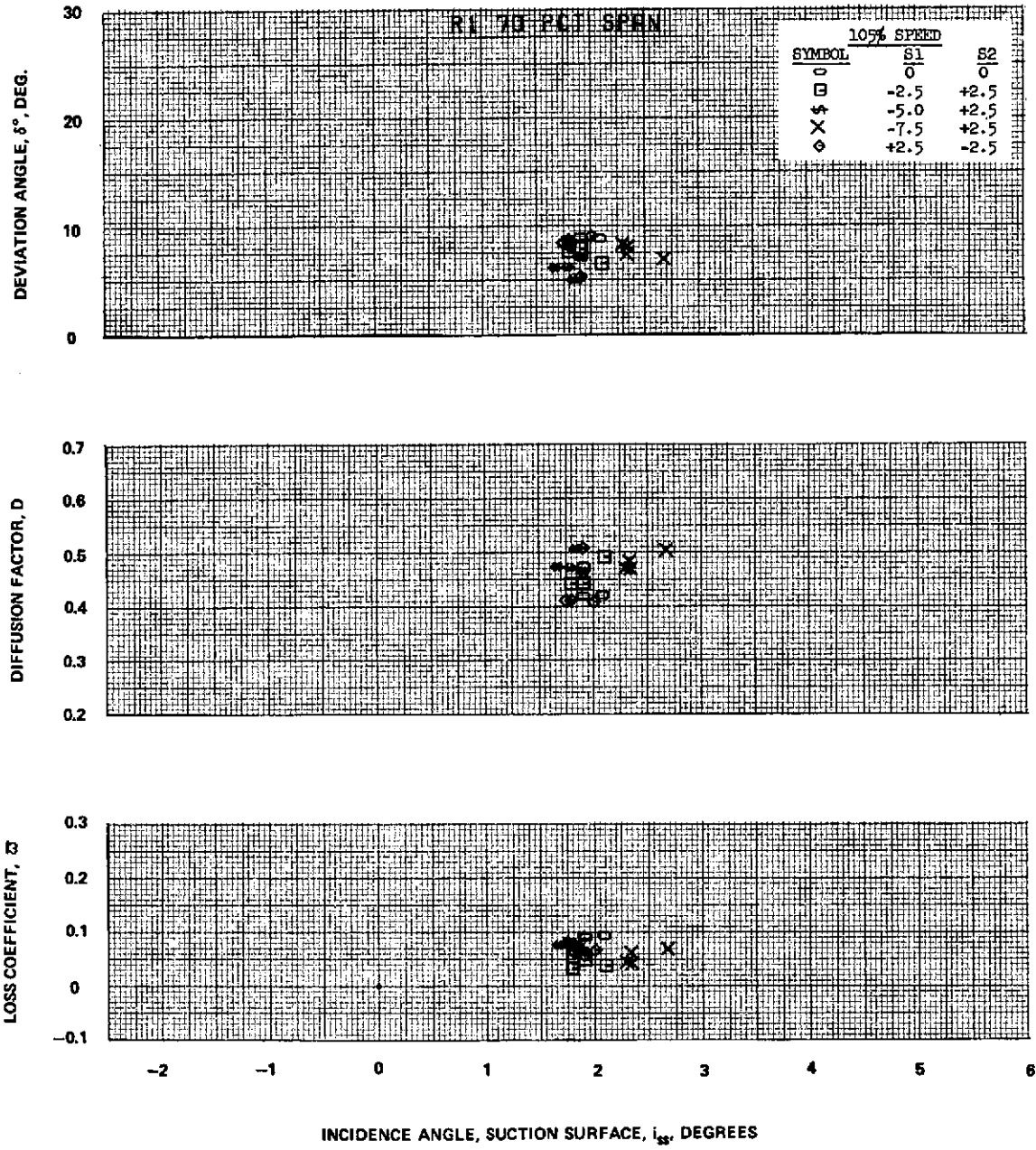


Figure 36D

Figure 36 (Cont'd) Blade-Element Performance for Rotor 1 at 105 Percent of Design Speed

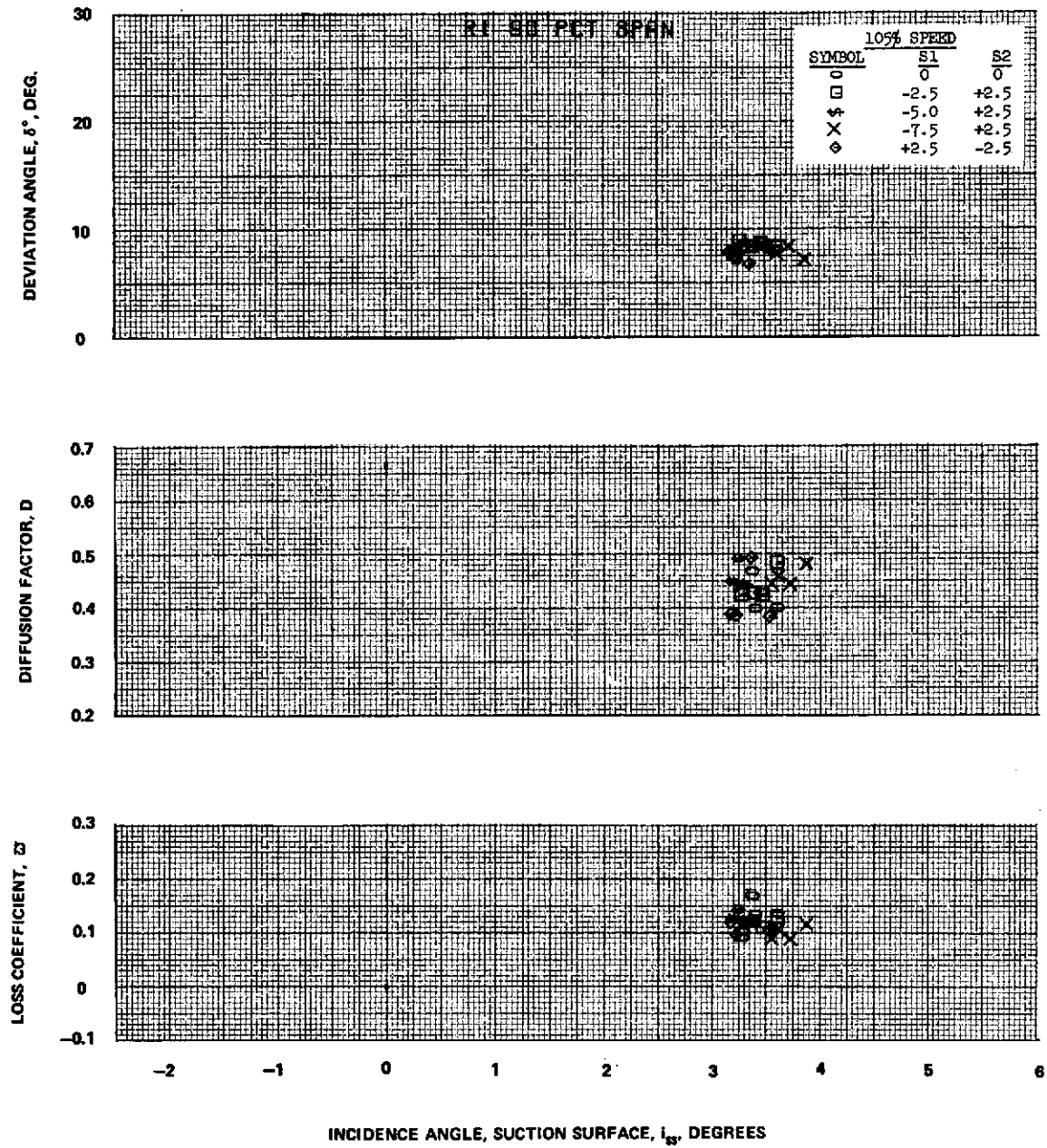


Figure 36E

Figure 36 (Cont'd) Blade-Element Performance for Rotor 1 at 105 Percent of Design Speed

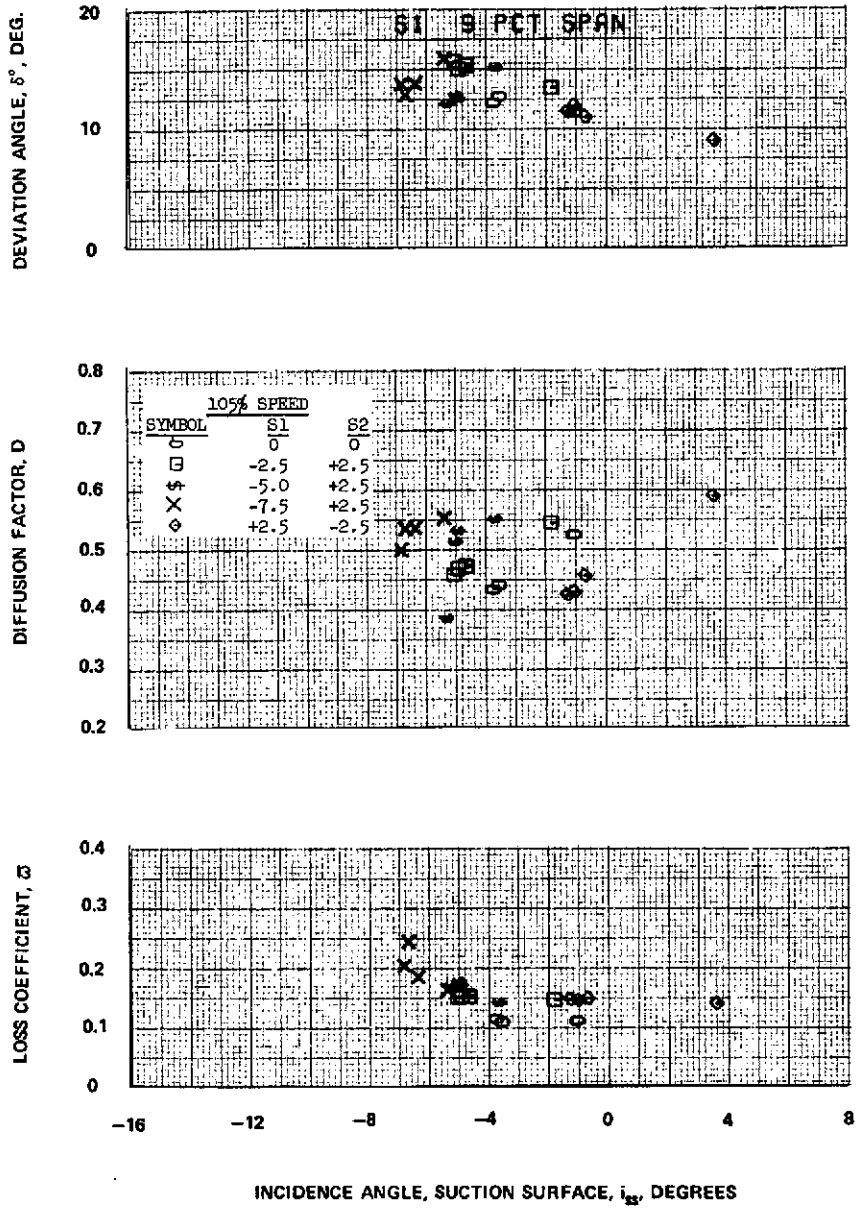


Figure 37A

Figure 37 Blade-Element Performance for Stator 1 at 105 Percent of Design Speed

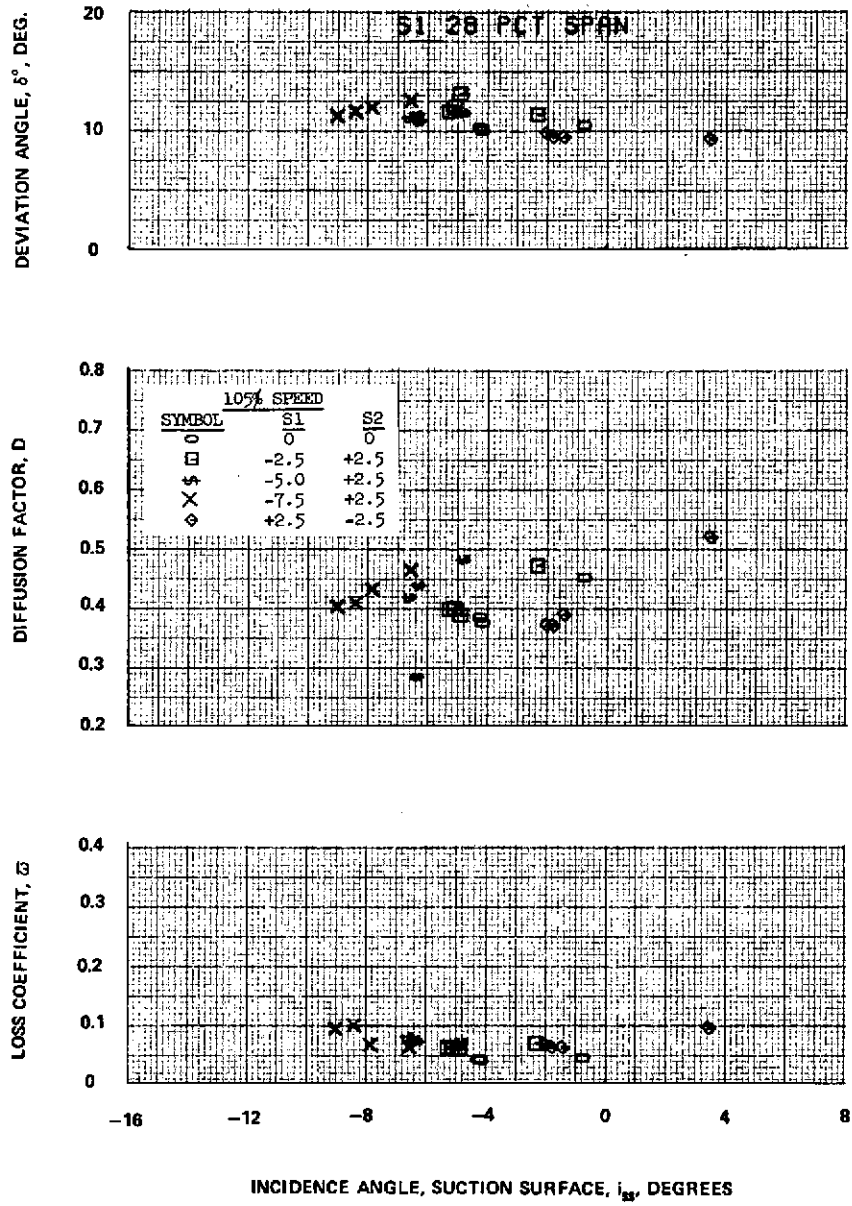


Figure 37B

Figure 37 (Cont'd) Blade-Element Performance for Stator 1 at 105 Percent of Design Speed

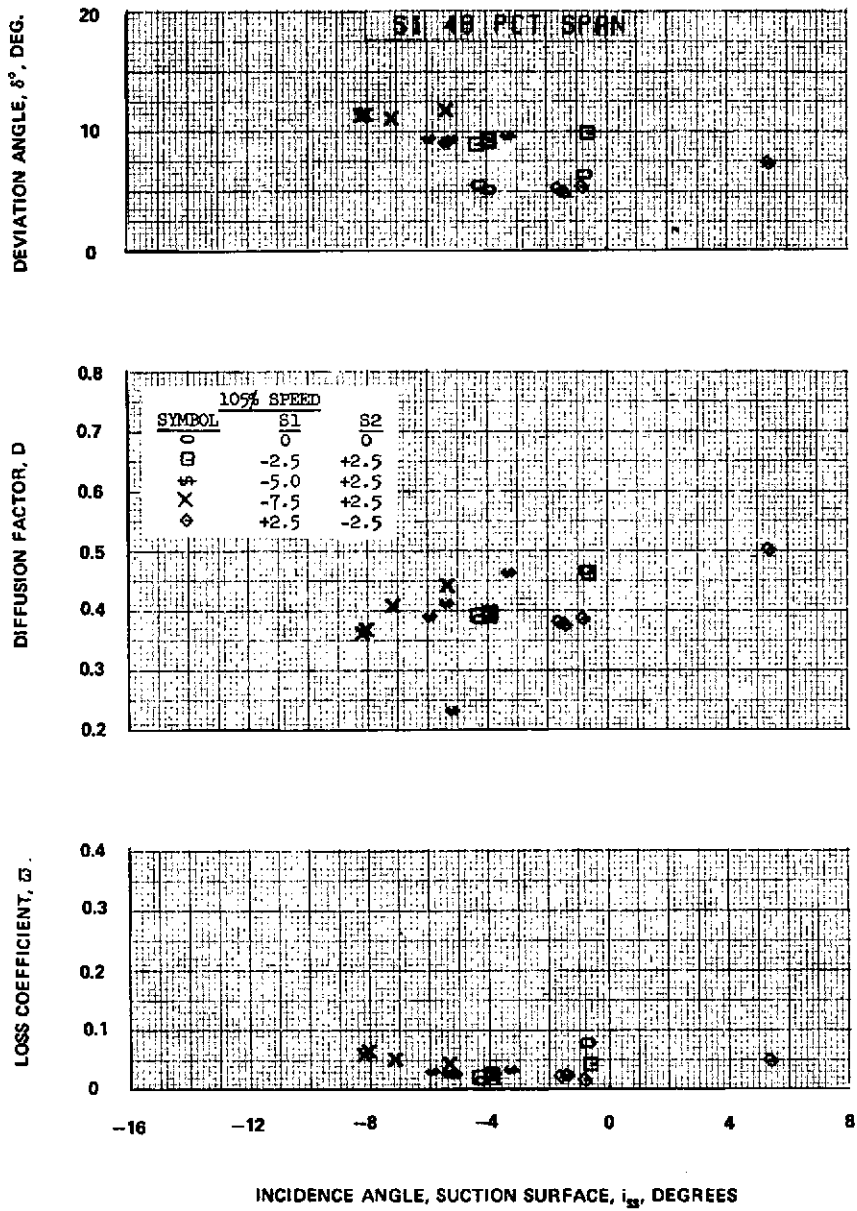


Figure 37C

Figure 37 (Cont'd) Blade-Element Performance for Stator 1 at 105 Percent of Design Speed

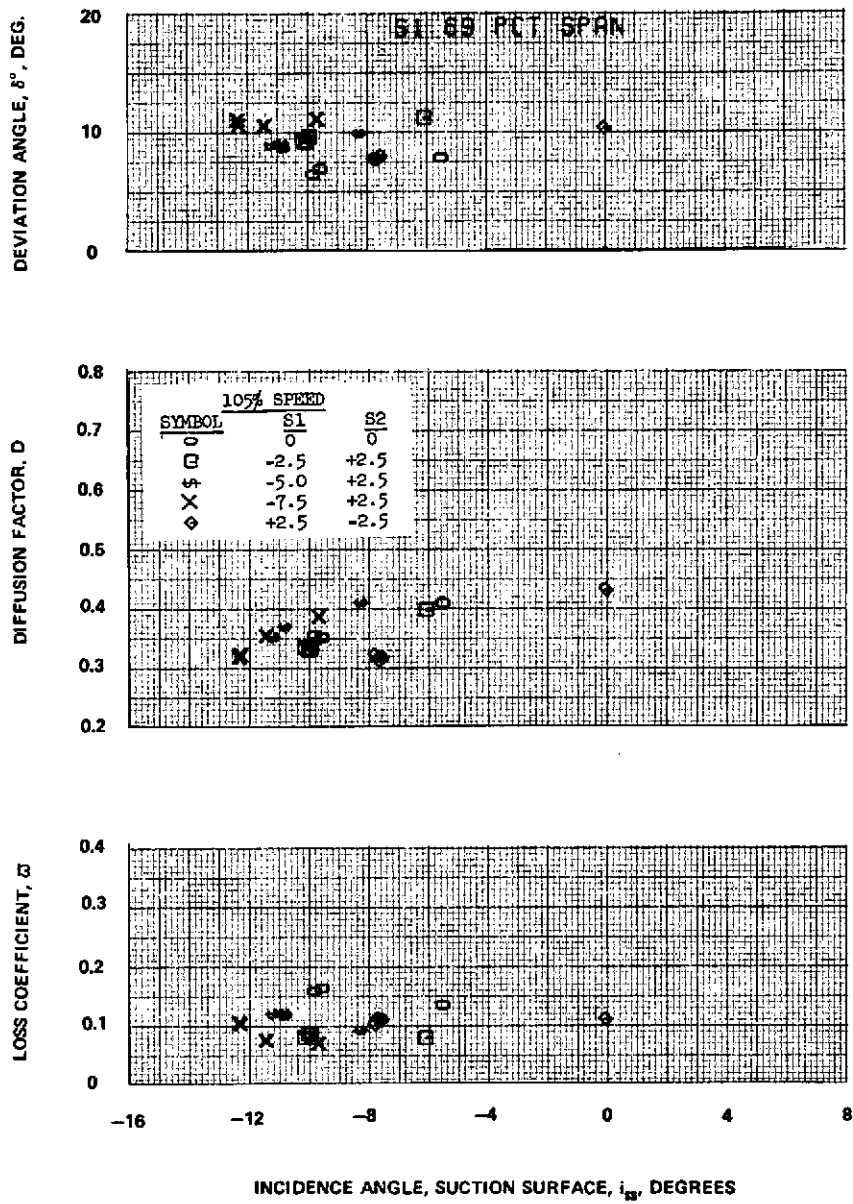


Figure 37D

Figure 37 (Cont'd) Blade-Element Performance for Stator 1 at 105 Percent of Design Speed

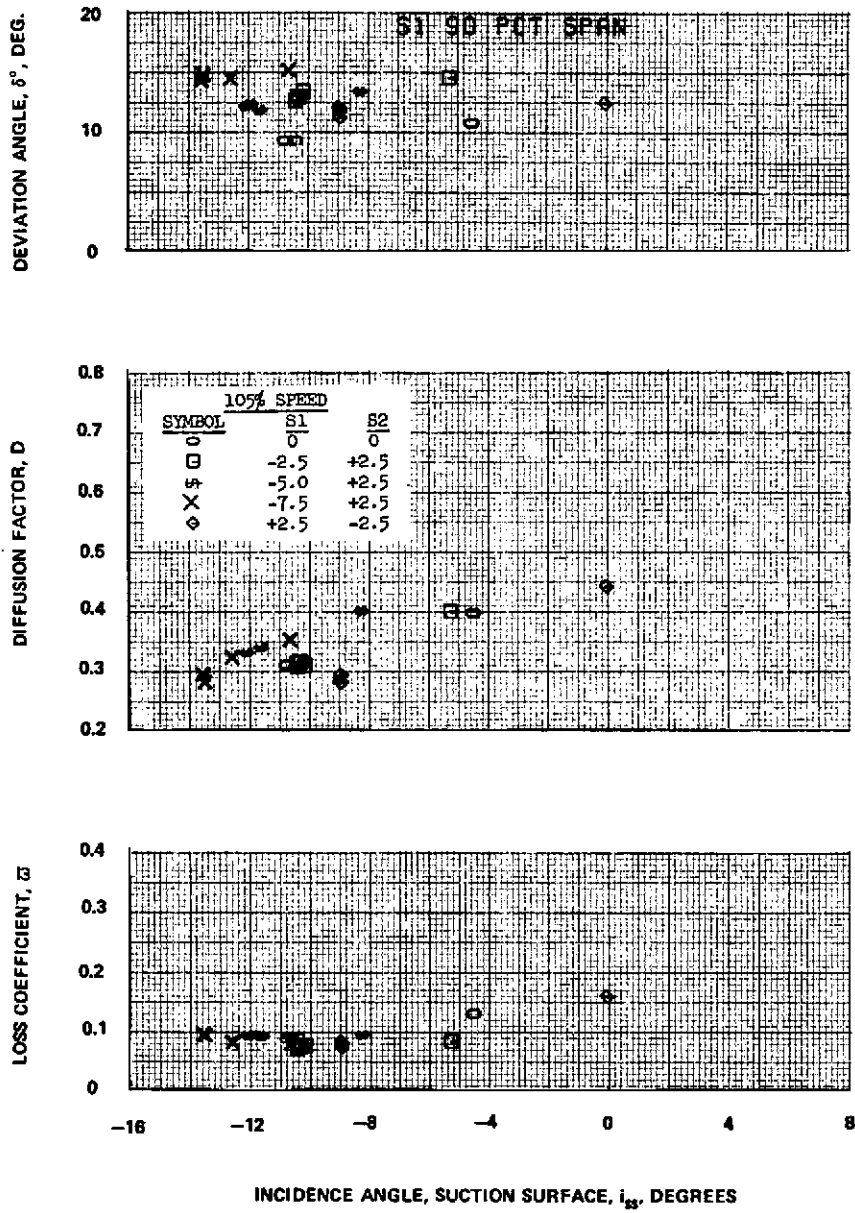


Figure 37E

Figure 37 (Cont'd) Blade-Element Performance for Stator 1 at 105 Percent of Design Speed

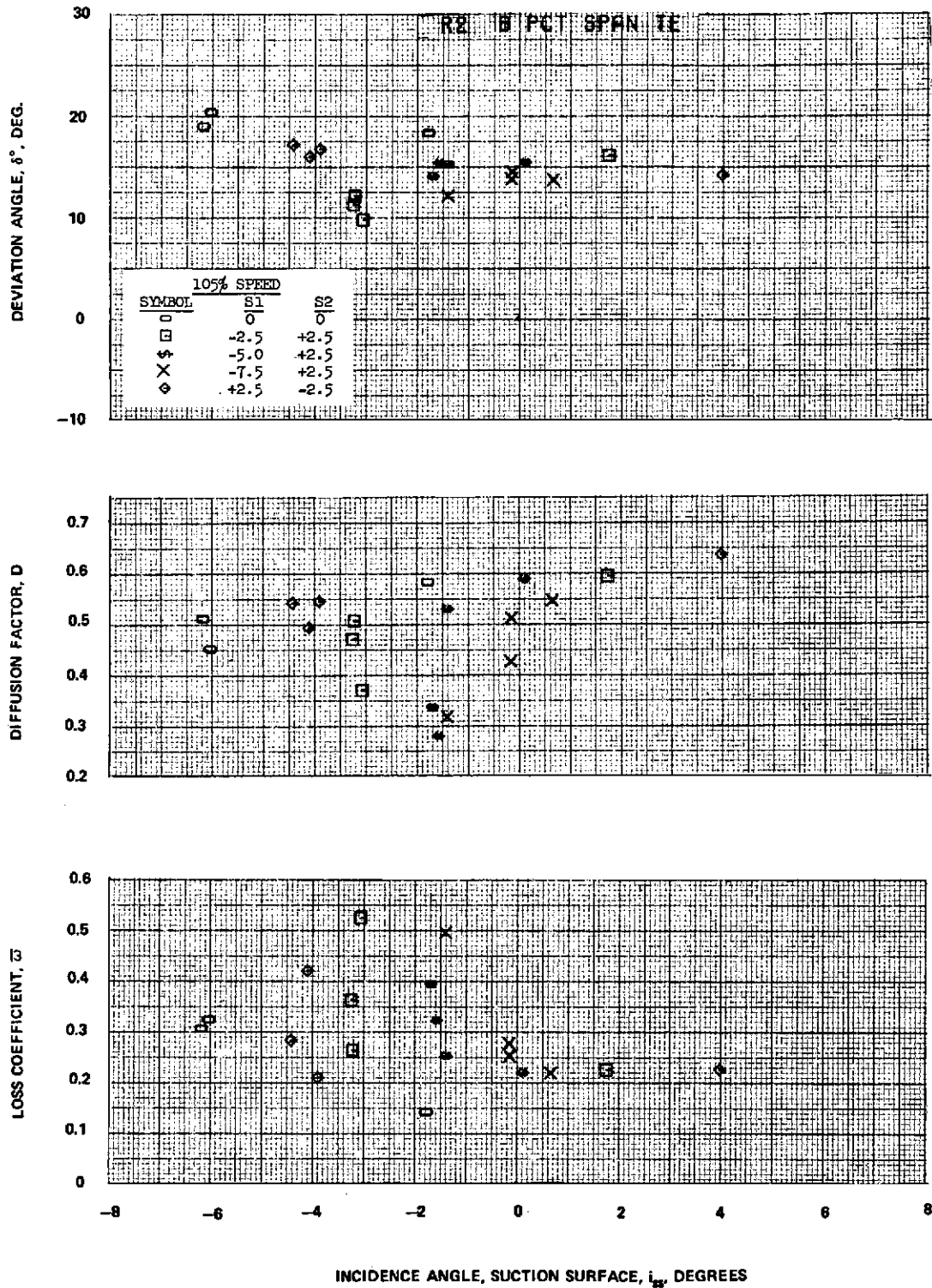


Figure 38A

Figure 38 Blade-Element Performance for Rotor 2 at 105 Percent of Design Speed

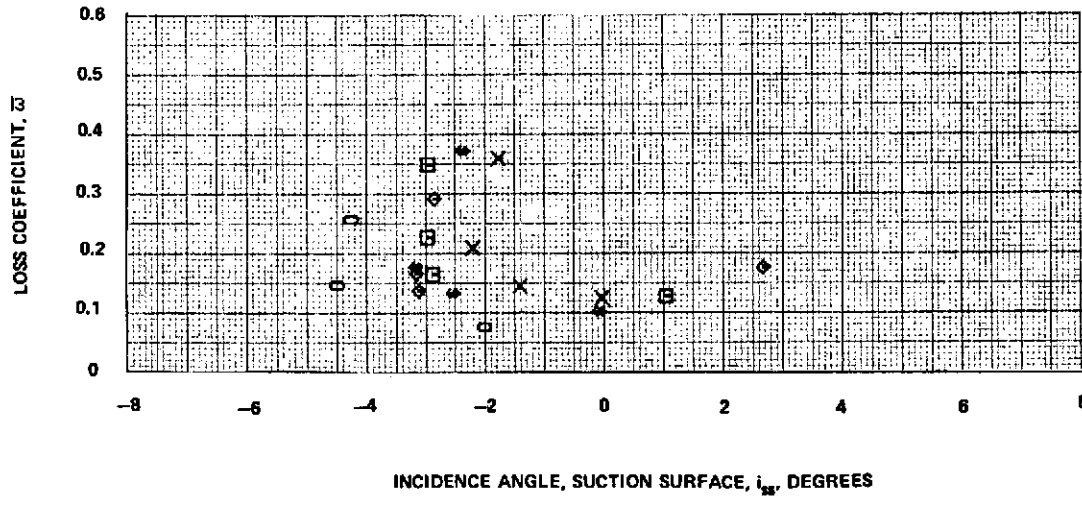
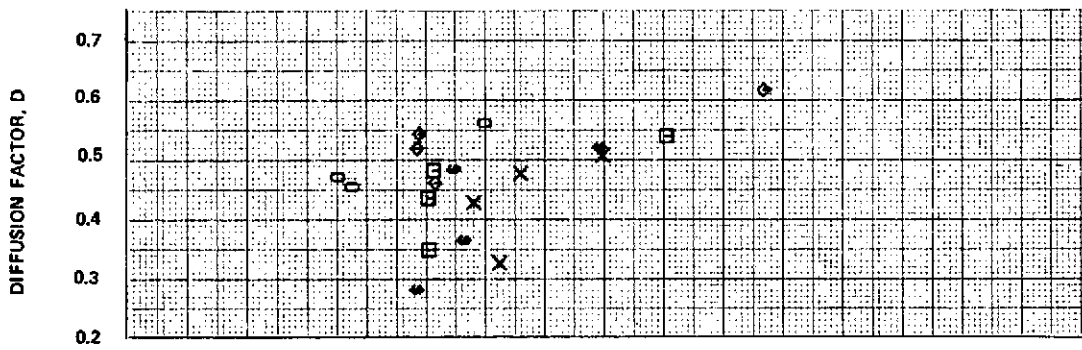
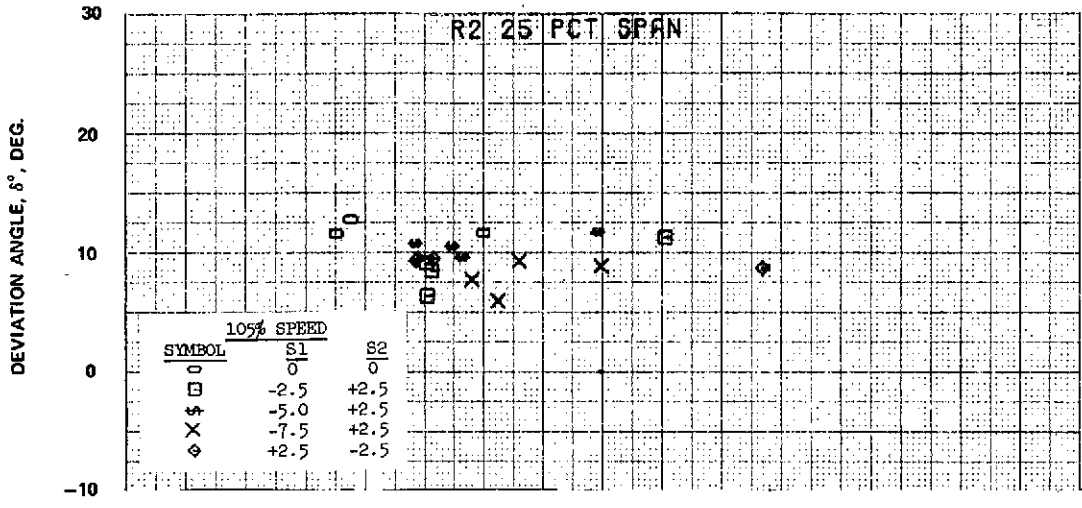


Figure 38B

Figure 38 (Cont'd) Blade-Element Performance for Rotor 2 at 105 Percent of Design Speed

C-2

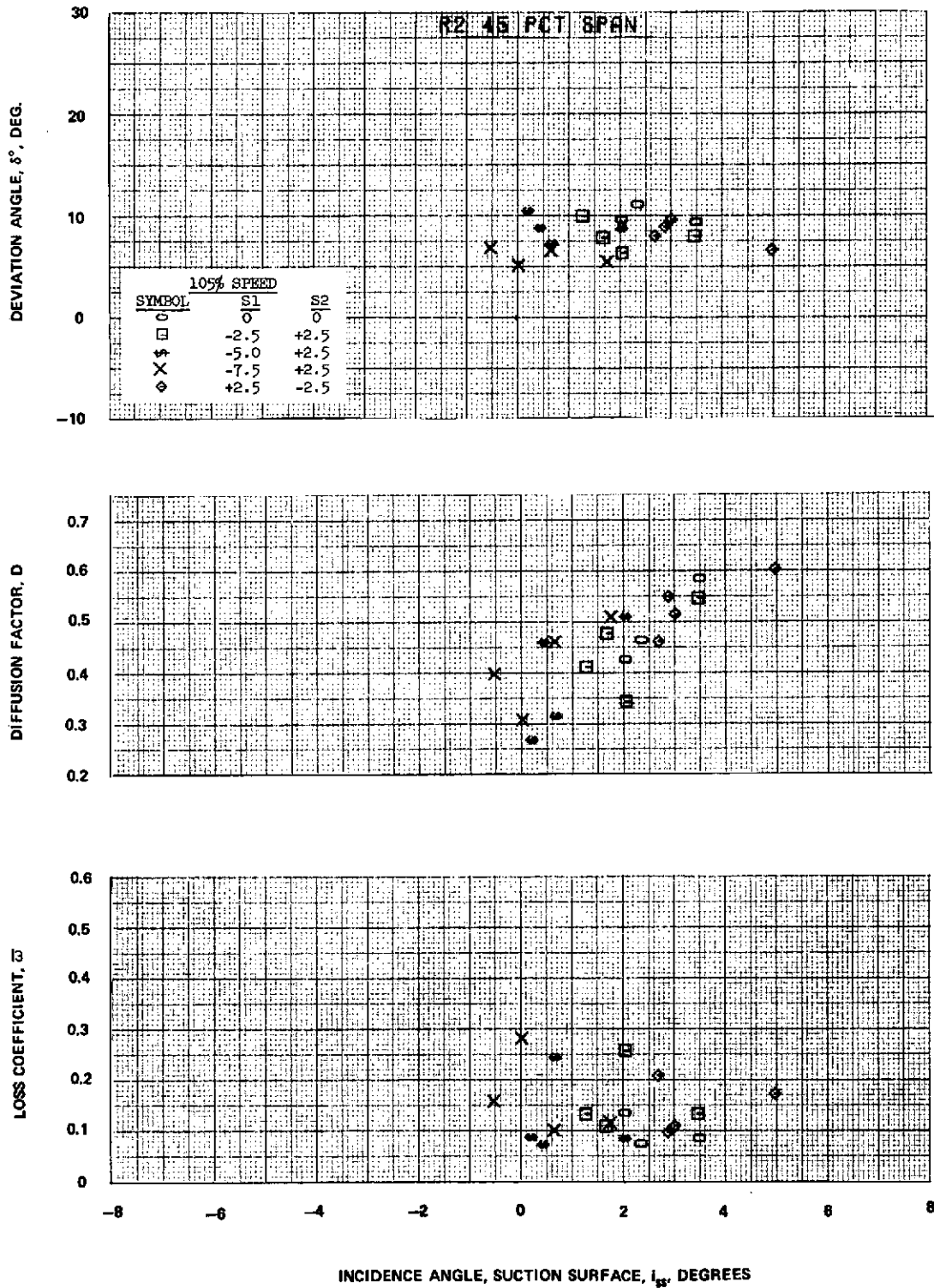


Figure 38C

Figure 38 (Cont'd) Blade-Element Performance for Rotor 2 at 105 Percent of Design Speed

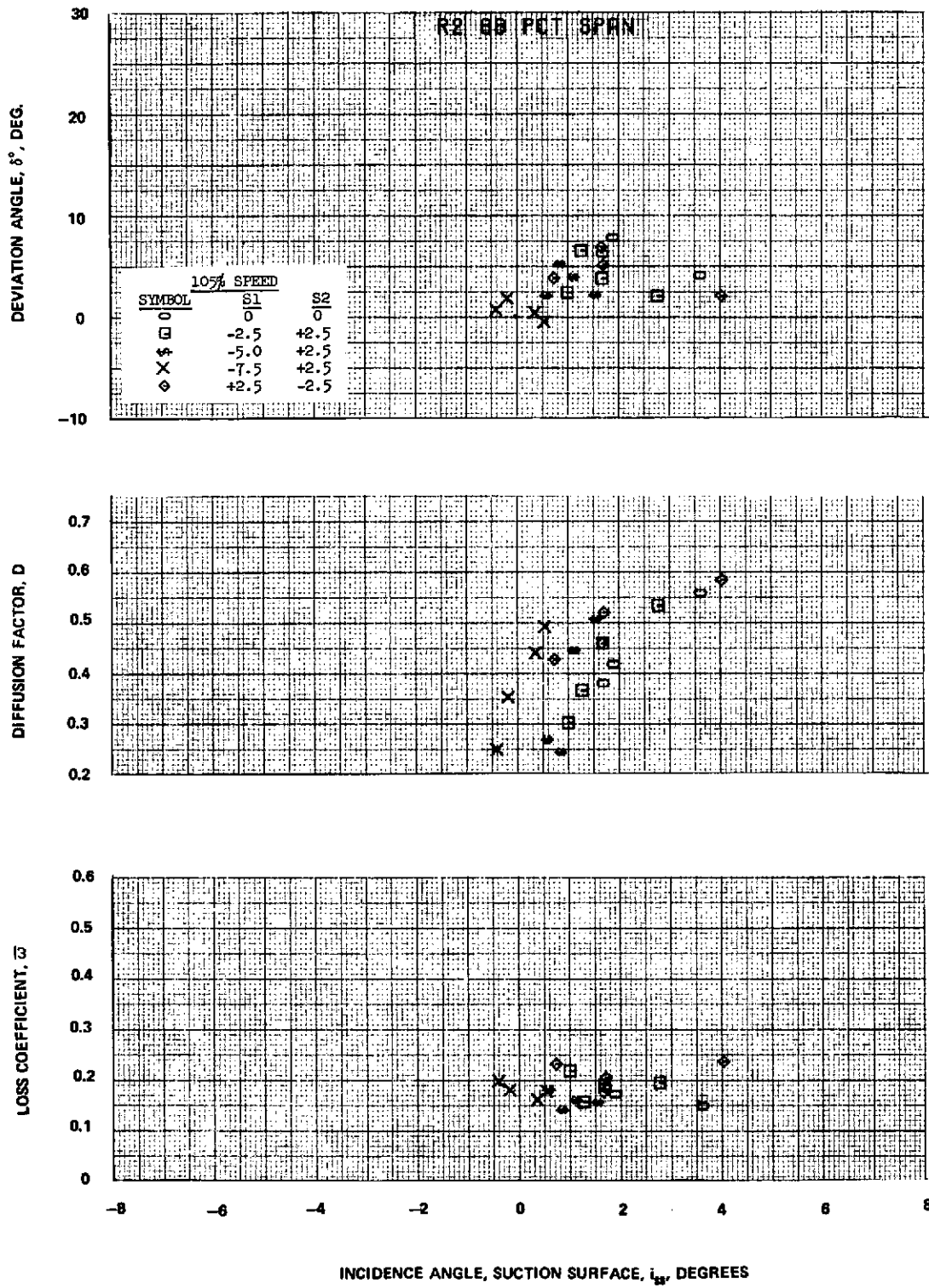


Figure 38D

Figure 38 (Cont'd) Blade-Element Performance for Rotor 2 at 105 Percent of Design Speed

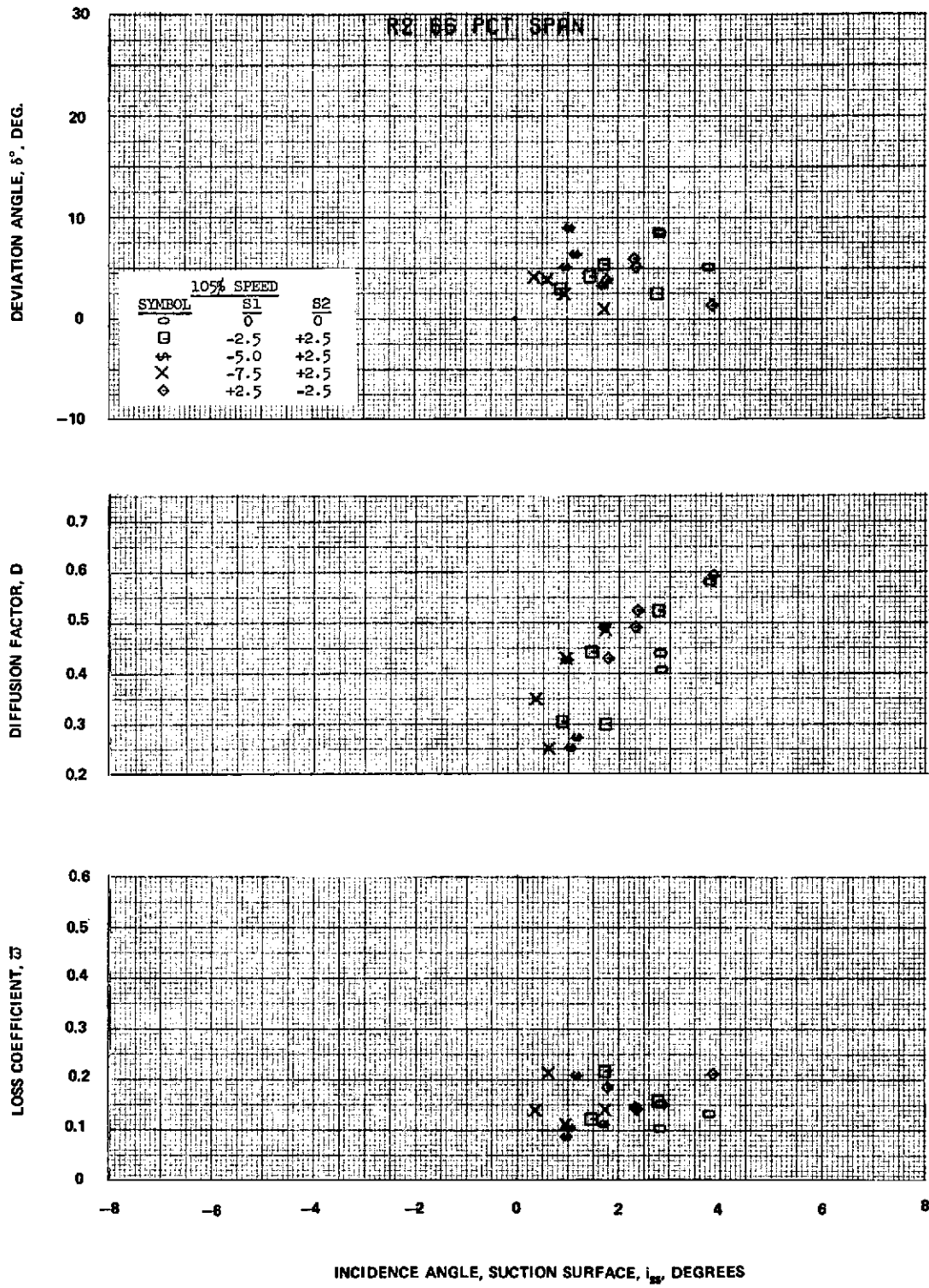


Figure 38E

Figure 38 (Cont'd) Blade-Element Performance for Rotor 2 at 105 Percent of Design Speed

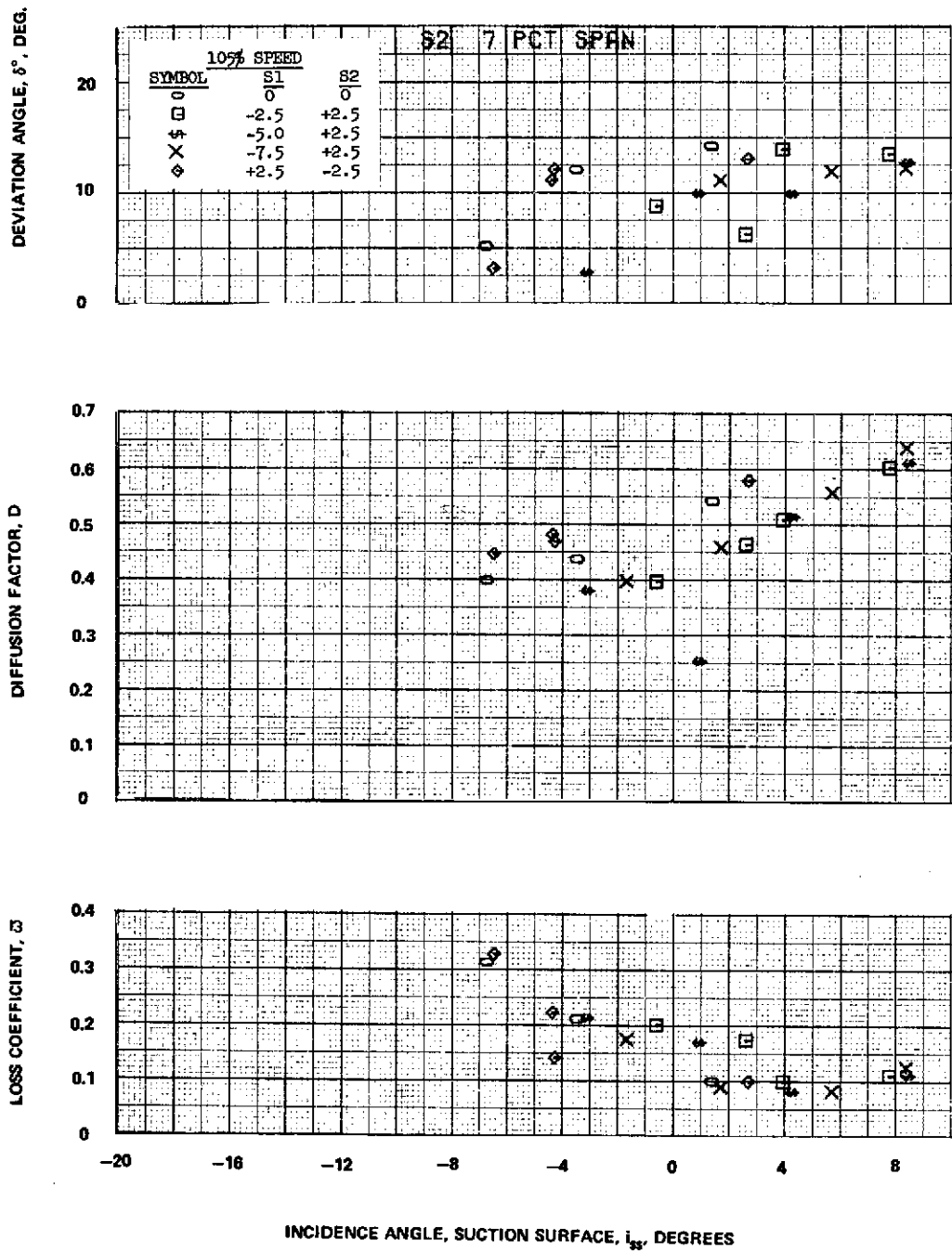


Figure 39A

Figure 39 Blade-Element Performance for Stator 2 at 105 Percent of Design Speed

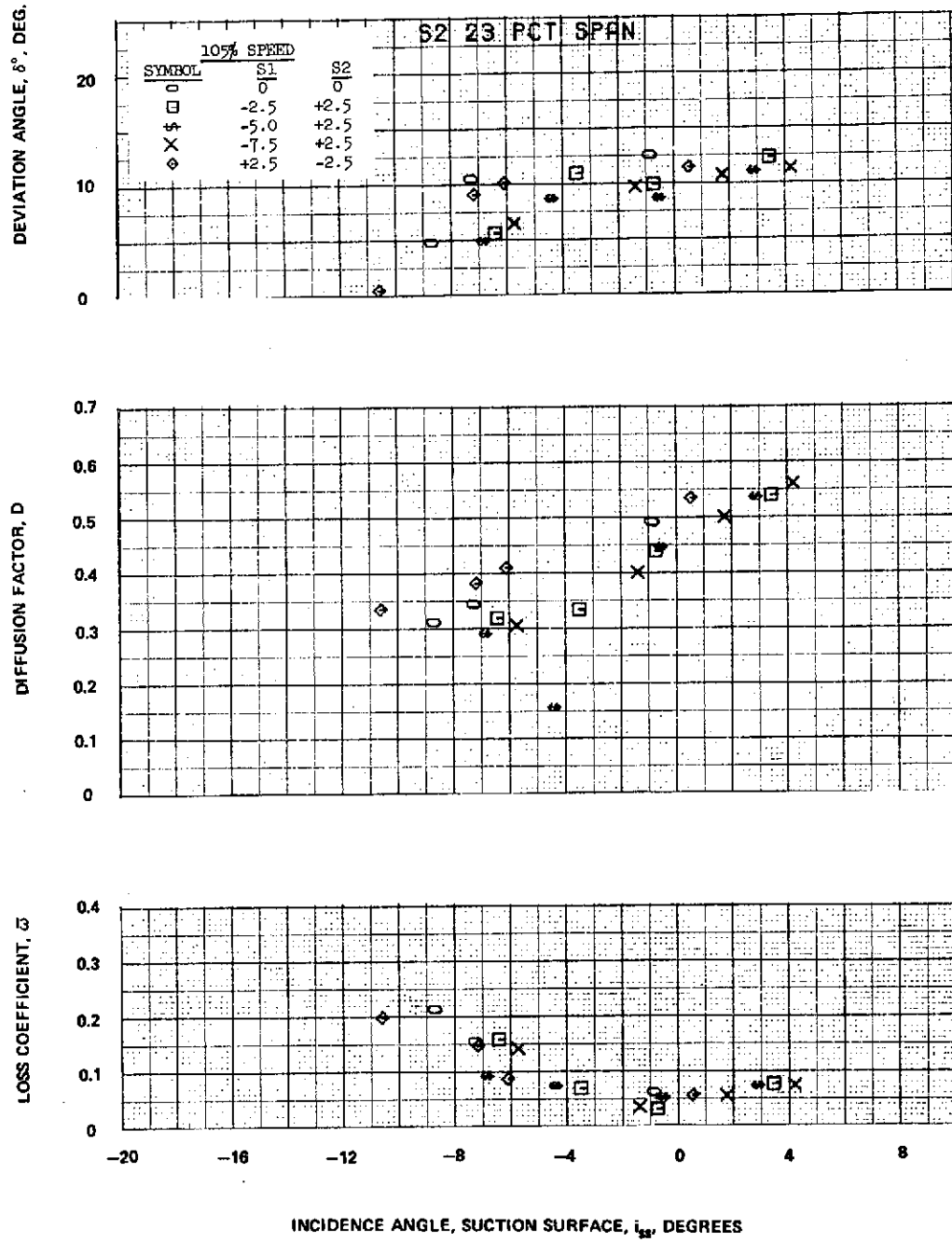


Figure 39B

Figure 39 (Cont'd) Blade-Element Performance for Stator 2 at 105 Percent of Design Speed

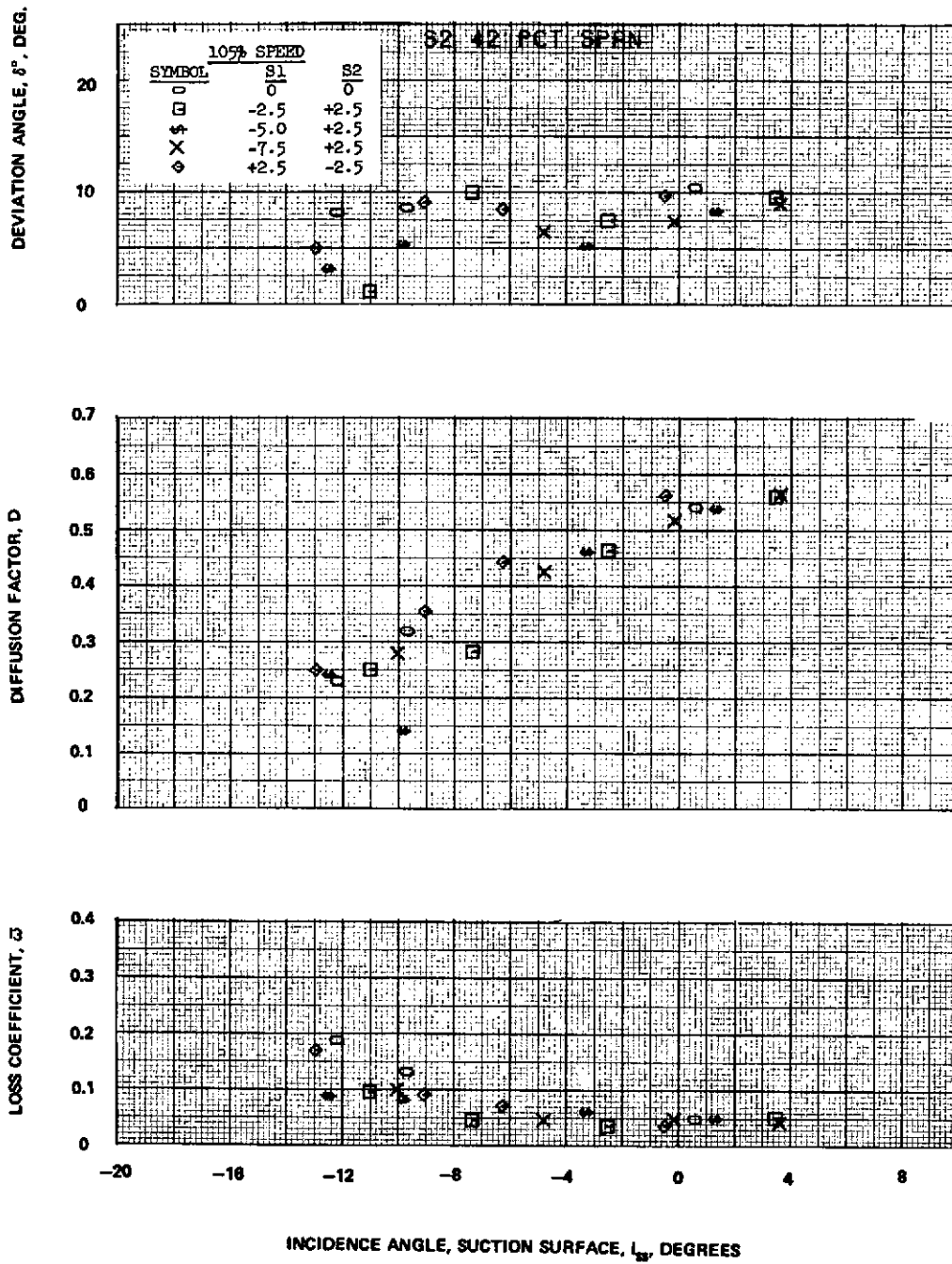


Figure 39C

Figure 39 (Cont'd) Blade-Element Performance for Stator 2 at 105 Percent of Design Speed

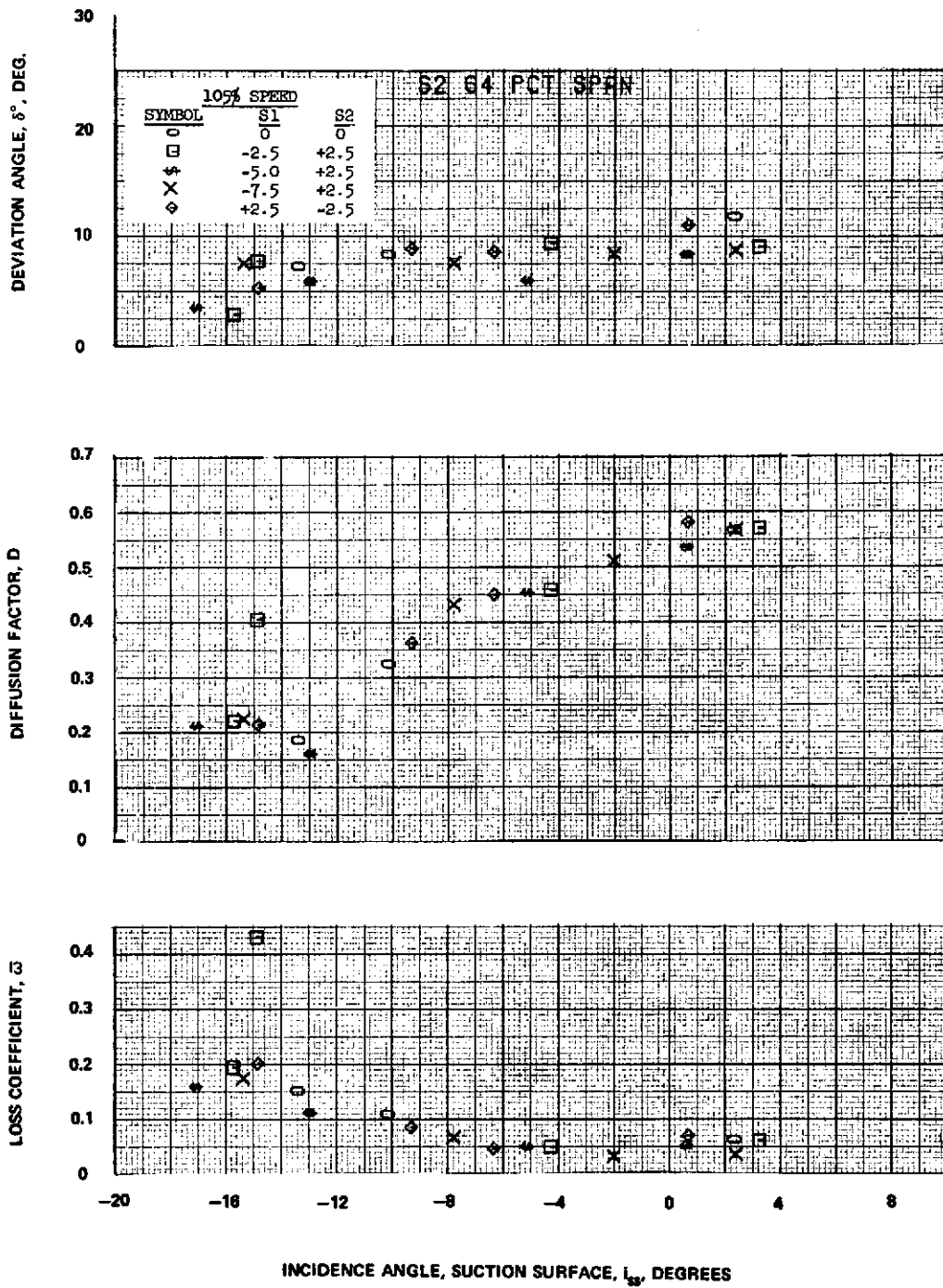


Figure 39D

Figure 39 (Cont'd) Blade-Element Performance for Stator 2 at 105 Percent of Design Speed

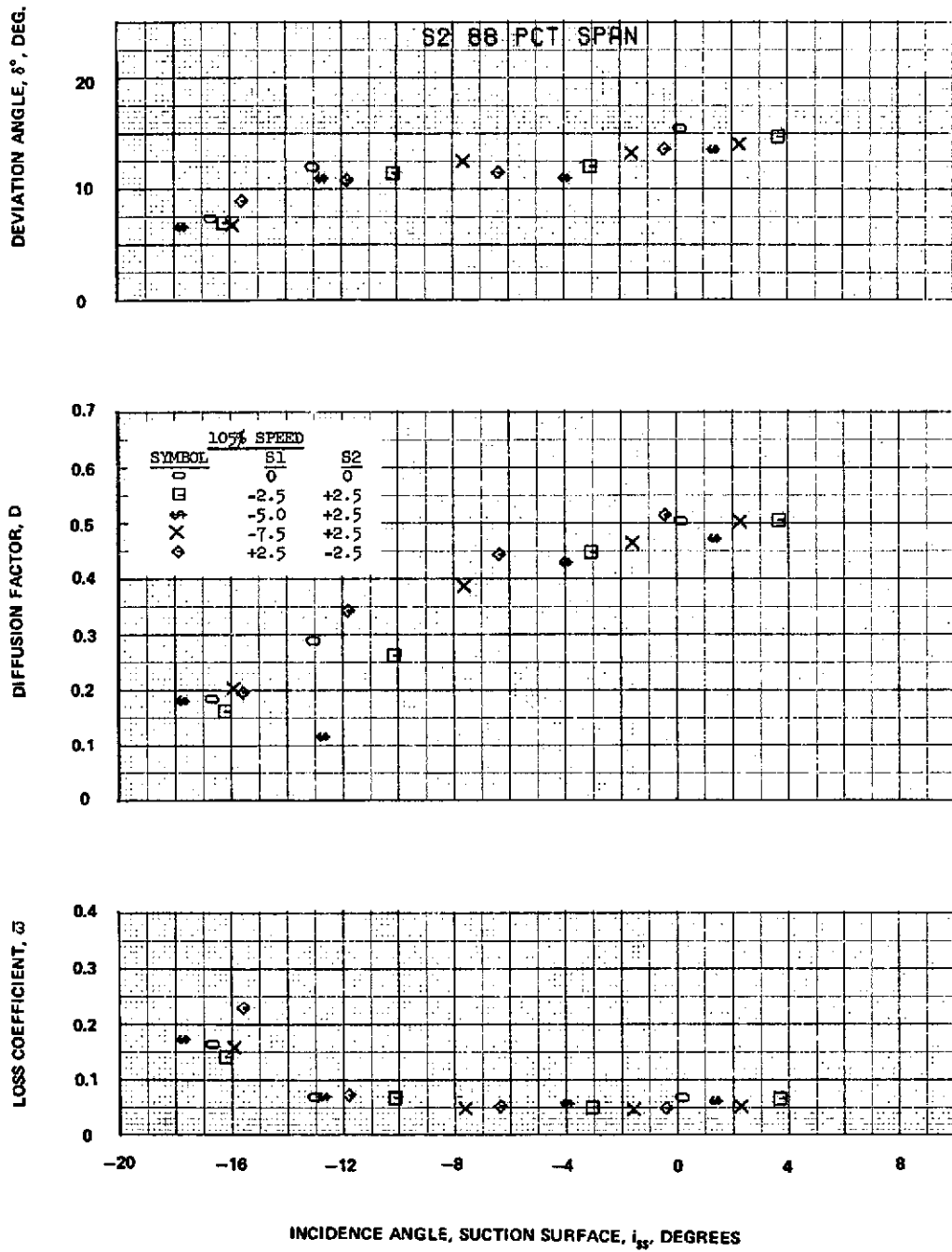


Figure 39E

Figure 39 (Cont'd) Blade-Element Performance for Stator 2 at 105 Percent of Design Speed

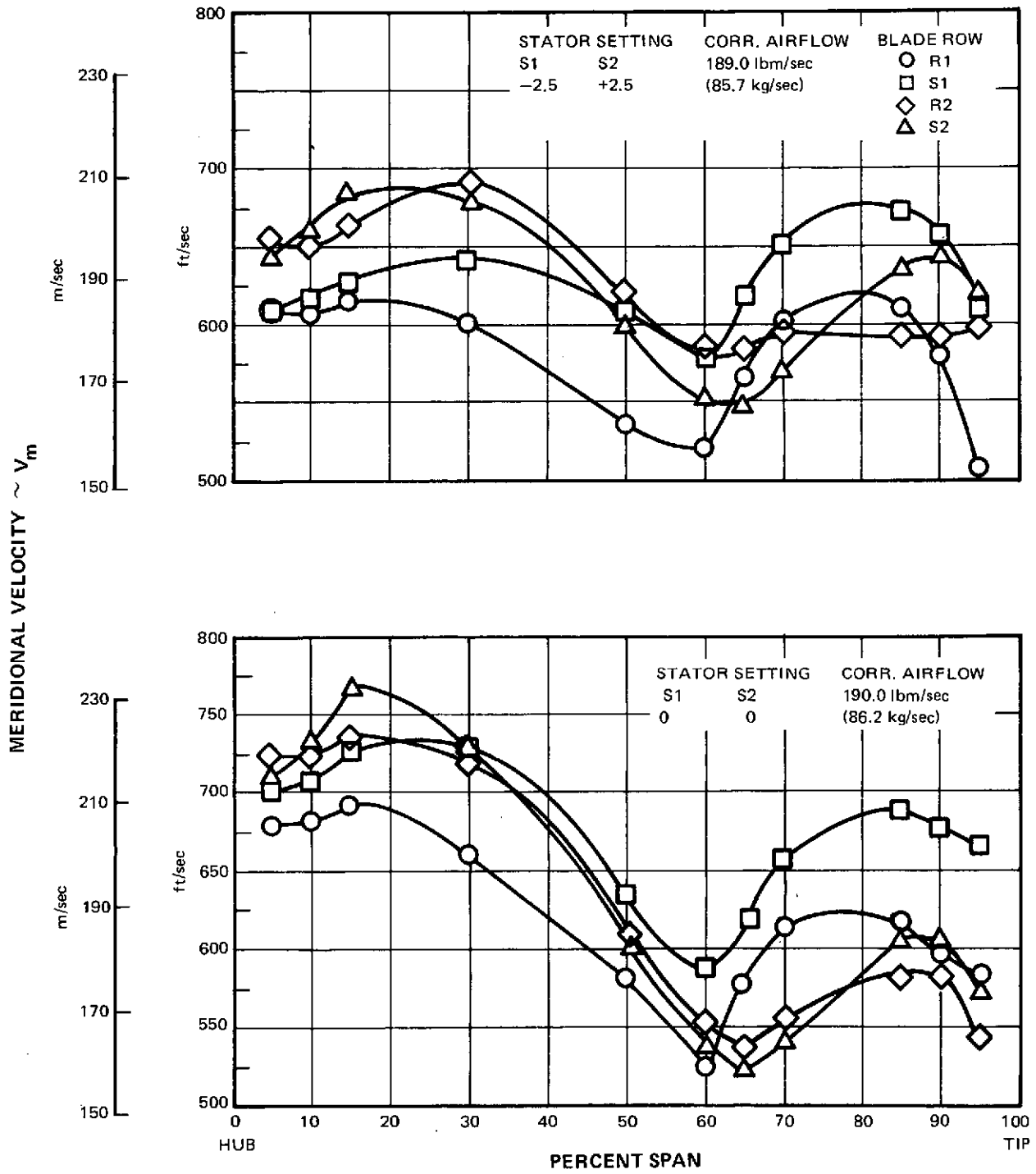


Figure 40 Meridional Velocity Versus Span for 105 Percent of Design Speed Showing Effects of Closing Stator 1 – Near-Stall Data

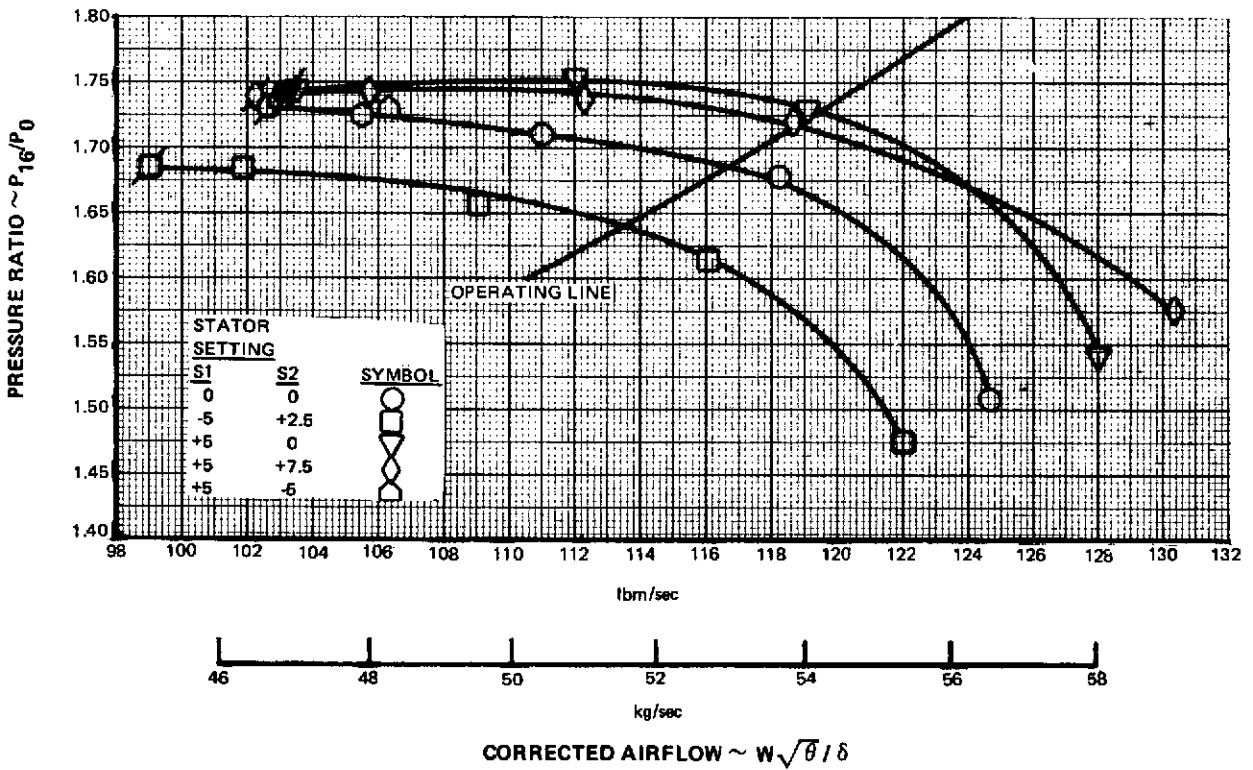
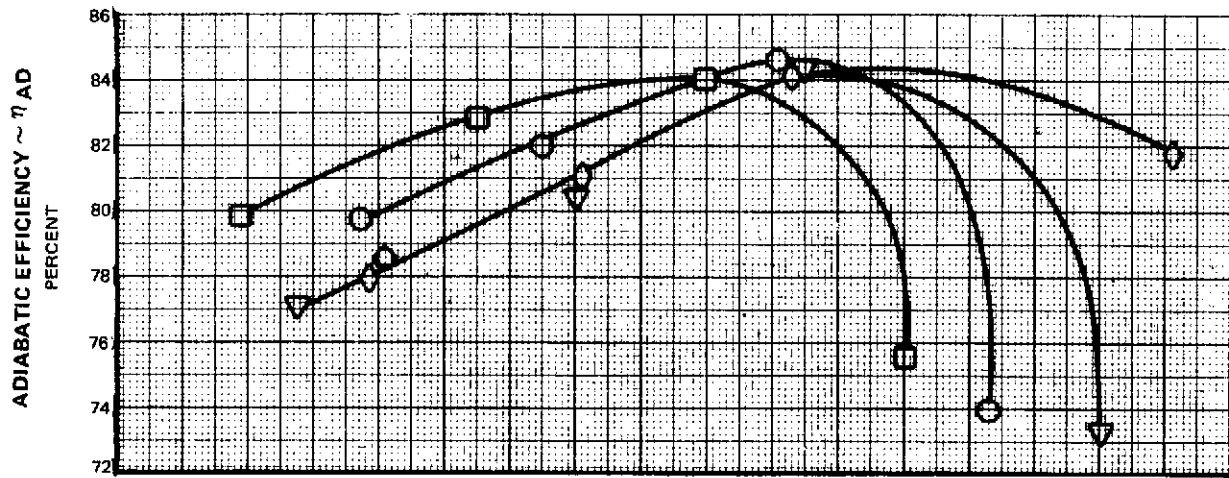


Figure 41 Fan Overall Performance at 70 Percent of Design Speed

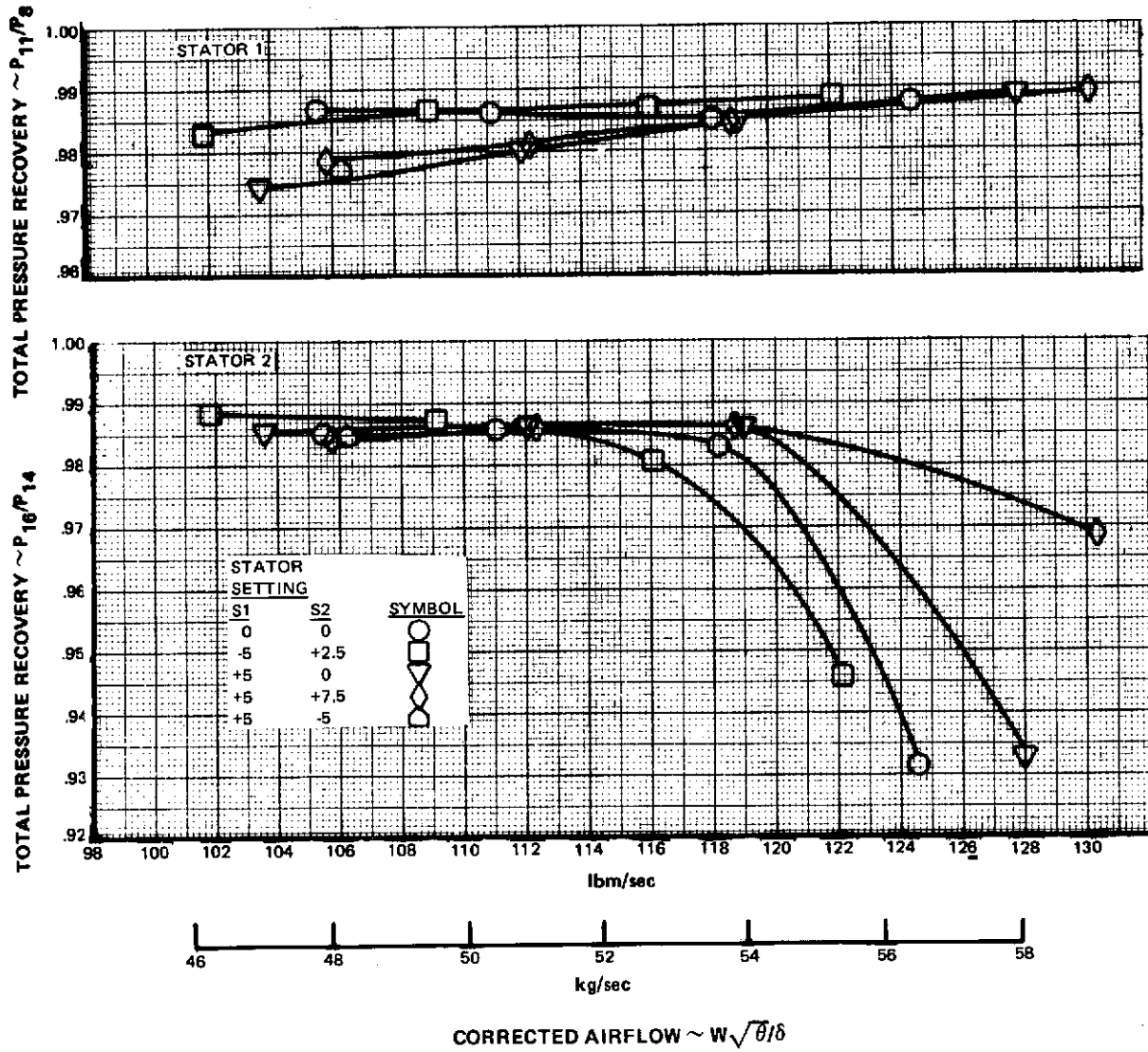


Figure 42 Stator 1 and Stator 2 Total Pressure Recovery Versus Flow at 70 Percent of Design Speed

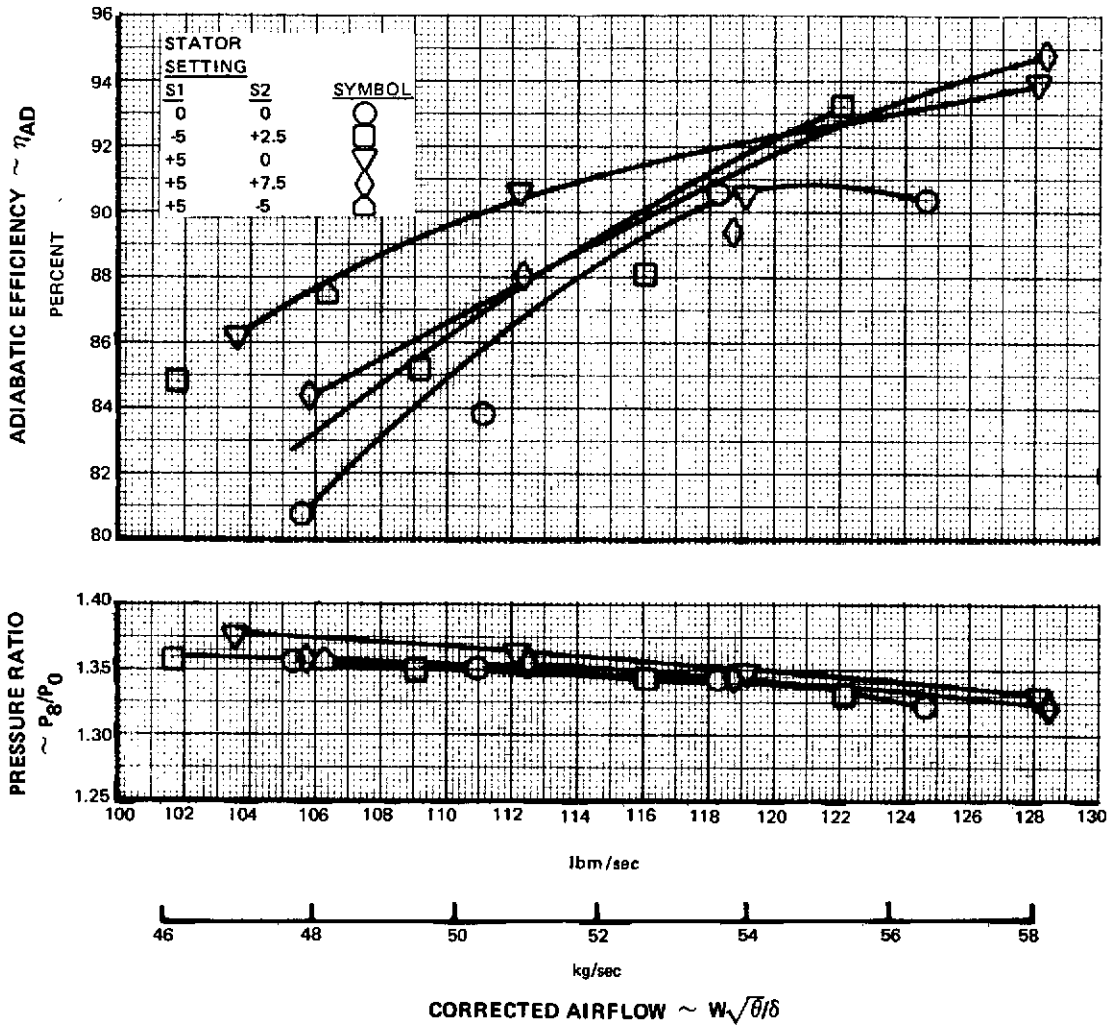


Figure 43 Rotor Performance at 70 Percent of Design Speed

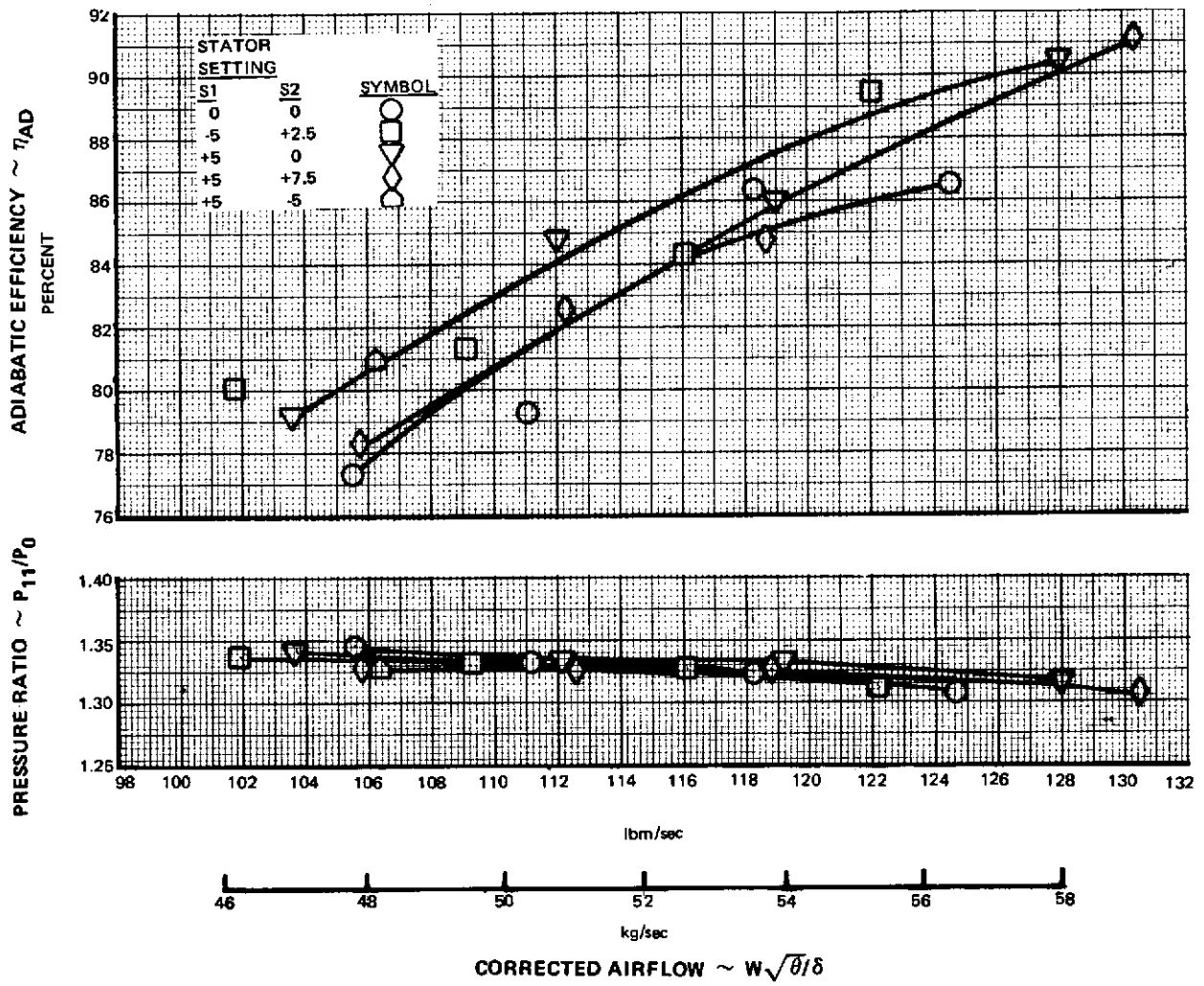


Figure 44 First-Stage Performance at 70 Percent of Design Speed

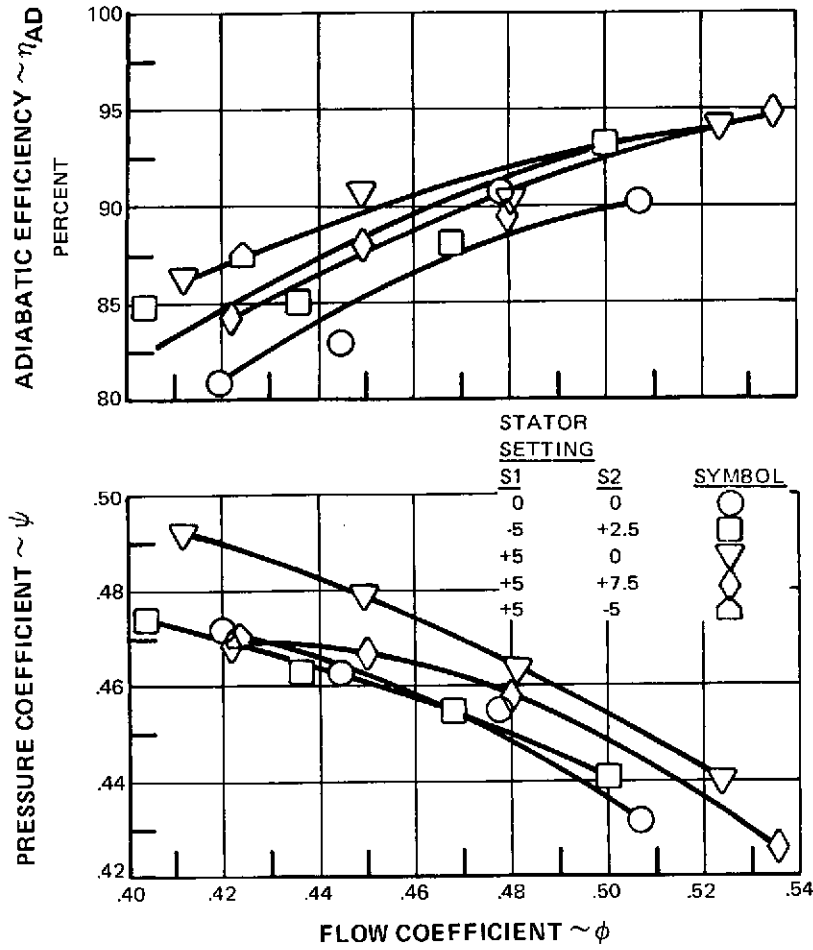


Figure 45 Pressure Coefficient and Adiabatic Efficiency Versus Flow Coefficient for Rotor 1 at 70 Percent of Design Speed

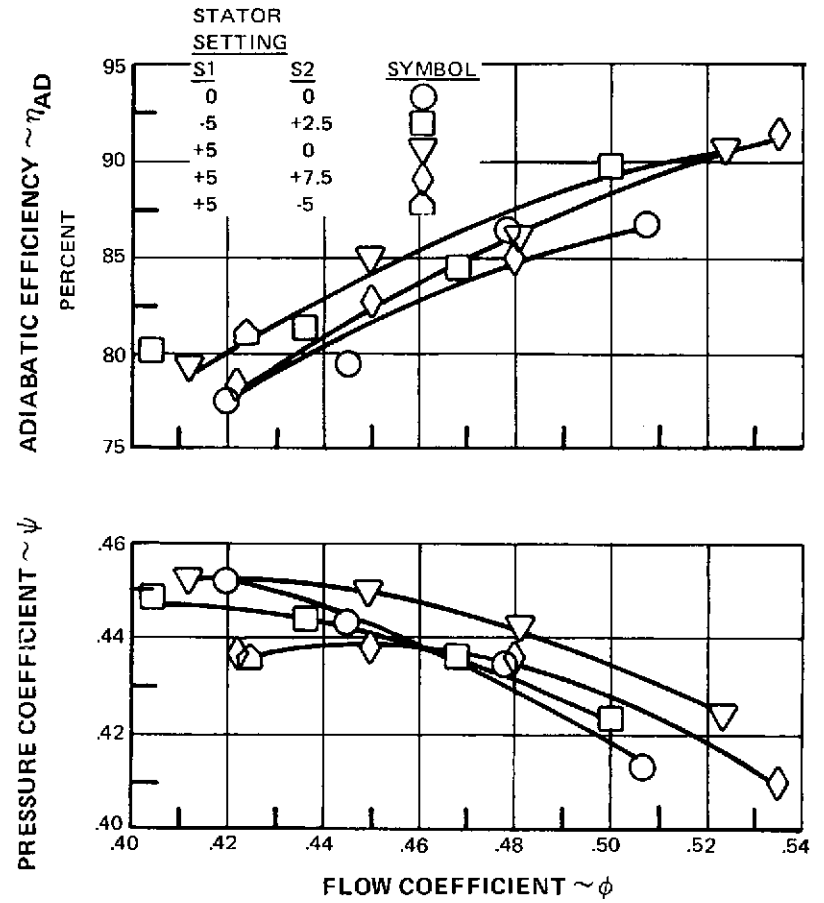


Figure 46 Pressure Coefficient and Adiabatic Efficiency Versus Flow Coefficient for the First Stage at 70 Percent of Design Speed

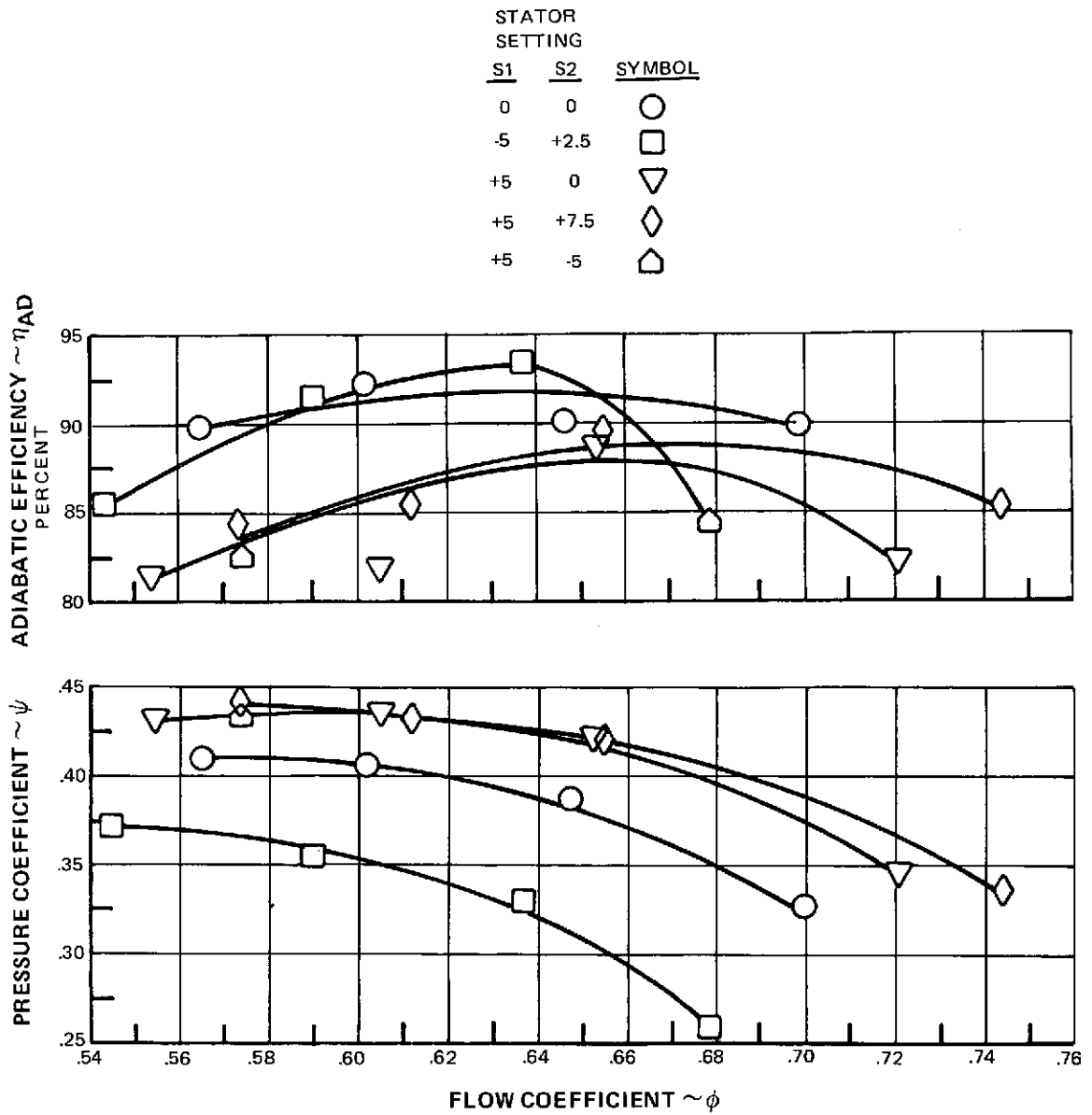


Figure 47 Pressure Coefficient and Adiabatic Efficiency Versus Flow Coefficient for Rotor 2 at 70 Percent of Design Speed

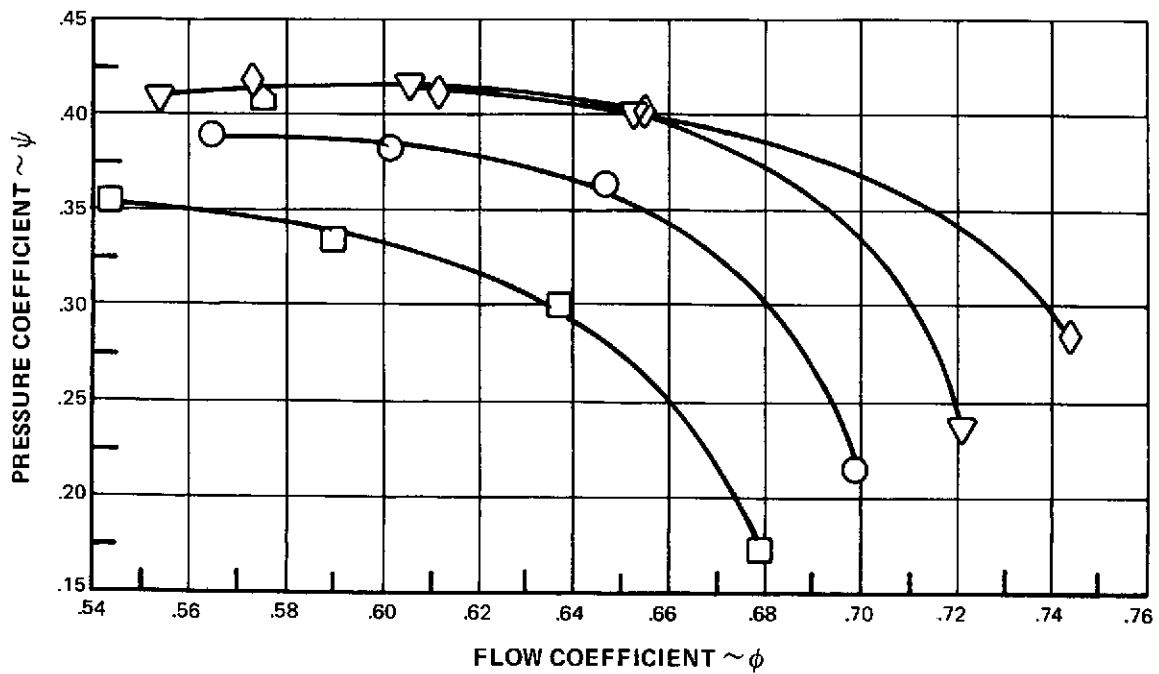
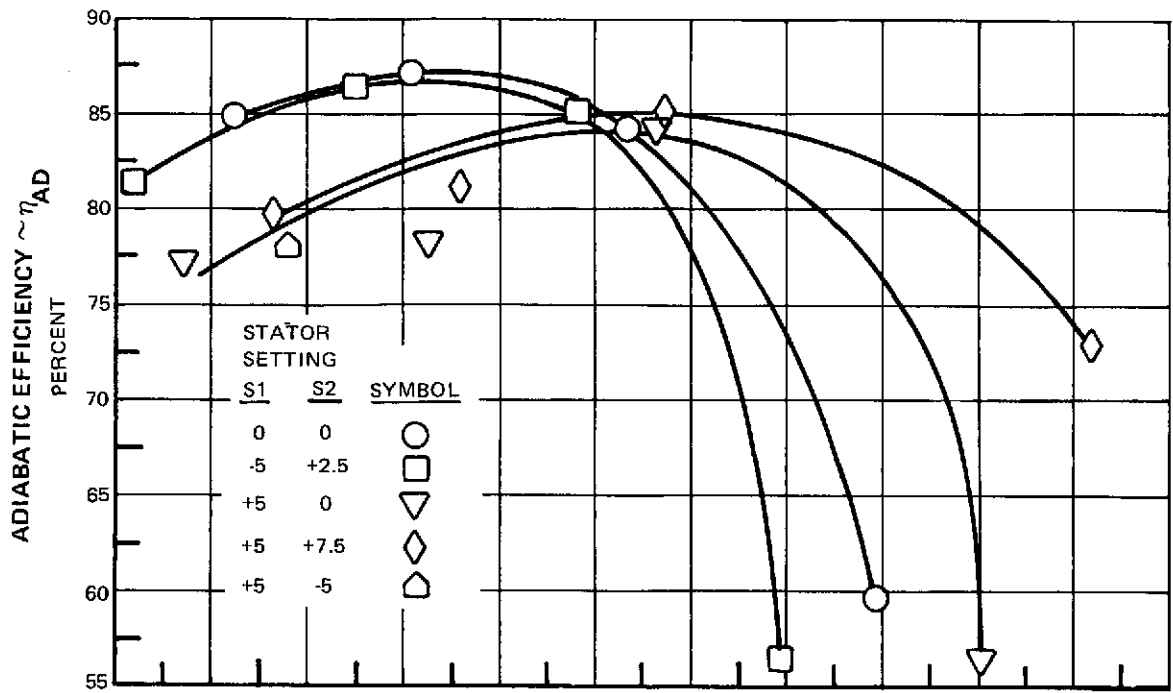


Figure 48 Pressure Coefficient and Adiabatic Efficiency Versus Flow Coefficient for the Second Stage at 70 Percent of Design Speed

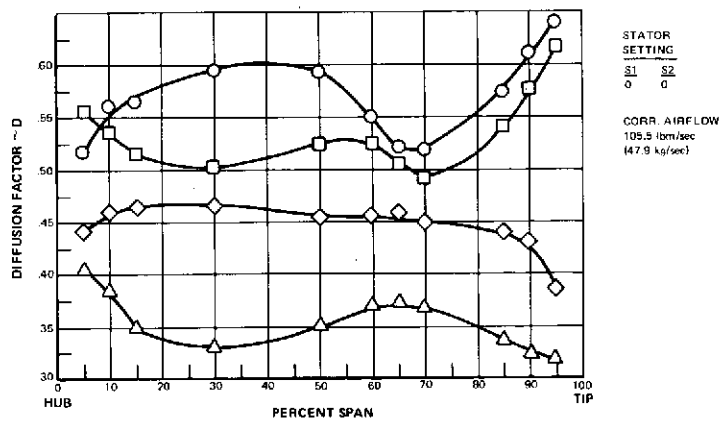
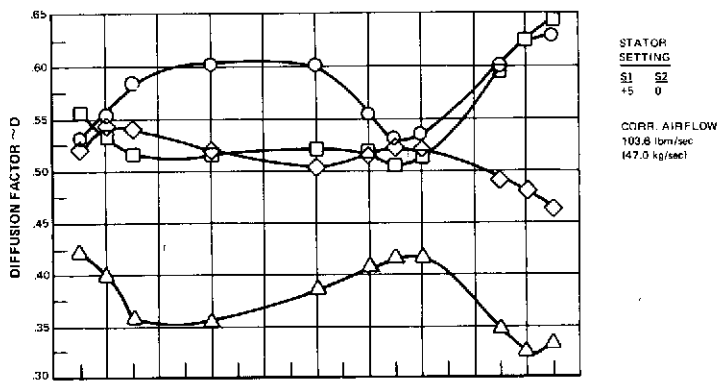
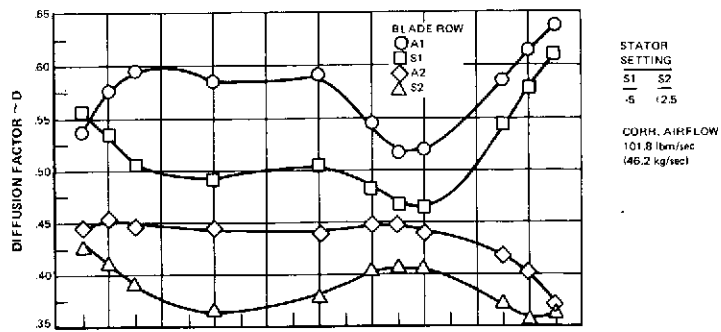


Figure 49 Near-Stall Diffusion Factors Versus Span for Each Blade Row, Showing Effects of Varying Stator Settings at 70 Percent of Design Speed

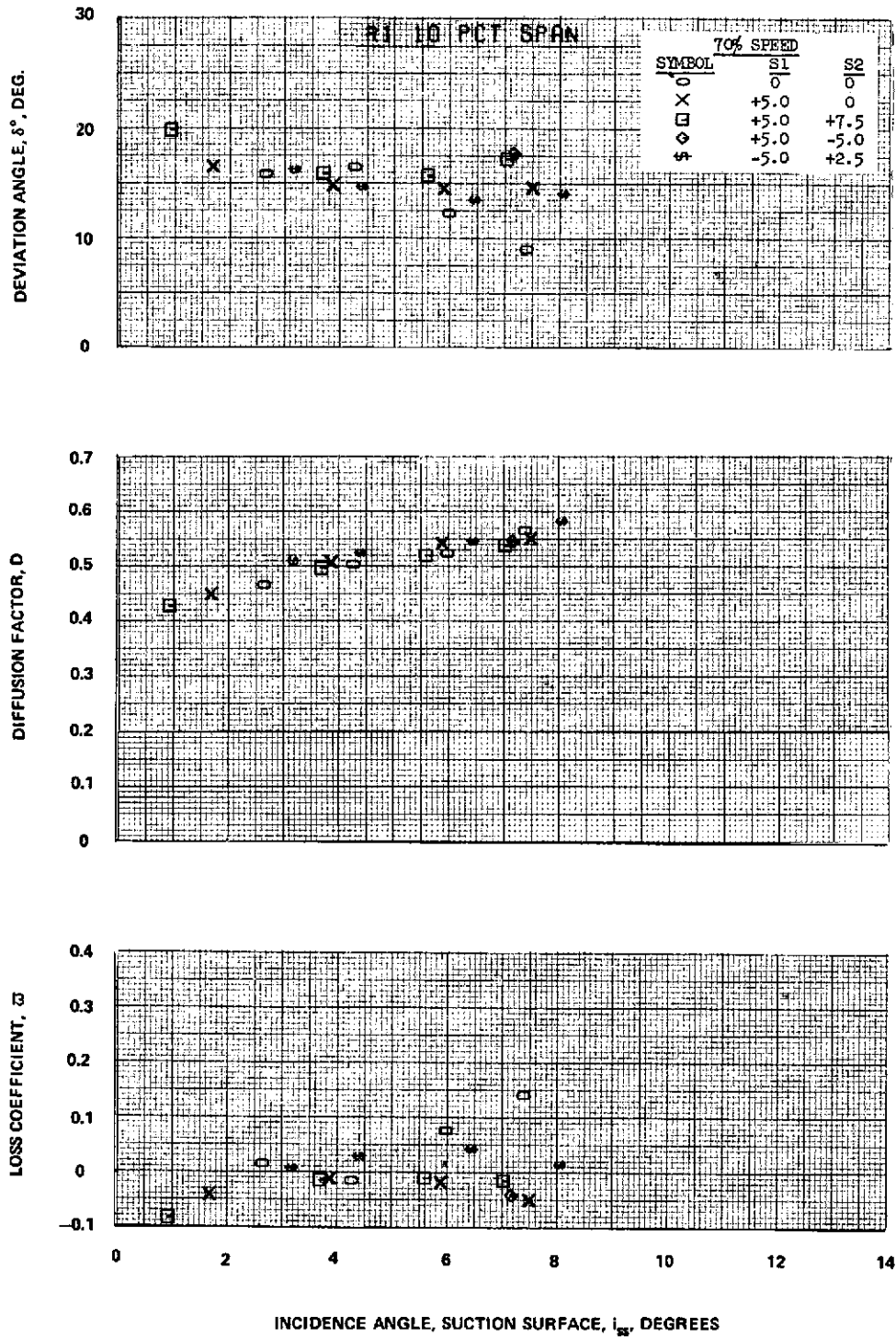


Figure 50A

Figure 50 Blade-Element Performance for Rotor 1 at 70 Percent of Design Speed

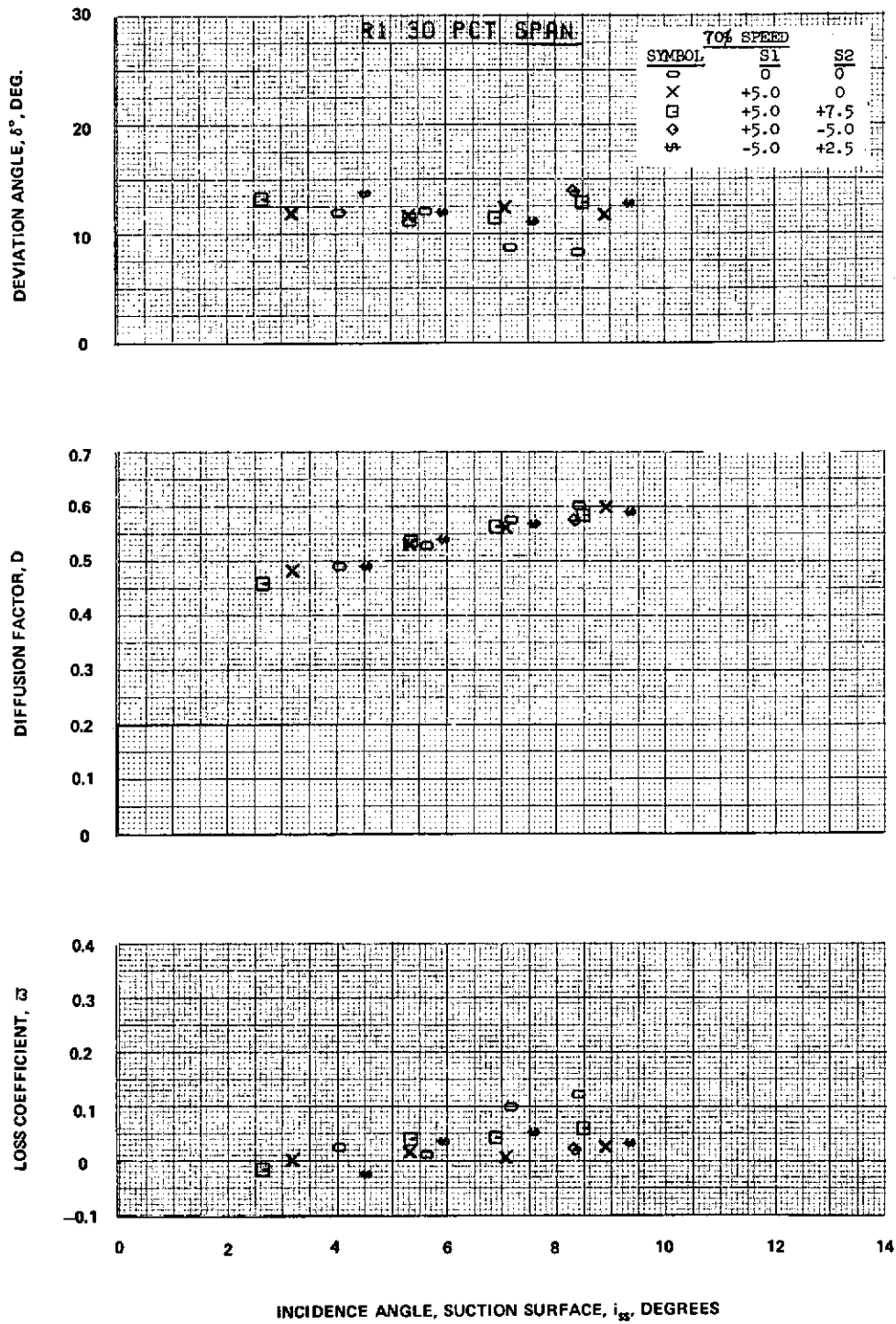


Figure 50B

Figure 50 (Cont'd) Blade-Element Performance for Rotor 1 at 70 Percent of Design Speed

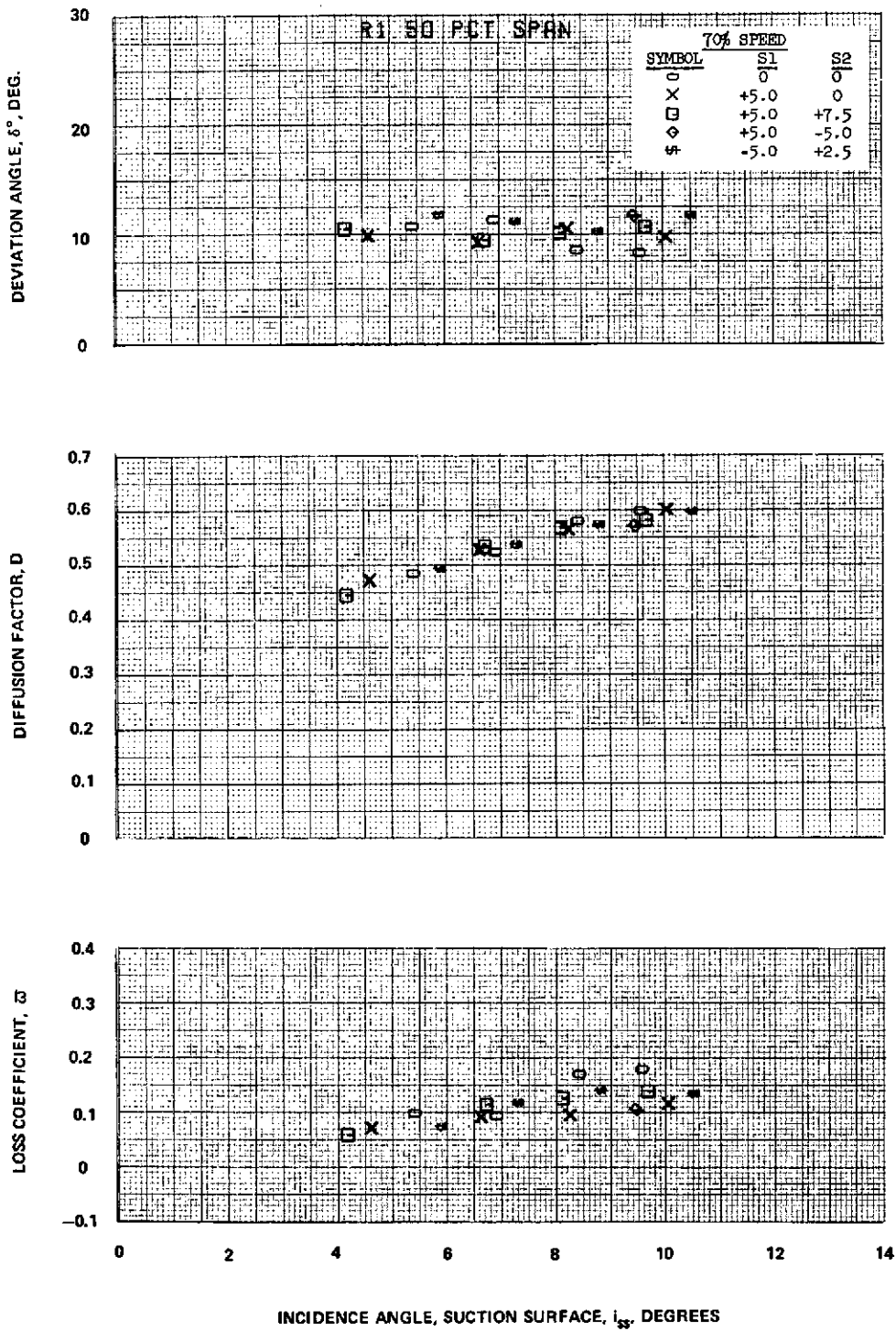


Figure 50C

Figure 50 (Cont'd) Blade-Element Performance for Rotor 1 at 70 Percent of Design Speed

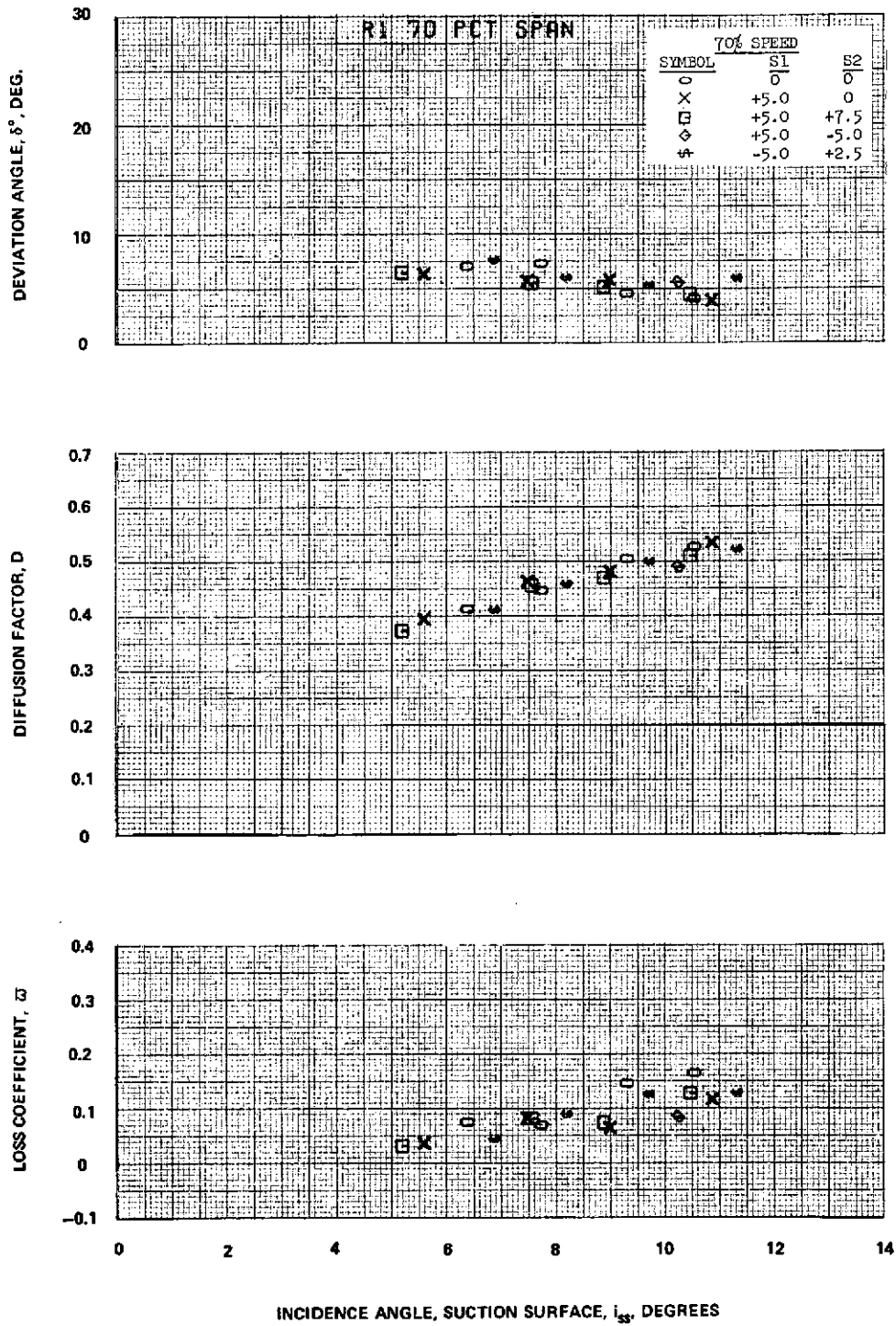


Figure 50D

Figure 50 (Cont'd) Blade-Element Performance for Rotor 1 at 70 Percent of Design Speed

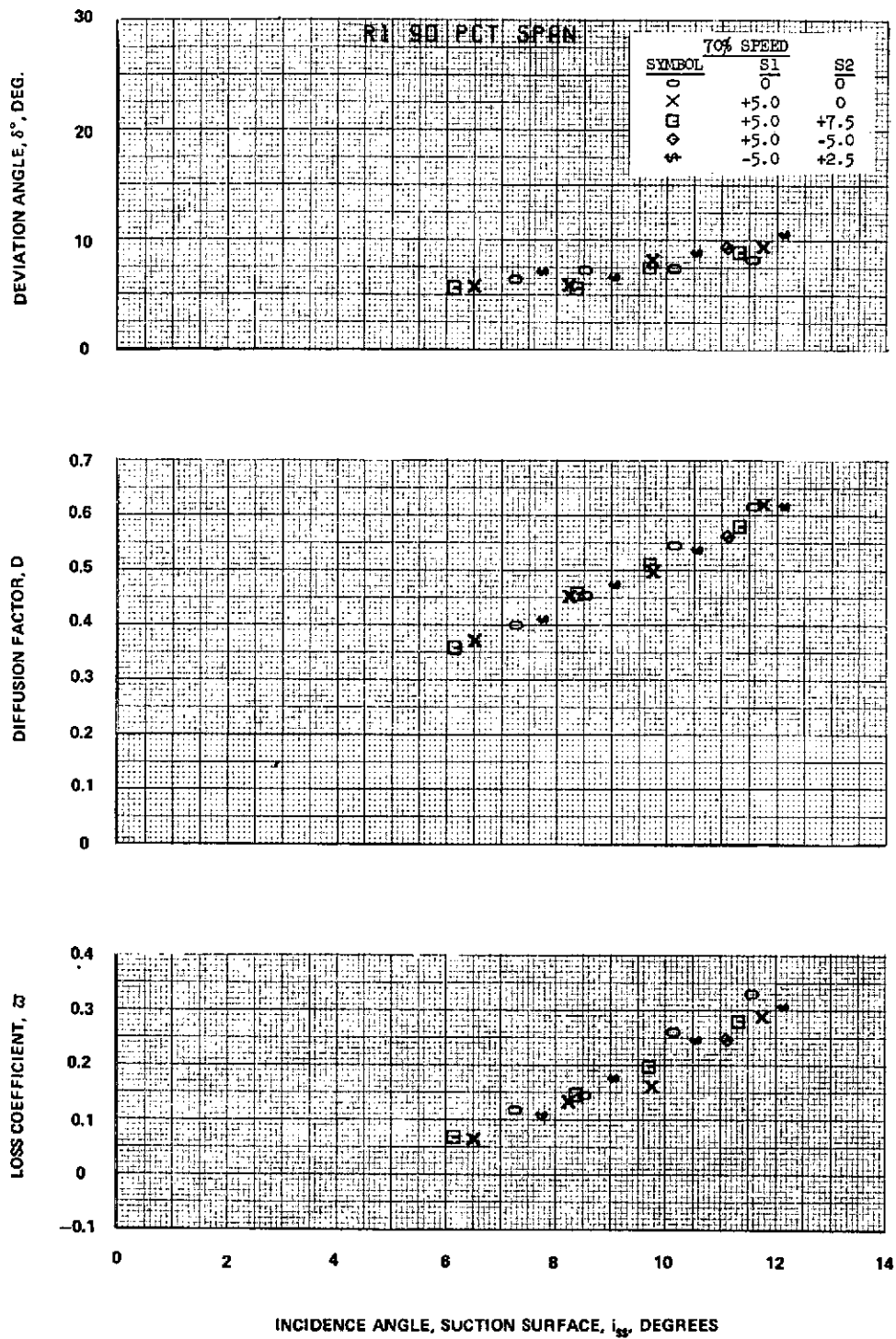


Figure 50E

Figure 50 (Cont'd) Blade-Element Performance for Rotor 1 at 70 Percent of Design Speed

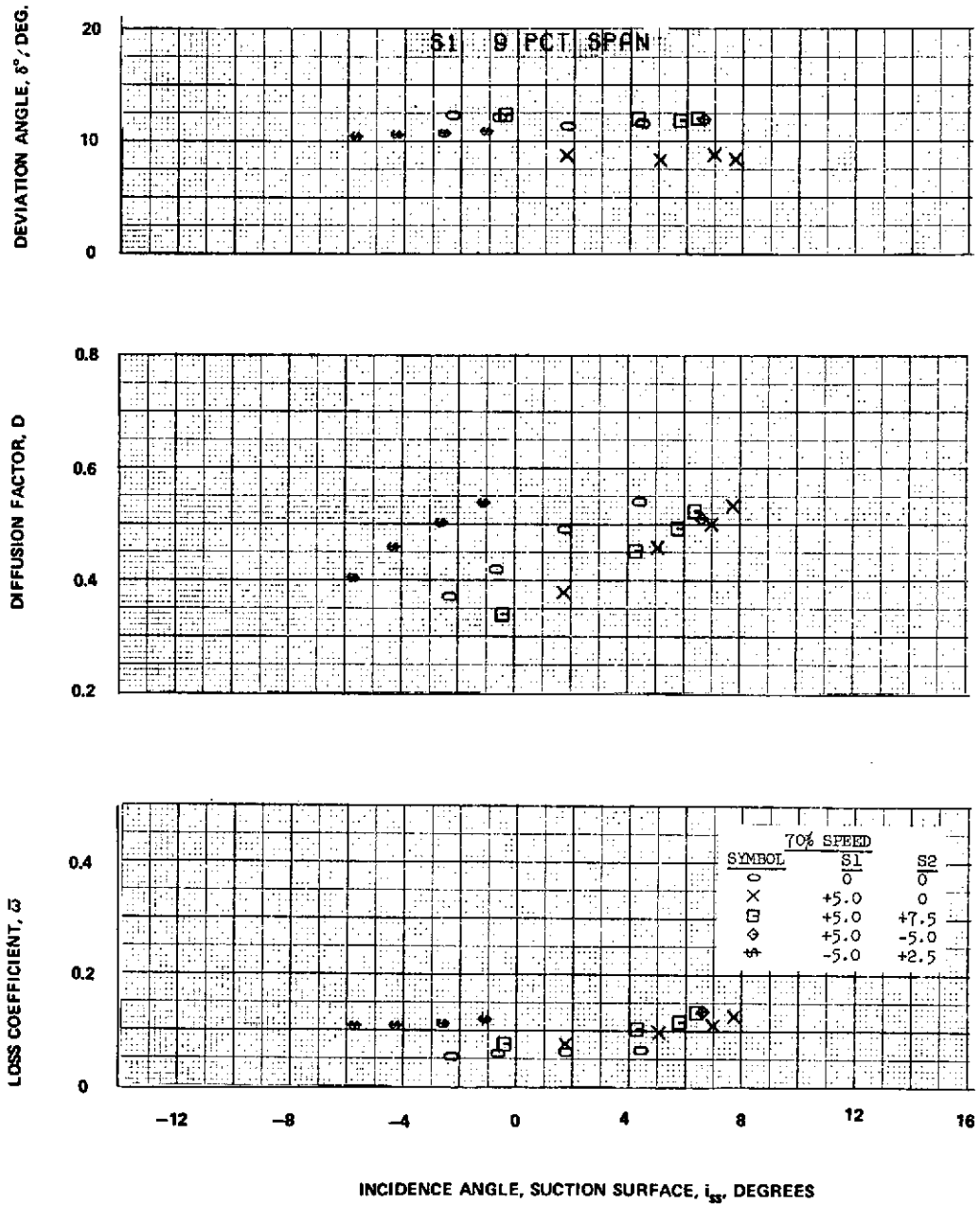


Figure 51A

Figure 51 Blade-Element Performance for Stator 1 at 70 Percent of Design Speed

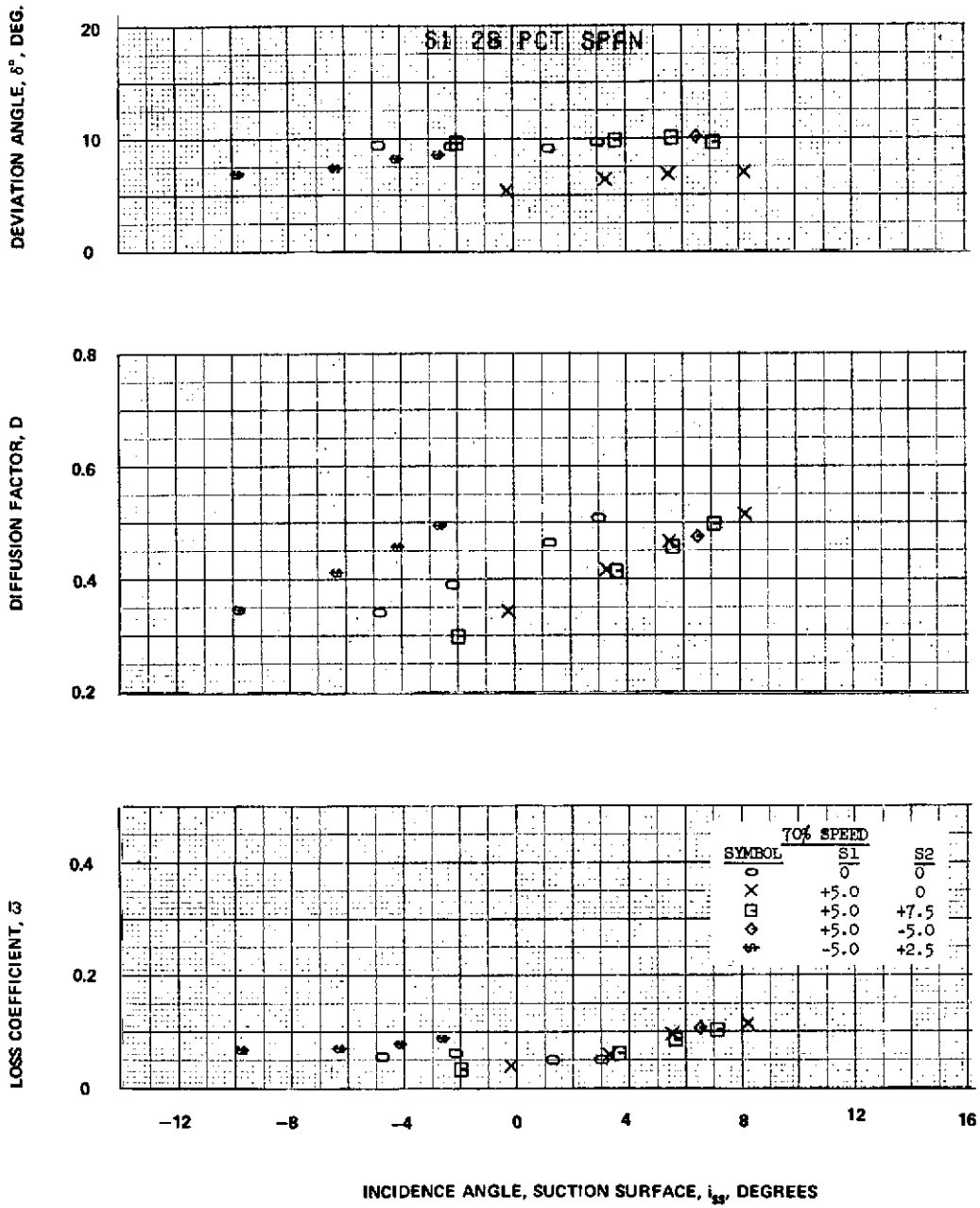


Figure 51B

Figure 51 (Cont'd) Blade-Element Performance for Stator 1 at 70 Percent of Design Speed

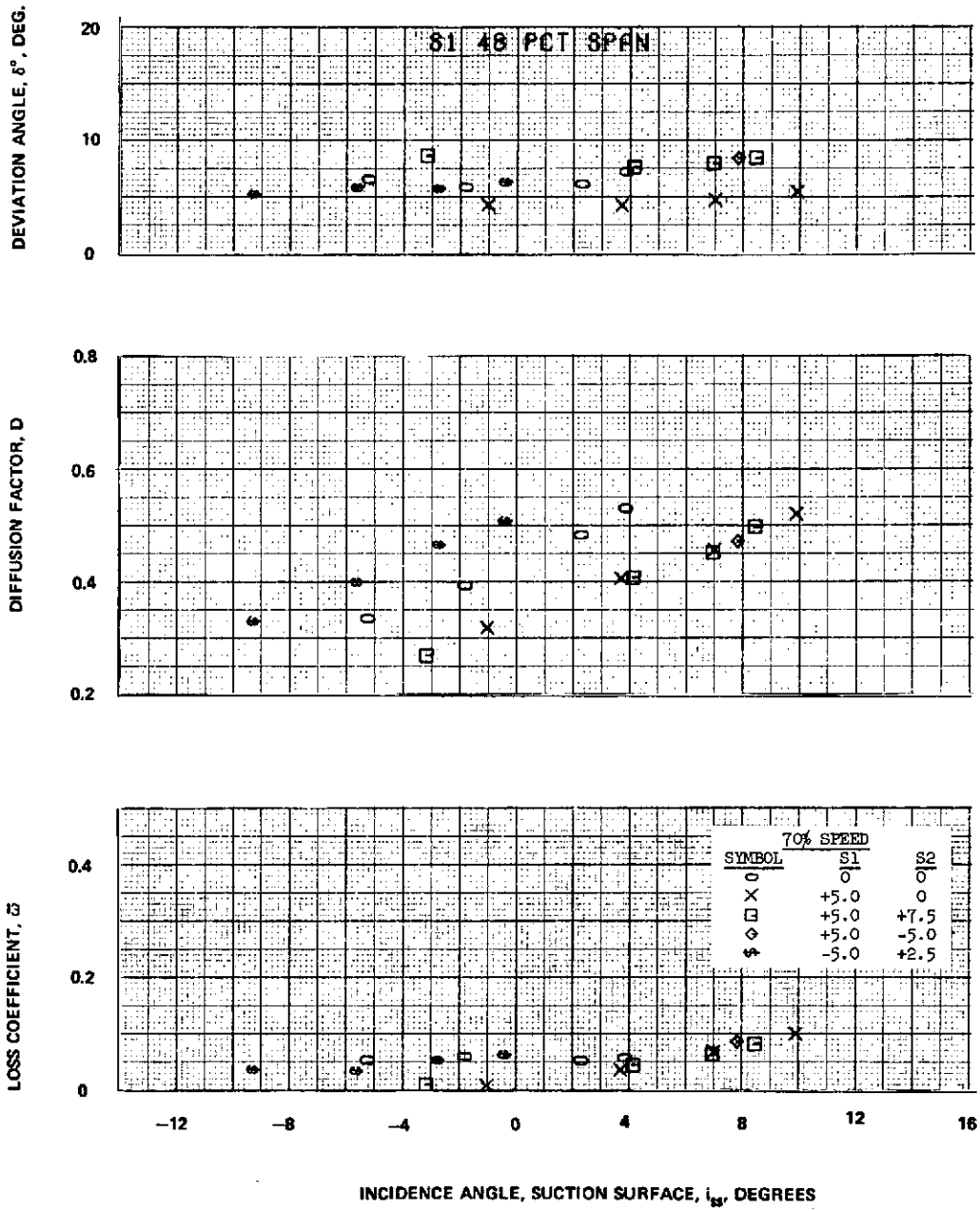


Figure 51C

Figure 51 (Cont'd) Blade-Element Performance for Stator 1 at 70 Percent of Design Speed

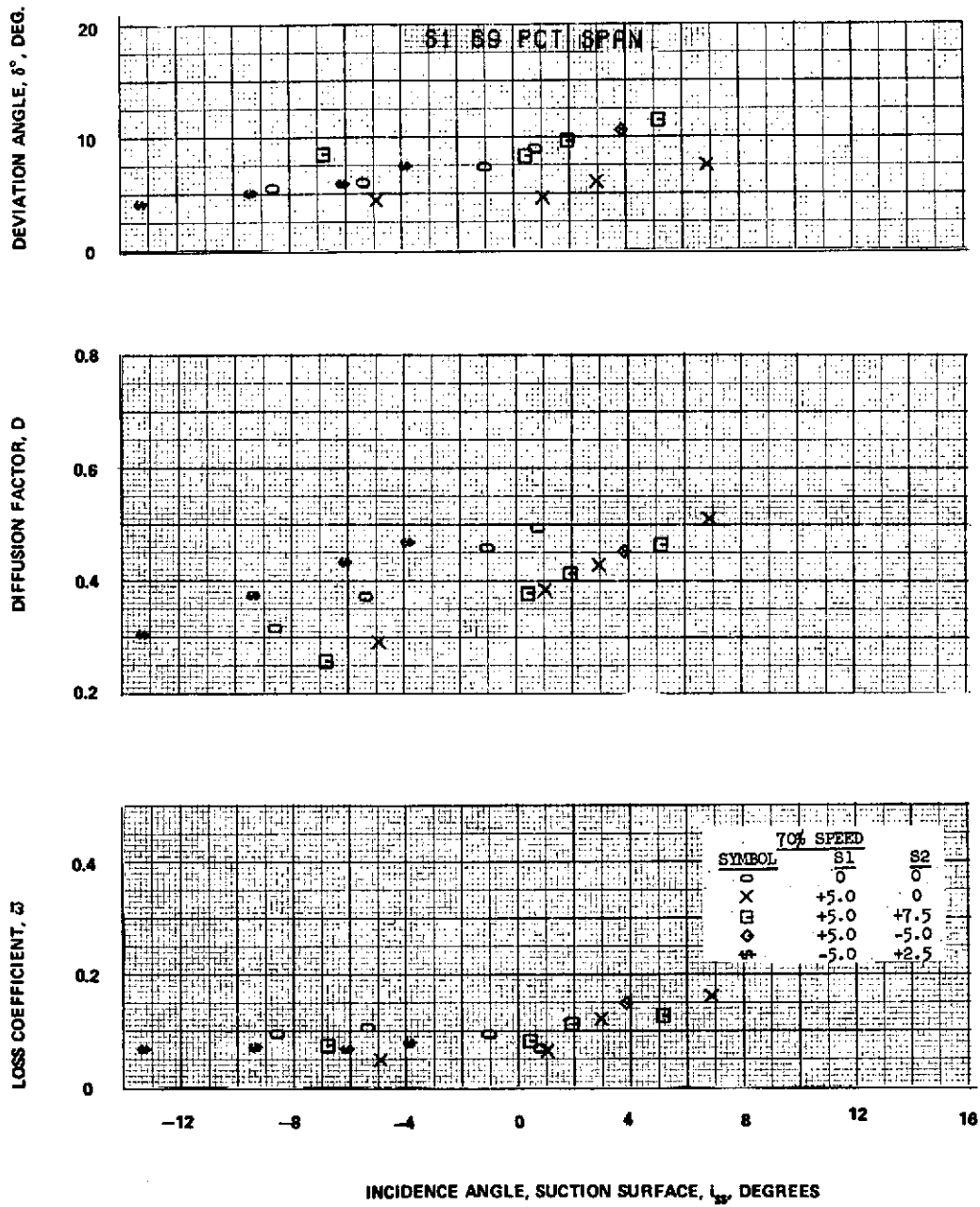


Figure 51D

Figure 51 (Cont'd) Blade-Element Performance for Stator 1 at 70 Percent of Design Speed

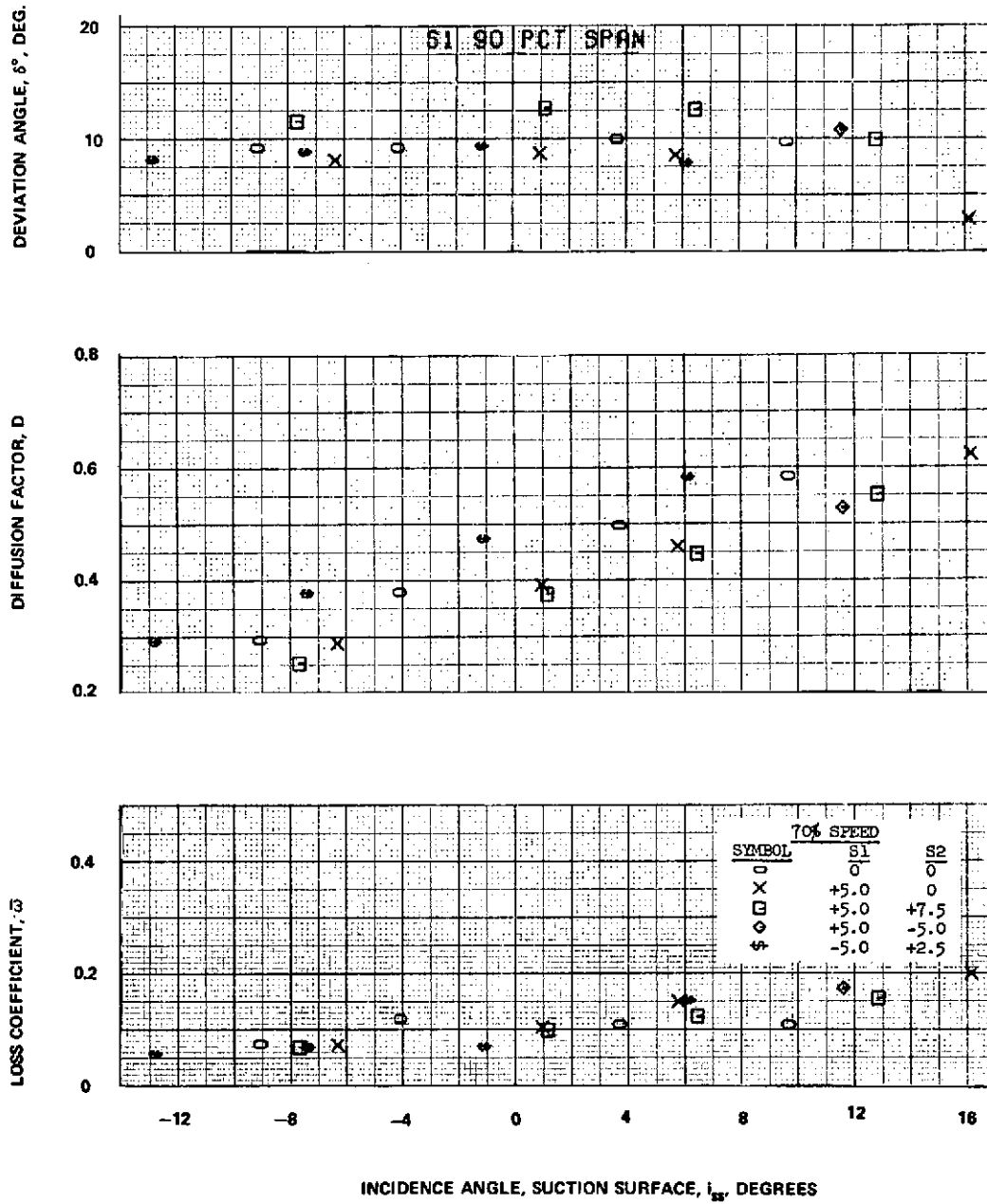


Figure 51E

Figure 51 (Cont'd) Blade-Element Performance for Stator 1 at 70 Percent of Design Speed

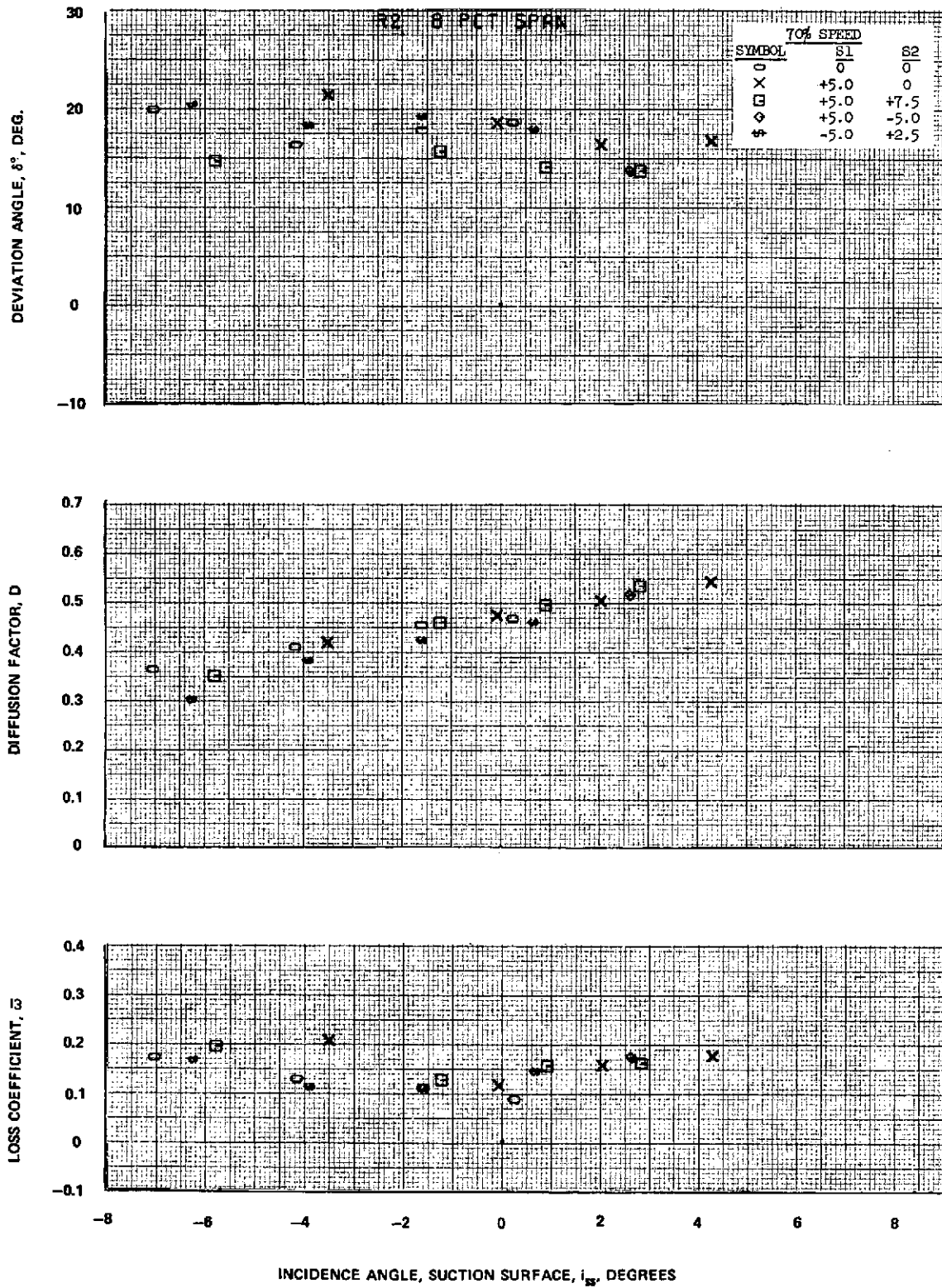


Figure 52A

Figure 52 Blade-Element Performance for Rotor 2 at 70 Percent of Design Speed

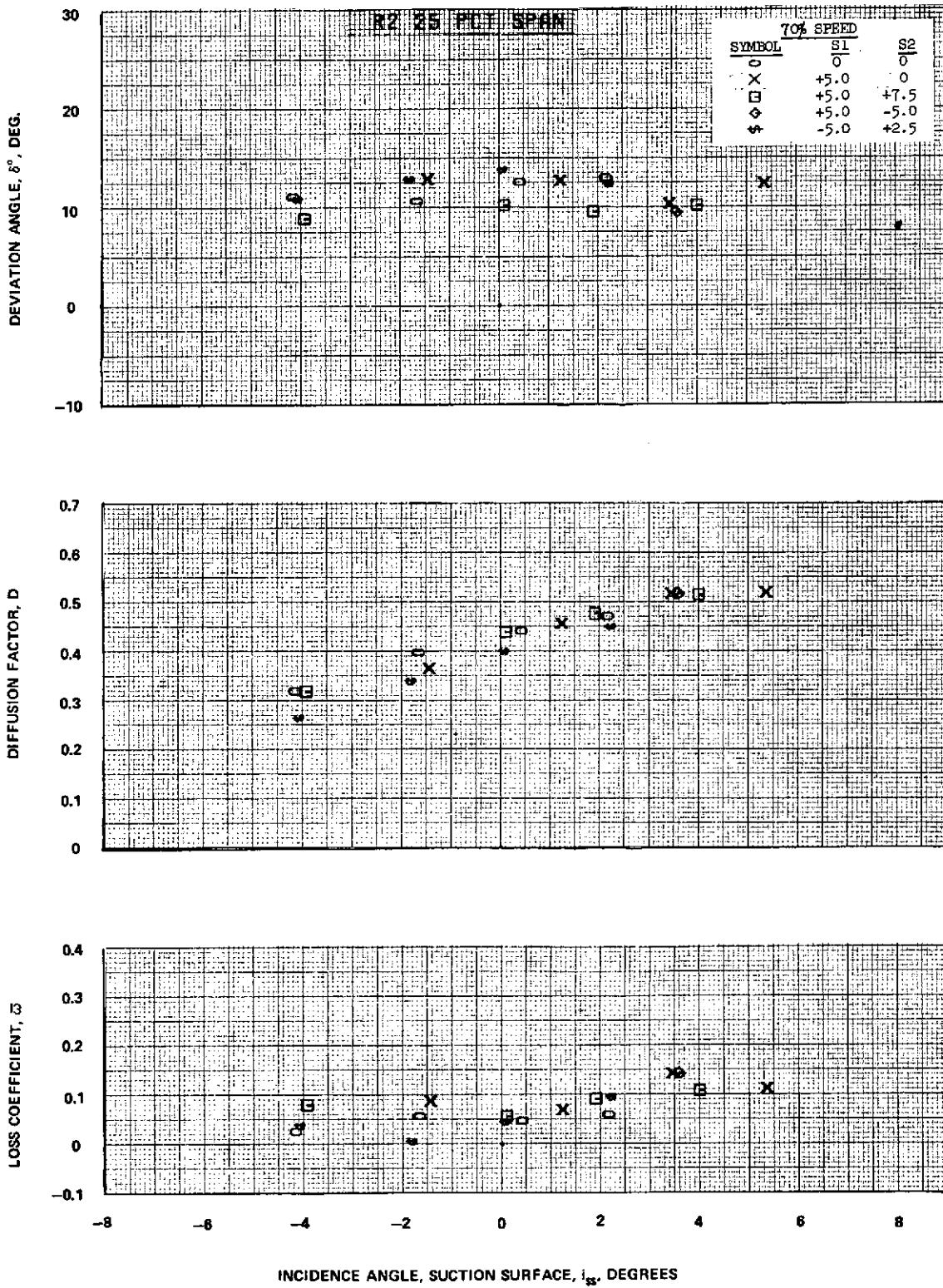


Figure 52B

Figure 52 (Cont'd) Blade-Element Performance for Rotor 2 at 70 Percent of Design Speed

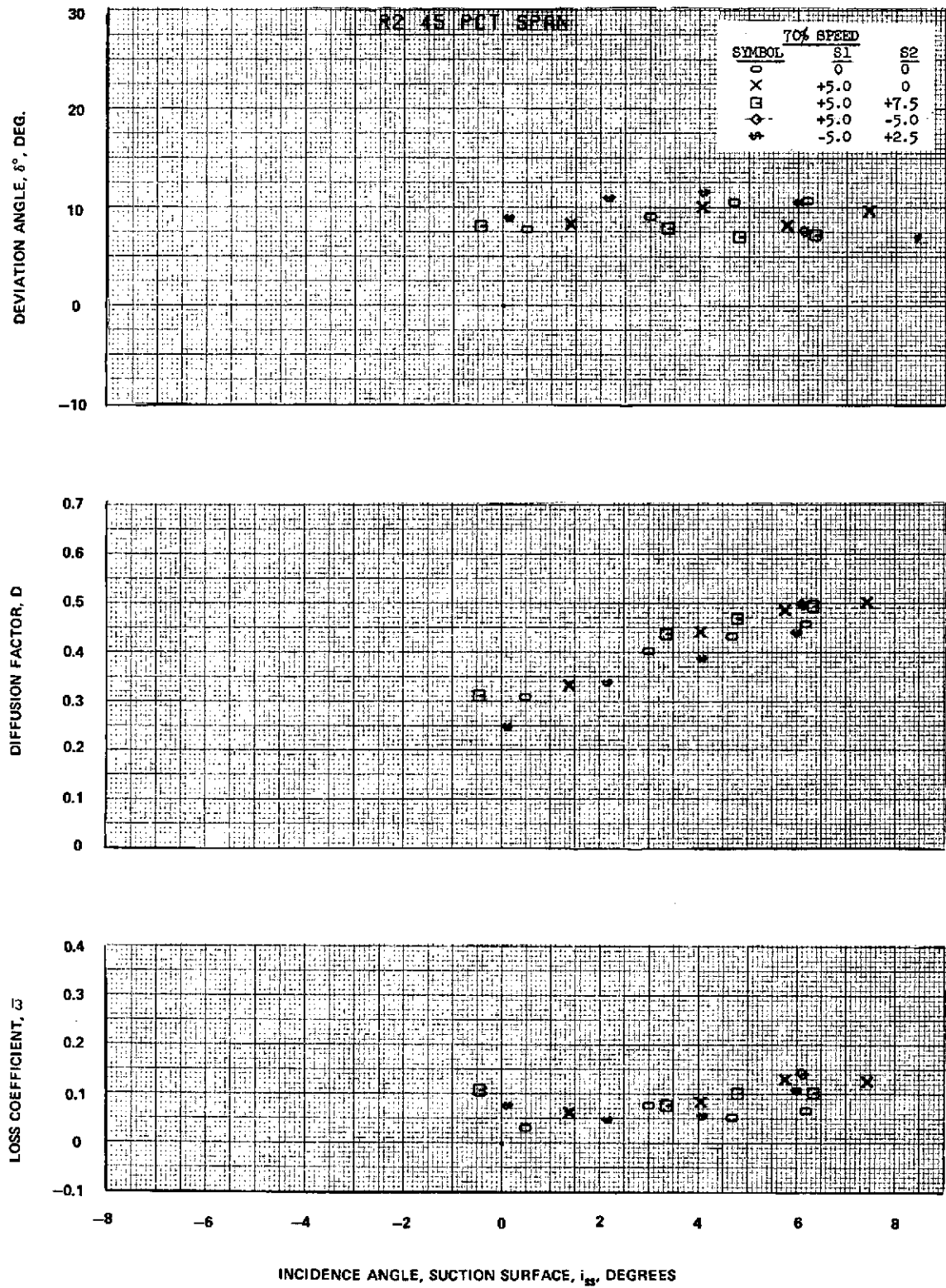


Figure 52C

Figure 52 (Cont'd) Blade-Element Performance for Rotor 2 at 70 Percent of Design Speed

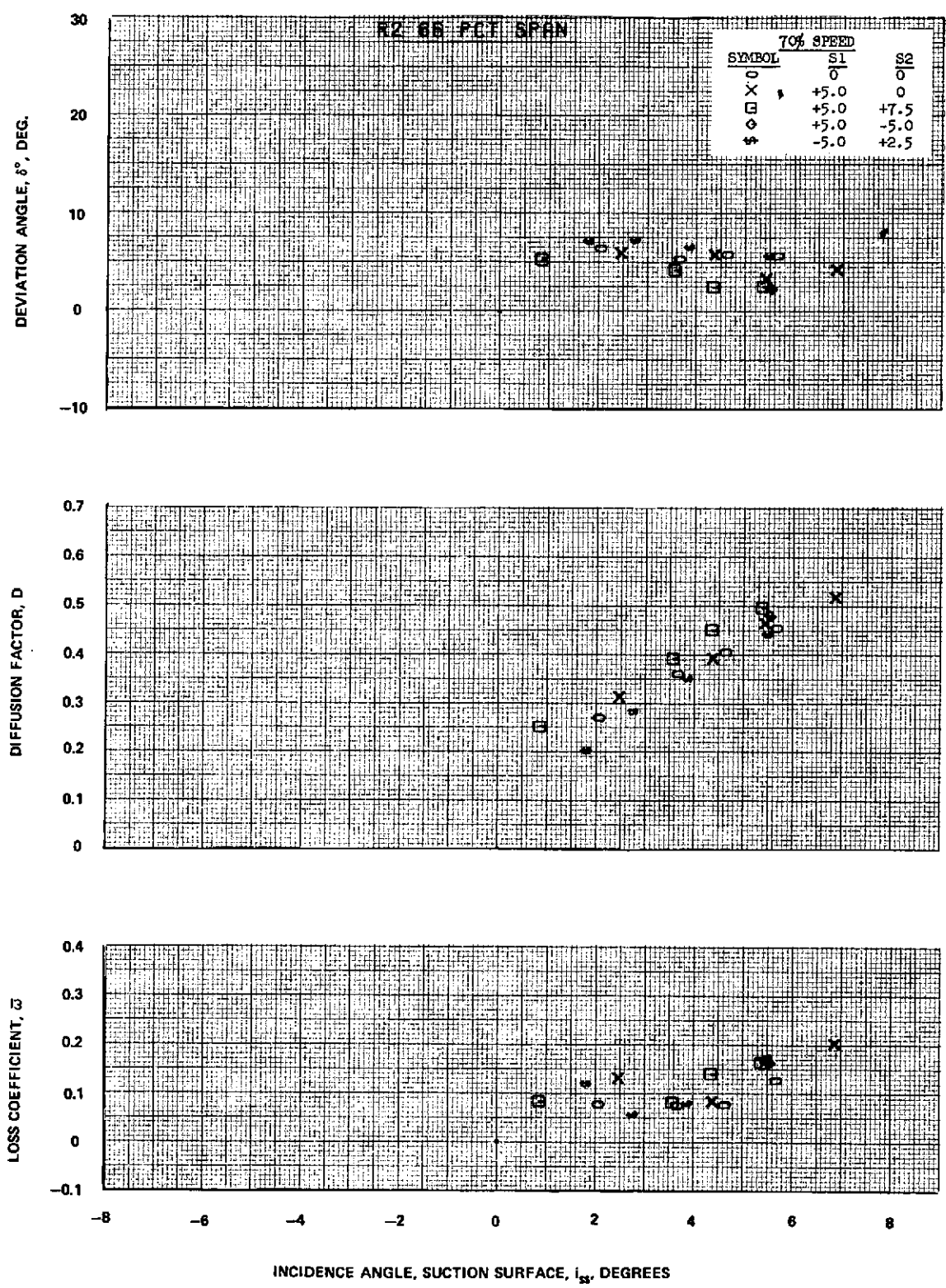


Figure 52D

Figure 52 (Cont'd) Blade-Element Performance for Rotor 2 at 70 Percent of Design Speed

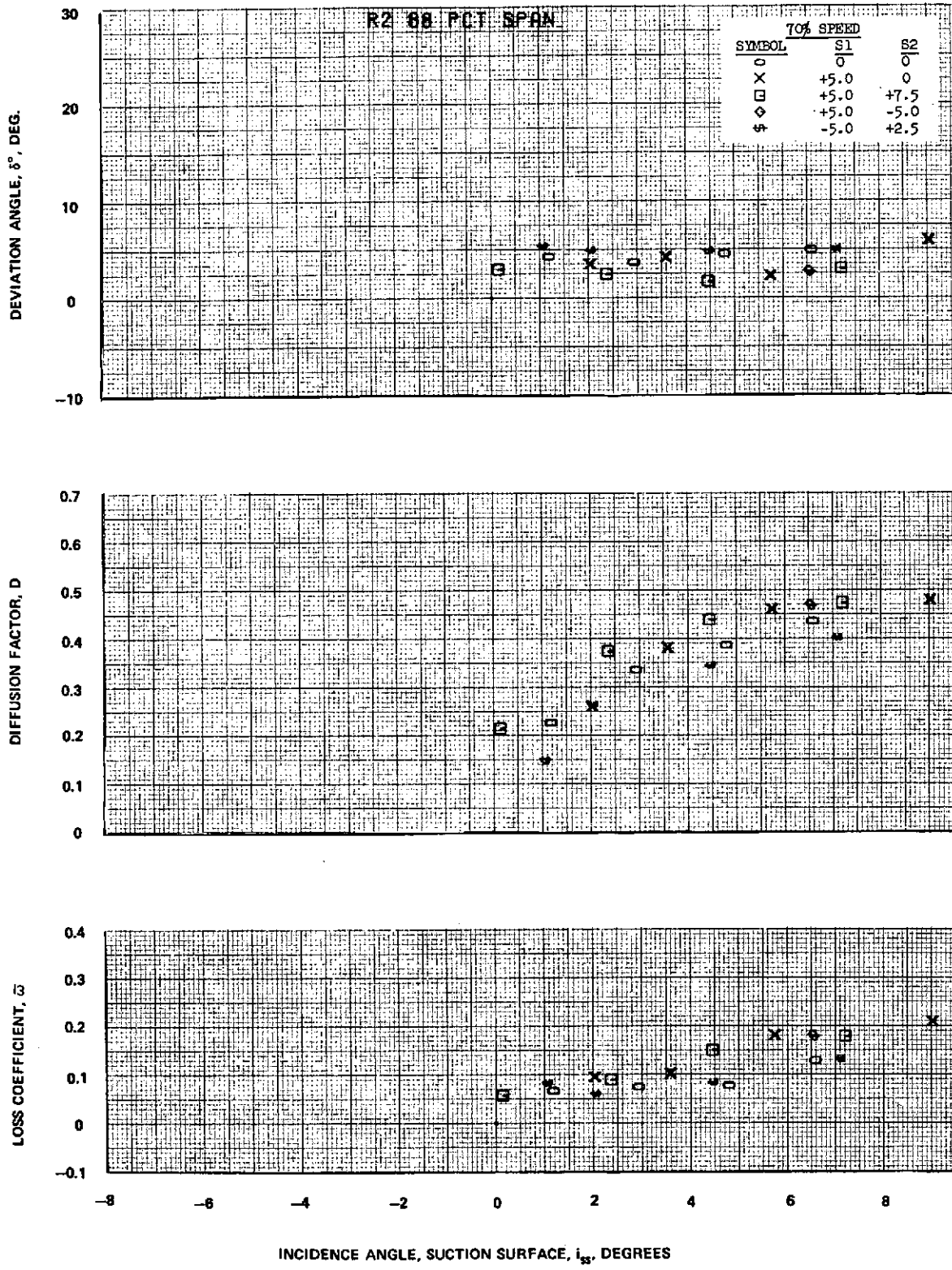


Figure 52E

Figure 52 (Cont'd) Blade-Element Performance for Rotor 2 at 70 Percent of Design Speed

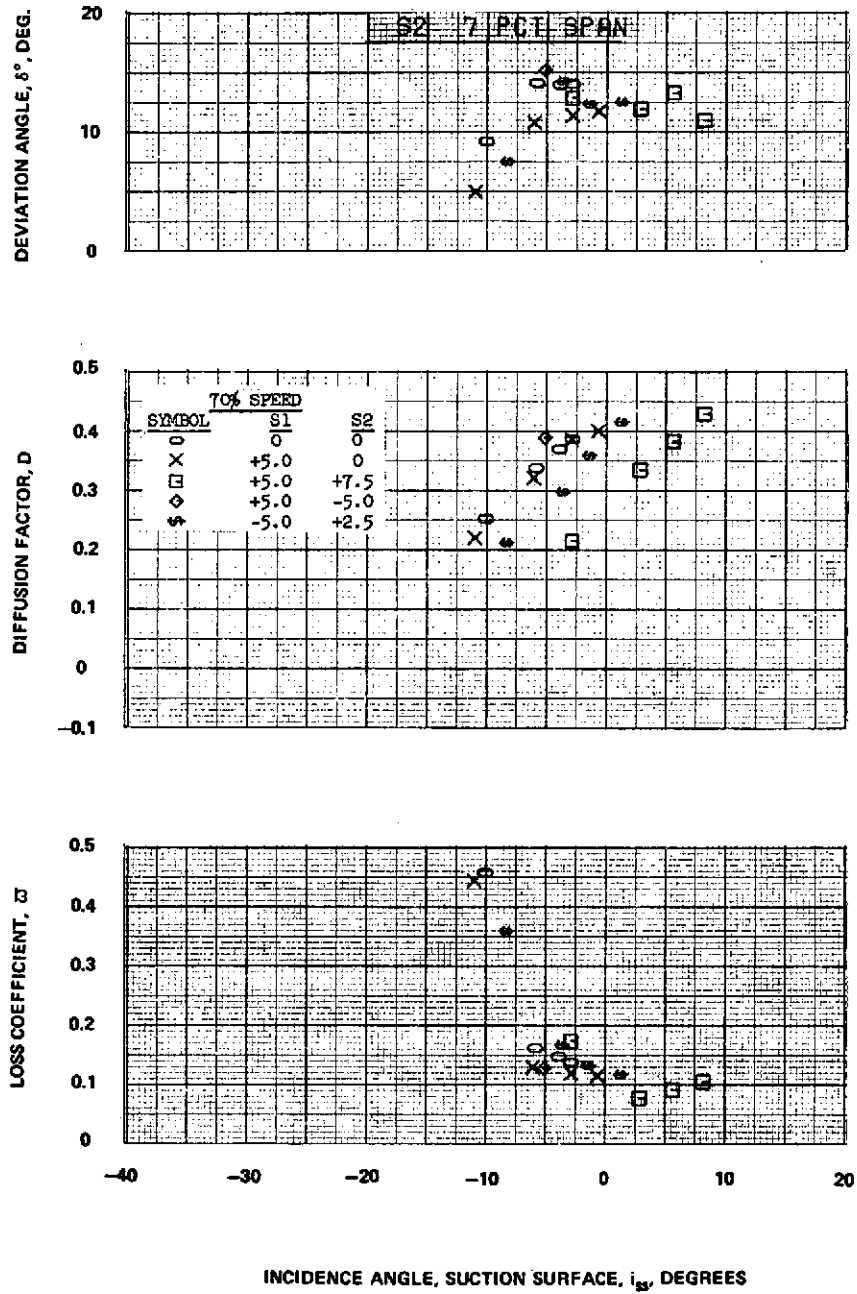


Figure 53A

Figure 53 Blade-Element Performance for Stator 2 at 70 Percent of Design Speed

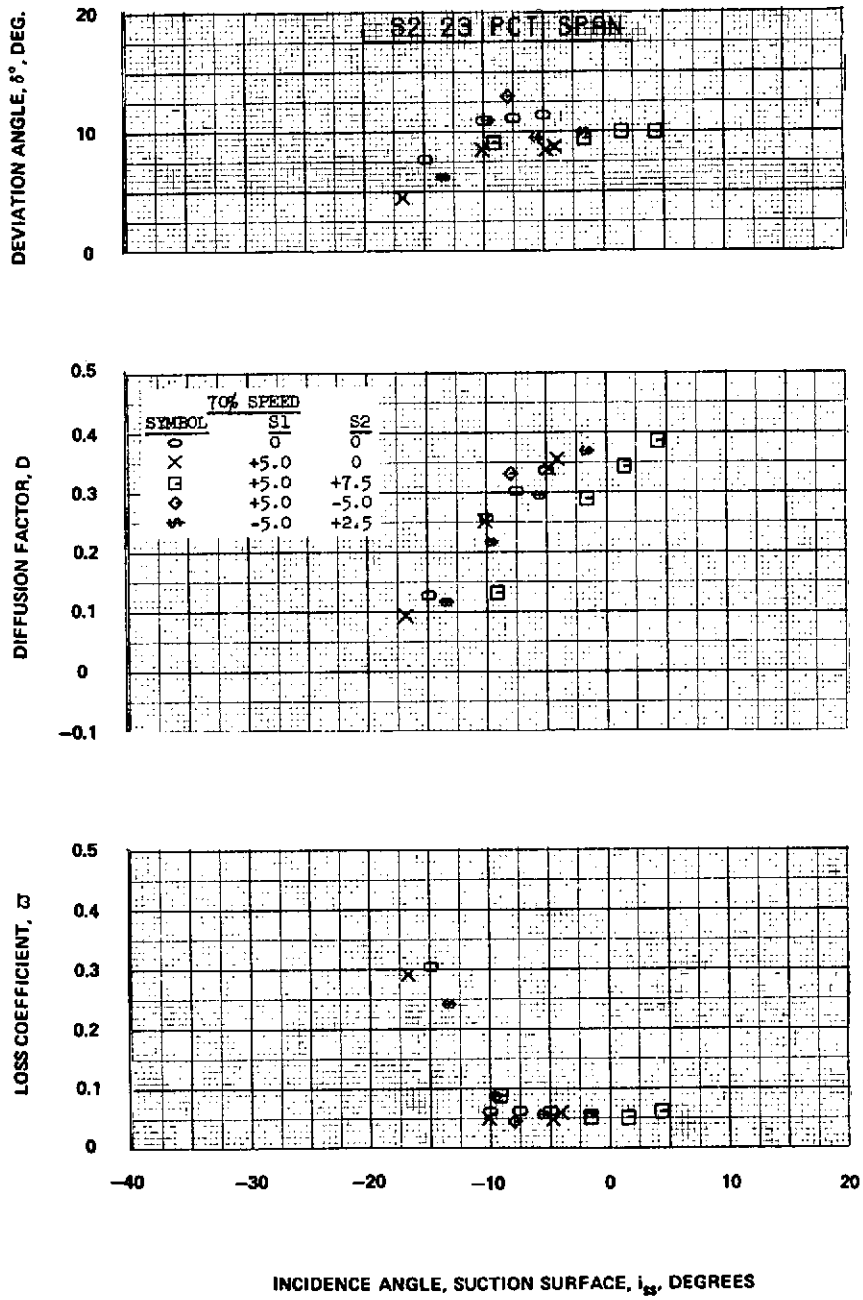


Figure 53B

Figure 53 (Cont'd) Blade-Element Performance for Stator 2 at 70 Percent of Design Speed

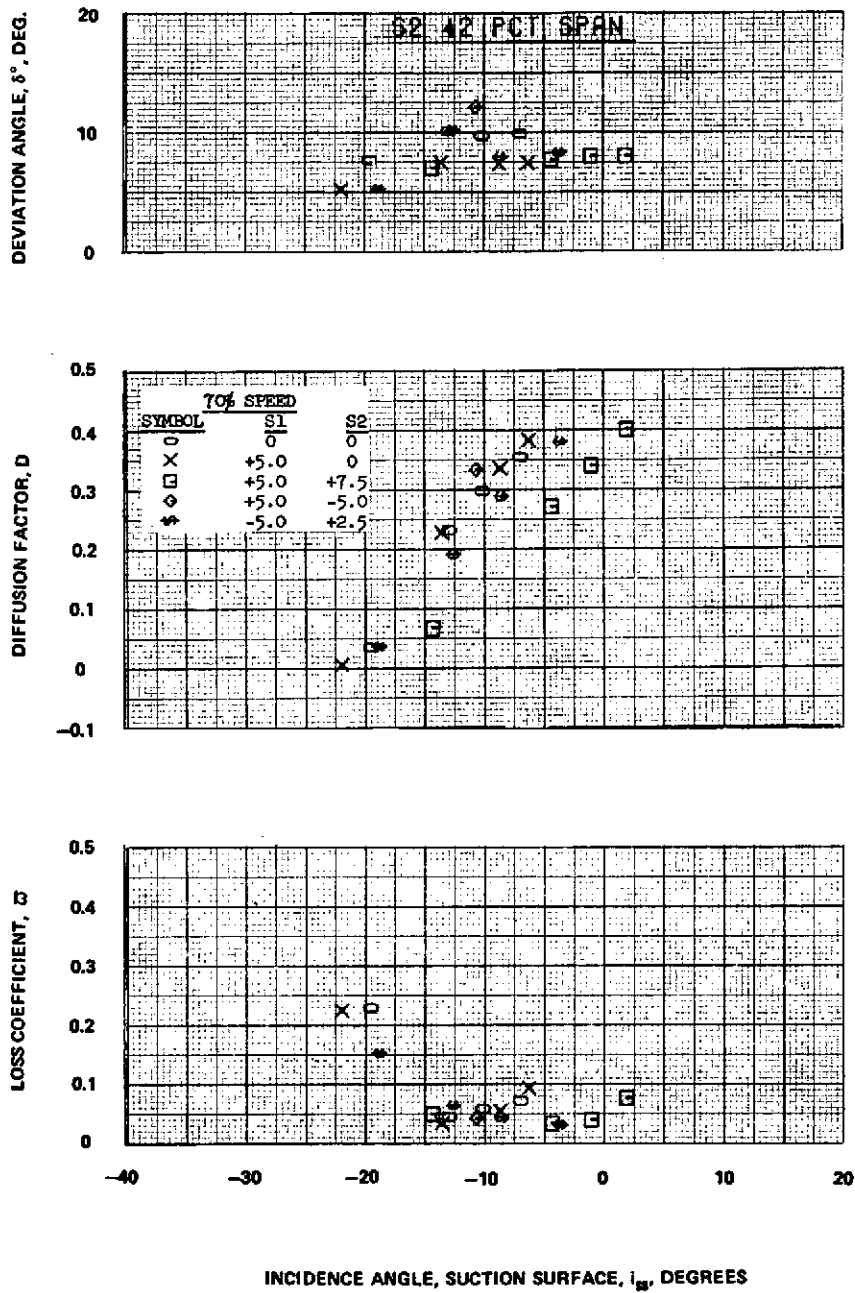


Figure 53C

Figure 53 (Cont'd) Blade-Element Performance for Stator 2 at 70 Percent of Design Speed

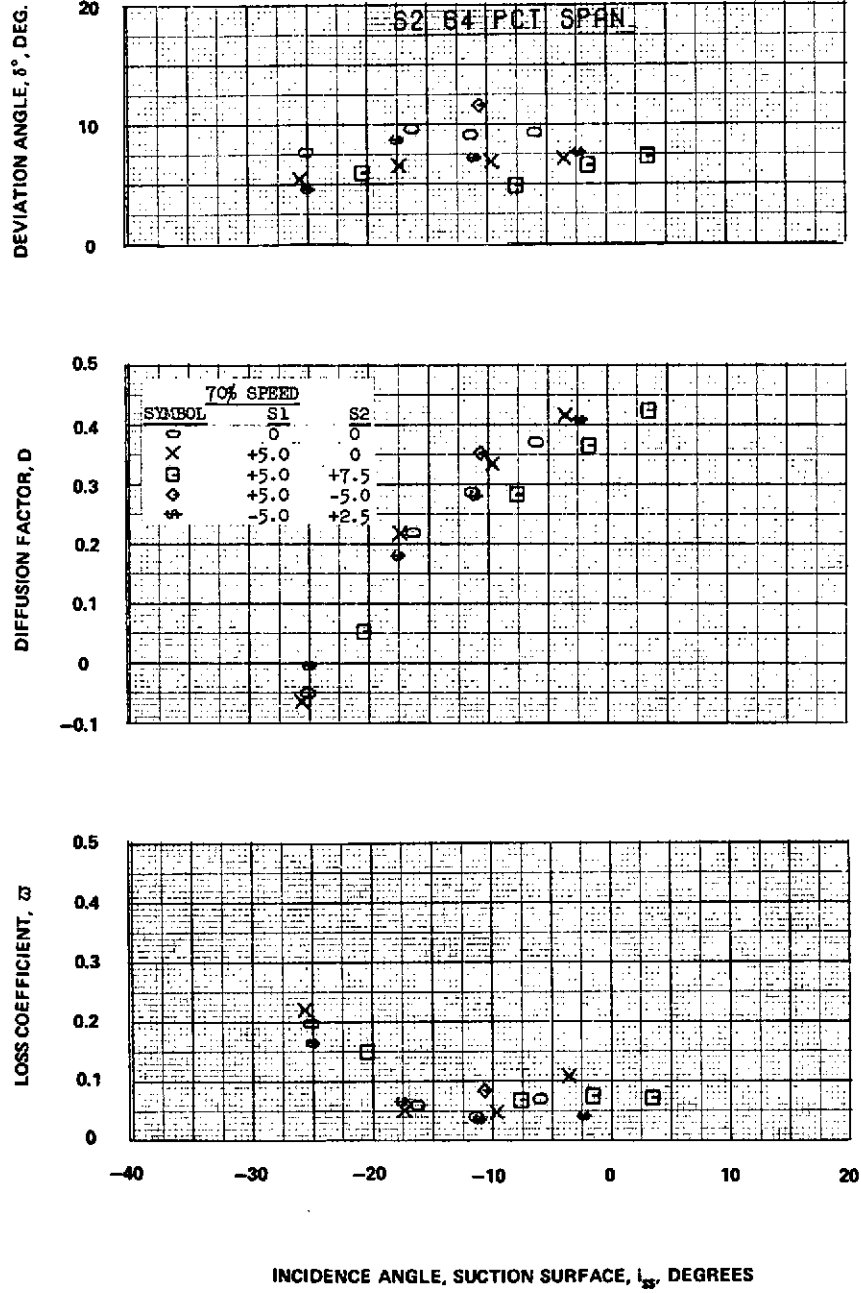


Figure 53D

Figure 53 (Cont'd) Blade-Element Performance for Stator 2 at 70 Percent of Design Speed

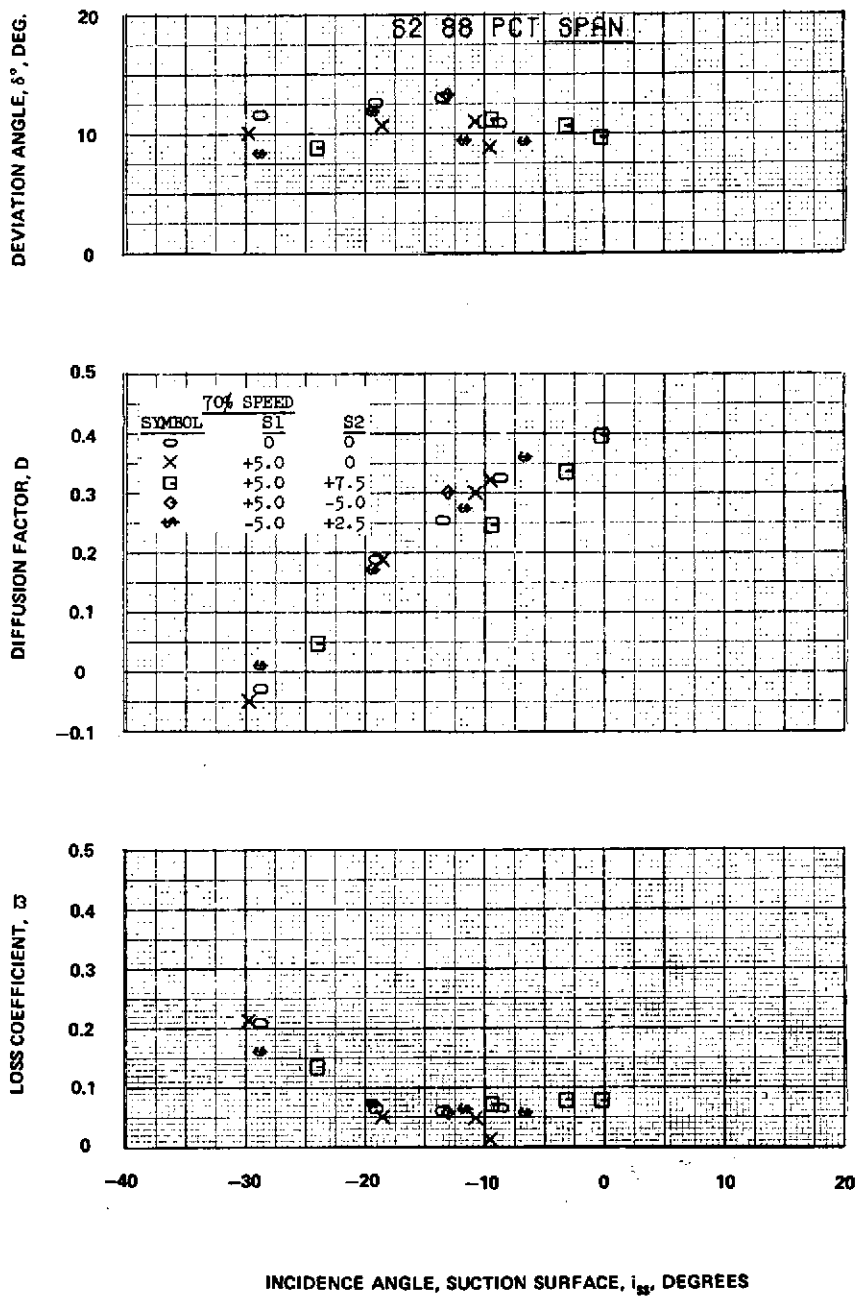


Figure 53E

Figure 53 (Cont'd) Blade-Element Performance for Stator 2 at 70 Percent of Design Speed

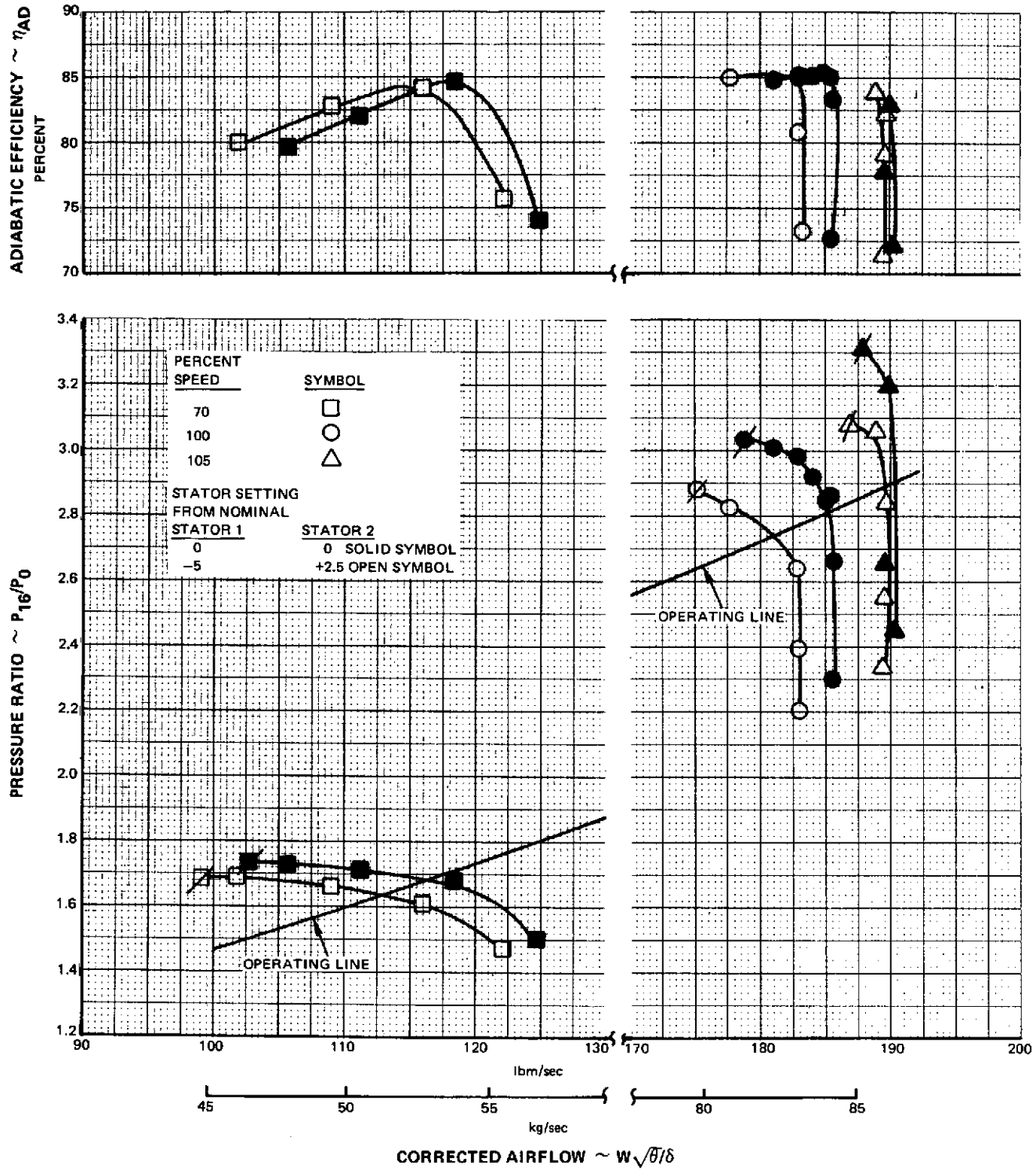


Figure 54 Fan Overall Performance for the (0, 0) and (-5, +2.5) Stator Configurations

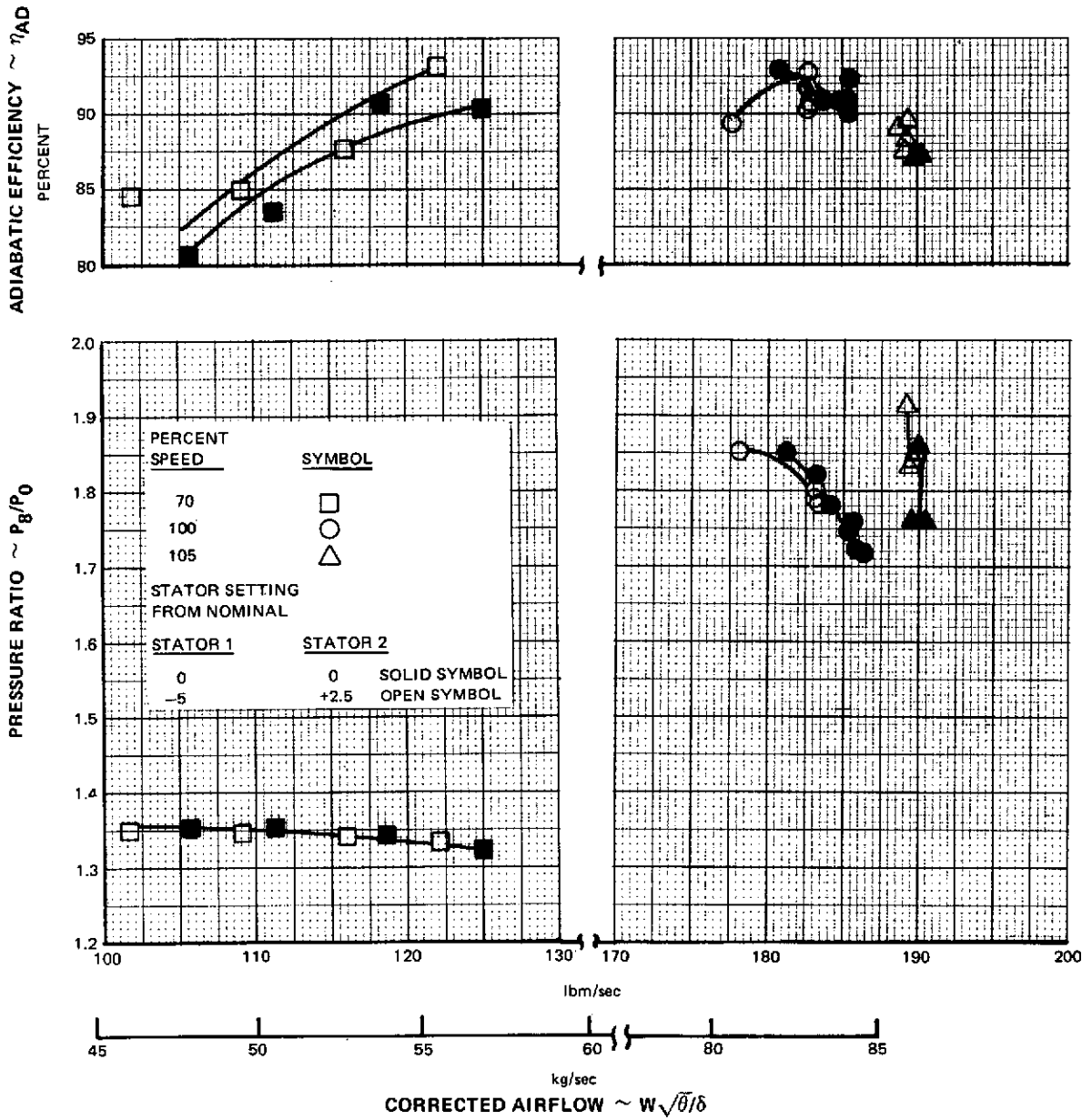


Figure 55 Rotor 1 Performance for the (0, 0) and (-5, +2.5) Stator Configurations

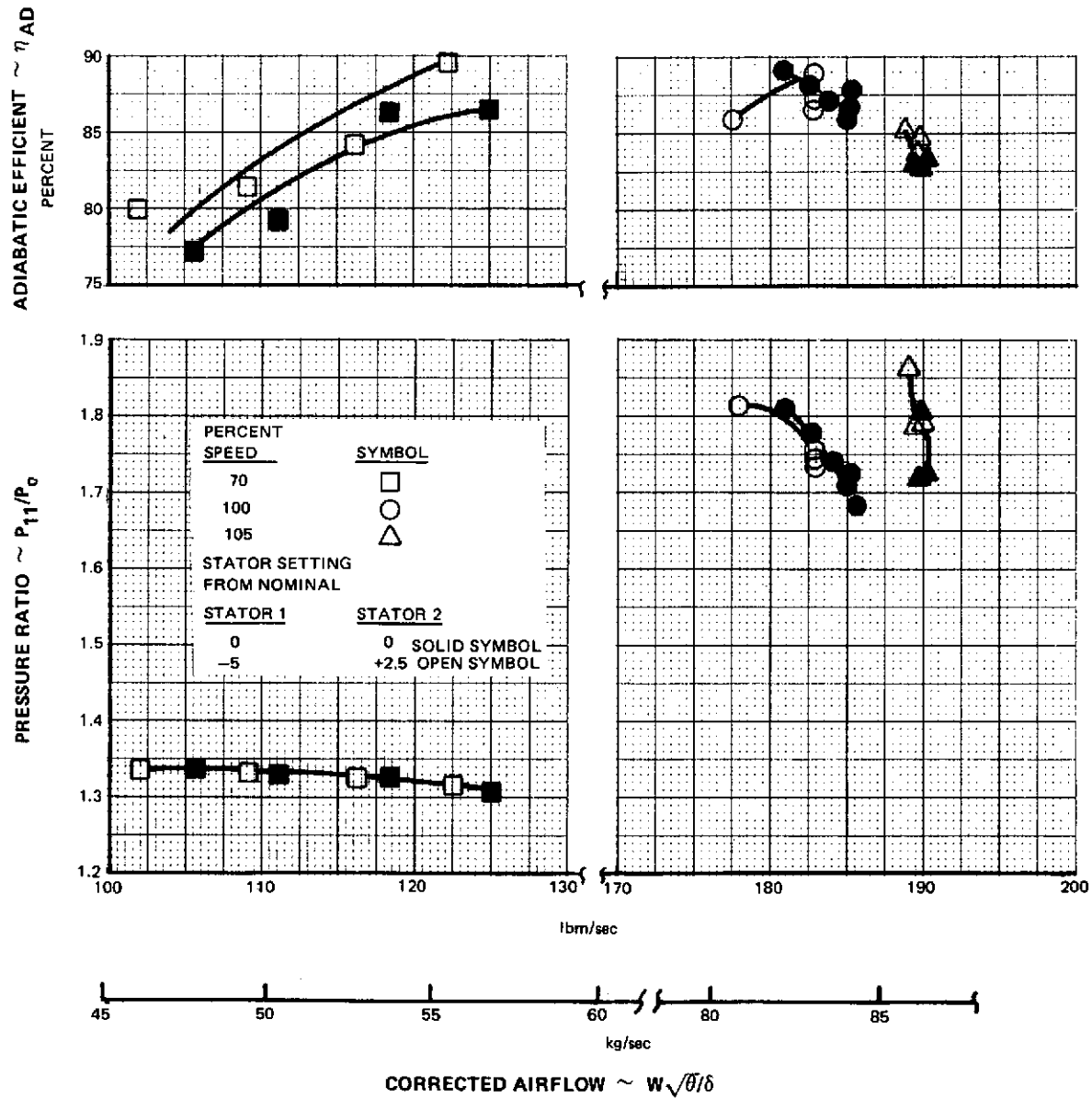


Figure 56 First-Stage Performance for the (0, 0) and (-5, +2.5) Stator Configurations

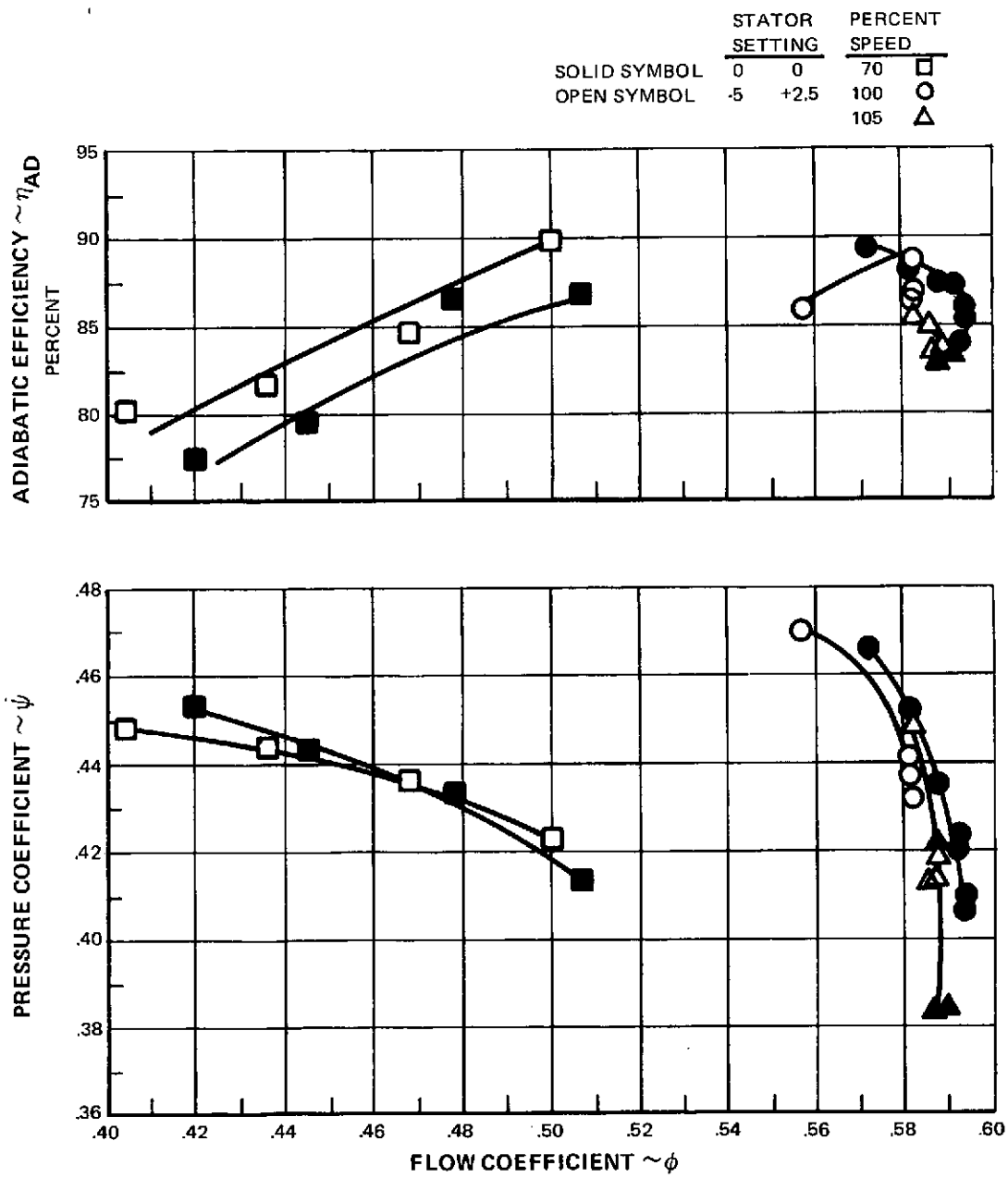


Figure 57 Pressure Coefficient and Adiabatic Efficiency Versus Flow Coefficient for the First-Stage (0, 0) and (-5, +2.5) Stator Configurations

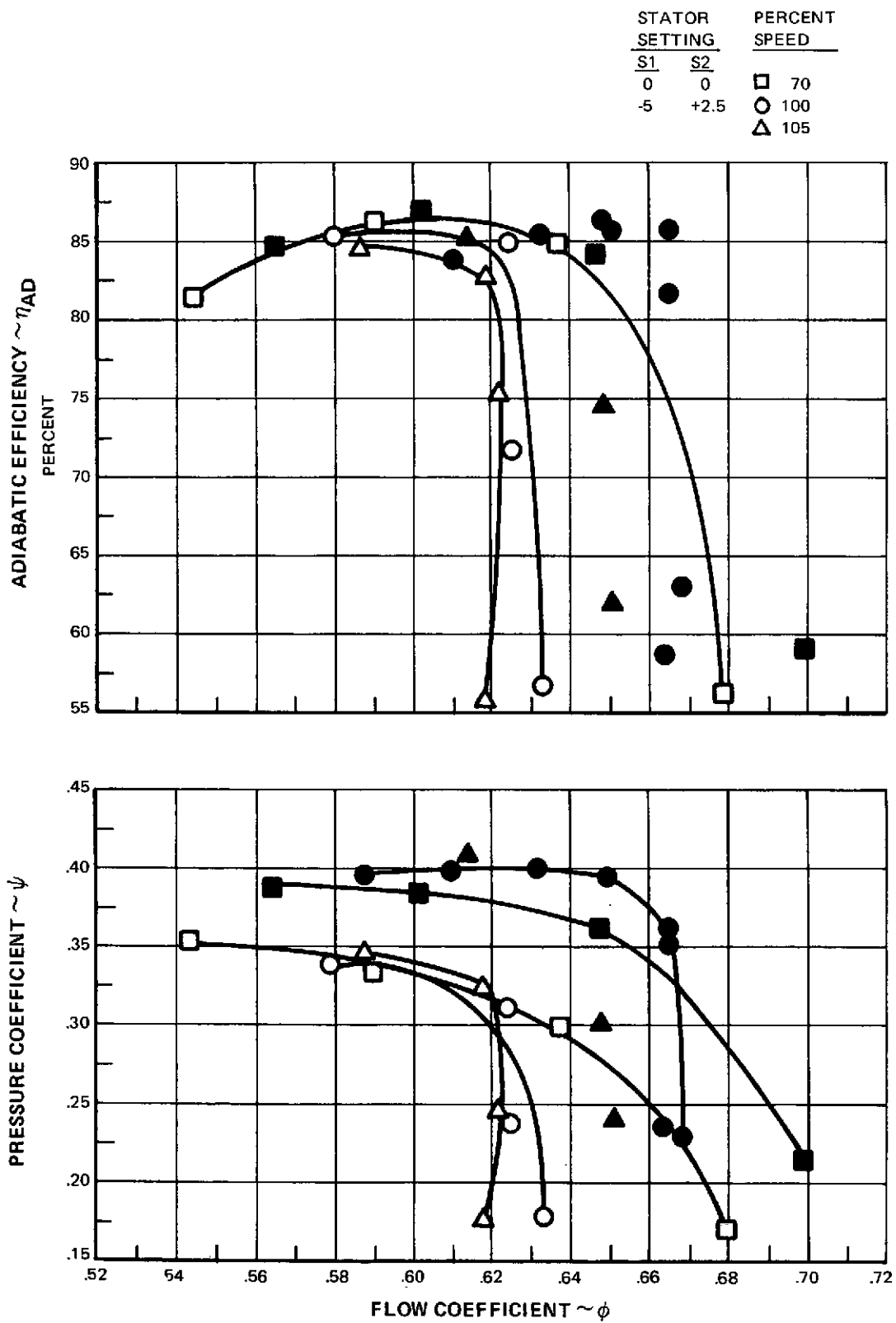


Figure 58 Pressure Coefficient and Adiabatic Efficiency Versus Flow Coefficient for the Second-Stage (0, 0) and (-5, +2.5) Stator Configurations

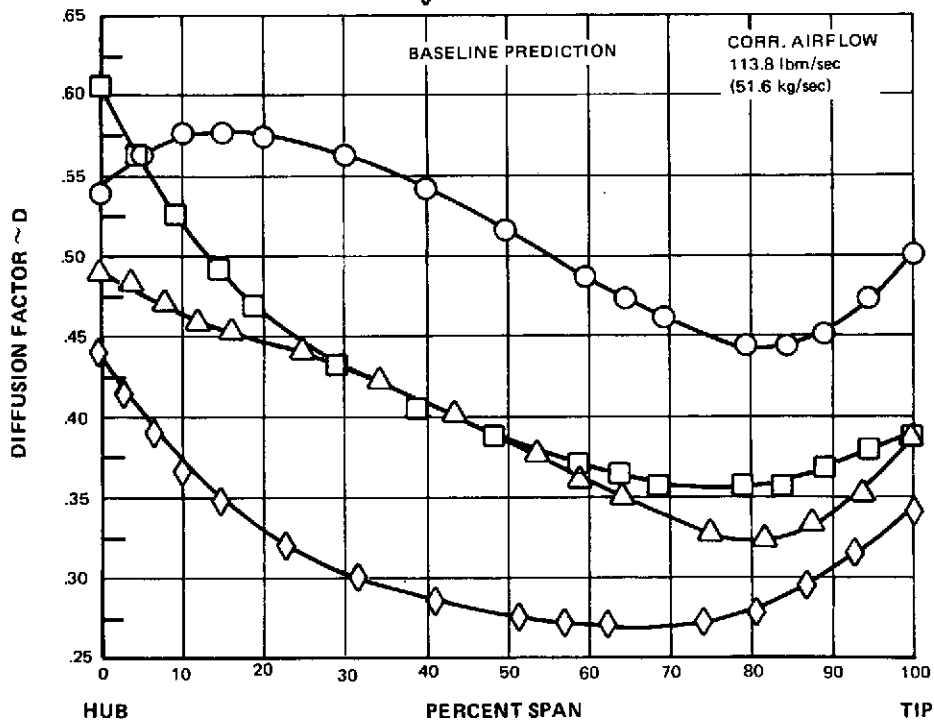
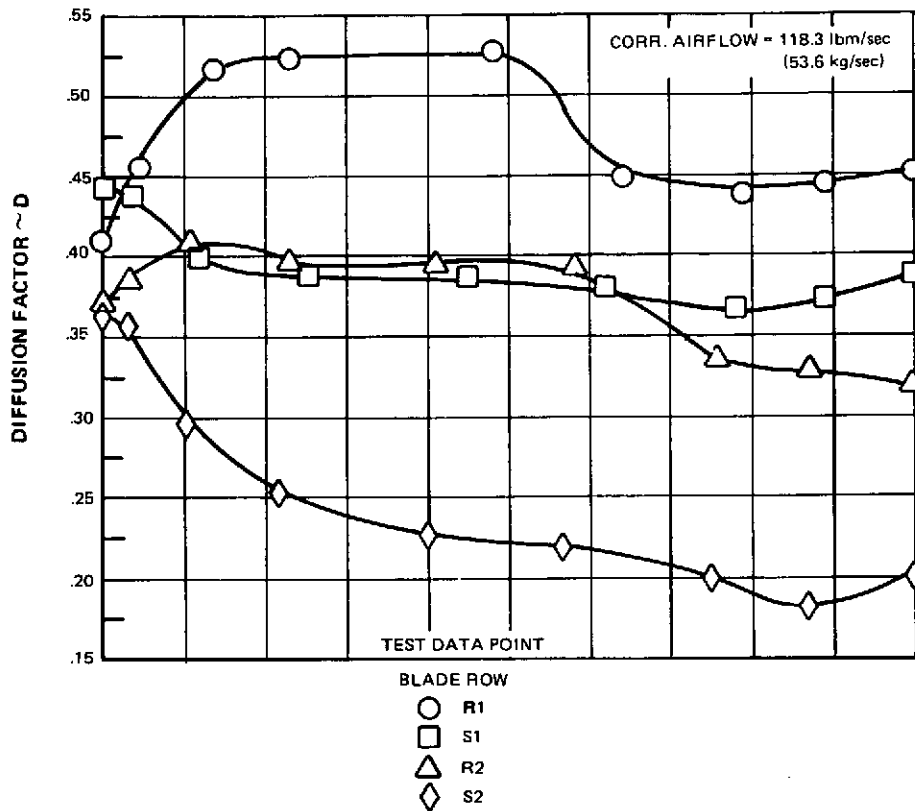


Figure 59 Diffusion Factors Versus Span for Each Blade Row at 70 Percent of Design Speed for Predicted and Test Operating Points

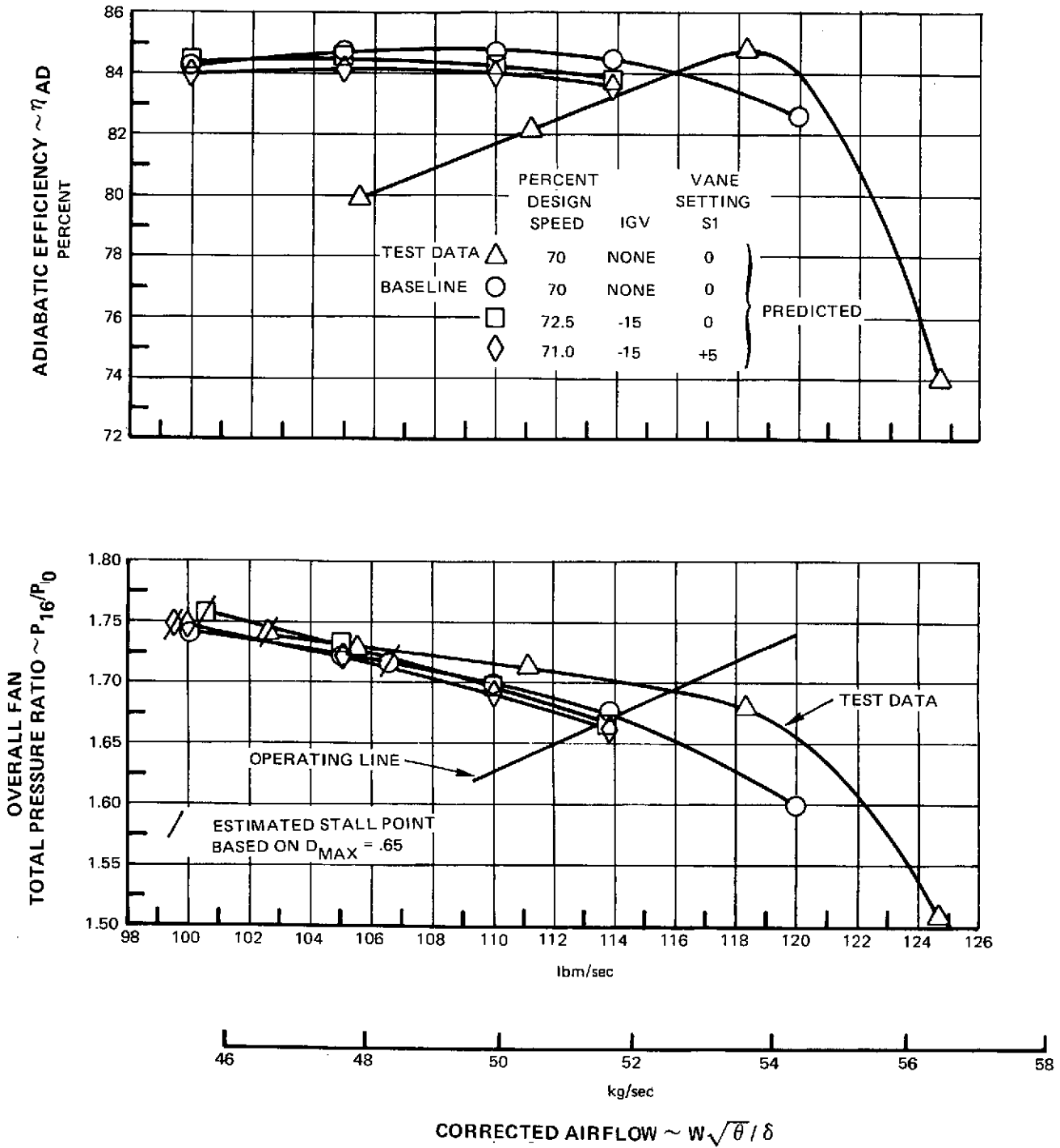


Figure 60 Estimated Overall Fan Performance at 70 Percent of Design Speed with an Inlet-Guide-Vane

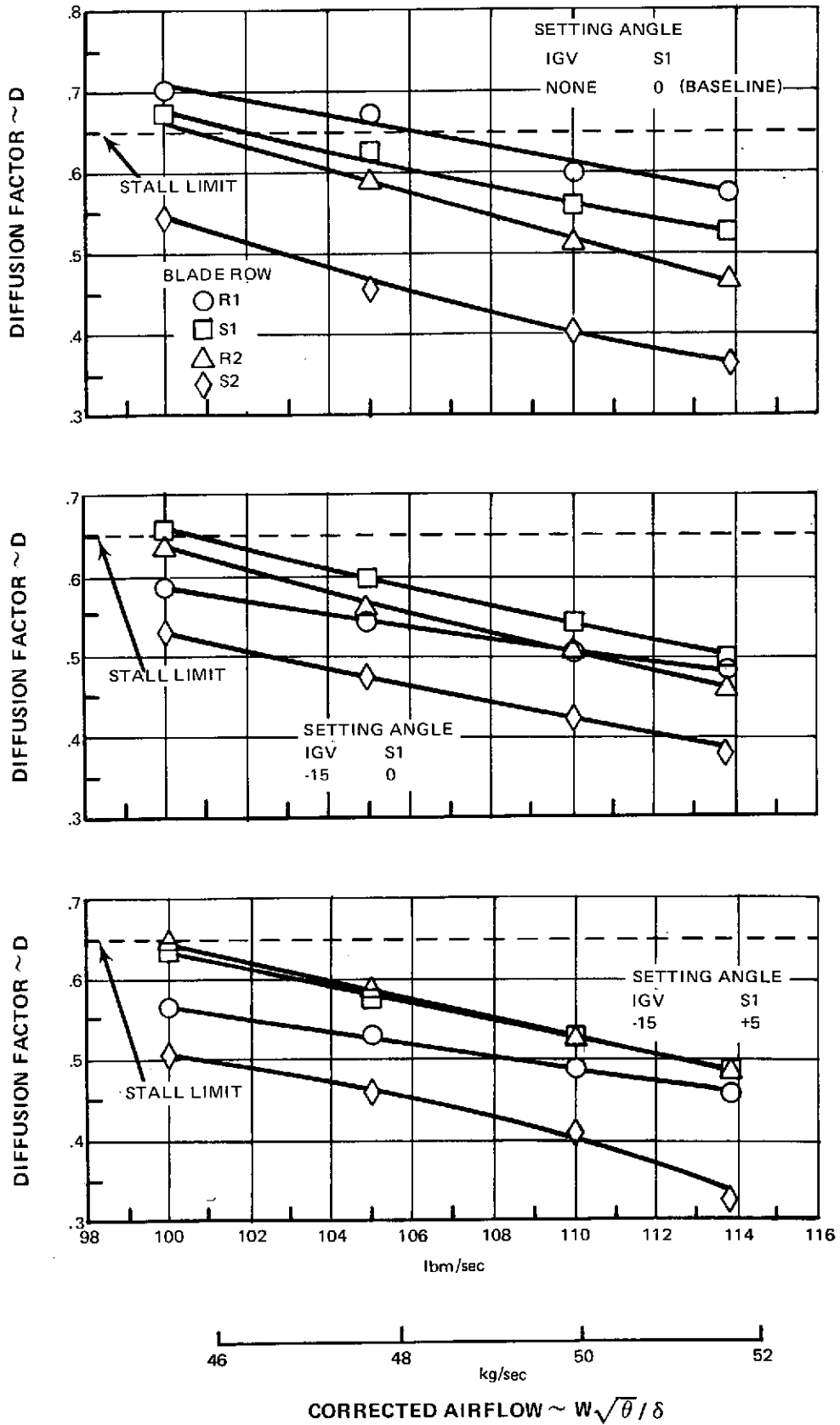


Figure 61 Maximum Diffusion Factors Versus Flow for Each Blade Row at 70 Percent of Design Speed

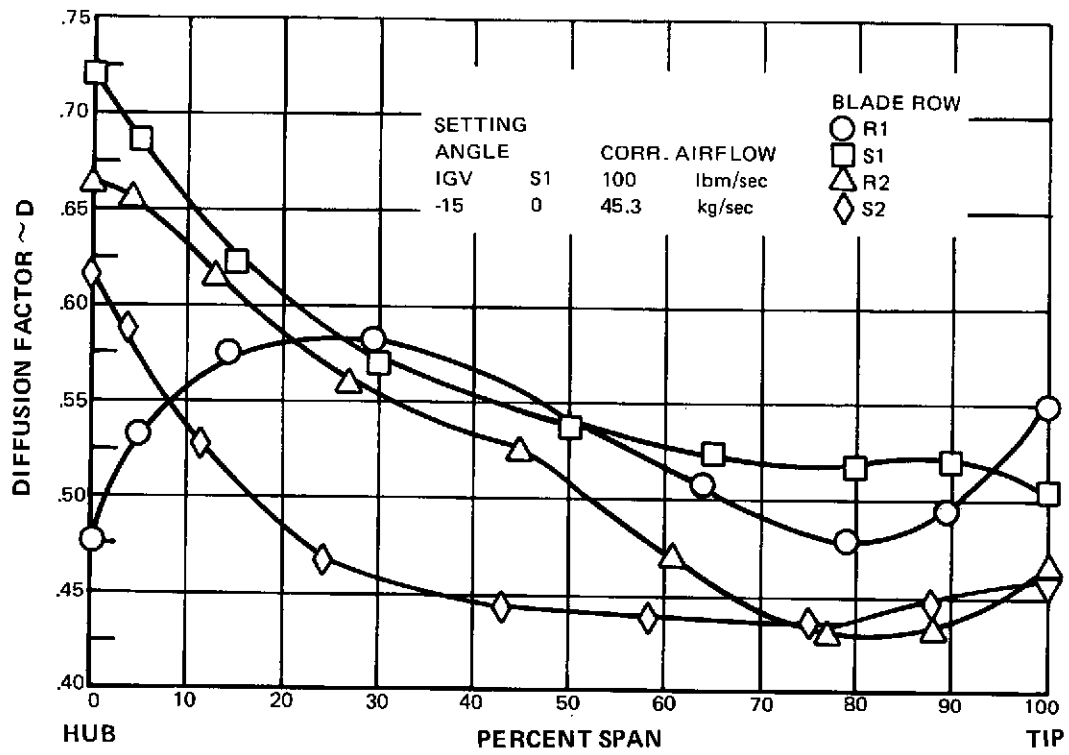


Figure 62 Diffusion Factors Versus Span for Each Blade Row for a Predicted Stall Flow at 70 Percent of Design Speed

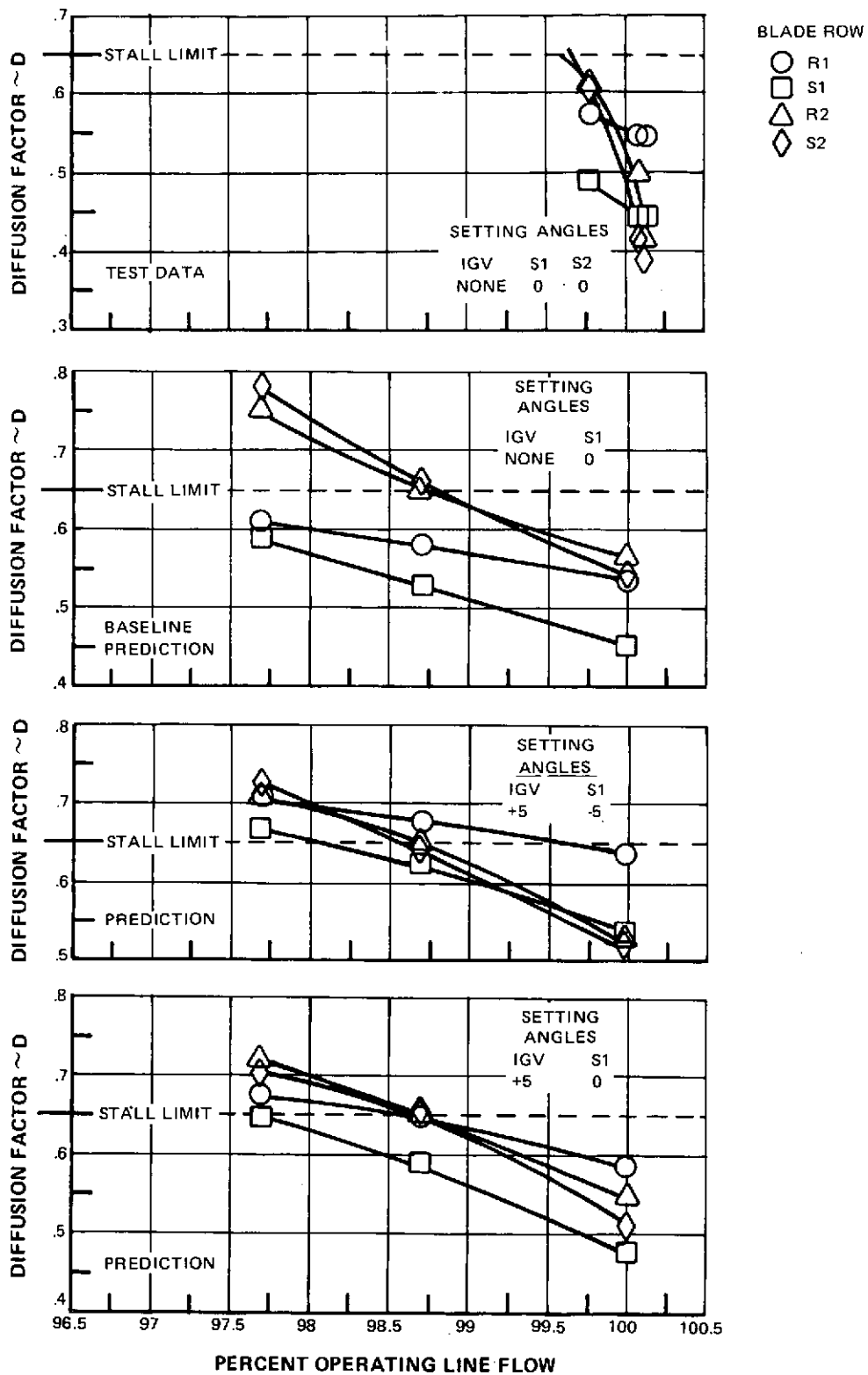


Figure 63 Maximum Diffusion Factors Versus Flow for Each Blade Row at 110 Percent of Design Speed

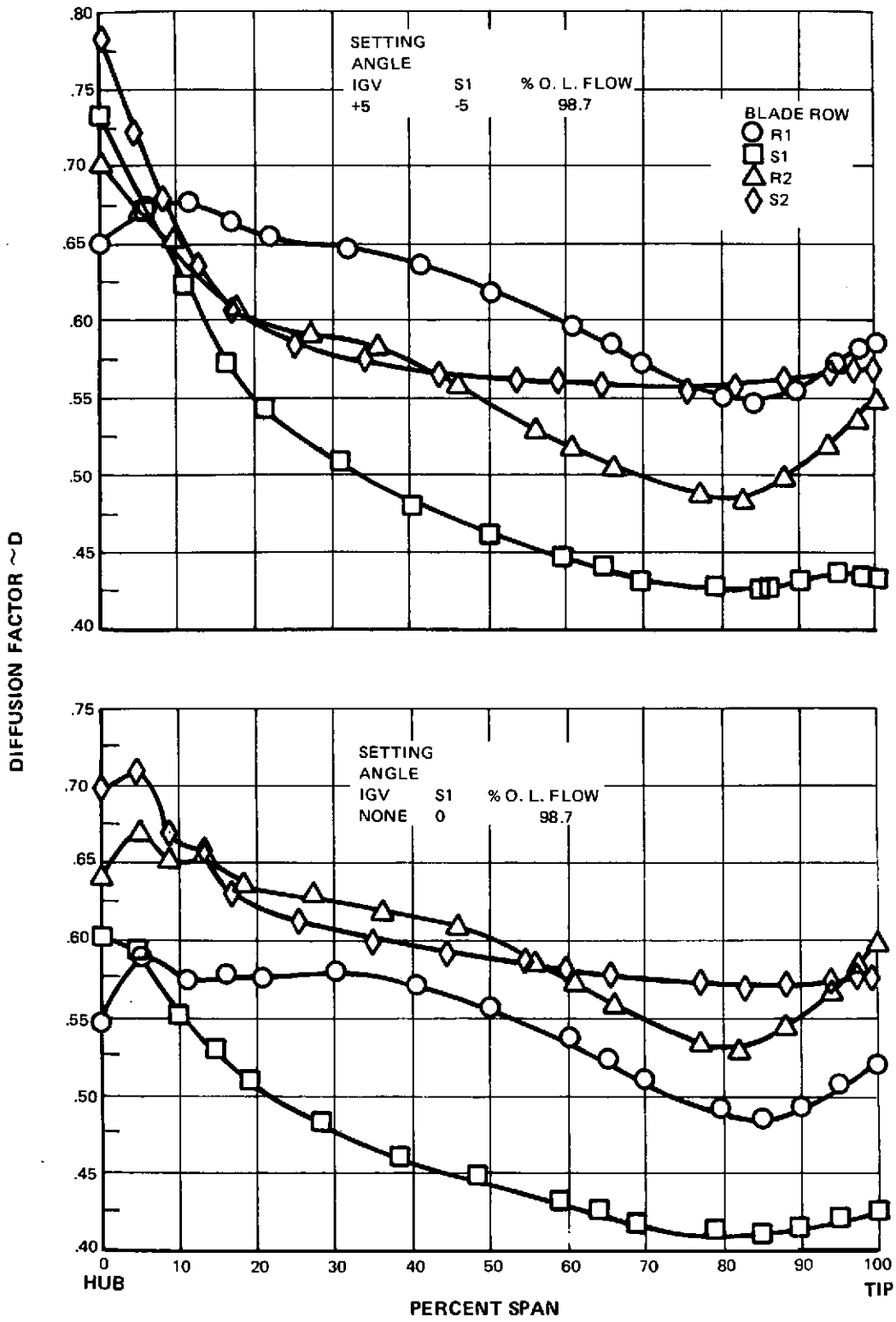


Figure 64 Diffusion Factors Versus Span for Each Blade Row at a Predicted Stall Flow at 110 Percent of Design Speed

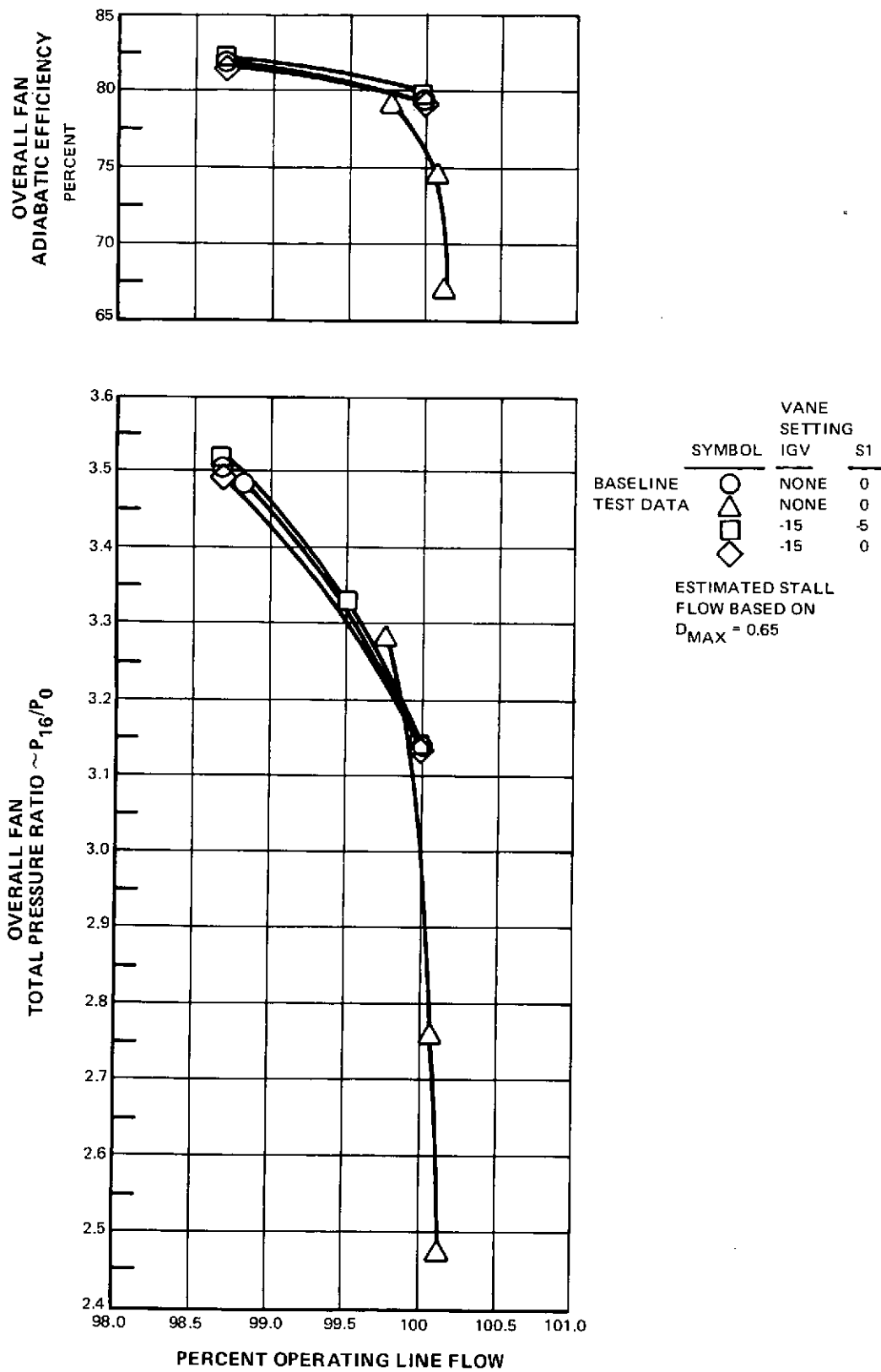


Figure 65 Estimated Overall Fan Performance at 110 Percent of Design Speed with an Inlet-Guide-Vane

APPENDIX A

SYMBOLS, PERFORMANCE PARAMETERS, AND COLUMN HEADING IDENTIFICATION

SYMBOLS

A	—	area, inches ² [meters ²]
C _p	—	ratio of specific heats, Btu/lbm-°R [joule/kg-°k]
D	—	diffusion factor
g _c	—	conversion factor, 32.17 lbm ft/lbf sec ²
i _m	—	incidence angle, angle between inlet air direction and line tangent to blade mean camber line at leading edge, degrees (labelled INCM, Table XI)
i _{ss}	—	incidence angle, angle between inlet air direction and line tangent to blade suction surface at leading edge, degrees (labelled INCS, Table XI)
J	—	conversion factor, 778 ft-lbf/Btu [1.00m-kj/joule]
N	—	rotor speed, rpm
P	—	total pressure, lbf/ft ² or n/m ²
p	—	static pressure, lbf/ft ² or n/m ²
R	—	gas constant for air
r	—	radius measured from rig centerline - inches [meters]
SL	—	streamline number
T	—	total temperature, °R [°K]
t	—	static temperature, °R or °K
	—	blade maximum thickness, inches [meters]
U	—	rotor speed, ft/sec [meters/sec]
V	—	air velocity, ft/sec [meters/sec]

APPENDIX A

V_m	– meridional velocity $(V_r^2 + V_z^2)^{1/2}$, ft/sec [m/sec] (labelled VM, Table XI)
W	– mass flow rate, lbm/sec [kg/sec]
z	– axial distance - inches [meters]
β	– absolute air angle, $\cot^{-1} (V_m/V\theta)$, degrees (labelled B, Table XI)
β'	– relative air angle, $\cot^{-1} (V_m/V\theta')$, degrees (labelled B', Table XI)
$\Delta\beta$	– air turning angle, degrees [radians]
γ	– ratio of specific heats for air
δ	– ratio of total pressure to standard pressure of 2116 lbf/ft ² [1.0125×10^5 N/M ²]
δ°	– deviation angle, exit air angle minus tangent to blade mean camber line at trailing edge - degrees [radians] (labelled DEV, Table XI)
ϵ	– angle between tangent to streamline projected on meridional plane and axial direction - degrees [radians] (labelled EPSI, Table XI)
η	– efficiency (percent)
θ	– ratio of total temperature to standard temperature of 518.7° R [288.16° K]
ρ	– mass density - lbm/ft ³ [kg/meters ³]
σ	– solidity, ratio of aerodynamic chord to gap between blades
ϕ	– flow coefficient
ψ	– pressure coefficient
ω	– angular velocity of rotor, radians/sec
$\bar{\omega}$	– total press loss coefficient

Superscripts

'	– relative to rotor
*	– blade metal angle

Subscripts

ad	—	adiabatic
act.	—	actual angle E
des.	—	design
f	—	front
Ef	—	refers to front camber definitions which include epse angle E
in	—	inlet
m	—	meridional direction (in δ - γ plane)
n	—	selected operating point
p	—	polytropic or profile
r	—	radial direction
	—	ratio (e.g. P_r = total pressure ratio)
ss	—	suction surface
sh	—	shock
t	—	transition
z	—	axial component
θ	—	tangential component
o	—	plenum camber
6	—	instrument plane upstream of rotor 1
7	—	station at rotor 1 leading edge
8	—	station at rotor 1 trailing edge
9	—	station at stator 1 leading edge
10	—	station at stator 1 trailing edge
11	—	instrument plane downstream stator 1

- 12 — station at rotor 2 leading edge
- 13 — station at rotor 2 trailing edge
- 14 — station at stator 2 leading edge
- 15 — station at stator 2 trailing edge
- 16 — instrument plane downstream stator 2

PERFORMANCE PARAMETERS

a) Relative total temperature

$$T'_7 = t_7 \left[1 + \frac{\gamma - 1}{2} (M'_7)^2 \right] \quad \text{(rotor 1) IN}$$

$$T'_8 = T'_7 + \left[\frac{(\omega_{r8})^2 - (\omega_{r7})^2}{\frac{2\gamma}{\gamma - 1} R_{gC}} \right] \quad \text{(rotor 1) OUT}$$

b) Incidence angle based on mean camber line

$$i_m = \beta'_7 - \beta'^*_7 \quad \text{(rotor 1)}$$

$$i_m = \beta_9 - \beta^*_9 \quad \text{(stator 1)}$$

Incidence angle based on suction surface metal angle

$$i_{ss} = \beta'_7 - \beta^*_{ss7} \quad \text{(rotor 1)}$$

$$i_{ss} = \beta_9 - \beta^*_{ss9} \quad \text{(stator 1)}$$

c) Deviation angle

$$\delta^\circ = \beta'_8 - \beta'^*_8 \quad \text{(rotor 1)}$$

$$\delta^\circ = \beta_{10} - \beta^*_{10} \quad \text{(stator 1)}$$

d) Diffusion factor

$$D = 1 - \frac{V'_8}{V'_7} + \frac{r_8 V_{\theta 8} - r_7 V_{\theta 7}}{(r_8 + r_7) \sigma V'_7} \quad (\text{rotor 1})$$

$$D = 1 - \frac{V_{10}}{V_9} + \frac{r_9 V_{\theta 9} - r_{10} V_{\theta 10}}{(r_9 + r_{10}) \sigma V_9} \quad (\text{stator 1})$$

e) Loss coefficient

$$\bar{\omega} = \frac{P'_7 \left[\frac{T'_8}{T'_7} \right]^{\frac{\gamma}{\gamma-1}} - P'_8}{P'_7 - p_7} \quad (\text{rotor 1})$$

$$\bar{\omega} = \frac{P_9 - P_{10}}{P_9 - p_9} \quad (\text{stator 1})$$

f) Loss parameter

$$\frac{\bar{\omega} \cos \beta'_8}{2\sigma} \quad (\text{rotor 1})$$

$$\frac{\bar{\omega} \cos \beta_{10}}{2\sigma} \quad (\text{stator 1})$$

g) Polytropic efficiency

$$1) \eta_p = \frac{\frac{\gamma - 1}{\gamma} \ln \left[\frac{P_8}{P_7} \right]}{\ln \left[\frac{T_8}{T_0} \right]} \quad \text{(rotor 1)}$$

$$2) \eta_p = \frac{\frac{\gamma - 1}{\gamma} \ln \left[\frac{P_{10}}{P_9} \right]}{\ln \left[\frac{t_{10}}{t_9} \right]} \quad \text{(stator 1)}$$

h) Adiabatic efficiency

$$\eta_{ad} = \frac{\left[\frac{P_8}{P_7} \right]^{\frac{\gamma - 1}{\gamma}} - 1}{\left[\frac{T_{10}}{T_0} \right] - 1} \quad \text{(rotor 1)}$$

$$\eta_{ad} = \frac{\left[\frac{P_{10}}{P_6} \right]^{\frac{\gamma - 1}{\gamma}} - 1}{\left[\frac{T_{10}}{T_0} \right] - 1} \quad \text{(stage 1)}$$

i) Stall margin

$$SM = \left[\left(\frac{P_{16}/P_6}{W\sqrt{\theta_6}/\delta_6} \right)_{\text{Stall}} \left(\frac{W\sqrt{\theta_6}/\delta_6}{P_{16}/P_6} \right)_{\text{Reference Point or Operating Point}} - 1 \right] 100$$

j) Flow coefficient $\phi = \frac{V_z}{U_{\text{mean flow}}}$

k) Pressure coefficient $\psi = \frac{\Delta H_{id}}{U_m^2}$
 $= \frac{\eta_{ad} \Delta T_{\text{actual}} c_p J g_c}{U_{\text{mean flow}}^2}$

TABLE XI – IDENTIFICATION OF OVERALL PERFORMANCE AND BLADE-ELEMENT DATA TABLE COLUMN HEADINGS

ROTOR 1

SL	EP81-1 DEGREE	EP81-2 DEGREE	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	V8-1 FT/SEC	V8-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	M-1	M-2	U-1 FT/SEC	U-2 FT/SEC	M'-1	M'-2	V'-1 FT/SEC	V'-2 FT/SEC
*	ϵ_7	ϵ_8	V_7	V_8	V_{m7}	V_{m8}	$V_{\theta 7}$	$V_{\theta 8}$	β_7	β_8	M_7	M_8	U_7	U_8	M'_7	M'_8	V'_7	V'_8
SL	INCS DEGREE	INCM DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B TOTAL	LOSS-P TOTAL	PO2/ PO1	%EFF-P TOT	%EFF-A TOT	B'-1 DEGREE	B'-2 DEGREE	V8'-1 FT/SEC	V8'-2 FT/SEC	PO/PO INLET	
*	i_{m7}	i_{m7}	δ_8°	$\Delta\beta$	$\rho_7 V_{m7}$	$\rho_8 V_{m8}$	D	$\bar{\omega}$	$\frac{\bar{\omega} \cos \beta'_8}{20}$	$\frac{P_8}{P_7}$	η_p	η_{ad}	β'_7	β'_8	$V'_{\theta 7}$	$V'_{\theta 8}$	$\frac{P_8}{P_0}$	
			TO/TO INLET	PO/PO INLET	EFF-AD INLET %	EFF-P INLET %	WC1/A1 LBM/SEC SQFT		TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %						
			$\frac{T_8}{T_0}$	$\frac{P_8}{P_0}$	η_{ad}	η_p	$\frac{W\sqrt{\beta_7}}{\delta_7 A_7}$		$\frac{T_8}{T_7}$	$\frac{P_8}{P_7}$	$\eta_{ad,8}$	η_{p8}						

STATOR 1

SL	EP81-1 DEGREE	EP81-2 DEGREE	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	V8-1 FT/SEC	V8-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	M-1	M-2	PO/PO INLET	TO/TO INLET	PO/PO STAGE	TO2/ TO1
*	ϵ_9	ϵ_{10}	V_9	V_{10}	V_{m9}	V_{m10}	$V_{\theta 9}$	$V_{\theta 10}$	β_9	β_{10}	M_9	M_{10}	$\frac{P_{10}}{P_0}$	$\frac{T_{10}}{T_0}$	$\frac{P_{10}}{P_7}$	$\frac{T_{10}}{T_7}$
SL	INCS DEGREE	INCM DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B TOTAL	LOSS-P TOTAL	PO2/ PO1	%EFF-P STATC-ST	%EFF-A TOT-INLET	%EFF-P TOT-INLET	%EFF-A TOT-STG	%EFF-P TOT-STG	
*	i_{m9}	i_{m9}	δ_{10}°	$\Delta\beta$	$\rho_9 V_{m9}$	$\rho_{10} V_{m10}$	D	$\bar{\omega}$	$\frac{\bar{\omega} \cos \beta_{10}}{20}$	$\frac{P_{10}}{P_0}$	η_{p-st}	η_{ad}	η_p	η_{ad-st}	η_{p-st}	
		NCORR INLET RPM	WCORR INLET LBM/SEC	TO/TO INLET	PO/PO INLET	EFF-AD INLET %	EFF-P INLET %		TO2/TO1	PO2/PO1	EFF-AD STAGE %					
		$\frac{N}{\sqrt{\beta_7}}$	$\frac{W\sqrt{\beta_7}}{\delta_7}$	$\frac{T_{10}}{T_0}$	$\frac{P_{10}}{P_0}$	η_{ad}	η_p		$\frac{T_{10}}{T_7}$	$\frac{P_{10}}{P_9}$	η_{ad-st}					

ROTOR 2

SL	EPSI-1 DEGREE	EPSI-2 DEGREE	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	Vθ-1 FT/SEC	Vθ-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	M-1	M-2	U-1 FT/SEC	U-2 FT/SEC	M'-1	M'-2	V'-1 FT/SEC	V'-2 FT/SEC
•	ϵ_{12}	ϵ_{13}	V_{12}	V_{13}	V_{m12}	V_{m13}	$V_{\theta 12}$	$V_{\theta 13}$	β_{12}	β_{13}	M_{12}	M_{13}	U_{12}	U_{13}	M'_{12}	M'_{13}	V'_{12}	V'_{13}
SL	INCS DEGREE	INCM DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-θ TOTAL	LOSS-P TOTAL	PO2/ PO1	%EFF-P TOT	%EFF-A TOT	B'-1 DEGREE	B'-2 DEGREE	Vθ'-1 FT/SEC	Vθ'-2 FT/SEC	PO/PO INLET	
•	i_{m12}	i_{m12}	δ_{13}^o	$\Delta\beta$	$\rho_{12} V_{m12}$	$\rho_{13} V_{m13}$	D	$\bar{\omega}$	$\frac{\bar{\omega} \cos \beta'_{13}}{20}$	$\frac{P_{13}}{P_{12}}$	η_p	η_{ad}	β'_{12}	β'_{13}	$V'_{\theta 12}$	$V'_{\theta 13}$	$\frac{P_{13}}{P_0}$	
			TO/TO INLET	PO/PO INLET	EFF-AD INLET %	EFF-P INLET %	WC1/A1 LBM/SEC SQFT		TO2/TO1	PO2/PO1	EFF-AD ROTOR %	EFF-P ROTOR %						
			$\frac{T_{13}}{T_0}$	$\frac{P_{13}}{P_0}$	η_{ad}	η_p	$\frac{W\sqrt{\theta}_{12}}{\delta_{12} A_{12}}$		$\frac{T_{13}}{T_{12}}$	$\frac{P_{13}}{P_{12}}$	η_{ad13}	η_{p13}						

STATOR 2

SL	EPSI-1 DEGREE	EPSI-2 DEGREE	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	Vθ-1 FT/SEC	Vθ-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	M-1	M-2	PO/PO INLET	TO/TO INLET	PO/PO STAGE	TO2/ TO1
•	ϵ_{14}	ϵ_{15}	V_{14}	V_{15}	V_{m14}	V_{m15}	$V_{\theta 14}$	$V_{\theta 15}$	β_{14}	β_{15}	M_{14}	M_{15}	$\frac{P_{15}}{P_0}$	$\frac{T_{15}}{T_0}$	$\frac{P_{15}}{P_{12}}$	$\frac{T_{15}}{T_{12}}$
SL	INCS DEGREE	INCM DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-θ TOTAL	LOSS-P TOTAL	PO2/ PO1	%EFF-P STATC-ST	%EFF-A TOT-INLET	%EFF-P TOT-INLET	%EFF-A TOT-STG	%EFF-P TOT-STG	
•	i_{m14}	i_{m14}	δ_{15}	$\Delta\beta$	$\rho_{14} V_{m14}$	$\rho_{15} V_{m15}$	D	$\bar{\omega}$	$\frac{\bar{\omega} \cos \beta_{15}}{20}$	$\frac{P_{15}}{P_{14}}$	η_{p-st}	η_{ad}	η_p	η_{ad-st}	η_{p-st}	
		NCORR INLET RPM	WCORR INLET LBM/SEC	TO/TO INLET	PO/PO INLET	EFF-AD INLET %	EFF-P INLET %		TO2/TO1	PO2/PO1	EFF-AD STAGE %					
		$\frac{N}{\sqrt{\theta}_{12}}$	$\frac{W\sqrt{\theta}_{12}}{\delta_{12}}$	$\frac{T_{16}}{T_0}$	$\frac{P_{16}}{P_0}$	η_{ad}	η_p		$\frac{T_{15}}{T_{12}}$	$\frac{P_{15}}{P_{14}}$	η_{ad-st}					

* SEE TABLE XII
SUBSCRIPTS REFER TO CALCULATION STATIONS

APPENDIX B

DESIGN VALUES OF OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

This appendix provides the design values of overall performance and blade-element data for rotor 1, stator 1, rotor 2, and stator 2. Spans and diameters for design and test blade-element data are given in Table XII, and design values of overall performance and blade-element data are given in Table XIII. The column headings for Table XIII are identified in Table XI of Appendix A.

TABLE XII – SPANS AND DIAMETERS FOR DESIGN AND TEST BLADE-ELEMENT-DATA

SL	Rotor 1 Inlet		Rotor 1 Exit		Stator 1 Inlet		Stator 1 Exit	
	Diameter	Span	Diameter	Span	Diameter	Span	Diameter	Span
	(inches)	(%)	(inches)	(%)	(inches)	(%)	(inches)	(%)
1	13.47	5.8	15.59	5.0	15.93	4.9	17.38	4.3
2	14.52	11.4	16.35	10.0	16.64	9.9	17.93	8.9
3	15.56	17.0	17.10	15.0	17.36	14.8	18.49	13.6
4	18.52	32.9	19.37	30.0	19.53	29.8	20.26	28.1
5	22.22	52.8	22.38	50.0	22.42	49.8	22.69	48.2
6	24.00	62.4	23.89	60.0	23.87	59.9	23.93	58.4
7	24.88	67.1	24.65	65.0	24.60	64.9	24.55	63.6
8	25.76	71.8	25.40	70.0	25.33	69.9	25.18	68.8
9	28.38	85.9	27.67	85.0	27.50	85.0	27.07	84.4
10	29.26	90.6	28.42	90.0	28.23	90.0	27.70	89.6
11	30.13	95.3	29.18	95.0	28.95	95.0	28.34	94.8

SL	Rotor 2 Inlet		Rotor 2 Exit		Stator 2 Inlet		Stator 2 Exit	
	Diameter	Span	Diameter	Span	Diameter	Span	Diameter	Span
	(inches)	(%)	(inches)	(%)	(inches)	(%)	(inches)	(%)
1	17.87	4.3	18.74	3.8	18.93	3.8	19.18	3.2
2	18.38	8.8	19.14	7.8	19.30	7.8	19.49	6.8
3	18.90	13.5	19.54	12.0	19.69	11.9	19.82	10.6
4	20.51	28.0	20.84	25.3	20.94	25.3	20.91	23.2
5	22.74	48.0	22.73	44.6	22.75	44.8	22.58	42.2
6	23.88	58.1	23.73	54.9	23.72	55.1	23.49	52.8
7	24.45	63.3	24.25	60.2	24.22	60.5	23.97	58.2
8	25.03	68.4	24.78	65.6	24.72	65.9	24.46	63.9
9	26.78	84.2	26.42	82.4	26.29	82.7	26.00	81.7
10	27.37	89.4	26.98	88.1	26.82	88.4	26.53	87.8
11	27.96	94.7	27.55	94.0	27.36	94.2	27.07	93.9

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APPENDIX C

OVERALL PERFORMANCE AND BLADE-ELEMENT DATA AT DESIGN SPEED

This appendix provides test overall performance and blade-element data at design speed for rotor 1, stator 1, rotor 2, and stator 2. The data is presented for seven combinations of stator settings at various flows and pressure ratios. An overall-performance and stall data summary is given in Table XIV, and the complete overall performance and blade-element data is given in Table XV through Table XXI. The column headings for Tables XV through XXI are identified in Table XI of Appendix A.

TABLE XIV – OVERALL PERFORMANCE AND STALL DATA SUMMARY FOR DESIGN SPEED

PERFORMANCE REF. TABLE ⁽¹⁾	STATOR SETTING ⁽²⁾		CORRECTED ⁽³⁾				
	S1	S2	FLOW lbm/sec	P_{11}/P_0	$\eta_{ad, 11}$ %	P_{16}/P_0	$\eta_{ad, 16}$ %
	XV(a)	0°	0°	185.6	1.684	88.09	2.306
XV(b)	0°	0°	185.3	1.722	85.94	2.868	85.16
XV(c)	0°	0°	185.2	1.712	87.07	2.860	85.30
XV(d)	0°	0°	184.2	1.743	87.28	2.926	85.37
XV(e)	0°	0°	182.9	1.779	88.07	2.980	84.95
XV(f)	0°	0°	181.0	1.809	89.22	3.016	84.72
XVI(a)	-5°	+2.5°	183.2	1.739	86.61	2.212	73.24
XVI(b)	-5°	+2.5°	183.2	1.750	88.68	2.398	80.63
XVI(c)	-5°	+2.5°	183.1	1.755	87.23	2.644	85.19
XVI(d)	-5°	+2.5°	177.9	1.817	86.11	2.830	84.76
XVII(a)	+2.5°	0°	186.1	1.691	87.17	2.295	71.33
XVII(b)	+2.5°	0°	186.0	1.713	87.79	2.851	84.65
XVII(c)	+2.5°	0°	184.4	1.772	88.43	2.985	84.26
XVII(d)	+2.5°	0°	183.0	1.804	88.66	3.021	83.99
XVIII(a)	0°	+5°	185.9	1.698	90.18	2.307	75.91
XVIII(b)	0°	+5°	185.5	1.712	89.61	2.784	84.65
XVIII(c)	0°	+5°	183.5	1.786	91.05	2.941	84.28
XIX(a)	0°	-5°	185.5	1.714	90.73	2.346	69.98
XIX(b)	0°	-5°	184.3	1.746	89.86	2.817	83.98
XIX(c)	0°	-5°	180.8	1.811	89.15	2.983	84.45
XIX(d)	0°	-5°	177.9	1.824	90.33	2.992	83.46
XX(a)	0°	-10°	178.2	1.817	87.37	2.774	79.15
XX(b)	0°	-10°	172.6	1.837	85.43	2.934	81.26
XXI(a)	+2.5°	-5°	186.2	1.672	86.06	2.377	69.08
XXI(b)	+2.5°	-5°	184.5	1.757	88.67	2.932	83.32
XXI(c)	+2.5°	-5°	181.5	1.772	85.94	3.001	82.95
XXI(d)	+2.5°	-5°	178.3	1.827	88.36	3.027	82.27

STALL POINT DATA

STATOR SETTING ⁽²⁾	STATOR SETTING ⁽²⁾	CORRECTED ⁽³⁾		
		FLOW lbm/sec	P_{16}/P_0	STALL MARGIN %
0°	0°	178.8	3.035	12.0
-5°	+2.5°	175.1	2.880	8.5
2.5°	0°	179.0	3.050	12.5
0°	+5°	180.1	2.936	7.5
0°	-5°	174.3	3.005	14.0
0°	-10°	167.8	2.960	16.2
+2.5°	-5°	176.9	3.024	13.1

- NOTES: (1) Refers to remaining Appendix C tables.
 (2) Stator Setting = $\beta^*_{des} - \beta^*_{act}$
 (3) Corrected Flow = $W \sqrt{\theta/\delta}$

APPENDIX C

TABLE XV (b) — OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

DESIGN SPEED
STATOR 1 (beta*_des - beta*_act.) = 0 degrees
STATOR 2 (beta*_des - beta*_act.) = 0 degrees
(Data from reference 3)

U. S. CUSTOMARY UNITS

ROTOR 1

Table with 18 columns: Inlet, Inlet, Dev, Turn, RMCVM-1, RMCVM-2, D-FAC, CMEGA-B, LUSS-P, P02, EFF-P, EFF-A, B-1, B-2, V-1, V-2, PC/PC, INLET. Rows 1-11.

Table with 18 columns: Inlet, Inlet, Dev, Turn, RMCVM-1, RMCVM-2, D-FAC, CMEGA-B, LUSS-P, P02, EFF-P, EFF-A, B-1, B-2, V-1, V-2, PC/PC, INLET. Rows 1-11.

STATOR 1

Table with 18 columns: Inlet, Inlet, Dev, Turn, RMCVM-1, RMCVM-2, D-FAC, CMEGA-B, LUSS-P, P02, EFF-P, EFF-A, B-1, B-2, V-1, V-2, PC/PC, INLET. Rows 1-11.

Table with 18 columns: Inlet, Inlet, Dev, Turn, RMCVM-1, RMCVM-2, D-FAC, CMEGA-B, LUSS-P, P02, EFF-P, EFF-A, B-1, B-2, V-1, V-2, PC/PC, INLET. Rows 1-11.

ROTOR 2

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, SPEED CODE, POINT NO, V-1, V-2. Contains 11 rows of data.

Table with columns: SL, INCS, INCM, DEV, TURN, RHQVM-1, RHQVM-2, C-FAC, OMEGA-B, LOSS-P, PQ2, %EFF-P, %EFF-A, B*-1, B*-2, V0*-1, V0*-2, PO/PO. Contains 11 rows of data.

Summary table with columns: TC/TD INLET, PD/PO INLET, EFF-AD INLET, EFF-P INLET, WCL/AL LB/M/SEC, TQ2/TQ1, PQ2/PQ1, %EFF-AD ROTOR, %EFF-P ROTOR. Values: 1.4088, 2.9207, 87.29, 89.03, 42.19, 1.1832, 1.7056, 85.33, 90.10.

STATOR 2

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, SPEED CODE, POINT NO. Contains 11 rows of data.

Table with columns: SL, INCS, INCM, DEV, TURN, RHQVM-1, RHQVM-2, C-FAC, OMEGA-B, LOSS-P, PQ2, %EFF-P, %EFF-A, %EFF-P, %EFF-A, %EFF-P. Contains 11 rows of data.

Summary table with columns: NCORR INLET, WCORR INLET, TO/TO INLET, PG/PO INLET, EFF-AD INLET, EFF-P INLET, TQ2/TQ1, PQ2/PQ1, %EFF-AD STAGE, %EFF-P STAGE. Values: 1.0708, 1.6516, 1.4088, 2.8595, 85.30, 87.27, 1.1832, 0.9750, 85.52.

APPENDIX C

TABLE XV (d) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

DESIGN SPEED
STATOR 1 (beta*des - beta*act) = 0 deg
STATOR 2 (beta*des - beta*act) = 0 deg
(Data from reference 3)

U. S. CUSTOMARY UNITS

ROTOR 1

Table with columns: SL, EPII-1, EPII-2, V-1, V-2, VM-1, VM-2, VO-1, VO-2, B-1, B-2, M-1, M-2, RUN NO, SPEED CODE, PC/PC, INLET, etc. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, U-FAC, CMEGA-B, LOSS-P, PO2, EFF-P, EFF-A, B-1, B-2, VB-1, VB-2, PC/PC, INLET, etc. Rows 1-11.

Summary table with columns: TO/TO INLET, PO/PO INLET, EFF-AD INLET, EFF-P INLET, WCI/A1 LBM/SEC, TO2/T01, PO2/PO1, EFF-AD ROTOR, EFF-P ROTOR. Values: 1.1970, 1.7838, 91.21, 91.88, 41.84, 1.1970, 1.7838, 91.21, 91.88.

STATOR 1

Table with columns: SL, EPII-1, EPII-2, V-1, V-2, VM-1, VM-2, VO-1, VO-2, B-1, B-2, M-1, M-2, RUN NO, SPEED CODE, PC/PC, TO/TO, PO/PO, TCT/STG, etc. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, U-FAC, CMEGA-B, LOSS-P, PO2, EFF-P, EFF-A, B-1, B-2, VB-1, VB-2, PC/PC, INLET, etc. Rows 1-11.

Summary table with columns: NCORR INLET, WCI/A1 LBM/SEC, TO/TO INLET, PO/PO INLET, EFF-AD INLET, EFF-P INLET, TO2/T01, PO2/PO1, EFF-AD STAGE, EFF-P STAGE. Values: 1.1970, 1.7838, 91.21, 91.88, 41.84, 1.1970, 1.7838, 91.21, 91.88.

APPENDIX C

TABLE XV (f) — OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

DESIGN SPEED
STATOR 1 (beta*_des - beta*_act) = 0
STATOR 2 (beta*_des - beta*_act) = 0
(Data from reference 3)

U. S. CUSTOMARY UNITS

ROTOR 1

Table with 25 columns: Row, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, S, SPEED, CODE, 10, POINT NO, 6, V1-1, V1-2. Rows 1-14.

Table with 18 columns: Row, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LCSS-P, POZ, XEFF-P, XEFF-A, B1-1, B1-2, V01-1, V01-2, PO/PU. Rows 1-14.

Summary table with 6 columns: TG/TQ, PG/PO, EFF-AD, EFF-P, WCL/WL, TQ2/TQ1. Values: 1.2067, 1.8538, 93.23, 93.78, 41.11, 1.2067.

STATOR 1

Table with 25 columns: Row, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, S, SPEED, CODE, 10, POINT NO, 6, V1-1, V1-2. Rows 1-14.

Table with 18 columns: Row, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LCSS-P, POZ, XEFF-P, XEFF-A, B1-1, B1-2, V01-1, V01-2, PO/PU. Rows 1-14.

Summary table with 6 columns: NGWR, NGCOR, TG/TQ, PG/PO, EFF-AD, EFF-P, TQ2/TQ1, POZ/PO1, EFF-AD, STAGE. Values: 1071.4, 161.00, 1.2067, 1.8090, 89.22, 90.06, 1.2067, 0.9758, 89.22.

ROTOR 2

Table with columns: RUN NO, SPEED, CUDE, POINT NO, etc. Rows contain numerical data for rotor 2.

Table with columns: INCS, INCM, DEV, TURN, RHOVM-1, etc. Rows contain numerical data for rotor 2.

Summary table with columns: TC/TD, PC/PC, EFF-AD, etc. Rows contain summary data for rotor 2.

STATOR 2

Table with columns: RUN NO, SPEED, CUDE, POINT NO, etc. Rows contain numerical data for stator 2.

Table with columns: INCS, INCM, DEV, TURN, RHOVM-1, etc. Rows contain numerical data for stator 2.

Summary table with columns: NCORR, WCORR, TC/TD, PC/PC, EFF-AD, etc. Rows contain summary data for stator 2.

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APPENDIX C

TABLE XVI (c) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

DESIGN SPEED
STATOR 1 (beta* des. - beta* act.) = -5.0
STATOR 2 (beta* des. - beta* act.) = +2.5

U. S. CUSTOMARY UNITS

ROTOR 1

Table with 20 columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO 13, SPEED CODE 10, POINT NO 13, U-1, U-2, M-1, M-2, V-1, V-2. Rows 1-11.

Table with 20 columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, P02, XEFF-P, XEFF-A, B*-1, B*-2, V0*-1, V0*-2, PO/PO. Rows 1-11.

Table with 8 columns: TO/TO, PO/PO, EFF-AD, EFF-P, WCI/A1, TO2/T01, P02/P01, EFF-AD, EFF-P. Rows 1-11.

STATOR 1

Table with 20 columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO 13, SPEED CODE 10, POINT NO 13, PO/PO, TO/TO, PO/PO, TO2/T01. Rows 1-11.

Table with 20 columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, P02, XEFF-P, XEFF-A, XEFF-P, XEFF-A, XEFF-P, XEFF-A, XEFF-P. Rows 1-11.

APPENDIX C

TABLE XVI (d) — OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

DESIGN SPEED
STATOR 1 (beta* des. - beta* act.) = -0
STATOR 2 (beta* des. - beta* act.) = +2.5

U. S. CUSTOMARY UNITS

ROTOR 1

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, 13, SPEED CODE, 10, POINT NO, 14, V*-1, V*-2. Rows 1-11.

Table with columns: SL, IMCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, P02/, XEFF-P, XEFF-A, B*-1, B*-2, V0*-1, V0*-2, PD/PO. Rows 1-11.

Summary table with columns: TO2/TO1, P02/P01, XEFF-P, XEFF-A, XEFF-P, XEFF-A. Values: 1.2158, 1.0560, 89.47, 90.33, 40.41, 1.2158, 1.0560, 89.47, 90.33.

STATOR 1

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, 13, SPEED CODE, 10, POINT NO, 14, PD/PO, TO2/TO1, P02/P01, XEFF-P, XEFF-A, XEFF-P, XEFF-A. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, P02/, XEFF-P, XEFF-A, XEFF-P, XEFF-A, XEFF-P, XEFF-A. Rows 1-11.

Summary table with columns: MCORR INLET, WCORR INLET, TO/TO, PO/PO, EFF-AD, EFF-P, TO2/TO1, P02/P01, EFF-AD, EFF-P, XEFF-P, XEFF-A. Values: 10653, 177.90, 1.2158, 1.8167, 86.11, 87.21, 1.2158, 0.9789, 86.11, 107.70.

ROTOR 2

Table with 15 columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, U-1, U-2, M*-1, M*-2, V1-1, V1-2. Rows 1-11 showing velocity and angular data.

Table with 15 columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, P02/, %EFF-P, %EFF-A, B*-1, B*-2, V0*-1, V0*-2, PO/PO. Rows 1-11 showing density and efficiency data.

Summary table with 8 columns: TO/TO, PO/PO, EFF-AD, EFF-P, W/L/A1, TO2/TO1, P02/P01, EFF-AD, EFF-P. Values: 1.4068, 2.8857, 86.59, 88.41, 38.61, 1.1571, 1.5884, 89.32, 90.00.

STATOR 2

Table with 15 columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, PO/PO, TO/TO, PD/PO, TO2/. Rows 1-11 showing velocity and efficiency data for the stator.

Table with 15 columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, O-FAC, OMEGA-B, LOSS-P, P02/, %EFF-P, %EFF-A, %EFF-P, %EFF-P. Rows 1-11 showing density and efficiency data for the stator.

Summary table with 8 columns: NCORR, WCORR, TO/TO, PD/PO, EFF-AD, EFF-P, TO2/TO1, P02/P01, EFF-AD, EFF-P. Values: 1.0653, 1.1790, 1.4068, 2.8302, 84.76, 86.79, 1.1571, 0.9808, 85.33, 265.04.

ROTOR 2

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO 17, SPEED CODE 10, POINT NO 1, U-1, U-2, M*-1, M*-2, V*-1, V*-2. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, CMEGA-B, LOSS-P, PO2, XEFF-P, XEFF-A, B*-1, B*-2, V0*-1, V0*-2, PC/PC, INLET, INLET, INLET, INLET, LBM/SEC, SOFT, TOT/TOT1, P02/P01, EFF-AD, EFF-P, ROTOR, ROTOR. Rows 1-11.

Summary table with columns: TO/T0, PO/PO, EFF-AD, EFF-P, WCI/A1, TOT/T01, P02/P01, EFF-AD, EFF-P. Values: 1.3544, 2.4667, 82.79, 84.80, 42.55, 1.1469, 1.4530, 76.28, 77.48.

STATOR 2

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO 17, SPEED CODE 10, POINT NO 1, PO/PC, TOT-INLET, INLET, INLET, INLET, INLET, INLET, TOT-INLET, TOT-INLET, TOT-INLET, TOT-INLET, TOT-INLET, TOT-INLET, TOT-INLET, TOT-INLET. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, CMEGA-B, LOSS-P, PO2, XEFF-P, XEFF-A, B*-1, B*-2, V0*-1, V0*-2, PC/PC, INLET, INLET, INLET, INLET, LBM/SEC, SOFT, TOT/TOT1, P02/P01, EFF-AD, EFF-P, ROTOR, ROTOR. Rows 1-11.

Summary table with columns: NLCORR, W CORR, TO/T0, PO/PC, EFF-AD, EFF-P, TOT/TOT1, P02/P01, EFF-AD, EFF-P. Values: 10726, 185.90, 1.3544, 2.3070, 75.91, 78.52, 1.1469, 0.9353, 62.02, 1374.69.

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ROTOR 2

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, VO-1, VO-2, B-1, B-2, M-1, M-2, RUN NO 17, SPEED CODE 10, POINT NO 4. Contains 11 rows of data.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, MEGA-8, LOSS-P, PD2, %EFF-P, %EFF-A, B*-1, B*-2, VB*-1, VB*-2, PC/PE. Contains 11 rows of data.

Summary table with columns: TO/T0, PD/PO, EFF-AD, EFF-P, WCI/A1, LOSS-P, PD2/P01, %EFF-A, %EFF-P. Contains 1 row of data.

STATOR 2

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, VO-1, VO-2, B-1, B-2, M-1, M-2, RUN NO 17, SPEED CODE 10, POINT NO 4. Contains 11 rows of data.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, MEGA-8, LOSS-P, PD2, %EFF-P, %EFF-A, %EFF-P, %EFF-A, %EFF-P. Contains 11 rows of data.

Summary table with columns: NGORP, W CORR, TO/T0, PD/PO, EFF-AD, EFF-P, LOSS-P, PD2/P01, %EFF-A, %EFF-P. Contains 1 row of data.

APPENDIX C

TABLE XIX (b) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

DESIGN SPEED
STATOR 1 (beta* des. - beta* act.) = 0 degrees
STATOR 2 (beta* des. - beta* act.) = -5 degrees

U. S. CUSTOMARY UNITS

ROTOR 1

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, U-1, U-2, M'-1, M'-2, V'-1, V'-2. Includes data for 11 rotor stages.

Table with columns: SL, INCS, INCM, DEV, TURN, RHQVM-1, RHQVM-2, D-FAC, OMEGA-B, LOSS-P, PDZ/P, %EFF-P, %EFF-A, B'-1, B'-2, V0'-1, V0'-2, PD/PO. Includes data for 11 rotor stages.

Summary table with columns: TO/TD, PO/PO, EFF-AD, EFF-P, WCI/A1, TO2/T01, PO2/P01, EFF-AD, EFF-P. Includes values for rotor and stator.

STATOR 1

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, TO/TO, PO/PO, TO2/T01, PD/PO. Includes data for 11 stator stages.

Table with columns: SL, INCS, INCM, DEV, TURN, RHQVM-1, RHQVM-2, D-FAC, OMEGA-B, LOSS-P, PDZ/P, %EFF-P, %EFF-A, B'-1, B'-2, V0'-1, V0'-2, PD/PO. Includes data for 11 stator stages.

Summary table with columns: NCORR, WCORR, TO/TD, PO/PO, EFF-AD, EFF-P, TO2/T01, PO2/P01, EFF-AD, EFF-P. Includes values for rotor and stator.

ROTOR 2

Table for Rotor 2 with columns: PUN NO 22, SPEED CODE LO, POINT NO 3, and various speed/velocity parameters (U-1, U-2, M-1, M-2, etc.).

Table for Rotor 2 with columns: INCs, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-P, LOSS-P, P02, W EFF-P, W EFF-A, B-1, B-2, V0-1, V0-2, PO/PO, INLET, and RPM.

T02/T01 002/P01 EFF-AD EFF-P ROTOR ROTOR W W W W W W W W W W W W W W W W

STATOR 2

Table for Stator 2 with columns: PUN NO 22, SPEED CODE LO, POINT NO 3, and various speed/velocity parameters (U-1, U-2, M-1, M-2, etc.).

Table for Stator 2 with columns: INCs, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, P02, W EFF-P, W EFF-A, B-1, B-2, V0-1, V0-2, PO/PO, INLET, and RPM.

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APPENDIX C

TABLE XX (b) — OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

DESIGN SPEED
STATOR 1 (beta_des - beta_act.) = 0 degrees
STATOR 2 (beta_des - beta_act.) = -10 degrees

U. S. CUSTOMARY UNITS

ROTOR 1

Table with 25 columns: SL, Epsi-1, Epsi-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, Run No, Speed Code, Point No, Inlet, Outlet. Rows 1-11.

Table with 25 columns: SL, INCS, INCM, DEGV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, PO2, %EFF-P, %EFF-A, B*-1, B*-2, V0*-1, V0*-2, PO/PO. Rows 1-11.

Summary table with 6 columns: TO2/T01, PO2/P01, EFF-AD, EFF-P, WCI/A1, LBM/SEC, % SOFT, TO2/T01, PO2/P01, EFF-AD, EFF-P, ROTOR, ROTNP, %, %. Values: 1.2219, 1.8926, 90.00, 90.84, 39.20, 1.2219, 1.8926, 90.00, 90.84.

STATOR 1

Table with 25 columns: SL, Epsi-1, Epsi-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, Run No, Speed Code, Point No, Inlet, Outlet. Rows 1-11.

Table with 25 columns: SL, INCS, INCM, DEGV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, PO2, %EFF-P, %EFF-A, B*-1, B*-2, V0*-1, V0*-2, PO/PO. Rows 1-11.

Summary table with 6 columns: NCORR, WCORR, TO2/T01, PO2/P01, EFF-AD, EFF-P, WCI/A1, LBM/SEC, % SOFT, TO2/T01, PO2/P01, EFF-AD, EFF-P, ROTOR, ROTNP, %, %. Values: 10679, 172.60, 1.2219, 1.8372, 85.43, 86.61, 1.2219, 0.9707, 85.43, 175.56.

ROTOR 2

RUN NO 24, SPEED CODE 10, POINT NO 1

Table with columns: SL, EPS1-1, EPS1-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, U-1, U-2, M'-1, M'-2, V'-1, V'-2. Rows 1-11 showing various degree and ft/sec values.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, CMEGA-B, LOSS-P, P02, %EFF-P, %EFF-A, B'-1, B'-2, V0'-1, V0'-2, PC/PC. Rows 1-11 showing degree and ft/sec values.

Summary table with columns: TO2/T01, P02/P01, EFF-AD, EFF-P, ROTOR, STAGE, etc. Values: 1.1867, 1.5184, 67.44, 69.28.

STATOR 2

RUN NO 24, SPEED CODE 10, POINT NO 1

Table with columns: SL, EPS1-1, EPS1-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, P0/PC, TO2/T01, PC/PC, TO2/T01, EFF-AD, EFF-P. Rows 1-11 showing various degree and ft/sec values.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, CMEGA-B, LOSS-P, P02, %EFF-P, %EFF-A, B'-1, B'-2, V0'-1, V0'-2, PC/PC. Rows 1-11 showing degree and ft/sec values.

Summary table with columns: NCORR, WCORR, TO2/T01, P02/P01, EFF-AD, EFF-P, ROTOR, STAGE, etc. Values: 1.4049, 2.5394, 75.07, 78.06, 43.32, 1.1867, 0.9361, 56.25, 252.09.

APPENDIX D

OVERALL PERFORMANCE AND BLADE-ELEMENT DATA AT 105 PERCENT OF DESIGN SPEED

This appendix provides test overall performance and blade-element data at 105 percent of design speed for rotor 1, stator 1, rotor 2, and stator 2. The data is presented for five combinations of stator settings at various flows and pressure ratios. An overall-performance and stall data summary is given in Table XXII, and the complete overall and blade-element data is given in Table XXIII to Table XXVII. The column headings for Tables XXIII through XXVII are identified in Table XI of Appendix A.

**TABLE XXII – OVERALL PERFORMANCE AND STALL DATA SUMMARY FOR
105 PERCENT OF DESIGN SPEED**

PERFORMANCE

REF. TABLE ⁽¹⁾	STATOR SETTING ⁽²⁾		CORRECTED ⁽³⁾				
	S1	S2	FLOW lbm/sec	P_{11}/P_0	$\eta_{ad, 11}$ %	P_{16}/P_0	$\eta_{ad, 16}$ %
XXIII(a)	0°	0°	190.3	1.721	83.21	2.442	71.79
XXIII(b)	0°	0°	190.0	1.805	82.80	3.207	82.72
XXIII(c)	0°	0°	189.6	1.719	82.92	2.651	72.68
XXIV(a)	-5°	+2.5°	190.0	1.798	83.96	2.847	82.30
XXIV(b)	-5°	+2.5°	189.6	1.790	83.53	2.558	78.87
XXIV(c)	-5°	+2.5°	189.5	1.789	84.95	2.328	71.22
XXIV(d)	-5°	+2.5°	189.0	1.868	85.19	3.062	83.73
XXV(a)	-7.5°	+2.5°	187.8	1.808	87.64	2.300	71.09
XXV(b)	-7.5°	+2.5°	187.8	1.808	87.21	2.643	80.80
XXV(c)	-7.5°	+2.5°	187.3	1.834	86.68	2.878	83.16
XXV(d)	-7.5°	+2.5°	185.8	1.874	86.62	3.018	83.34
XXVI(a)	-2.5°	+2.5°	190.2	1.771	86.28	2.581	78.63
XXVI(b)	-2.5°	+2.5°	190.1	1.784	88.73	2.349	71.11
XXVI(c)	-2.5°	+2.5°	189.9	1.778	86.96	2.855	82.41
XXVI(d)	-2.5°	+2.5°	189.0	1.883	88.33	3.145	83.62
XXVII(a)	+2.5°	-2.5°	190.3	1.717	84.43	2.930	80.43
XXVII(b)	+2.5°	-2.5°	190.2	1.704	82.93	2.446	68.33
XXVII(c)	+2.5°	-2.5°	189.8	1.708	84.73	2.760	78.32
XXVII(d)	+2.5°	-2.5°	188.8	1.875	85.41	3.278	80.37

STALL POINT DATA

STATOR SETTING ⁽²⁾		CORRECTED ⁽³⁾		STALL MARGIN
S1	S2	FLOW lbm/sec	P_{16}/P_0	%
0°	0°	188.2	3.300	15.7
-5°	+2.5°	186.9	3.078	8.5
-7.5°	+2.5°	185.6	3.020	7.4
-2.5°	+2.5°	187.8	3.145	11.0
+2.5°	-2.5°	188.7	3.282	14.7

NOTES: (1) Refers to remaining Appendix D tables.

(2) Stator Setting = $\beta^*_{des} - \beta^*_{act}$.

(3) Corrected Flow = $W \sqrt{\theta/\delta}$

APPENDIX D

TABLE XXIII (b) — OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

105% OF DESIGN SPEED
STATOR 1 (beta_des - beta_act) = 0
STATOR 2 (beta_des - beta_act) = 0
(Data from reference 3)

U. S. CUSTOMARY UNITS

ROTOR 1

Table with columns: SL, CPSI-1, CPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, SPEED, C/JUE, POINT NO, etc. Rows 1-14.

Table with columns: SL, INCL, INCLM, DEV, TURN, RHOMV-1, RHOMV-2, D-FAC, OMEGA-T, LOSS-P, POZ/P, W/FF-P, W/FF-A, B-1, B-2, VM-1, VM-2, PO/PL, etc. Rows 1-14.

Summary table with columns: TO/TO, PU/PL, EFF-AD, EFF-P, WCI/A1, TOZ/T01, PCZ/PO1, EFF-AD, EFF-P. Values: 1.2218, 1.8624, 87.56, 88.59, 43.15, 1.2218, 1.8624, 87.56, 88.59.

STATOR 1

Table with columns: SL, CPSI-1, CPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, SPEED, C/JUE, POINT NO, etc. Rows 1-14.

Table with columns: SL, INCL, INCLM, DEV, TURN, RHOMV-1, RHOMV-2, D-FAC, OMEGA-T, LOSS-P, POZ/P, W/FF-P, W/FF-A, B-1, B-2, VM-1, VM-2, PO/PL, etc. Rows 1-14.

Summary table with columns: W/URK, W/URK, TO/TO, PU/PU, EFF-AD, EFF-P, TOZ/T01, PCZ/PO1, EFF-AD, EFF-P. Values: 1124.9, 190.00, 1.2218, 1.8053, 82.80, 84.15, 1.2218, 0.9695, 82.80.

TABLE XXIII (c) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

105% OF DESIGN SPEED
STATOR 1 (beta_des - beta_act) = 0
STATOR 2 (beta_des - beta_act) = 0
(Data from reference 3)

U. S. CUSTOMARY UNITS

ROTOR 1

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V1-2, B-1, B-2, M-1, M-2, RUN NO, 3, SPEED CODE, 15, POINT NO, 2, U-1, U-2, M*-1, M*-2, V*-1, V*-2. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, PO2/P01, XEFF-P, XEFF-A, B*-1, B*-2, V0*-1, V0*-2, PO/PO. Rows 1-11.

Summary table with columns: TO/TD INLET, PO/PO INLET, EFF-AD INLET, EFF-P INLET, WCI/A1 LBM/SEC % SOFT, TOZ/T01, POZ/P01, EFF-AD ROTOR, EFF-P ROTOR. Values: 1.2017, 1.7657, 87.37, 88.32, 43.06, 1.2017, 1.7657, 87.37, 88.32.

STATOR 1

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, PO/PO, TO/TD, PO/PO, TOZ/T01. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, PO2/P01, XEFF-P, XEFF-A, XEFF-P, XEFF-A, XEFF-P. Rows 1-11.

Summary table with columns: WCI/A1 INLET, WCI/A1 INLET, TO/TD INLET, PO/PO INLET, EFF-AD INLET, EFF-P INLET, TOZ/T01, POZ/P01, EFF-AD STAGE, EFF-P STAGE. Values: 11236, 18960, 1.2017, 1.7190, 82.92, 84.15, 1.2017, 0.9735, 82.92.

TABLE XXIV (a) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

105% OF DESIGN SPEED

STATOR 1 (beta^* - beta^act) = -5 degrees
STATOR 2 (beta^* - beta^act) = +2.5 degrees

U. S. CUSTOMARY UNITS

ROTOR 1

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO 13, SPEED CODE 15, PCINT NC 3, U-1, U-2, M*1, M*2, V*1, V*2. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHQVM-1, RHCVM-2, D-FAC, OMEGA-B, LOSS-P, P02/P01, XEFF-P, XEFF-A, B*1, B*2, VE*1, VE*2, FC/FG. Rows 1-11.

Summary table with columns: TO/TQ, PD/PO, EFF-AD, EFF-P, WCI/A1, T02/T01, P02/P01, EFF-AD, EFF-P. Values: 1.2172, 1.8514, 88.50, 89.44, 43.15, 1.2172, 1.8514, 88.50, 89.44.

STATOR 1

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO 13, SPEED CODE 15, PCINT NC 3, PG/PO, TC/TQ, PC/PC, T02. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHQVM-1, RHCVM-2, D-FAC, OMEGA-B, LOSS-P, P02/P01, XEFF-P, XEFF-A, XEFF-P, TOT-INLET, TOT-STG. Rows 1-11.

Summary table with columns: WCGRR, WCGRR, TO/TQ, PG/PO, EFF-AD, EFF-P, T02/T01, P02/P01, EFF-AD, EFF-P. Values: 11202, 190.00, 1.2172, 1.7983, 83.96, 85.21, 1.2172, 0.9713, 83.96, 197.76.

ROTOR 2

Table for Rotor 2 showing 16 columns of data (SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, VO-1, VO-2, B-1, B-2, M-1, M-2, RUN NO 16, SPEED CODE 15, POINT NO 31, U-1, U-2, V-1, V-2) and 11 rows of values.

Table for Rotor 2 showing 16 columns of data (SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, O-FAC, OMEGA-B, LOSS-P, P02, XEFF-P, XEFF-A, B*-1, B*-2, V0*-1, V0*-2, PO/PO, TOZ/T01, P02/P01, EFF-AD, EFF-P) and 11 rows of values, including summary statistics at the bottom.

STATOR 2

Table for Stator 2 showing 16 columns of data (SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, VO-1, VO-2, B-1, B-2, M-1, M-2, RUN NO 16, SPEED CODE 15, POINT NO 31, PD/PO, TOZ/T01, P02/P01, EFF-AD, EFF-P) and 11 rows of values.

Table for Stator 2 showing 16 columns of data (SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, O-FAC, OMEGA-B, LOSS-P, P02, XEFF-P, XEFF-A, B*-1, B*-2, V0*-1, V0*-2, PO/PO, TOZ/T01, P02/P01, EFF-AD, EFF-P) and 11 rows of values, including summary statistics at the bottom.

ROTOR 2

Table with 15 columns: EP1-1, EP1-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, U-1, U-2, M-1, M-2, V1-1, V1-2. Includes data rows 1 through 11.

Table with 15 columns: INLS, INCM, DEV, TURN, RHCVM-1, RHCVM-2, U-FAC, OMEGA-B, LOSS-P, PO2, XEFF-P, XEFF-A, B-1, B-2, V0-1, V0-2, PC/PC. Includes data rows 1 through 11.

STATOR 2

Table with 15 columns: EP1-1, EP1-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, U-1, U-2, M-1, M-2, V1-1, V1-2. Includes data rows 1 through 11.

Table with 15 columns: INLS, INCM, DEV, TURN, RHCVM-1, RHCVM-2, U-FAC, OMEGA-B, LOSS-P, PO2, XEFF-P, XEFF-A, B-1, B-2, V0-1, V0-2, PC/PC. Includes data rows 1 through 11.

Summary table with 10 columns: INLET, INLET, INLET, INLET, INLET, INLET, INLET, INLET, INLET, INLET. Includes data rows 1 through 11.

TABLE XXVI (a) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

105% OF DESIGN SPEED
STATOR 1 (beta_des - beta_act) = -2.5 degrees
STATOR 2 (beta_des - beta_act) = +2.5 degrees

U. S. CUSTOMARY UNITS

ROTOR 1

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, SPEED CODE, POINT NO, U-1, U-2, M-1, M-2, V-1, V-2. Rows 1-11.

Table with columns: SL, INCL, INCL, DEV, TURN, RHOVM-1, RHOVM-2, U-FAC, UMEGA-B, LOSS-P, P02, XEFF-P, XEFF-A, B-1, B-2, V6-1, V6-2, P0/P0, INLET. Rows 1-11.

Summary table with columns: TG/TG, PU/PU, EFF-AD, EFF-P, WCL/A1, T02/T01, P02/P01, EFF-AD, EFF-P, INLET, INLET, INLET, INLET, LBM/SEC, SOFT, RUTOR, RUTOR, STAGE, TOT-STG. Values: 1.2054, 1.0623, 90.42, 54.28, 45.20, 1.2054, 1.8103, 90.43, 91.28.

STATOR 1

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, SPEED CODE, POINT NO, P0/P0, TG/TG, PU/PU, T02/T01, XEFF-P, XEFF-A, XEFF-P, XEFF-A, XEFF-P, XEFF-A. Rows 1-11.

Table with columns: SL, INCL, INCL, DEV, TURN, RHOVM-1, RHOVM-2, U-FAC, UMEGA-B, LOSS-P, P02, XEFF-P, XEFF-A, B-1, B-2, V6-1, V6-2, P0/P0, INLET, TG/TG, PU/PU, T02/T01, XEFF-P, XEFF-A, XEFF-P, XEFF-A. Rows 1-11.

Summary table with columns: INCL, INCL, DEV, TURN, RHOVM-1, RHOVM-2, U-FAC, UMEGA-B, LOSS-P, P02/P01, XEFF-P, XEFF-A, INLET, INLET, INLET, INLET, LBM/SEC, SOFT, RUTOR, RUTOR, STAGE, TOT-STG. Values: 1.2054, 1.0771, 80.26, 57.22, 1.2054, 0.9750, 80.28, 206.77.

ROTOR 2

Table with 20 columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, VO-1, VO-2, 0-1, 0-2, M-1, M-2, RUN NO, 19, SPEED, CODE, 15, POINT NO, 1, V1-1, V1-2. Includes data rows 1 through 11.

Table with 18 columns: SL, INCS, INCM, DEV, TURN, RHGV-1, RHLV-2, D-FAC, CMEGA-B, LOSS-P, P02, ZEFF-P, ZEFF-A, B-1, B-2, V0-1, V0-2, PC/PO. Includes data rows 1 through 11.

Summary table with 8 columns: TO/T0, PC/PC, EFF-AD, EFF-P, W01/01, W02/T01, PC2/PO1, EFF-AD, EFF-P. Includes values like 1.2872, 2.5048, 71.20, 19.69, 41.79, 1.1536, 1.4041, 65.86, 67.44.

STATOR 2

Table with 20 columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, VO-1, VO-2, 0-1, 0-2, M-1, M-2, RUN NO, 19, SPEED, CODE, 15, POINT NO, 1, V1-1, V1-2. Includes data rows 1 through 11.

Table with 18 columns: SL, INCS, INCM, DEV, TURN, RHGV-1, RHLV-2, D-FAC, CMEGA-B, LOSS-P, P02, ZEFF-P, ZEFF-A, B-1, B-2, V0-1, V0-2, PC/PO. Includes data rows 1 through 11.

Summary table with 8 columns: W01/01, W02/T01, PC2/PO1, EFF-AD, EFF-P, TO/T0, PC/PC, EFF-AD, EFF-P. Includes values like 1.1536, 0.9377, 52.89, 2292.57.

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APPENDIX D

TABLE XXVI (c) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

105% OF DESIGN SPEED

STATOR 1 (β^{*}_{des.} - β^{*}_{act.}) = -2.5°

STATOR 2 (β^{*}_{des.} - β^{*}_{act.}) = +2.5°

U. S. CUSTOMARY UNITS

ROTOR 1

Table for Rotor 1 performance data. Columns include: SL, Epsi-1, Epsi-2, V-1, V-2, VM-1, VM-2, VO-1, VO-2, B-1, B-2, M-1, M-2, RUN NO, U-1, U-2, M-1, M-2, V1-1, V1-2, FT/SEC, FT/SEC, FT/SEC, FT/SEC, LEGRKE, LEGRKE, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC.

Table for Rotor 1 blade element data. Columns include: SL, INCS, INCH, DEV, TURN, RHOVM-1, RHOVM-2, U-FAC, OMEGA-B, LOSS-P, P02/P01, XEFF-P, XEFF-A, B*-1, B*-2, VB*-1, VG*-2, P0/P0, TO2/TO1, XEFF-P, XEFF-A, B*-1, B*-2, VB*-1, VG*-2, P0/P0, INLET.

Summary table for Rotor 1 blade element data. Columns include: TO/T0, P0/P0, EFF-AL, EFF-P, WCI/A1, TO2/TO1, P02/P01, EFF-AD, EFF-P, INLET.

STATOR 1

Table for Stator 1 performance data. Columns include: SL, Epsi-1, Epsi-2, V-1, V-2, VM-1, VM-2, VO-1, VO-2, B-1, B-2, M-1, M-2, RUN NO, U-1, U-2, M-1, M-2, V1-1, V1-2, FT/SEC, FT/SEC, FT/SEC, FT/SEC, LEGRKE, LEGRKE, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC, FT/SEC.

Table for Stator 1 blade element data. Columns include: SL, INCS, INCH, DEV, TURN, RHOVM-1, RHOVM-2, U-FAC, OMEGA-B, LOSS-P, P02/P01, XEFF-P, XEFF-A, B*-1, B*-2, VB*-1, VG*-2, P0/P0, TO2/TO1, XEFF-P, XEFF-A, B*-1, B*-2, VB*-1, VG*-2, P0/P0, INLET.

Summary table for Stator 1 blade element data. Columns include: NCURR, WCURR, TO/T0, P0/P0, EFF-AD, EFF-P, TO2/TO1, P02/P01, EFF-AD, EFF-P, INLET.

TABLE XXVI (d) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

105% OF DESIGN SPEED
STATOR 1 (beta^des. - beta^act.) = -2.5 degrees
STATOR 2 (beta^des. - beta^act.) = +2.5 degrees

U. S. CUSTOMARY UNITS

ROTOR 1

Table with 21 columns: SL, ESSI-1, ESSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, 19, SPEED CODE, 15, POINT NO, 4, U-1, U-2, M*-1, M*-2, V*-1, V*-2. Rows 1-11.

Table with 21 columns: SL, INCS, INCM, DEV, TURN, PHOVM-1, RHCVM-2, D-FAC, OMEGA-B, LOSS-P, PO2/, XEFF-P, XEFF-A, B*-1, B*-2, V0*-1, V0*-2, PC/PG. Rows 1-11.

Summary table with 6 columns: TD/TO, PC/PC, EFF-AD, EFF-P, WCI/A1, T02/T01, P02/P01, EFF-AD, EFF-P. Values: 1.2241, 1.9340, 92.44, 93.09, 42.93, 1.2241, 1.9340, 92.44, 93.09.

STATOR 1

Table with 21 columns: SL, ESSI-1, ESSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, 19, SPEED CODE, 15, POINT NO, 4, U-1, U-2, M*-1, M*-2, V*-1, V*-2. Rows 1-11.

Table with 21 columns: SL, INCS, INCM, DEV, TURN, PHOVM-1, RHCVM-2, D-FAC, OMEGA-B, LOSS-P, PO2/, XEFF-P, XEFF-A, B*-1, B*-2, V0*-1, V0*-2, PC/PG. Rows 1-11.

Summary table with 6 columns: TD/TO, PC/PC, EFF-AD, EFF-P, WCI/A1, T02/T01, P02/P01, EFF-AD, EFF-P. Values: 1.2241, 1.8829, 88.33, 89.31, 1.2241, 0.9735, 88.33, 166.07.

TABLE XXVII (a) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

105% OF DESIGN SPEED
STATOR 1 (beta_des - beta_act) = +2.5 degrees
STATOR 2 (beta_des - beta_act) = -2.5 degrees

U. S. CUSTOMARY UNITS

ROTOR 1

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, U-1, U-2, M'-1, M'-2, PO/P0, TO/T0, PO/P0, TOT, INLET, STAGE, TOT-STG.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, Q-FAC, OMEGA-B, LOSS-P, PO2, %EFF-P, %EFF-A, B-1, B-2, V0-1, V0-2, PO/P0.

Summary table with columns: TO/TO, PO/P0, EFF-AL, EFF-F, NC1/A1, TO2/TO2, PO2/PO1, EFF-AD, EFF-P.

STATOR 1

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, U-1, U-2, PO/P0, TO/T0, INLET, STAGE, TOT, TOT-STG.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, Q-FAC, OMEGA-B, LOSS-P, PO2, %EFF-P, %EFF-A, B-1, B-2, V0-1, V0-2, PO/P0.

Summary table with columns: NCORR, MCORR, TO/TO, PO/P0, EFF-AL, EFF-F, TO2/TO1, PO2/PO1, EFF-AD, EFF-P.

ROTOR 2

Table with 18 columns: SL, EPS1-1, EPS1-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, U-1, U-2, V1-1, V1-2. Includes Run No 23, Speed Code 15, Point No 1. Rows 1-11.

Table with 16 columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, P02/P01, XEFF-P, XEFF-A, B1-1, B1-2, V01-1, V01-2, PC/PC. Rows 1-11.

Summary table with 4 columns: TO2/T01, P02/P01, EFF-AD, EFF-P. Values: 1.1888, 1.5557, 71.22, 72.95.

STATOR 2

Table with 18 columns: SL, EPS1-1, EPS1-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, U-1, U-2, V1-1, V1-2. Includes Run No 23, Speed Code 15, Point No 1. Rows 1-11.

Table with 16 columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, P02/P01, XEFF-P, XEFF-A, XEFF-B, XEFF-C, PC/PC. Rows 1-11.

Summary table with 8 columns: NCURR, WCOFF, TO2/T01, P02/P01, EFF-AD, EFF-P, TO2/T01, P02/P01. Values: 11218, 190.20, 1.4244, 2.4457, 68.33, 71.96, 1.1888, 0.9202, 57.21, 217.05.

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APPENDIX E

OVERALL PERFORMANCE AND BLADE-ELEMENT DATA AT 70 PERCENT OF DESIGN SPEED

This appendix provides test overall performance and blade data at 70 percent of design speed for rotor 1, stator 1, rotor 2, and stator 2. The data is presented for five combinations of stator settings at various flows and pressure ratios. An overall-performance and stall data summary is given in Table XXVIII, and the complete overall performance and blade-element data is given in Table XXIX to Table XXXIII. The column headings for Tables XXIX to XXXIII are identified in Table XI of Appendix A.

TABLE XXVIII – OVERALL PERFORMANCE AND STALL DATA SUMMARY FOR
70 PERCENT OF DESIGN SPEED

PERFORMANCE

REF. TABLE ⁽¹⁾	STATOR SETTING ⁽²⁾		CORRECTED ⁽³⁾ FLOW lbm/sec	P_{11}/P_0	$\eta_{ad, 11}$ %	P_{16}/P_0	$\eta_{ad, 16}$ %
	S1	S2					
XXIX (a)	0°	0°	124.7	1.310	86.62	1.510	74.00
XXIX (b)	0°	0°	118.3	1.326	86.48	1.681	84.88
XXIX (c)	0°	0°	111.1	1.334	79.47	1.713	82.19
XXIX (d)	0°	0°	105.5	1.342	77.45	1.729	79.91
XXX (a)	-5°	+2.5°	122.3	1.318	89.67	1.478	75.72
XXX (b)	-5°	+2.5°	116.2	1.328	84.47	1.618	84.25
XXX (c)	-5°	+2.5°	109.1	1.334	81.49	1.662	82.95
XXX (d)	-5°	+2.5°	101.8	1.338	80.18	1.688	80.04
XXXI (a)	+5°	0°	128.2	1.318	90.61	1.541	73.44
XXXI (b)	+5°	0°	119.2	1.333	86.08	1.731	84.53
XXXI (c)	+5°	0°	112.1	1.339	84.85	1.755	80.69
XXXI (d)	+5°	0°	103.6	3.341	79.22	1.750	77.28
XXXII (a)	+5°	+7.5°	130.5	1.307	91.26	1.577	81.98
XXXII (b)	+5°	+7.5°	118.8	1.327	84.84	1.723	84.33
XXXII (c)	+5°	+7.5°	112.4	1.330	82.68	1.737	81.24
XXXII (d)	+5°	+7.5°	105.8	1.329	78.39	1.745	78.15
XXXIII	+5°	-5°	106.3	1.327	81.01	1.732	78.77

STALL POINT DATA

STATOR SETTING ⁽²⁾		CORRECTED ⁽³⁾ FLOW lbm/sec	P_{16}/P_0	STALL MARGIN %
S1	S2			
0°	0°	102.6	1.735	17.1
-5°	+2.5°	99.0	1.688	17.9
+5°	0°	103.4	1.747	16.9
+5°	+7.5°	102.3	1.743	17.9
+5°	-5°	103.1	1.736	---

NOTES: (1) Refers to remaining Appendix E tables.

(2) Stator Setting = $\beta^*_{des} - \beta^*_{act}$.

(3) Corrected flow = $W\sqrt{\theta/\delta}$

ROTOR 2

SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	VO-1	VO-2	B-1	B-2	M-1	M-2	3. SPEED	CODE	70. POINT	NO 2	V1-1	V1-2
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			FT/SEC	FT/SEC			FT/SEC	FT/SEC
1	11.590	11.091	577.0	893.6	577.0	645.1	0.1	618.4	0.0	43.7	0.5059	0.7666	584.7	613.3	0.7202	0.5555	821.4	845.2
2	10.753	9.842	578.0	875.3	577.9	635.9	6.5	601.4	0.6	43.3	0.5070	0.7501	601.2	626.1	0.7274	0.5454	829.3	836.4
3	7.761	8.860	577.6	850.5	577.5	629.5	9.5	571.9	0.9	42.2	0.5070	0.7285	618.3	639.5	0.7363	0.5423	839.4	833.1
4	0.024	5.311	563.3	764.4	563.3	610.5	-1.3	460.0	-0.1	37.0	0.4441	0.6528	671.2	682.0	0.7694	0.5548	877.2	649.6
5	0.424	0.854	513.1	630.8	512.3	528.3	-29.0	344.7	-3.2	33.1	0.4487	0.5348	744.1	743.6	0.8109	0.5612	927.5	662.0
6	-2.050	-1.214	497.6	509.2	496.6	478.9	-31.4	307.7	-3.6	32.7	0.4348	0.4812	781.3	776.4	0.8321	0.5666	954.4	670.1
7	-3.041	-2.114	502.9	558.4	502.1	477.3	-28.5	289.8	-3.2	31.2	0.4396	0.4723	800.0	793.4	0.8468	0.5869	966.8	693.8
8	-3.926	-3.010	508.6	561.8	507.8	491.2	-29.1	272.1	-3.3	28.9	0.4443	0.4753	818.9	810.7	0.8635	0.6168	988.4	726.7
9	-4.923	-4.146	522.6	577.9	522.0	515.3	-25.2	261.4	-2.8	26.8	0.4547	0.4872	836.4	824.7	0.9063	0.6686	1041.7	793.1
10	-7.914	-7.358	526.5	578.9	526.0	517.4	-23.7	259.6	-2.6	26.5	0.4571	0.4868	856.6	842.8	0.9195	0.6810	1059.1	809.9
11	-8.729	-8.568	518.8	549.3	518.2	492.4	-24.5	243.7	-2.7	26.2	0.4488	0.4601	914.9	901.5	0.9281	0.6881	1072.8	821.6

SL	INCS	INCM	DEV	TURN	RHOVN-1	RHOVN-2	E-FAC	OMEGA-B	LOSS-P	P02/	EFF-P	EFF-A	B1-1	B1-2	V01-1	V01-2	PO/PO
DEGREE	DEGREE	DEGREE	DEGREE					TOTAL	TOTAL	P01	TOT	TOT	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	-0.18	0.14	19.95	45.75	48.44	58.19	0.3902	0.1319	0.0301	1.3908	89.52	89.04	45.30	-0.45	-584.6	5.1	1.8976
2	-0.15	0.30	16.64	43.58	48.34	57.93	0.4034	0.1238	0.0289	1.3853	89.84	89.36	45.80	-2.22	-594.7	-2.4	1.8905
3	-0.83	0.75	13.84	40.42	48.51	57.94	0.4078	0.1079	0.0257	1.3750	90.70	90.30	46.53	-6.11	-608.8	-67.5	1.8745
4	-1.00	3.13	10.42	30.10	47.08	57.44	0.3945	0.0527	0.0127	1.3394	94.54	94.33	50.09	19.98	-672.4	-222.0	1.8040
5	3.00	7.57	8.84	19.40	42.35	49.93	0.3995	0.0734	0.0160	1.2827	90.38	90.07	56.47	37.07	-773.1	-399.0	1.6781
6	4.19	8.53	8.15	14.20	41.25	45.19	0.4019	0.1043	0.0221	1.2492	85.08	84.63	54.36	44.36	-812.6	-468.8	1.6236
7	3.88	7.46	7.23	12.28	41.76	45.15	0.3835	0.0949	0.0199	1.2398	85.61	85.20	58.74	46.48	-828.6	-503.6	1.6167
8	3.67	7.48	5.23	11.56	42.19	46.57	0.3575	0.0716	0.0151	1.2398	84.45	84.12	59.05	47.55	-848.1	-538.4	1.6215
9	3.04	5.72	2.25	10.51	43.08	48.59	0.3357	0.0633	0.0144	1.1430	89.07	88.74	59.85	49.35	-901.5	-602.8	1.4637
10	2.94	5.12	3.49	9.97	43.27	48.54	0.3315	0.0710	0.0185	1.2392	87.49	87.14	60.14	50.17	-919.3	-623.1	1.4374
11	3.52	5.21	7.42	7.95	42.39	45.82	0.3270	0.0792	0.0180	1.2229	85.28	84.89	61.03	53.08	-939.4	-657.8	1.6100

TO/TO	PO/PO	EFF-AD	EFF-P	MCI/A1	T02/T01	P02/P01	EFF-AD	EFF-P
INLET	INLET	INLET	INLET	LBN/SEC	%	%	RGTOR	%
1.1884	1.7088	87.75	86.62	33.41	1.0831	1.2884	90.20	90.52

STATOR 2

SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	VO-1	VO-2	B-1	B-2	M-1	M-2	3. SPEED	CODE	70. POINT	NO 2	T02/
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			FT/SEC	FT/SEC			T06
1	0.625	0.837	422.1	723.0	689.5	722.1	642.1	35.5	41.9	2.8	0.7941	0.6080	1.7768	1.2189	1.3023	1.1109	
2	7.556	0.748	902.4	731.9	677.3	731.1	596.3	34.2	41.6	2.7	0.7761	0.6166	1.7937	1.2165	1.3143	1.1095	
3	0.498	0.534	876.8	750.1	667.9	749.7	568.1	22.6	40.6	1.7	0.7534	0.6344	1.8242	1.2113	1.3373	1.1062	
4	3.830	-0.299	788.7	706.6	641.6	708.6	458.6	4.5	35.0	0.4	0.6753	0.5995	1.7810	1.1951	1.3211	1.0949	
5	1.037	-0.969	654.1	603.0	550.0	603.0	344.5	-4.1	31.8	-0.4	0.5557	0.5099	1.6700	1.1811	1.2754	1.0819	
6	-0.578	-1.229	592.6	548.3	500.3	548.4	507.9	-6.2	31.3	-0.6	0.5019	0.4628	1.6180	1.1752	1.2453	1.0778	
7	-1.461	-1.326	581.5	537.6	504.0	537.6	290.2	-6.9	29.9	-0.7	0.4928	0.4540	1.6080	1.1719	1.2335	1.0745	
8	-2.251	-1.368	584.6	558.6	517.0	538.6	272.9	-6.7	27.8	-0.7	0.4958	0.4551	1.6073	1.1707	1.2291	1.0718	
9	-4.180	-1.147	604.7	563.2	544.6	563.2	262.8	4.3	25.8	0.6	0.5110	0.4743	1.6196	1.1827	1.2294	1.0721	
10	-4.852	-1.323	609.1	569.3	550.3	569.0	261.2	16.2	25.4	1.0	0.5135	0.4783	1.6212	1.1886	1.2270	1.0724	
11	-3.713	-1.232	585.9	540.8	532.0	540.5	245.4	18.8	24.8	2.0	0.4921	0.4527	1.5928	1.1926	1.2099	1.0696	

SL	INCS	INCM	DEV	TURN	RHOVN-1	RHOVN-2	D-FAC	OMEGA-B	LOSS-P	P02/	EFF-P	EFF-A	EFF-P	EFF-A	EFF-P	EFF-A	EFF-P
DEGREE	DEGREE	DEGREE	DEGREE					TOTAL	TOTAL	P01	STATC-ST	TOT-INLET	TOT-INLET	TOT-INLET	TOT-INLET	TOT-INLET	TOT-INLET
1	-0.58	-5.02	14.63	39.04	61.02	67.35	0.3576	0.1874	0.0423	0.9360	60.57	81.47	82.88	85.10	74.01	74.97	
2	-5.84	-3.82	13.93	34.90	60.61	68.63	0.3348	0.1582	0.0364	0.9476	62.93	83.85	86.50	86.50	81.42	82.14	
3	-0.03	-3.59	12.57	38.83	60.46	71.14	0.2959	0.0917	0.0213	0.9709	75.21	88.59	90.50	89.01	82.14	82.14	
4	-3.95	-6.08	10.66	35.25	59.57	67.69	0.2528	0.0570	0.0142	0.9849	76.77	91.81	92.43	87.95	87.06	88.04	
5	-12.94	-7.64	9.91	32.16	52.01	57.42	0.2281	0.0406	0.0109	0.9921	78.11	87.07	85.10	83.03	83.54	83.54	
6	-13.41	-7.33	9.57	31.92	47.32	51.99	0.2244	0.0271	0.0075	0.9957	83.33	86.08	85.51	82.82	83.29	83.29	
7	-14.63	-8.24	9.43	30.63	47.23	50.99	0.2200	0.0337	0.0094	0.9948	78.99	84.53	85.98	84.45	84.87	84.87	
8	-16.25	-10.04	9.39	28.52	48.50	51.09	0.2150	0.0956	0.0158	0.9914	66.39	85.03	82.07	84.18	84.60	84.60	
9	-18.02	-11.32	10.61	23.34	50.77	52.84	0.1946	0.0669	0.0196	0.9891	54.34	80.84	79.77	82.99	83.45	83.45	
10	-19.03	-12.15	12.40	23.80	50.97	53.06	0.1451	0.0598	0.0177	0.9902	37.31	78.38	79.77	80.26	80.75	80.75	
11	-21.90	-13.80	13.92	22.84	48.80	49.93	0.1432	0.0697	0.0208	0.9894	57.17	73.82	75.45	80.26	80.75	80.75	

NCORR	NCORR	TO/TO	PO/PO	EFF-AD	EFF-P	T02/T01	P02/P01	EFF-AD
INLET	INLET	INLET	INLET	INLET	INLET	%	%	STAGE
7499.	118.30	1.1884	1.4812	84.88	85.93	1.0831	0.9839	84.22

TABLE XXIX (c) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

70% OF DESIGN SPEED
STATOR 1 (beta^*_des - beta^*_act) = 0^0
STATOR 2 (beta^*_des - beta^*_act) = 0^0
(Data from reference 3)

U. S. CUSTOMARY UNITS

ROTOR 1

Table with columns: SL, ESSI-1, ESSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, RUN NO, SPEED, CODE, 70, POINT NO, V1-1, V1-2. Includes detailed performance metrics for Rotor 1.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, PO2, XEFF-P, XEFF-A, B*-1, B*-2, V0*-1, V0*-2, PU/PO. Includes detailed performance metrics for Rotor 1.

STATOR 1

Table with columns: SL, ESSI-1, ESSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, RUN NO, SPEED, CODE, 70, POINT NO, T02/T01, PU/PO. Includes detailed performance metrics for Stator 1.

APPENDIX E

TABLE XXIX (d) – OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

70% OF DESIGN SPEED
 STATOR 1 ($\beta^{\circ}_{des} - \beta^{\circ}_{act}$) = 0°
 STATOR 2 ($\beta^{\circ}_{des} - \beta^{\circ}_{act}$) = 0°
 (Data from reference 3)

U. S. CUSTOMARY UNITS

ROTOR 1

SL	E PSI-1		V-1		VH-1		V0-1		B-1	B-2	M-1	RUN NO M-2	S, SPEED CODE 70,		POINT NO 4		V'-1	V'-2
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC					DEGREE	DEGREE	FT/SEC	FT/SEC		
1	10.607	10.021	320.9	758.1	320.9	391.9	0.0	0.0	0.0	58.4	0.2897	0.0743	440.8	510.3	0.4923	0.3697	543.2	615.7
2	11.102	11.389	327.5	726.8	327.5	395.2	0.0	0.0	0.0	57.0	0.2958	0.0446	475.3	535.0	0.5214	0.3568	577.2	602.3
3	11.833	12.994	334.3	694.6	334.3	407.2	0.0	0.0	0.0	54.3	0.3021	0.0194	509.1	559.0	0.5504	0.3606	609.6	607.3
4	11.980	0.960	349.1	644.1	349.1	400.7	0.0	0.0	0.0	51.5	0.3157	0.5608	606.2	633.7	0.6326	0.3705	699.5	621.1
5	12.500	0.622	353.3	574.1	353.3	363.7	0.0	0.0	0.0	50.7	0.3196	0.5015	727.2	732.5	0.7313	0.4053	808.5	664.1
6	13.060	-2.048	351.3	560.7	351.3	373.4	0.0	0.0	0.0	48.3	0.3177	0.4890	785.5	781.8	0.7782	0.4566	860.5	521.2
7	15.292	-3.336	349.4	567.3	349.4	392.1	0.0	0.0	0.0	46.3	0.3160	0.4948	814.2	806.5	0.8013	0.4864	886.0	557.7
8	16.949	-4.644	346.3	571.7	346.3	395.3	0.0	0.0	0.0	46.3	0.3132	0.4979	843.0	831.2	0.8440	0.5012	911.3	575.5
9	18.529	-8.579	333.0	572.6	333.0	355.8	0.0	0.0	0.0	51.6	0.3008	0.4940	928.8	905.3	0.8915	0.4995	986.6	578.9
10	19.522	-9.764	327.8	569.4	327.8	321.3	0.0	0.0	0.0	55.6	0.2961	0.4889	957.4	930.0	0.9140	0.4817	1011.9	561.0
11	20.732	-10.196	323.4	566.8	323.4	291.1	0.0	0.0	0.0	59.1	0.2920	0.4846	985.9	954.6	0.9370	0.4714	1037.6	551.4

SL	INCS DEGREE	INCM DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P TOTAL	P02/ P01	EFF-P TUT	EFF-A TUT	E-1 DEGREE	E-2 DEGREE	V'-1 FT/SEC	V'-2 FT/SEC	PQ/PD INLET
1	7.35	11.95	8.47	73.21	23.94	30.34	0.5202	0.1493	0.0310	1.3924	93.65	93.37	53.73	-19.48	-440.8	138.7	1.3924
2	7.39	11.69	8.89	65.92	23.98	31.03	0.5625	0.1376	0.0311	1.3847	93.37	93.09	55.21	-10.71	-475.3	75.0	1.3847
3	7.50	11.61	10.23	57.81	24.44	32.36	0.5682	0.1062	0.0254	1.3783	94.21	93.97	56.51	-1.30	-509.1	9.3	1.3783
4	8.41	11.88	8.19	42.04	25.41	32.51	0.5982	0.1187	0.0301	1.3672	91.51	91.16	59.91	17.87	-606.2	-129.5	1.3672
5	9.57	12.25	8.12	25.70	25.68	29.84	0.5955	0.1701	0.0414	1.3397	84.11	83.47	64.09	38.39	-727.2	-288.3	1.3397
6	10.01	12.29	6.91	21.70	25.56	30.81	0.5915	0.1634	0.0370	1.3402	83.81	83.16	65.95	44.25	-785.5	-363.6	1.3402
7	10.23	12.30	5.03	21.50	25.43	32.45	0.5239	0.1475	0.0336	1.3490	84.81	84.18	66.84	45.34	-814.2	-396.6	1.3490
8	10.55	12.50	3.78	21.13	25.23	32.68	0.5217	0.1619	0.0369	1.3542	83.02	82.30	67.76	46.04	-843.0	-418.2	1.3542
9	11.41	12.83	5.30	16.34	24.35	28.98	0.5763	0.2749	0.0599	1.3549	71.15	69.92	70.46	52.10	-928.8	-456.7	1.3549
10	11.58	12.88	8.06	16.21	24.00	29.98	0.6134	0.3276	0.0679	1.3555	66.33	64.89	71.27	55.06	-957.4	-459.9	1.3555
11	11.59	12.75	11.74	13.84	23.70	23.42	0.6404	0.3688	0.0719	1.3560	62.62	61.01	71.93	58.08	-985.9	-468.3	1.3560

TOQ/TO1 1.1131 P02/P01 1.3584 EFF-AD 80.87 EFF-P 81.65
 INLET INLET INLET INLET LBM/SEC % SOFT
 TOQ/TO1 P02/P01 EFF-AD EFF-P
 ROTOR RUTUM
 1.1131 1.3584 80.87 81.65

STATOR 1

SL	E PSI-1		V-1		VH-1		V0-1		B-1	B-2	M-1	M-2	RUN NO	S, SPEED CODE 70,		POINT NO 4		V'-1	V'-2
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC						DEGREE	DEGREE	FT/SEC	FT/SEC		
1	17.332	14.704	757.2	459.9	412.2	459.8	835.2	-4.3	57.2	-0.5	0.6734	0.3978	1.3613	1.1062	1.3613	1.4062	1.4062		
2	13.392	12.827	728.9	458.4	415.4	458.4	599.0	1.7	55.3	0.2	0.6466	0.3968	1.3628	1.1045	1.3628	1.4045	1.4045		
3	13.167	11.112	704.0	457.1	426.4	457.1	560.3	6.4	52.7	0.7	0.6236	0.3961	1.3635	1.1020	1.3635	1.4020	1.4020		
4	7.948	6.514	652.1	441.6	418.3	441.6	500.2	1.8	50.1	0.2	0.5743	0.3822	1.3538	1.1026	1.3538	1.4026	1.4026		
5	8.111	1.309	583.8	401.1	379.7	400.7	443.5	-16.1	49.4	-2.3	0.5104	0.3459	1.3279	1.1045	1.3279	1.4045	1.4045		
6	10.248	-0.924	570.7	393.9	387.8	393.6	418.6	-15.3	47.2	-2.2	0.4982	0.3399	1.3236	1.1050	1.3236	1.4050	1.4050		
7	11.126	-1.792	577.0	406.3	405.2	406.4	410.8	-7.8	45.4	-1.1	0.5037	0.3505	1.3310	1.1058	1.3310	1.4058	1.4058		
8	11.925	-2.545	581.4	418.7	408.0	419.7	414.2	-4.5	45.4	-0.6	0.5067	0.3616	1.3394	1.1069	1.3394	1.4069	1.4069		
9	14.663	-4.989	583.0	409.6	389.6	409.4	450.8	-12.1	50.7	-1.7	0.5034	0.3496	1.3383	1.1280	1.3383	1.4280	1.4280		
10	15.944	-6.124	580.2	387.4	356.3	397.0	472.8	-15.9	54.6	-1.3	0.4987	0.3375	1.3332	1.1373	1.3332	1.4373	1.4373		
11	17.523	-7.529	577.9	387.1	306.2	386.5	490.1	-22.4	58.1	-3.3	0.4945	0.3269	1.3290	1.1488	1.3290	1.4488	1.4488		

SL	INCS DEGREE	INCM DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P TOTAL	P02/ P01	EFF-P STAT-5T	EFF-A TOT-INLET	EFF-P TOT-INLET	EFF-A TOT-STG	EFF-P TOT-STG
1	4.61	6.72	11.80	57.70	31.93	40.03	0.5574	0.0893	0.0172	0.9779	88.48	86.77	87.31	87.31	
2	6.47	6.87	11.43	32.37	40.03	0.5371	0.0628	0.0133	0.9846	90.95	88.52	88.98	88.52	88.98	
3	3.21	5.99	11.13	31.99	33.80	40.03	0.5173	0.0455	0.0100	0.9895	91.08	90.87	91.23	91.23	
4	4.07	6.79	9.50	48.84	33.80	38.58	0.5056	0.0471	0.0115	0.9906	92.18	88.15	88.61	88.61	
5	3.91	8.96	7.02	31.70	31.02	34.73	0.5272	0.0539	0.0147	0.9913	90.62	80.86	81.58	81.58	
6	2.17	7.78	7.14	49.41	31.87	34.06	0.5270	0.0758	0.0217	0.9882	88.62	79.50	80.27	80.27	
7	0.53	6.47	8.29	46.49	33.39	33.21	0.5062	0.0788	0.0230	0.9875	85.60	80.49	81.23	81.23	
8	0.83	6.98	8.32	48.04	33.38	34.34	0.4901	0.0655	0.0194	0.9895	87.42	80.07	80.85	80.85	
9	0.04	12.92	8.85	32.34	29.98	34.97	0.5436	0.0857	0.0267	0.9863	84.48	67.94	69.20	69.20	
10	9.67	16.72	9.47	56.91	27.07	33.64	0.5799	0.1049	0.0332	0.9835	81.85	62.52	63.97	63.97	
11	12.46	19.61	9.99	61.41	24.52	32.43	0.6172	0.1272	0.0437	0.9804	78.64	58.91	58.57	58.57	

NGQAR NGQAR TOQ/TO1 PO/PO EFF-AD EFF-P TOQ/TO1 P02/P01 EFF-AD
 INLET INLET INLET INLET INLET INLET INLET INLET INLET INLET INLET
 RPM LBM/SEC
 7499. 105.50 1.1131 1.3416 77.45 78.34 1.1131 0.9876 77.45

ROTOR 2

SL	EPSI-1		V-1		V-2		VH-1		VH-2		VW-1		VW-2		B-1		B-2		M-1		M-2		3. SPEED CODE TO POINT NO 4		V'-1		V'-2	
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC
1	11.336	10.986	496.9	823.0	496.8	568.5	-4.2	598.2	-0.5	46.2	0.4309	0.6983	584.8	613.3	0.6683	0.4826	770.5	559.8										
2	4.625	9.648	499.0	807.3	499.0	558.1	1.7	583.2	0.2	46.1	0.4332	0.6845	602.3	626.2	0.6772	0.4747	780.1	559.8										
3	4.554	8.391	500.2	786.4	500.1	552.9	5.8	561.9	0.7	45.4	0.4348	0.6685	618.3	639.5	0.6873	0.4735	790.8	558.4										
4	5.749	4.919	488.4	700.2	488.4	520.8	1.7	468.0	0.2	41.9	0.4240	0.5912	671.2	682.0	0.7195	0.4754	828.7	563.0										
5	4.309	0.497	445.3	593.6	445.0	461.4	-16.0	373.5	-2.1	39.0	0.3851	0.4980	744.2	743.7	0.7618	0.4962	880.9	591.5										
6	-2.247	-1.715	433.3	549.5	433.0	423.4	-15.3	350.3	-2.0	39.6	0.3743	0.4597	781.4	776.5	0.7834	0.5025	906.8	600.7										
7	-3.158	-2.616	442.6	540.4	442.5	413.1	-7.9	348.5	-1.0	40.1	0.3824	0.4516	800.1	793.4	0.7961	0.5073	921.2	607.1										
8	-4.814	-3.379	454.5	544.1	454.5	420.2	-4.4	345.6	-0.6	39.4	0.3926	0.4541	819.0	810.7	0.8123	0.5232	940.5	626.9										
9	-6.852	-5.670	453.5	552.7	453.3	434.1	-12.1	342.0	-1.5	38.1	0.3883	0.4508	876.4	864.4	0.8644	0.5614	997.4	679.2										
10	-8.799	-6.651	446.2	548.3	446.0	435.8	-15.7	332.8	-2.0	37.2	0.3803	0.4514	895.6	882.8	0.8647	0.5777	1014.6	701.8										
11	-10.003	-8.007	440.0	533.3	439.4	445.6	-22.5	293.0	-2.9	33.2	0.3728	0.4373	915.0	901.6	0.8772	0.6185	1035.4	754.3										

SL	INCS DEGREE	INCM DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-TOTAL	LOSS-P	PO2/PO1	EFF-P	EFF-A	B'-1	B'-2	VW'-1	VW'-2	PO/PU
1	0.29	4.61	22.22	47.95	42.68	53.54	0.4435	0.0795	0.0181	1.3970	94.23	93.97	49.77	1.82	-589.6	-18.2	1.9018
2	0.25	4.70	18.20	45.82	42.94	53.03	0.4602	0.0801	0.0187	1.3924	94.00	93.73	50.20	4.38	-599.6	-42.9	1.8977
3	0.41	4.99	15.49	42.81	43.13	53.05	0.4657	0.0705	0.0167	1.3461	94.49	94.25	50.77	7.96	-612.5	-77.6	1.8897
4	2.16	6.95	12.77	31.58	41.98	50.68	0.4659	0.0554	0.0132	1.3419	94.75	94.55	53.91	22.33	-669.5	-214.0	1.8161
5	0.19	10.76	10.32	20.92	38.03	49.05	0.4559	0.0637	0.0141	1.3003	92.67	92.42	59.66	38.74	-760.2	-370.2	1.7262
6	7.09	11.43	8.96	16.30	37.02	41.27	0.4572	0.0960	0.0201	1.2766	88.14	87.75	61.46	45.17	-796.7	-26.2	1.6904
7	6.40	10.48	7.83	14.18	37.89	40.24	0.4590	0.1168	0.0242	1.2650	85.16	84.69	61.27	47.09	-808.0	-445.0	1.6893
8	5.68	9.49	5.52	13.22	38.92	40.91	0.4497	0.1222	0.0297	1.2615	84.01	83.50	61.06	47.84	-814	-465.1	1.6896
9	6.04	8.72	3.03	12.73	38.22	41.67	0.4406	0.1362	0.0305	1.2706	81.61	81.21	62.85	50.12	-814	-522.4	1.7018
10	6.53	8.77	4.76	12.34	37.24	41.59	0.4300	0.1240	0.0261	1.2742	83.11	82.54	63.79	51.44	-911.4	-550.0	1.7001
11	7.25	8.95	7.98	11.13	36.30	42.29	0.3844	0.0699	0.0197	1.2709	89.51	89.18	64.76	53.64	-937.9	-608.6	1.6893

TO2/TO1	PO2/PO1	EFF-AD	EFF-P	WCL/A1
1.2117	1.7347	82.26	83.58	29.67

TO2/TO1	PO2/PO1	EFF-AD	EFF-P
1.0885	1.3079	89.84	90.20

STATOR 2

SL	EPSI-1		V-1		V-2		VH-1		VH-2		VW-1		VW-2		B-1		B-2		M-1		M-2		3. SPEED CODE TO POINT NO 4		TO2/TO1	
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC
1	6.647	0.836	843.6	629.4	603.7	629.8	589.2	26.7	44.6	2.4	0.7174	0.5235	1.8137	1.2241	1.3324	1.1064										
2	7.602	0.733	826.7	637.2	590.8	636.6	578.2	28.6	44.6	2.4	0.7025	0.5309	1.8267	1.2218	1.3406	1.1059										
3	8.566	0.494	808.9	652.5	582.9	652.0	557.9	23.1	43.9	2.0	0.6857	0.5455	1.8490	1.2188	1.3559	1.1040										
4	9.911	-0.349	717.6	596.2	545.4	596.2	466.4	8.8	40.8	0.8	0.6070	0.4984	1.7966	1.2051	1.3268	1.0930										
5	1.077	-0.874	610.0	500.0	482.5	500.0	373.2	-4.9	37.7	-0.6	0.5124	0.4164	1.7097	1.1976	1.2873	1.0843										
6	-0.262	-0.920	506.2	457.8	444.8	457.8	350.5	-4.0	36.2	-1.0	0.4762	0.3805	1.6762	1.1958	1.2688	1.0822										
7	-1.085	-0.940	357.3	449.8	434.6	449.8	348.9	-7.9	38.7	-1.0	0.4669	0.3716	1.6699	1.1962	1.2558	1.0819										
8	-1.964	-0.984	361.4	453.9	441.8	453.9	346.4	-8.0	38.1	-1.0	0.4692	0.3784	1.6733	1.1986	1.2497	1.0818										
9	-4.475	-1.212	373.7	484.8	456.4	484.7	343.7	-8.2	36.8	-1.0	0.4749	0.3988	1.6866	1.2240	1.2592	1.0870										
10	-6.316	-1.308	372.2	487.8	464.2	487.8	334.5	-8.7	35.8	-0.1	0.4718	0.3997	1.6850	1.2331	1.2631	1.0864										
11	-8.069	-1.264	362.0	471.0	476.4	471.0	295.0	1.7	31.8	0.2	0.4618	0.3844	1.6690	1.2396	1.2537	1.0792										

SL	INCS DEGREE	INCM DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-TOTAL	LOSS-P	PO2/PO1	EFF-P	EFF-A	B'-1	B'-2	VW'-1	VW'-2	PO/PU
1	-3.87	-2.51	14.24	42.13	56.15	62.38	0.4046	0.1596	0.0360	0.9525	69.49	62.66	84.03	80.09	80.85		
2	-2.81	-0.80	12.82	42.04	55.49	63.44	0.3834	0.1244	0.0309	0.9620	72.35	84.63	85.06	82.33	83.02		
3	-2.72	-0.22	12.88	41.66	55.33	65.38	0.3499	0.0823	0.0193	0.9776	80.22	86.48	89.41	87.24	87.76		
4	-4.90	-1.09	11.16	39.75	52.62	60.18	0.3325	0.0579	0.0144	0.9871	84.04	88.74	89.61	90.30	90.66		
5	-7.00	-1.89	9.73	38.27	46.79	58.12	0.3513	0.0485	0.0163	0.9887	81.42	83.79	84.90	88.54	88.91		
6	-8.19	-0.81	9.21	35.20	43.67	45.49	0.3700	0.0663	0.0189	0.9901	82.10	81.14	82.46	84.64	85.31		
7	-5.51	0.49	9.16	35.73	42.06	44.62	0.3723	0.0583	0.0163	0.9919	84.36	80.37	81.72	81.91	82.45		
8	-5.99	0.22	9.10	35.07	42.72	43.34	0.3670	0.0637	0.0167	0.9908	82.62	79.74	81.23	80.20	80.79		
9	-8.98	-0.27	9.20	37.81	48.79	47.23	0.3361	0.0424	0.0163	0.9911	79.76	71.85	73.61	78.06	78.72		
10	-8.62	-1.74	10.49	35.93	43.89	47.10	0.3214	0.0615	0.0182	0.9913	79.12	68.90	71.06	79.65	80.29		
11	-13.98	-4.88	12.13	31.55	40.91	43.09	0.3182	0.0878	0.0262	0.9881	72.52	65.71	68.05	64.64	65.10		

WGORA	WGORA	TO2/TO1	PO2/PO1	EFF-AD	EFF-P	TO2/TO1	PO2/PO1	EFF-AD	EFF-P
1499.	105.90	1.2117	1.7288	79.91	81.38	1.0885	0.9853	84.69	84.69

ORIGINAL PAGE IS
OF POOR QUALITY

APPENDIX E

TABLE XXX (a) — OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

70% OF DESIGN SPEED

STATOR 1 ($\beta^*_{des} - \beta^*_{act.}$) = -5°

STATOR 2 ($\beta^*_{des} - \beta^*_{act.}$) = +2.5°

U. S. CUSTOMARY UNITS

ROTOR 1

SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	VO-1	VO-2	B-1	B-2	M-1	M-2	U-1	U-2	M-1	M-2	V-1	V-2
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			FT/SEC	FT/SEC			FT/SEC	FT/SEC
1	16.686	18.002	373.5	738.8	373.5	426.2	0.0	603.5	0.0	54.8	0.3383	0.4581	440.2	509.6	0.5228	0.3887	577.3	436.4
2	14.244	15.484	381.3	710.7	381.3	436.8	0.0	560.7	0.0	52.0	0.3455	0.6318	474.7	534.3	0.5517	0.3890	608.9	437.6
3	11.934	13.105	388.5	687.3	388.9	450.0	0.0	519.4	0.0	49.0	0.3525	0.6102	508.5	558.9	0.5803	0.4011	640.1	451.8
4	5.615	6.987	405.8	630.1	405.8	454.6	0.0	436.3	0.0	43.8	0.3682	0.5574	605.4	632.9	0.6614	0.4382	728.8	495.3
5	-0.214	0.431	411.9	545.8	411.9	400.9	0.0	370.4	0.0	42.7	0.3740	0.4795	726.3	731.5	0.7580	0.4740	835.0	534.5
6	-2.000	-2.227	411.2	527.2	411.2	401.8	0.0	341.6	0.0	42.4	0.3733	0.4628	784.5	780.8	0.8041	0.5227	885.7	595.4
7	-3.055	-3.424	410.4	531.1	410.4	420.1	0.0	325.0	0.0	37.8	0.3726	0.4667	813.2	805.5	0.8269	0.5608	910.4	638.2
8	-4.288	-4.579	409.1	533.3	409.1	422.6	0.0	322.0	0.0	37.3	0.3713	0.4664	841.9	830.1	0.8496	0.5803	936.0	660.9
9	-8.313	-8.009	401.0	542.8	401.0	431.5	0.0	328.7	0.0	37.3	0.3638	0.4748	927.5	904.1	0.9168	0.6294	1010.5	719.5
10	-9.769	-9.202	396.9	546.0	396.9	430.8	0.0	335.4	0.0	37.9	0.3600	0.4767	956.1	928.8	0.9389	0.6402	1035.2	733.2
11	-11.119	-10.410	392.2	534.0	392.2	414.6	0.0	336.5	0.0	39.0	0.3556	0.4651	984.6	953.4	0.9610	0.6474	1059.9	743.2

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	O-FAC	OMEGA-B	LOSS-P	PO2/	EFF-P	EFF-A	B-1	B-2	VB-1	VB-2	PC/PO
DEGREE	DEGREE	DEGREE	DEGREE					TOTAL	TOTAL	P01	TOT	TOT	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	3.08	7.69	15.52	61.90	26.99	33.37	0.4917	0.0238	0.0051	1.3848	98.81	98.78	49.47	-12.43	-440.2	94.0	1.3848
2	3.10	7.48	16.15	54.46	27.49	34.65	0.5067	0.0041	0.0009	1.3779	99.78	99.80	51.00	-3.45	-474.7	26.4	1.3779
3	3.38	7.49	16.53	47.39	27.97	36.11	0.4991	-0.0258	-0.0061	1.3729	101.65	101.76	52.39	5.00	-508.5	-39.5	1.3729
4	4.53	8.00	13.66	32.70	29.02	37.22	0.4865	-0.0277	-0.0068	1.3554	102.30	102.43	56.04	23.34	-605.4	-196.6	1.3554
5	5.91	8.60	11.73	18.43	29.40	32.97	0.4899	0.0721	0.0161	1.3082	92.04	91.76	60.43	42.00	-726.3	-361.1	1.3082
6	6.41	8.69	10.24	14.76	29.36	33.20	0.4499	0.0648	0.0138	1.3028	92.07	91.81	62.35	47.58	-784.4	-439.5	1.3028
7	6.65	8.75	8.54	14.37	29.31	34.88	0.4145	0.0347	0.0074	1.3095	95.90	95.36	63.23	48.86	-813.2	-480.4	1.3095
8	6.88	8.83	7.42	13.82	29.23	35.11	0.4071	0.0423	0.0090	1.3123	94.37	94.18	64.09	50.28	-841.9	-508.2	1.3123
9	7.57	9.00	6.29	13.54	28.73	35.81	0.4019	0.0841	0.0179	1.3280	88.49	88.05	66.62	53.09	-927.5	-575.4	1.3280
10	7.77	9.07	6.97	13.49	28.47	35.62	0.4074	0.1078	0.0229	1.3289	85.26	84.68	67.45	53.97	-956.1	-593.3	1.3289
11	7.93	9.08	9.67	12.25	28.18	34.14	0.4141	0.1368	0.0282	1.3203	81.00	80.27	68.27	56.01	-984.6	-616.9	1.3203

TO/TO PO/PO EFF-AD EFF-P WCI/A1 T02/T01 P02/P01 EFF-AD EFF-P
INLET INLET INLET INLET LBM/SEC ROTOR ROTOR
% SQFT % %
1.0915 1.3321 93.32 93.56 27.78 1.0915 1.3321 93.32 93.56

STATOR 1

SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	VO-1	VO-2	B-1	B-2	M-1	M-2	PO/PO	TO/TO	PO/PO	T02/T01
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			INLET	INLET	INLET	STAGE T01
1	17.835	14.651	742.3	532.9	449.6	531.9	590.7	33.0	52.9	3.5	0.6615	0.4651	1.3397	1.0986	1.3397	1.0986
2	15.214	12.705	717.3	532.9	459.9	531.5	550.5	37.9	50.2	4.0	0.6382	0.4657	1.3431	1.0959	1.3431	1.0959
3	12.916	10.898	696.2	537.3	472.4	535.9	511.4	38.8	47.2	4.1	0.6188	0.4704	1.3489	1.0929	1.3489	1.0929
4	7.426	5.955	642.9	519.5	475.4	519.0	432.7	22.0	42.2	2.4	0.5694	0.4551	1.3365	1.0886	1.3365	1.0886
5	1.330	-0.365	560.5	475.7	421.3	475.7	369.7	5.9	41.2	0.7	0.4931	0.4157	1.3014	1.0869	1.3014	1.0869
6	-1.461	-3.135	542.0	467.9	421.0	467.9	341.4	-0.4	39.0	-0.0	0.4764	0.4090	1.2938	1.0854	1.2938	1.0854
7	-2.581	-4.202	545.5	475.1	437.4	475.1	325.9	-1.5	36.7	-0.2	0.4799	0.4156	1.2977	1.0842	1.2977	1.0842
8	-3.549	-5.085	545.7	479.9	439.6	479.9	323.3	-3.8	36.4	-0.5	0.4797	0.4196	1.3004	1.0860	1.3004	1.0860
9	-6.271	-7.355	557.7	502.6	448.9	502.6	330.9	3.3	36.5	0.4	0.4885	0.4383	1.3169	1.0954	1.3169	1.0954
10	-7.163	-8.012	561.1	505.0	448.0	504.9	337.8	9.7	37.1	1.1	0.4905	0.4395	1.3185	1.1000	1.3185	1.1000
11	-8.137	-8.624	549.9	495.1	432.9	494.9	339.1	14.1	38.2	1.6	0.4796	0.4299	1.3116	1.1030	1.3116	1.1030

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	O-FAC	OMEGA-B	LOSS-P	PO2/	EFF-P	EFF-A	EFF-P	EFF-A	EFF-P
DEGREE	DEGREE	DEGREE	DEGREE					TOTAL	TOTAL	P01	STAGE-ST	TOT-INLET	TOT-INLET	TOT-STG	TOT-STG
1	-4.69	-2.58	10.84	49.35	35.13	44.62	0.4272	0.1272	0.0260	0.9677	77.27	88.45	88.89	88.89	88.89
2	-5.68	-3.28	10.26	46.13	36.35	44.80	0.4004	0.1041	0.0221	0.9751	79.71	91.81	92.11	91.81	92.11
3	-7.28	-4.49	9.50	43.14	37.72	45.39	0.3700	0.0750	0.0165	0.9830	83.73	96.16	96.29	96.16	96.29
4	-9.76	-6.04	8.69	39.83	38.67	44.03	0.3421	0.0644	0.0157	0.9873	83.30	97.62	97.62	97.62	97.62
5	-9.26	-4.22	7.02	40.53	34.43	40.01	0.3262	0.0319	0.0087	0.9952	89.38	90.01	90.34	90.01	90.34
6	-10.97	-5.36	4.31	39.10	34.58	39.29	0.3172	0.0528	0.0151	0.9924	80.97	89.56	89.90	89.56	89.90
7	-13.09	-7.21	4.21	36.89	36.11	39.94	0.3046	0.0637	0.0186	0.9907	75.80	91.82	92.09	91.82	92.09
8	-13.23	-7.09	3.58	36.82	36.31	40.30	0.2995	0.0638	0.0189	0.9907	74.26	90.70	91.00	90.70	91.00
9	-13.14	-6.26	5.93	36.10	36.98	42.05	0.2832	0.0456	0.0142	0.9931	77.75	85.01	86.32	85.01	86.32
10	-12.82	-5.77	7.89	36.00	36.80	42.09	0.2871	0.0518	0.0164	0.9921	75.20	82.25	82.90	82.25	82.90
11	-12.43	-5.28	9.96	36.95	35.41	41.10	0.2913	0.0452	0.0145	0.9934	78.16	78.28	79.07	78.28	79.07
WCI/A1 WCI/A1 TO/TO PO/PO EFF-AD EFF-P T02/T01 P02/P01 EFF-AD EFF-P															
RPM LBM/SEC INLET INLET INLET INLET INLET STAGE TOT-STG															
7489 122.30 1.0915 1.3178 89.67 90.04 1.0915 0.9893 89.67 233.01															

ROTOR 2

SL	EPLSI-1		EPLSI-2		V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	V0-1 FT/SEC	V0-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	M-1	M-2	RUN NO 13, SPEED CODE 70, POINT NO 1		V*-1 FT/SEC	V*-2 FT/SEC
	DEGREE	DEGREE	U-1 FT/SEC	U-2 FT/SEC											M*-1	M*-2		
1	11.506	11.080	584.8	885.0	584.0	687.5	32.2	557.3	3.1	38.9	0.5127	0.7641	584.0	612.5	0.7044	0.5955	803.5	689.7
2	10.579	9.816	589.8	881.9	588.6	690.6	37.0	548.5	3.6	36.8	0.5267	0.7590	617.5	638.7	0.7326	0.6150	832.3	710.1
3	9.484	8.613	598.4	876.3	597.2	701.1	37.9	525.8	4.1	30.8	0.5209	0.7126	670.4	681.2	0.7733	0.6521	877.4	752.1
4	5.346	5.117	591.0	821.9	590.6	705.8	21.5	421.2	0.6	24.4	0.4780	0.5828	743.2	742.7	0.8053	0.6642	916.6	770.1
5	-1.391	0.058	544.1	675.7	544.1	615.2	5.5	279.5	0.6	22.8	0.4625	0.4953	780.3	775.5	0.8270	0.6585	941.9	766.4
6	-4.191	-2.182	526.6	576.4	526.8	531.4	-0.5	223.2	-0.1	20.4	0.4637	0.4836	799.1	792.4	0.8425	0.6847	959.2	796.0
7	-5.038	-3.033	528.0	562.2	528.0	527.0	-1.8	195.8	-0.4	17.4	0.4653	0.4943	817.9	809.7	0.8582	0.7247	977.7	840.5
8	-5.727	-3.893	530.1	573.3	530.1	547.0	-3.6	171.5	-0.4	14.1	0.4791	0.5180	875.2	863.3	0.9005	0.7966	1029.2	923.2
9	-8.166	-6.924	547.5	600.3	547.5	582.1	3.8	146.8	1.1	14.0	0.4773	0.5129	894.5	881.7	0.9078	0.8072	1039.7	937.0
10	-8.934	-8.044	546.7	595.4	546.6	577.7	10.1	144.0	1.5	14.1	0.4656	0.4742	913.8	900.4	0.9113	0.8016	1046.2	933.9
11	-9.422	-9.065	534.5	552.4	534.3	535.6	14.3	135.4										

SL	INCS DEGREE	INCH DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-0		LSS-P	P02/ P01	XEFF-P	XEFF-A	B*-1 DEGREE	B*-2 DEGREE	V0*-1 FT/SEC	V0*-2 FT/SEC	PC/PC INLET
								TOTAL	TOTAL									
1	-6.18	-1.87	24.98	38.72	47.91	57.73	0.2945	0.1910	0.0434	1.2983	82.75	82.13	43.30	4.58	-551.8	-55.3	1.7394	
2	-6.24	-1.79	20.15	37.38	48.42	58.75	0.2872	0.1609	0.0374	1.3068	85.10	84.55	43.71	6.33	-563.5	-76.9	1.7554	
3	-6.21	-1.64	16.65	35.02	49.26	60.50	0.2897	0.1224	0.0290	1.3107	88.00	87.56	44.14	9.12	-579.7	-112.9	1.7682	
4	-4.006	0.74	10.65	27.48	48.58	62.38	0.2815	0.0537	0.0081	1.2949	96.10	95.98	47.69	20.21	-648.8	-259.9	1.7318	
5	0.13	4.71	8.76	16.62	44.53	53.77	0.2460	0.0727	0.0165	1.1966	86.40	86.13	53.60	36.98	-737.7	-463.2	1.5547	
6	1.66	6.00	9.88	9.95	43.27	45.72	0.2602	0.1715	0.0353	1.1166	62.38	61.87	56.03	46.09	-780.8	-552.2	1.4467	
7	1.77	5.85	9.26	8.13	43.50	45.27	0.2368	0.1613	0.0326	1.1013	61.00	60.52	56.64	48.52	-800.9	-556.6	1.4300	
8	1.81	5.62	7.03	7.85	43.67	47.05	0.1991	0.1167	0.0238	1.1024	68.20	67.82	57.20	49.35	-821.6	-638.2	1.4351	
9	1.05	3.73	3.73	7.03	44.98	49.65	0.1518	0.0769	0.0170	1.0957	73.85	73.57	57.86	50.83	-871.5	-716.5	1.4432	
10	1.07	3.25	5.16	6.41	44.81	48.94	0.1453	0.0794	0.0179	1.0879	71.07	70.80	58.27	51.85	-884.4	-737.7	1.4335	
11	1.73	3.43	9.27	43.69	44.91	44.91	0.1511	0.1133	0.0246	1.0620	95.13	54.83	59.25	54.93	-899.5	-765.0	1.3928	

TOT/INLET	PO/PO INLET	EFF-AD INLET	EFF-P INLET	MC1/A1 LBM/SEC % SOFT	T02/T01	P02/P01	EFF-AD ROTOR %	EFF-P ROTOR %
1.1560	1.5622	87.13	87.89	34.67	1.0590	1.1855	84.28	84.82

STATOR 2

SL	EPLSI-1		EPLSI-2		V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	V0-1 FT/SEC	V0-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	M-1	M-2	RUN NO 13, SPEED CODE 70, POINT NO 1			
	DEGREE	DEGREE	PO/PO INLET	T02/T01 INLET											XEFF-A TOT-INLET	XEFF-P TOT-INLET	XEFF-A TOT-STG	XEFF-P TOT-STG
1	8.703	1.005	922.0	859.1	738.8	853.4	551.7	-99.4	37.0	-6.6	0.8001	0.7392	1.5101	1.2022	1.1274	1.0941		
2	7.746	1.097	916.4	873.8	737.6	868.2	543.8	-98.7	36.6	-6.5	0.7958	0.7540	1.5379	1.1998	1.1461	1.0941		
3	6.880	1.114	909.0	891.8	743.9	886.1	522.4	-101.2	35.3	-6.5	0.7906	0.7731	1.5731	1.1951	1.1677	1.0927		
4	4.891	0.930	851.7	899.2	740.7	892.8	420.6	-107.1	29.7	-6.8	0.7412	0.7863	1.6127	1.1788	1.2038	1.0826		
5	2.704	0.192	707.7	813.9	649.7	805.4	280.7	-110.0	23.4	-7.8	0.6123	0.7118	1.5273	1.1553	1.1732	1.0629		
6	0.935	-0.352	610.4	734.4	567.7	726.8	224.1	-105.3	21.5	-8.2	0.5259	0.6401	1.4429	1.1425	1.1149	1.0528		
7	-0.246	-0.676	593.5	701.8	565.0	694.3	196.7	-102.4	19.3	-8.4	0.5119	0.6113	1.4110	1.1364	1.0871	1.0479		
8	-1.300	-0.912	603.8	685.7	578.8	678.5	172.0	-98.9	16.5	-8.3	0.5219	0.5974	1.3956	1.1323	1.0727	1.0423		
9	-3.625	-1.119	633.4	689.4	616.0	685.9	147.5	-88.7	13.5	-5.7	0.5482	0.6000	1.3940	1.1353	1.0585	1.0360		
10	-4.395	-1.163	633.0	691.4	616.2	688.6	144.9	-81.5	13.2	-5.1	0.5472	0.6011	1.3933	1.1381	1.0572	1.0344		
11	-5.411	-1.162	597.5	642.1	581.8	639.8	136.4	-53.7	13.2	-4.8	0.5149	0.5555	1.3435	1.1279	1.0243	1.0316		

SL	INCS DEGREE	INCH DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-0		LSS-P	P02/ P01	XEFF-P	XEFF-A STG	B*-1 DEGREE	B*-2 DEGREE	V0*-1 FT/SEC	V0*-2 FT/SEC	PC/PC INLET
								TOTAL	TOTAL									
1	-8.93	-7.37	7.68	43.65	60.49	63.25	0.2281	0.3802	0.0893	0.8689	134.93	61.78	63.89	36.98	38.00			
2	-8.30	-6.28	7.27	43.10	61.25	65.01	0.2085	0.3554	0.0813	0.8785	220.14	65.47	67.46	42.16	43.22			
3	-8.89	-6.38	6.83	41.77	62.80	67.25	0.1853	0.3234	0.0754	0.8899	499.82	70.79	72.56	48.80	49.88			
4	-13.38	-9.51	5.98	36.52	44.27	69.79	0.1121	0.2381	0.0587	0.9259	284.72	81.80	82.96	65.79	66.64			
5	-18.84	-13.53	5.04	31.13	55.96	64.02	0.0323	0.1487	0.0394	0.9645	152.98	82.75	83.72	73.95	74.48			
6	-20.38	-14.59	4.48	29.75	48.18	57.64	0.0241	0.0825	0.0226	0.9848	120.14	77.50	78.60	59.56	60.12			
7	-22.40	-16.41	4.29	27.71	47.46	55.05	0.0414	0.0742	0.0206	0.9878	118.38	75.79	76.91	50.29	50.82			
8	-25.02	-18.81	4.32	24.81	49.12	53.82	0.0092	0.1601	0.0450	0.9729	150.85	75.51	76.81	47.79	48.24			
9	-27.84	-21.14	6.96	19.17	51.75	54.13	0.0115	0.1854	0.0541	0.9658	188.30	73.59	74.77	45.45	45.82			
10	-28.72	-21.84	8.18	18.33	51.33	54.14	0.0060	0.1572	0.0463	0.9711	173.82	71.99	73.24	46.38	46.70			
11	-30.01	-22.91	9.64	18.02	47.86	49.73	0.0205	0.2152	0.0640	0.9645	230.31	63.83	65.27	21.78	21.97			

NCORR INLET RPM	MCORR INLET LBM/SEC	T02/T01	PO/PO INLET	EFF-AD INLET	EFF-P INLET	T02/T01	P02/P01	EFF-AD STAGE %	EFF-P TOT-STG %
7489	122.30	1.1560	1.4782	75.72	77.00	1.0590	0.9462	56.46	-161.25

TABLE XXX (b) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

70% OF DESIGN SPEED
STATOR 1 (beta*_des. - beta*_act.) = -5.0
STATOR 2 (beta*_des. - beta*_act.) = +2.5

U. S. CUSTOMARY UNITS

ROTOR 1

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, IS, SPEED CODE, T0, POINT NO, V*-1, V*-2. Contains performance data for Rotor 1 at various points.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, P02/TOT, %EFF-P, %EFF-A, B*-1, B*-2, V0*-1, V0*-2, PO/PO, INLET. Includes summary statistics for Rotor 1.

STATOR 1

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, IS, SPEED CODE, T0, POINT NO, PO/PO, INLET, STAGE, TOT. Contains performance data for Stator 1 at various points.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, P02/TOT, %EFF-P, %EFF-A, B*-1, B*-2, V0*-1, V0*-2, PO/PO, INLET, STAGE, TOT. Includes summary statistics for Stator 1.

ROTOR 2

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, R-1, R-2, M-1, M-2, RUN NO 13, SPEED CODE TG, POINT NO 2, U-1, U-2, M'-1, M'-2, V'-1, V'-2. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, O-FAC, OMEGA-B, LDSS-P, PO2/POL, %EFF-P, %EFF-A, B'-1, B'-2, V0'-1, V0'-2, PO/PO. Rows 1-11.

Summary table with columns: TO2/TO1, PO2/PO1, EFF-AD, EFF-P, RQTOR, RDTOR. Values: 1.1749, 1.6489, 87.79, 88.60, 32.81, 1.0680, 1.2414, 93.58, 93.74.

STATOR 2

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, R-1, R-2, M-1, M-2, PO/PO, TO2/TO1, PO/PO, INLET, STAGE, TO1, TO2. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, O-FAC, OMEGA-B, LDSS-P, PO2/POL, %EFF-P, %EFF-A, %EFF-P, %EFF-A, %EFF-P. Rows 1-11.

Summary table with columns: NCORR, WCORR, TO2/TO1, PO2/PO1, EFF-AD, EFF-P, TO2/TO1, PO2/PO1, EFF-AD, EFF-P. Values: 74.84, 116.20, 1.1749, 1.6180, 84.25, 85.26, 1.0680, 0.9813, 85.1829277-27.

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TABLE XXX (c) — OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

70% OF DESIGN SPEED

STATOR 1 (β_{des.} - β_{act.}) = -5.0°

STATOR 2 (β_{des.} - β_{act.}) = +2.5°

U. S. CUSTOMARY UNITS

ROTOR 1

SL	EPSI-1 DEGREE	EPSI-2 DEGREE	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	V0-1 FT/SEC	V0-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	M-1	M-2	U-1 FT/SEC	U-2 FT/SEC	M*-1	M*-2	V*-1 FT/SEC	V*-2 FT/SEC
1	16.517	18.081	330.3	732.5	330.3	405.4	0.0	610.1	0.0	56.4	0.2984	0.6517	439.4	508.7	0.4966	0.3718	549.7	417.9
2	13.896	15.521	337.7	706.0	337.7	405.8	0.0	577.7	0.0	54.9	0.3052	0.6264	473.5	533.4	0.5259	0.3622	581.9	408.2
3	11.553	13.164	344.7	679.2	344.7	401.6	0.0	547.7	0.0	53.7	0.3117	0.6011	507.6	558.0	0.5548	0.3556	613.6	401.8
4	5.229	7.123	355.8	628.9	355.8	409.7	0.0	477.1	0.0	49.3	0.3255	0.5541	604.3	631.8	0.6364	0.3859	703.3	438.0
5	-1.012	0.758	364.0	556.3	364.0	364.0	0.0	420.6	0.0	49.1	0.3295	0.4865	725.1	730.3	0.7343	0.4179	811.3	477.9
6	-3.126	-1.887	362.5	545.0	362.5	375.5	0.0	395.0	0.0	46.5	0.3281	0.4761	783.1	779.5	0.7810	0.4695	863.0	537.4
7	-4.460	-3.158	361.2	556.0	361.2	396.3	0.0	390.0	0.0	44.6	0.3269	0.4858	811.8	804.1	0.8041	0.5007	888.5	573.1
8	-6.032	-4.440	359.0	556.5	359.0	397.3	0.0	389.6	0.0	44.5	0.3249	0.4855	840.4	828.7	0.8270	0.5166	913.9	592.2
9	-10.167	-8.233	348.4	545.8	348.4	363.9	0.0	406.8	0.0	48.2	0.3151	0.4725	926.0	902.6	0.8947	0.5325	989.4	615.6
10	-11.155	-9.435	344.2	541.7	344.2	349.6	0.0	413.8	0.0	49.8	0.3112	0.4678	954.5	927.2	0.9173	0.5363	1014.6	621.1
11	-11.831	-10.571	340.2	538.9	340.2	333.3	0.0	423.5	0.0	51.7	0.3075	0.4639	983.0	951.8	0.9402	0.5376	1040.2	624.4

SL	INCS DEGREE	INCM DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B TOTAL	LOSS-P TOTAL	PO2/PO1	%EFF-P TOT	%EFF-A TOT	0*-1 DEGREE	0*-2 DEGREE	V0*-1 FT/SEC	V0*-2 FT/SEC	PO/PO INLET
1	6.45	11.05	13.92	66.87	24.17	31.91	0.5040	0.0318	0.0068	1.3876	98.54	98.51	52.83	-14.04	-439.4	101.4	1.3876
2	6.45	10.74	13.38	60.49	24.66	32.30	0.5431	0.0388	0.0089	1.3819	97.98	97.92	54.26	-6.23	-473.5	44.4	1.3819
3	6.58	10.68	12.99	54.13	25.13	32.26	0.5718	0.0547	0.0131	1.3733	96.85	96.73	55.58	1.46	-507.6	-10.2	1.3733
4	7.59	11.06	10.97	38.44	26.11	33.59	0.5655	0.0494	0.0123	1.3649	96.24	96.10	59.09	20.66	-604.3	-154.8	1.3649
5	8.82	11.50	10.10	22.96	26.38	30.05	0.5706	0.1377	0.0315	1.3312	86.94	86.43	63.33	40.38	-725.1	-309.7	1.3312
6	9.25	11.53	8.34	19.50	26.29	31.17	0.5243	0.1244	0.0275	1.3327	87.05	86.54	65.19	45.68	-783.1	-384.5	1.3327
7	9.48	11.58	5.96	19.79	26.20	32.99	0.4993	0.1095	0.0246	1.3448	88.24	87.77	66.06	46.27	-811.8	-414.0	1.3448
8	9.72	11.67	5.02	19.06	26.06	33.06	0.4952	0.1227	0.0273	1.3475	86.49	85.94	66.94	47.88	-840.4	-439.1	1.3475
9	10.43	11.86	6.93	15.76	25.37	29.98	0.5250	0.2148	0.0451	1.3432	75.71	74.71	69.48	53.72	-926.0	-495.8	1.3432
10	10.57	11.86	8.71	14.54	25.09	28.70	0.5351	0.2436	0.0497	1.3419	72.39	71.26	70.25	55.71	-954.5	-513.4	1.3419
11	10.60	11.76	11.34	13.26	24.83	27.25	0.5484	0.2744	0.0541	1.3419	69.05	67.77	70.94	57.68	-983.0	-528.3	1.3419

TO/T01 1.1053 PO/PO1 1.3507 EFF-AD 85.22 EFF-P 85.60

INLET INLET INLET INLET INLET INLET

% SQFT %

STATOR 1

SL	EPSI-1 DEGREE	EPSI-2 DEGREE	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	V0-1 FT/SEC	V0-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	M-1	M-2	U-1 FT/SEC	U-2 FT/SEC	M*-1	M*-2	V*-1 FT/SEC	V*-2 FT/SEC
1	16.124	14.852	732.5	463.1	424.8	462.4	597.2	25.1	54.8	3.1	0.6521	0.4019	1.3433	1.0996	1.3433	1.0996	1.0996	1.0996
2	15.764	13.073	708.9	463.5	425.0	462.1	567.4	35.5	53.3	4.4	0.6292	0.4024	1.3466	1.0989	1.3466	1.0989	1.0989	1.0989
3	13.556	11.374	684.3	465.3	420.9	463.3	539.5	42.5	52.1	5.2	0.6060	0.4041	1.3499	1.0981	1.3499	1.0981	1.0981	1.0981
4	8.087	6.767	637.6	454.7	427.3	453.7	473.2	29.6	47.9	3.7	0.5623	0.3949	1.3452	1.0968	1.3452	1.0968	1.0968	1.0968
5	2.207	1.307	566.9	417.0	380.9	416.9	419.9	8.6	47.8	1.2	0.4963	0.3609	1.3212	1.0986	1.3212	1.0986	1.0986	1.0986
6	-0.409	-1.091	556.2	416.0	391.1	416.0	395.4	3.4	45.3	0.5	0.4863	0.3601	1.3206	1.0988	1.3206	1.0988	1.0988	1.0988
7	-1.415	-2.057	566.9	429.6	410.6	429.6	390.9	8.8	43.6	1.2	0.4957	0.3719	1.3288	1.1005	1.3288	1.1005	1.1005	1.1005
8	-2.317	-2.929	567.4	437.1	411.4	437.0	390.8	9.8	43.5	1.3	0.4955	0.3781	1.3342	1.1030	1.3342	1.1030	1.1030	1.1030
9	-3.312	-5.707	557.6	426.3	378.9	426.2	409.1	10.8	47.2	1.5	0.4833	0.3661	1.3312	1.1171	1.3312	1.1171	1.1171	1.1171
10	-6.526	-6.781	553.9	420.8	365.1	420.4	416.5	17.1	48.8	2.3	0.4787	0.3604	1.3291	1.1223	1.3291	1.1223	1.1223	1.1223
11	-7.857	-7.941	551.3	412.7	348.9	412.3	426.8	17.7	50.8	2.5	0.4750	0.3521	1.3252	1.1294	1.3252	1.1294	1.1294	1.1294

SL	INCS DEGREE	INCM DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B TOTAL	LOSS-P TOTAL	PO2/PO1	%EFF-P STATC-ST	%EFF-A TOT-INLET	%EFF-P TOT-INLET	%EFF-A TOT-INLET	%EFF-P TOT-STG	%EFF-A TOT-STG
1	-2.79	-0.68	10.41	51.67	33.42	39.90	0.5205	0.1282	0.0262	0.9681	81.41	88.35	88.80	88.35	88.80	
2	-2.56	-0.16	10.98	48.92	33.77	39.99	0.4990	0.1086	0.0230	0.9745	83.40	89.77	90.16	89.77	90.16	
3	-2.44	0.35	10.60	46.88	33.72	40.19	0.4744	0.0771	0.0169	0.9830	87.37	91.29	91.42	91.29	91.62	
4	-4.10	-0.38	7.99	44.19	34.88	39.41	0.4535	0.0745	0.0181	0.9856	86.43	91.41	91.73	91.41	91.73	
5	-2.73	2.31	5.90	46.58	31.30	35.95	0.4622	0.0489	0.0134	0.9924	90.21	84.05	84.63	84.05	84.63	
6	-4.71	0.91	4.83	44.85	32.32	35.87	0.4525	0.0599	0.0160	0.9916	88.22	83.79	84.38	83.79	84.38	
7	-6.21	-0.33	5.56	42.42	34.03	37.05	0.4385	0.0746	0.0218	0.9885	83.86	84.26	84.85	84.26	84.85	
8	-6.06	0.09	5.71	42.26	34.07	37.67	0.4290	0.0641	0.0190	0.9901	85.51	83.43	84.06	83.43	84.06	
9	-2.39	4.49	7.00	45.77	31.07	36.35	0.4595	0.0620	0.0193	0.9908	86.25	72.77	73.82	72.77	73.82	
10	-1.11	5.94	9.11	46.49	29.82	35.71	0.4696	0.0654	0.0207	0.9905	85.70	69.33	70.51	69.33	70.51	
11	0.21	7.36	10.79	48.36	28.39	34.80	0.4922	0.0866	0.0277	0.9876	81.74	64.78	66.12	64.78	66.12	

NCORR INLET 747.7 NCORR INLET 109.10 TO/T01 1.1053 PO/PO1 1.3338

EFF-AD 81.49 EFF-P 82.20 T02/T01 1.1053 PO2/PO1 0.9874

EFF-AD 81.49 EFF-P 176.79

ROTOR 2

RUN NO 13, SPEED CODE 70, POINT NO 3																		
SL	EP1-1	EP1-2	V-1	V-2	VM-1	VM-2	VO-1	VO-2	B-1	B-2	M-1	M-2	U-1	U-2	PO-1	PO-2	V+1	V+2
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			FT/SEC	FT/SEC			FT/SEC	FT/SEC
1	11.590	10.973	497.9	821.3	497.3	575.4	24.4	586.1	2.8	45.4	0.4332	0.7010	583.0	611.5	0.6507	0.4916	747.9	575.9
2	10.734	9.620	502.9	807.0	501.7	567.7	34.6	573.6	3.9	45.2	0.4378	0.6886	599.5	524.3	0.6578	0.4863	755.5	570.0
3	9.699	8.346	508.6	790.4	506.9	572.4	41.6	545.0	4.7	43.5	0.4431	0.6748	616.5	637.6	0.6678	0.4951	766.4	579.9
4	5.802	4.801	504.6	707.6	503.7	550.9	29.2	444.1	3.3	38.8	0.4398	0.6025	669.2	680.0	0.7099	0.5103	814.5	599.3
5	0.265	0.413	466.1	592.3	466.1	485.7	8.6	339.0	1.1	34.9	0.4048	0.5012	741.9	741.5	0.7546	0.5338	868.9	630.8
6	-2.153	-1.608	461.0	544.2	461.0	451.0	3.4	304.5	0.4	34.0	0.4001	0.4594	779.0	774.2	0.7832	0.5497	902.2	651.1
7	-3.032	-2.441	471.9	535.6	471.8	449.2	8.8	291.6	1.1	32.9	0.4096	0.4521	757.7	791.0	0.7979	0.5671	919.2	671.8
8	-3.800	-3.218	479.1	539.9	479.0	459.6	9.9	285.4	1.2	31.6	0.4156	0.4557	816.5	808.3	0.8138	0.5888	938.1	697.7
9	-6.519	-5.995	474.1	552.4	474.0	476.1	10.6	280.1	1.3	30.3	0.4085	0.4630	873.7	861.8	0.8483	0.6302	984.7	751.8
10	-7.551	-7.165	470.2	551.9	469.8	469.5	17.3	290.1	2.1	31.6	0.4040	0.4611	893.0	880.2	0.8539	0.6300	993.7	754.0
11	-8.512	-8.427	462.9	538.4	462.6	457.8	18.0	283.3	2.2	31.6	0.3962	0.4480	912.2	898.9	0.8618	0.6393	1006.8	767.1

SL	INCS	INCH	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-8	LOSS-P	PO2/	VEFF-P	VEFF-A	B*-1	B*-2	VB*-1	VB*-2	PC/PD
	DEGREE	DEGREE	DEGREE	DEGREE				TOTAL	TOTAL	PO1	TOT	TOT	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	-1.23	3.08	22.92	45.73	42.37	52.54	0.4056	0.1136	0.0259	1.3593	91.62	91.27	48.25	2.52	-558.6	-25.4	1.8262
2	-1.59	2.86	18.90	43.29	42.79	52.33	0.4160	0.1002	0.0233	1.3548	92.34	92.03	48.37	5.08	-564.9	-50.7	1.8246
3	-1.75	2.83	16.69	39.45	43.27	53.35	0.4042	0.0615	0.0145	1.3489	95.03	94.84	48.61	9.16	-574.8	-92.6	1.8209
4	0.07	4.86	13.61	28.45	42.97	52.26	0.3965	0.0409	0.0097	1.3057	95.79	95.66	51.82	23.17	-640.0	-235.9	1.7557
5	4.09	8.67	11.42	17.92	39.54	46.19	0.3826	0.0521	0.0114	1.2532	93.02	92.83	57.56	39.65	-733.4	-402.5	1.6555
6	4.89	9.23	9.93	13.13	39.16	42.83	0.3778	0.0851	0.0175	1.2230	87.42	87.09	59.26	46.14	-775.6	-469.6	1.6160
7	4.22	8.30	8.73	11.10	40.12	42.70	0.3629	0.0834	0.0170	1.2118	86.83	86.50	59.09	47.99	-788.9	-499.5	1.6104
8	3.88	7.69	6.41	10.53	40.70	43.69	0.3470	0.0753	0.0156	1.2108	87.60	87.29	59.26	48.73	-806.7	-524.9	1.6154
9	4.32	7.00	3.48	10.56	39.80	44.78	0.3311	0.0678	0.0150	1.2222	88.54	88.24	61.13	50.57	-863.1	-581.8	1.6273
10	4.48	6.66	4.68	10.33	39.28	43.92	0.3396	0.0794	0.0180	1.2236	86.76	86.41	61.68	51.35	-875.7	-590.1	1.6268
11	5.04	6.73	7.58	9.31	38.42	42.51	0.3363	0.0801	0.0181	1.2188	86.24	85.88	62.55	53.24	-894.2	-615.6	1.6193

TO/TO	PO/PO	EFF-AD	EFF-P	WCI/A1	TO2/T01	PO2/PO1	EFF-AD	EFF-P
INLET	INLET	INLET	INLET	LB/SEC			%	%
1.1882	1.6829	85.15	86.18	30.75	1.0750	1.2618	91.42	91.67

STATOR 2

RUN NO 13, SPEED CODE 70, POINT NO 3																	
SL	EP1-1	EP1-2	V-1	V-2	VM-1	VM-2	VO-1	VO-2	B-1	B-2	M-1	M-2	PO/PO	TO/TO	PO/PO	TO2/	TC2/
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			INLET	INLET	INLET	STAGE	TOT
1	8.560	0.775	844.7	664.0	813.9	663.7	580.2	-17.3	43.7	-1.6	0.7230	0.5573	1.7459	1.2100	1.2998	1.1004	
2	7.432	0.617	829.2	670.4	603.5	670.1	588.7	-18.7	43.5	-1.6	0.7094	0.5636	1.7577	1.2075	1.3056	1.0988	
3	6.358	0.359	811.7	684.7	605.0	684.1	541.1	-28.9	42.0	-2.4	0.6947	0.5779	1.7797	1.2020	1.3184	1.0946	
4	3.800	-0.434	727.6	638.8	577.5	637.6	442.5	-39.9	37.5	-3.6	0.6208	0.5402	1.7377	1.1878	1.2918	1.0830	
5	0.916	-1.059	611.4	543.2	509.0	541.1	338.8	-47.4	33.6	-5.0	0.5182	0.4578	1.6469	1.1775	1.2465	1.0718	
6	-0.574	-1.192	563.5	498.9	474.0	496.5	304.7	-48.7	32.7	-5.6	0.4765	0.4197	1.6092	1.1737	1.2186	1.0682	
7	-1.384	-1.220	553.0	493.5	472.0	491.0	291.9	-48.9	31.7	-5.7	0.4692	0.4153	1.6044	1.1721	1.2078	1.0652	
8	-2.158	-1.235	555.5	499.7	482.0	497.2	284.0	-49.3	30.5	-5.7	0.4729	0.4205	1.6080	1.1733	1.2052	1.0642	
9	-4.182	-1.285	575.9	520.8	502.5	518.9	281.4	-44.3	29.3	-4.9	0.4837	0.4356	1.6166	1.1910	1.2142	1.0667	
10	-4.903	-1.295	578.7	519.9	494.8	518.6	291.8	-36.7	30.3	-4.0	0.4846	0.4334	1.6123	1.1985	1.2127	1.0686	
11	-5.766	-1.228	570.2	499.3	493.7	498.2	285.3	-32.9	30.1	-3.8	0.4756	0.4143	1.5925	1.2057	1.2016	1.0676	

SL	INCS	INCH	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-8	LOSS-P	PO2/	VEFF-P	VEFF-A	VEFF-P	VEFF-A	VEFF-P	VEFF-A	VEFF-P
	DEGREE	DEGREE	DEGREE	DEGREE				TOTAL	TOTAL	PO1	STATC-ST	TOT-INLET	TOT-INLET	TOT-STG	TOT-STG	TOT-STG	TOT-STG
1	-2.30	-0.74	12.83	45.14	55.26	62.99	0.3736	0.1494	0.0337	0.9560	67.34	82.11	83.43	80.01	80.72	78.10	
2	-1.41	0.61	12.15	45.11	54.90	63.95	0.3957	0.1287	0.0296	0.9631	69.12	84.19	85.37	80.01	80.72	84.24	
3	-2.17	0.33	10.93	44.39	53.69	65.90	0.3236	0.0829	0.0194	0.9770	76.23	88.57	89.44	86.75	87.24	91.52	
4	-5.54	-1.67	9.24	41.10	54.23	61.89	0.2904	0.0517	0.0128	0.9881	81.08	90.97	91.63	90.36	91.52	90.62	
5	-8.58	-3.27	7.79	38.64	48.01	52.22	0.2849	0.0394	0.0105	0.9933	83.67	86.27	87.18	90.36	90.62	89.45	
6	-9.19	-3.40	7.13	38.30	44.67	47.74	0.2906	0.0332	0.0091	0.9952	86.16	83.80	84.82	85.07	85.45	85.20	
7	-10.02	-4.03	6.98	37.38	44.67	47.22	0.2834	0.0246	0.0068	0.9966	89.03	83.88	84.99	84.84	85.20	85.45	
8	-11.07	-4.86	6.55	36.14	45.48	47.77	0.2762	0.0308	0.0087	0.9956	85.84	83.84	84.86	85.21	85.45	85.68	
9	-12.03	-5.33	7.80	34.13	46.83	49.08	0.2620	0.0443	0.0130	0.9935	77.71	76.99	78.47	85.32	85.68	82.91	
10	-11.63	-4.75	9.23	34.37	46.25	48.66	0.2703	0.0601	0.0177	0.9911	71.54	73.64	75.32	82.47	82.91	80.05	
11	-13.13	-6.03	10.66	33.88	45.29	46.25	0.2917	0.0980	0.0292	0.9859	61.34	69.08	71.01	79.56	80.05		

NCORR	WGORR	TO/TO	PO/PO	EFF-AD	EFF-P	TO2/T01	PO2/PO1	EFF-AD	EFF-P
INLET	INLET	INLET	INLET	INLET	INLET			%	%
7477.	109.10	1.1882	1.6820	82.95	84.10	1.0750	0.9876	86.35	474.61

ORIGINAL PAGE IS
OF POOR QUALITY

APPENDIX E

TABLE XXX (d) – OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

70% OF DESIGN SPEED
 STATOR 1 ($\beta^*_{des.} - \beta^*_{act.}$) = -6°
 STATOR 2 ($\beta^*_{des.} - \beta^*_{act.}$) = $+2.5^\circ$

U. S. CUSTOMARY UNITS

ROTOR 1

SL	EPS1-1	EPS1-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	U-1	U-2	M-1	M-2	V*1	V*2
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			FT/SEC	FT/SEC			FT/SEC	FT/SEC
1	16.364	18.118	311.5	711.9	311.5	380.8	0.0	601.5	0.0	57.7	0.2811	0.6323	439.6	508.9	0.4862	0.3481	538.7	391.9
2	13.646	15.574	317.7	685.2	317.7	378.5	0.0	571.2	0.0	56.4	0.2868	0.6070	474.0	533.5	0.5151	0.3370	576.6	380.4
3	11.202	13.230	323.4	658.4	323.4	379.6	0.0	537.9	0.0	54.7	0.2921	0.5820	507.8	558.1	0.5437	0.3360	602.0	380.1
4	4.766	7.175	334.6	610.8	334.6	386.1	0.0	473.4	0.0	50.7	0.3026	0.5375	604.5	632.0	0.6245	0.3673	691.1	417.4
5	-1.602	-0.706	337.6	545.2	337.6	340.3	0.0	425.9	0.0	51.4	0.3051	0.4760	725.3	730.5	0.7230	0.3588	800.0	456.7
6	-3.803	-2.022	335.7	535.1	335.7	353.9	0.0	401.3	0.0	48.6	0.3034	0.4667	783.3	779.7	0.7701	0.4519	852.2	518.1
7	-5.174	-3.309	334.2	546.3	334.2	376.8	0.0	395.6	0.0	46.4	0.3020	0.4765	812.0	804.3	0.7935	0.4849	878.1	555.9
8	-6.811	-4.635	331.8	551.1	331.8	378.7	0.0	400.4	0.0	46.6	0.2998	0.4799	840.7	829.0	0.8166	0.4980	903.8	571.9
9	-11.332	-8.520	320.3	547.1	320.3	324.1	0.0	440.7	0.0	53.7	0.2892	0.4716	926.2	902.8	0.8849	0.4865	980.0	564.4
10	-12.180	-9.659	315.8	548.7	315.8	298.5	0.0	460.5	0.0	57.0	0.2850	0.4710	954.8	927.4	0.9078	0.4757	1005.6	554.2
11	-12.420	-10.701	311.6	551.1	311.6	282.9	0.0	472.9	0.0	59.1	0.2815	0.4715	983.2	952.0	0.9310	0.4761	1031.5	556.4

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	O-FAC	OMEGA-0	LCSS-P	P02/	%EFF-P	%EFF-A	B*1	B*2	V0*1	V0*2	PC/P0
	DEGREE	DEGREE	DEGREE	DEGREE				TOTAL	TOTAL	P01	TOT	TOT	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	8.04	12.64	14.28	68.16	22.91	30.39	0.5382	-0.0051	-0.0011	1.3892	100.22	100.26	54.42	-13.68	-439.6	92.7	1.3892
2	8.07	12.37	13.93	61.56	23.32	30.54	0.5795	0.0109	0.0025	1.3837	99.44	95.44	55.89	-5.67	-474.0	37.7	1.3837
3	8.24	12.34	14.57	54.21	23.71	30.91	0.5554	0.0169	0.0040	1.3757	99.05	99.03	57.24	3.04	-507.8	-20.2	1.3757
4	9.35	12.82	12.62	38.55	24.48	32.03	0.5869	0.0292	0.0072	1.3685	97.77	97.70	60.86	22.30	-604.5	-158.7	1.3685
5	10.52	13.20	11.55	23.22	24.65	28.38	0.5942	0.1310	0.0295	1.3399	87.84	87.36	65.04	41.82	-725.3	-304.6	1.3399
6	10.91	13.19	9.59	19.92	24.53	29.65	0.5451	0.1215	0.0263	1.3415	87.71	87.22	66.84	46.93	-783.3	-378.4	1.3415
7	11.11	13.21	7.04	20.54	24.43	31.65	0.5169	0.1065	0.0234	1.3530	88.84	88.38	67.69	47.35	-812.0	-408.8	1.3530
8	11.33	13.29	5.76	19.99	24.27	31.76	0.5176	0.1261	0.0277	1.3582	86.59	86.02	68.55	48.56	-840.7	-428.6	1.3582
9	12.04	13.47	8.18	16.12	23.50	26.76	0.5851	0.2588	0.0527	1.3574	72.74	71.57	71.09	54.67	-926.2	-462.1	1.3574
10	12.16	13.45	10.44	14.43	23.19	24.50	0.6140	0.3043	0.0593	1.3608	68.59	67.23	71.84	57.40	-954.8	-467.0	1.3608
11	12.13	13.28	13.04	13.08	22.93	23.16	0.6286	0.3326	0.0625	1.3661	66.02	64.52	72.47	59.38	-983.2	-479.1	1.3661

TO/TO	PO/PC	EFF-AD	EFF-P	WCI/A1
INLET	INLET	INLET	INLET	LBM/SEC
		%	%	SQFT
1.1084	1.3602	84.83	85.45	23.12

T02/T01	P02/P01	EFF-AD	EFF-P
		ROTOR	ROTOR
		%	%
1.1084	1.3602	84.83	85.45

STATOR 1

SL	EPS1-1	EPS1-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	U-1	U-2	M-1	M-2	V*1	V*2
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			FT/SEC	FT/SEC			FT/SEC	FT/SEC
1	18.182	14.953	711.9	426.2	400.2	425.6	588.9	22.2	56.0	3.0	0.6323	0.3692	1.3446	1.0983	1.3446	1.0983	1.3446	1.0983
2	15.847	13.246	687.8	427.6	397.9	426.2	561.0	34.0	54.8	4.5	0.6094	0.3705	1.3480	1.0979	1.3480	1.0979	1.3480	1.0979
3	13.686	11.619	662.9	430.9	398.4	428.8	529.9	42.1	53.1	5.6	0.5862	0.3737	1.3520	1.0964	1.3520	1.0964	1.3520	1.0964
4	8.461	7.212	618.4	420.2	402.4	419.2	469.5	30.1	49.4	4.1	0.5445	0.3643	1.3477	1.0960	1.3477	1.0960	1.3477	1.0960
5	2.703	1.886	554.0	387.4	355.2	387.2	425.2	12.1	50.1	1.8	0.4841	0.3346	1.3285	1.0999	1.3285	1.0999	1.3285	1.0999
6	0.052	-0.454	544.1	390.8	367.1	390.7	401.7	10.8	47.6	1.6	0.4749	0.3375	1.3301	1.1003	1.3301	1.1003	1.3301	1.1003
7	-0.933	-1.381	555.1	404.5	388.6	404.1	396.3	17.7	45.6	2.5	0.4845	0.3493	1.3378	1.1017	1.3378	1.1017	1.3378	1.1017
8	-1.798	-2.202	560.0	411.7	390.4	411.1	401.4	20.7	45.8	2.9	0.4880	0.3551	1.3425	1.1053	1.3425	1.1053	1.3425	1.1053
9	-4.689	-4.921	556.7	387.3	337.5	387.1	442.8	9.7	52.7	1.4	0.4803	0.3305	1.3329	1.1253	1.3329	1.1253	1.3329	1.1253
10	-6.037	-6.146	558.6	378.9	312.2	378.9	463.2	5.6	56.1	0.9	0.4799	0.3219	1.3299	1.1349	1.3299	1.1349	1.3299	1.1349
11	-7.595	-7.581	561.2	373.5	296.3	373.5	476.6	1.1	58.2	0.2	0.4806	0.3158	1.3282	1.1444	1.3282	1.1444	1.3282	1.1444

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	O-FAC	OMEGA-0	LCSS-P	P02/	%EFF-P	%EFF-A	B*1	B*2	V0*1	V0*2	PC/P0
	DEGREE	DEGREE	DEGREE	DEGREE				TOTAL	TOTAL	P01	STATC-ST	TOT-INLET	TOT-INLET	TOT-STG	TOT-STG		
1	-1.56	0.55	10.29	53.03	31.93	37.25	0.5570	0.1360	0.0278	0.9678	81.36	89.88	90.26	89.88	90.26	89.88	90.26
2	-1.07	1.33	10.75	50.25	32.06	37.40	0.5348	0.1165	0.0247	0.9740	83.22	91.06	91.40	91.06	91.40	91.06	91.40
3	-1.40	1.38	10.51	47.54	32.37	37.74	0.5069	0.0829	0.0182	0.9827	87.25	93.39	93.64	93.39	93.64	93.39	93.64
4	-2.59	1.13	8.37	45.31	33.27	36.92	0.4913	0.0844	0.0206	0.9845	85.83	92.76	93.03	92.76	93.03	92.76	93.03
5	-0.38	4.66	6.10	48.33	29.50	33.84	0.5045	0.0589	0.0161	0.9912	89.42	84.71	85.28	84.71	85.28	84.71	85.28
6	-2.45	3.17	5.95	45.99	30.44	34.14	0.4856	0.0500	0.0143	0.9928	90.30	84.68	85.25	84.68	85.25	84.68	85.25
7	-4.24	1.64	6.90	43.05	32.53	35.33	0.4685	0.0682	0.0199	0.9899	86.46	85.31	85.87	85.31	85.87	85.31	85.87
8	-3.80	2.35	7.31	42.93	32.62	35.88	0.4651	0.0756	0.0224	0.9886	84.85	83.60	84.24	83.60	84.24	83.60	84.24
9	3.08	9.96	6.98	51.26	27.75	33.22	0.5450	0.1222	0.0381	0.9821	78.05	68.43	69.85	68.43	69.85	68.43	69.85
10	6.11	13.16	7.63	55.20	25.53	32.25	0.5791	0.1488	0.0471	0.9783	74.31	62.99	64.41	62.99	64.41	62.99	64.41
11	7.58	14.73	8.48	58.04	24.16	31.55	0.6092	0.1882	0.0603	0.9724	68.54	58.49	60.09	58.49	60.09	58.49	60.09

NCORR	NCORR	TO/TO	PO/PC	EFF-AD	EFF-P	T02/T01	P02/P01	EFF-AD	EFF-P
INLET	INLET	INLET	INLET	INLET	INLET				
RPM	LBM/SEC			%	%			%	%
7479.	101.80	1.1084	1.3363	80.18	80.94	1.1084	0.9839	80.18	162.28

ROTOR 2

RUN NO 13, SPEED CODE 70, PG1NT NC 4

SL	EPS1-1	EPS1-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	U-1	U-2	M*-1	M*-2	V*-1	V*-2
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			FT/SEC	FT/SEC			FT/SEC	FT/SEC
1	11.054	10.987	460.5	807.6	460.4	538.0	21.5	602.3	2.7	48.1	0.4002	0.6874	583.2	611.7	0.6308	0.4580	726.3	538.1
2	10.849	9.640	466.0	794.6	464.9	532.7	32.9	589.6	4.1	47.8	0.4049	0.6763	599.7	624.5	0.6368	0.4544	733.0	533.9
3	9.860	8.369	472.4	775.5	470.6	534.1	41.4	567.8	5.0	46.7	0.4108	0.6638	616.7	637.8	0.6464	0.4587	743.2	538.6
4	8.148	4.841	466.7	700.3	465.7	513.9	29.9	475.7	3.7	42.8	0.4058	0.5943	669.4	680.2	0.6875	0.4693	791.1	553.1
5	0.607	0.384	430.6	591.4	430.4	454.1	12.2	378.9	1.6	39.8	0.3728	0.4983	742.2	741.7	0.7337	0.4896	847.4	581.2
6	-1.854	-1.662	426.4	548.1	420.2	415.2	10.6	357.7	1.4	40.7	0.3690	0.4603	779.2	774.4	0.7607	0.4940	878.9	588.2
7	-2.701	-2.465	436.1	540.5	435.7	406.7	17.5	356.0	2.3	41.2	0.3774	0.4535	797.9	791.3	0.7736	0.4997	893.8	595.7
8	-3.317	-3.144	442.1	541.9	442.2	410.7	20.9	353.5	2.7	40.6	0.3827	0.4540	816.8	808.5	0.7871	0.5158	910.4	613.0
9	-5.567	-5.440	428.2	549.4	428.1	430.7	10.1	341.1	1.3	38.2	0.3665	0.4559	874.0	862.1	0.8252	0.5609	964.1	675.9
10	-6.731	-6.602	424.0	545.7	424.0	436.5	6.0	327.5	0.8	36.7	0.3612	0.4509	893.2	880.4	0.8377	0.5821	983.3	704.4
11	-8.039	-8.062	421.5	532.7	421.5	438.6	1.2	302.4	0.2	34.4	0.3574	0.4384	912.5	899.1	0.8514	0.6094	1004.1	740.8

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P	P02/	EFF-P	EFF-A	B*-1	B*-2	V0*-1	V0*-2	PC/PO
	DEGREE	DEGREE	DEGREE	DEGREE				TOTAL	TOTAL	P01	TOT	TCT	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	1.12	5.43	21.39	49.60	39.84	45.59	0.4461	0.1588	0.0362	1.3620	89.20	88.74	50.59	1.00	-561.7	-9.4	1.8314
2	0.67	5.12	17.54	46.90	40.26	49.58	0.4531	0.1367	0.0319	1.3590	90.37	89.96	50.63	3.72	-566.7	-34.8	1.8321
3	0.39	4.97	14.97	43.31	40.84	50.25	0.4487	0.1077	0.0256	1.3539	91.99	91.67	50.74	7.44	-575.3	-65.9	1.8305
4	2.23	7.02	12.12	32.30	40.39	49.16	0.4470	0.0912	0.0218	1.3147	91.64	91.34	53.58	21.68	-639.6	-204.4	1.7715
5	6.01	10.58	10.40	20.86	37.12	43.54	0.4373	0.1052	0.0233	1.2651	87.80	87.42	59.48	38.62	-730.0	-362.7	1.6806
6	6.60	10.94	8.87	15.90	36.83	39.72	0.4481	0.1545	0.0324	1.2374	80.72	80.16	60.98	45.08	-768.7	-416.7	1.6463
7	5.92	10.00	7.64	13.90	37.71	38.90	0.4486	0.1708	0.0356	1.2277	78.02	77.41	60.79	48.90	-780.6	-435.3	1.6423
8	5.50	9.31	5.54	13.03	38.23	39.25	0.4401	0.1716	0.0361	1.2259	77.38	76.75	60.88	47.86	-795.8	-455.0	1.6460
9	6.70	9.38	3.16	13.26	36.32	40.67	0.4155	0.1489	0.0332	1.2445	79.82	79.21	63.51	50.26	-863.5	-520.9	1.6598
10	7.12	9.30	4.86	12.79	35.65	40.98	0.3991	0.1285	0.0290	1.2472	81.93	81.38	64.33	51.54	-887.2	-552.9	1.6591
11	7.55	9.24	7.88	11.52	35.12	40.92	0.3736	0.1012	0.0227	1.2424	84.70	84.25	65.06	53.54	-911.3	-596.8	1.6503

TO/TO INLET PO/PO INLET EFF-AD INLET EFF-P INLET WCI/AI LBM/SEC T02/T01 P02/P01 EFF-AD ROTOR EFF-P ROTOR

1.2015 1.7071 81.89 83.18 28.64 1.0840 1.2755 85.56 86.02

STATOR 2

RUN NO 13, SPEED CODE 70, PG1NT NC 4

SL	EPS1-1	EPS1-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	PO/PO	T0/T0	PO/PO	TU2/
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			INLET	INLET	STAGE	T01
1	8.582	0.770	826.3	612.4	572.1	612.2	596.3	-14.7	46.5	-1.4	0.7050	0.5111	1.7667	1.2124	1.3141	1.1639
2	7.492	0.623	812.4	616.4	564.1	616.2	584.6	-15.6	46.2	-1.4	0.6928	0.5152	1.7747	1.2101	1.3170	1.1020
3	6.458	0.408	796.5	625.2	562.7	624.9	563.8	-21.2	45.2	-1.9	0.6756	0.5241	1.7885	1.2050	1.3230	1.0589
4	3.907	-0.287	716.6	584.3	537.5	583.4	474.0	-31.3	41.5	-3.1	0.6091	0.4905	1.7541	1.1939	1.3012	1.0894
5	1.137	-0.903	607.8	494.1	475.5	492.5	378.6	-40.2	38.5	-4.7	0.5128	0.4132	1.6762	1.1872	1.2617	1.0794
6	-0.297	-1.028	564.9	448.3	437.1	446.5	357.8	-40.7	39.3	-5.2	0.4750	0.3739	1.6410	1.1863	1.2344	1.0782
7	-1.160	-1.070	557.6	441.8	428.8	439.9	356.5	-40.2	39.7	-5.2	0.4684	0.3682	1.6359	1.1871	1.2238	1.0779
8	-2.088	-1.118	559.3	445.1	432.8	443.3	354.3	-40.4	39.3	-5.2	0.4692	0.3706	1.6371	1.1899	1.2191	1.0778
9	-4.029	-1.308	570.5	471.1	458.1	469.6	342.8	-37.7	37.0	-4.6	0.4742	0.3888	1.6474	1.2141	1.2352	1.0812
10	-5.352	-1.343	569.9	474.6	465.0	473.4	329.4	-34.1	35.4	-4.1	0.4718	0.3903	1.6463	1.2233	1.2376	1.0797
11	-6.046	-1.259	561.8	459.5	472.2	458.4	304.5	-32.0	32.9	-4.0	0.4633	0.3763	1.6320	1.2210	1.2287	1.0757

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P	P02/	EFF-P	EFF-A	EFF-A	EFF-P	
	DEGREE	DEGREE	DEGREE	DEGREE				TOTAL	TOTAL	P01	STATC-ST	TOT-INLET	TOT-INLET	TOT-STG	TOT-STG
1	0.50	2.06	12.94	47.83	52.15	60.06	0.4257	0.1248	0.0282	0.9647	76.62	83.04	84.32	77.95	78.76
2	1.31	3.33	12.31	47.08	51.96	60.73	0.4120	0.1137	0.0262	0.9687	77.37	84.71	85.88	80.08	80.81
3	1.08	3.58	11.40	47.17	52.43	62.04	0.3897	0.0876	0.0205	0.9766	80.80	88.06	88.98	84.02	84.62
4	-1.58	2.29	9.74	44.55	51.00	58.28	0.3648	0.0528	0.0131	0.9881	86.57	89.76	90.52	87.24	87.88
5	-3.70	1.61	8.14	43.17	45.28	48.88	0.3765	0.0275	0.0073	0.9954	92.69	84.88	85.92	86.27	86.88
6	-2.63	3.16	7.52	44.47	41.54	44.08	0.4034	0.0276	0.0076	0.9960	93.10	81.56	82.98	79.19	79.77
7	-2.03	3.97	7.45	44.91	40.73	43.36	0.4075	0.0259	0.0072	0.9964	93.45	80.65	81.92	76.14	76.78
8	-2.28	3.93	7.41	44.47	41.08	43.58	0.4048	0.0364	0.0103	0.9949	90.67	79.61	80.95	74.71	75.38
9	-4.34	2.36	8.09	41.54	42.72	45.23	0.3708	0.0525	0.0153	0.9925	84.63	71.56	73.46	76.41	77.08
10	-6.58	0.30	9.16	39.49	43.26	45.20	0.3501	0.0536	0.0158	0.9924	83.67	68.48	70.58	78.59	79.20
11	-10.32	-3.23	15.44	36.90	43.58	43.34	0.3614	0.0803	0.0239	0.9890	77.40	64.97	67.26	79.87	80.42

NCORR MCCR INLET TO/TO PO/PO EFF-AD EFF-P T02/T01 P02/P01 EFF-AD EFF-P STAGE TOT-STG

7479. 101.80 1.2015 1.6881 80.04 81.43 1.0840 0.9888 81.49 275.77

ORIGINAL PAGE IS OF POOR QUALITY

ROTOR 2

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, 14, SPEED CODE, TO, POINT NO, U-1, U-2, M*-1, M*-I, V*-1, V*-2. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, O-FAC, MEGA-B, LOSS-P, P02/P01, %EFF-P, %EFF-A, B*-1, B*-2, V0*-1, V0*-2, PC2/PC1, PC1/PC1, EFF-AD, EFF-P. Rows 1-11.

Summary table with columns: TO/TO INLET, PO/PO INLET, EFF-AD INLET, EFF-P INLET, MCI/A1 LBM/SEC, % SQFT, T02/T01, P02/P01, EFF-AD ROTOR, EFF-P ROTOR. Values: 1.1791, 1.6530, 86.17, 87.10, 36.33, 1.0811, 1.2541, 82.30, 82.83.

STATOR 2

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, 14, SPEED CODE, TO, POINT NO, PO/PO INLET, TO/TO INLET, PC2/PC1, PC1/PC1, EFF-AD, EFF-P. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, O-FAC, MEGA-B, LOSS-P, P02/P01, %EFF-P, %EFF-A, %EFF-P, %EFF-A, %EFF-P. Rows 1-11.

Summary table with columns: NCORR INLET, MCORR INLET, TO/TO INLET, PO/PO INLET, EFF-AD INLET, EFF-P INLET, T02/T01, P02/P01, EFF-AD STAGE, EFF-P TO-TSTG. Values: 7490, 128.20, 1.1791, 1.5414, 73.44, 74.98, 1.0811, 0.9325, 56.34, 1458.46.

ORIGINAL PAGE IS OF POOR QUALITY

TABLE XXXI (b) – OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

70% OF DESIGN SPEED
STATOR 1 (beta^* des. - beta^* act.) = +5^0
STATOR 2 (beta^* des. - beta^* act.) = 0^0

U. S. CUSTOMARY UNITS

ROTOR 1

Table with 20 columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, 14, SPEED CODE 70, POINT NO 2, U-1, U-2, M*-1, M*-2, V1-1, V1-2.

Table with 18 columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, PO2/P01, XEFF-P, XEFF-A, B*-1, B*-2, V0*-1, V0*-2, PC/PO.

Summary table with 6 columns: TO/T0, PO/PO, EFF-AD, EFF-P, W1/A1, W2/T01, P02/P01, EFF-AD, EFF-P.

STATOR 1

Table with 20 columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO, 14, SPEED CODE 70, POINT NO 2, PO/PO, TO/T0, PC/PC, EFF-P, EFF-A, TO2/T01.

Table with 18 columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, OMEGA-B, LOSS-P, PO2/P01, XEFF-P, XEFF-A, XEFF-P, XEFF-A, TO2/T01, P02/P01, EFF-AD, EFF-P.

Summary table with 6 columns: NCORR INLET, NCORR INLET, TO/T0, PO/PO, EFF-AD, EFF-P, TO2/T01, P02/P01, EFF-AD, EFF-P.

ROTOR 2

															RUN NO 14, SPEED CODE 70, POINT NO 2			
SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	0-1	0-2	M-1	M-2	U-1	U-2	M*-1	M*-2	V*-1	V*-2
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			FT/SEC	FT/SEC			FT/SEC	FT/SEC
1	11.541	11.016	503.2	858.5	558.5	622.0	-72.4	592.3	-7.4	43.5	0.4927	0.7304	582.7	611.1	0.7532	0.5292	800.9	622.3
2	10.648	9.697	566.8	838.9	562.5	611.7	-69.2	574.1	-7.0	43.1	0.4964	0.7127	599.1	623.9	0.7651	0.5214	873.6	613.8
3	9.610	8.458	569.3	812.4	565.3	604.5	-68.2	542.8	-6.9	41.8	0.4993	0.6898	616.1	637.2	0.7784	0.5195	887.4	611.9
4	5.827	4.586	560.1	732.7	555.9	586.0	-67.9	439.9	-7.0	36.9	0.4911	0.6205	668.8	679.6	0.8093	0.5366	922.9	633.1
5	0.228	0.558	530.6	615.9	524.2	519.6	-82.3	330.6	-8.9	32.5	0.4639	0.5186	741.5	741.0	0.8538	0.5576	976.5	662.1
6	-2.142	-1.406	522.1	562.2	515.3	479.8	-84.0	293.1	-9.3	31.4	0.4560	0.4722	778.6	773.7	0.8776	0.5703	1004.8	679.1
7	-3.061	-2.258	526.4	551.5	520.2	476.9	-80.9	277.0	-8.8	30.1	0.4599	0.4632	797.2	790.6	0.8917	0.5887	1020.0	700.8
8	-3.935	-3.112	528.1	553.6	521.9	489.6	-81.1	258.9	-8.8	27.8	0.4611	0.4655	816.0	807.8	0.9061	0.6182	1037.9	735.0
9	-6.758	-6.090	537.5	569.2	532.7	506.4	-72.0	259.9	-7.7	27.1	0.4675	0.4762	873.2	861.3	0.9437	0.6579	1085.0	786.2
10	-7.613	-7.153	539.6	565.2	535.2	502.5	-69.2	258.6	-7.3	27.1	0.4685	0.4718	892.4	879.7	0.9555	0.6669	1100.5	798.9
11	-8.450	-8.338	521.9	546.3	516.7	492.2	-73.9	237.2	-8.1	25.6	0.4515	0.4550	911.7	898.3	0.9627	0.6864	1112.8	824.3

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P	PO2/	%EFF-P	%EFF-A	B*-1	B*-2	V0*-1	V0*-2	PC/PO
	DEGREE	DEGREE	DEGREE	DEGREE				TOTAL	TOTAL	PO1	TOT	TOT	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	-0.01	4.31	22.12	47.75	46.60	58.05	0.4566	0.1038	0.0236	1.4309	91.67	91.25	49.47	1.72	-655.1	-18.8	1.9317
2	-0.07	4.38	18.46	45.25	47.03	57.59	0.4722	0.1137	0.0265	1.4199	90.51	90.05	49.88	4.64	-668.3	-49.8	1.9209
3	0.09	4.67	16.38	41.55	47.34	57.42	0.4776	0.1148	0.0272	1.4037	89.89	89.41	50.45	8.85	-684.3	-94.4	1.9011
4	1.24	6.03	12.60	30.15	46.44	56.78	0.4560	0.0692	0.0165	1.3675	92.81	92.51	52.99	22.24	-736.7	-239.7	1.8375
5	4.06	8.64	10.08	19.23	43.59	50.51	0.4418	0.0851	0.0189	1.3078	89.01	88.61	57.53	38.31	-823.8	-410.4	1.7291
6	4.76	9.10	8.82	14.11	42.86	46.52	0.4357	0.1116	0.0234	1.2744	84.27	82.75	59.13	45.03	-862.6	-480.6	1.6811
7	4.46	8.54	7.82	12.25	43.32	46.31	0.4200	0.1077	0.0224	1.2647	84.07	83.56	59.33	47.08	-878.1	-513.6	1.6734
8	4.39	8.20	5.88	11.57	43.42	47.64	0.3933	0.0841	0.0175	1.2659	86.93	86.51	59.77	48.20	-897.1	-549.0	1.6771
9	3.71	6.39	2.88	10.74	44.07	48.93	0.3812	0.0916	0.0206	1.2698	85.32	84.84	60.52	49.77	-945.3	-601.5	1.6918
10	3.60	5.78	4.20	9.92	44.18	48.35	0.3812	0.1024	0.0235	1.2636	83.29	82.76	60.80	50.88	-961.6	-621.0	1.6879
11	4.72	6.41	7.55	9.02	42.40	47.15	0.3640	0.0827	0.0187	1.2630	85.95	85.51	62.23	53.21	-985.0	-661.2	1.6712

TO/TO	PO/PO	EFF-AD	EFF-P	WCI/AL	TOT/TOT	PO2/PO1	%EFF-AD	%EFF-P
INLET	INLET	%	%	LBM/SEC	%	%	%	%
1.2006	1.7543	86.79	87.77	33.53	1.0920	1.3161	88.61	89.03

STATOR 2

															RUN NO 14, SPEED CODE 70, POINT NO 2			
SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	0-1	0-2	M-1	M-2	PO/PO	TO/TO	PC/PO	TC/TO		
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			INLET	INLET	STAGE	TOT		
1	8.615	0.788	886.4	716.9	664.7	716.9	586.5	6.8	41.7	0.5	0.7563	0.6000	1.8358	1.2287	1.3601	1.1179		
2	7.541	0.854	865.2	721.3	651.5	721.3	569.3	-5.5	41.4	-0.4	0.7373	0.6046	1.8470	1.2280	1.3657	1.1171		
3	6.483	0.426	837.8	731.5	641.4	731.4	539.0	-12.6	40.2	-1.0	0.7134	0.6153	1.8668	1.2203	1.3779	1.1142		
4	3.779	-0.362	756.1	683.2	616.1	682.9	438.3	-22.1	35.5	-1.9	0.6423	0.5759	1.8180	1.2046	1.3524	1.1016		
5	0.926	-1.008	638.3	592.2	546.2	591.5	330.4	-28.7	31.2	-2.8	0.5386	0.4976	1.7218	1.1929	1.3019	1.0900		
6	-0.648	-1.243	584.8	544.5	506.0	543.6	243.3	-30.9	30.1	-3.2	0.4920	0.4566	1.6759	1.1890	1.2708	1.0857		
7	-1.497	-1.319	574.0	532.7	502.6	531.7	277.3	-32.5	28.9	-3.5	0.4830	0.4468	1.6646	1.1864	1.2581	1.0831		
8	-2.278	-1.344	576.3	533.6	514.6	532.5	259.4	-33.4	26.7	-3.6	0.4852	0.4478	1.6640	1.1852	1.2561	1.0804		
9	-4.289	-1.340	595.3	557.5	535.0	557.3	261.2	-11.0	26.0	-1.1	0.4992	0.4660	1.6756	1.1984	1.2576	1.0831		
10	-5.051	-1.345	594.6	560.0	534.7	560.0	260.1	-0.8	26.0	-0.1	0.4975	0.4673	1.6742	1.2032	1.2535	1.0833		
11	-5.897	-1.262	581.3	532.3	529.9	532.3	238.9	0.7	24.3	0.1	0.4854	0.4428	1.6463	1.2053	1.2444	1.0805		

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P	PO2/	%EFF-P	%EFF-A	%EFF-P	%EFF-A	%EFF-P	%EFF-A
	DEGREE	DEGREE	DEGREE	DEGREE				TOTAL	TOTAL	PO1	STAT-5T	TOT-INLET	TOT-INLET	TOT-STG	TOT-STG	TOT-STG
1	-6.76	-5.20	12.35	41.15	60.97	68.85	0.3394	0.1582	0.0357	0.9499	62.54	82.80	84.18	77.72	78.64	78.64
2	-6.05	-4.04	10.81	41.81	60.34	69.66	0.3219	0.1304	0.0300	0.9602	65.39	84.68	85.93	79.33	80.20	80.20
3	-6.43	-3.93	9.86	41.20	60.01	71.29	0.2857	0.0685	0.0161	0.9801	77.02	88.54	89.48	83.63	84.53	84.53
4	-10.07	-6.20	8.47	37.34	58.96	67.12	0.2523	0.0506	0.0126	0.9877	77.39	90.96	91.67	88.53	88.98	88.98
5	-13.56	-8.25	7.52	33.93	52.58	57.84	0.2286	0.0345	0.0092	0.9937	79.46	86.98	87.91	86.82	87.28	87.28
6	-14.33	-8.54	6.97	33.32	48.61	52.91	0.2245	0.0245	0.0068	0.9963	83.72	84.05	85.14	82.53	83.09	83.09
7	-15.37	-9.38	6.67	32.35	48.37	51.73	0.2245	0.0347	0.0097	0.9949	77.17	84.03	85.12	81.44	82.00	82.00
8	-17.32	-11.11	6.52	30.32	49.63	51.83	0.2185	0.0516	0.0146	0.9923	66.67	84.54	85.56	83.60	84.09	84.09
9	-17.76	-11.06	9.03	27.17	51.14	53.58	0.1985	0.0613	0.0180	0.9904	54.94	80.03	81.40	81.32	81.64	81.64
10	-18.47	-11.59	10.70	26.06	50.83	53.55	0.1882	0.0510	0.0151	0.9921	59.08	78.02	79.53	79.91	80.52	80.52
11	-21.40	-14.30	12.01	24.26	50.08	50.50	0.2071	0.0993	0.0296	0.9852	43.77	74.52	76.21	79.92	80.50	80.50

NCORR	MCORR	TO/TO	PO/PO	EFF-AD	EFF-P	TOT/TOT	PO2/PO1	%EFF-AD	%EFF-P
INLET	INLET	INLET	INLET	%	%	%	%	%	%
		1.2006	1.7308	84.93	85.66	1.0920	0.9866	84.08	256.49

TABLE XXXI (c) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

70% OF DESIGN SPEED

STATOR 1 ($\beta^*_{des.} - \beta^*_{act.}$) = +5°

STATOR 2 ($\beta^*_{des.} - \beta^*_{act.}$) = 0°

U. S. CUSTOMARY UNITS

ROTOR 1

SL	EPSI-1		EPSI-2		V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	RUN NO 14, SPEED CODE 70, POINT NO 3		V*-1	V*-2	
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SIC	FT/SIC	FT/SIC	FT/SIC	FT/SIC	FT/SIC	DEGREE	DEGREE	DEGREE	DEGREE	U-1	U-2	M*-1	M*-1	FT/SIC	FT/SEC
1	16.567	18.121	337.7	725.0	337.7	401.7	0.0	603.5	0.0	56.4	0.3052	0.6447	439.7	509.1	0.5011	0.3670	554.4	412.7	
2	14.007	15.590	345.1	696.3	345.1	405.0	0.0	568.8	0.0	54.5	0.3120	0.6195	474.2	533.7	0.5302	0.3607	566.4	406.5	
3	11.683	13.264	352.7	673.8	352.7	405.7	0.0	538.0	0.0	52.9	0.3166	0.5965	507.9	556.3	0.5591	0.3596	618.1	406.2	
4	5.510	7.254	357.4	617.7	367.4	404.9	0.0	466.5	0.0	49.0	0.3326	0.5443	604.7	632.3	0.6406	0.3855	707.6	437.6	
5	-0.191	0.950	373.1	552.0	373.1	362.3	0.0	416.4	0.0	49.0	0.3379	0.4827	725.5	750.7	0.7588	0.4195	815.8	479.7	
6	-2.207	-1.061	373.1	546.5	373.1	375.1	0.0	397.2	0.0	46.6	0.3379	0.4772	783.6	780.0	0.7860	0.4661	867.9	535.9	
7	-3.496	-2.904	372.6	549.8	372.6	395.2	0.0	382.7	0.0	44.1	0.3375	0.4605	812.3	804.6	0.8094	0.5055	893.7	576.4	
8	-5.009	-4.144	371.5	546.1	371.5	397.2	0.0	377.7	0.0	43.6	0.3362	0.4766	841.0	829.3	0.8324	0.5204	919.3	601.4	
9	-9.353	-7.950	362.9	545.2	362.9	384.1	0.0	384.2	0.0	45.0	0.3285	0.4717	926.6	903.1	0.9006	0.5606	995.1	645.7	
10	-10.636	-9.402	359.0	539.0	359.0	369.9	0.0	392.4	0.0	46.6	0.3249	0.4669	955.1	927.8	0.9233	0.5634	1020.4	650.8	
11	-11.609	-10.437	355.0	528.7	355.0	349.7	0.0	396.5	0.0	48.5	0.3211	0.4564	983.6	952.4	0.9460	0.5670	1045.7	656.8	

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	U-FAC	OMEGA-B	LOSS-P	P02/P01	ZEFF-P	ZEFF-A	B*-1	B*-2	V0*-1	V0*-2	PO/PU
DEGREE	DEGREE	DEGREE	DEGREE	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOT	TOT	TOT	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	2.486	10.447	14.77	65.48	24.66	31.92	0.5144	-0.0196	-0.0042	1.3940	100.91	100.98	52.25	-13.23	-439.7	94.4	1.3940
2	5.669	10.15	14.06	58.65	25.15	32.57	0.5452	-0.0158	-0.0036	1.3884	100.83	100.90	53.71	-4.95	-474.2	35.1	1.3884
3	6.03	10.14	14.40	52.17	25.62	32.94	0.5632	-0.0086	-0.0021	1.3823	100.50	100.55	55.04	2.87	-507.9	-20.4	1.3823
4	7.06	10.55	12.54	36.36	26.60	33.53	0.5640	0.0092	0.0023	1.3691	99.24	99.24	58.59	22.23	-604.7	-165.8	1.3691
5	8.26	10.94	10.06	21.84	26.97	30.27	0.5678	0.0980	0.0222	1.3441	90.67	90.30	62.78	40.94	-725.5	-314.4	1.3441
6	8.62	10.90	8.25	18.96	26.97	31.56	0.5278	0.0880	0.0195	1.3522	90.95	90.58	64.55	45.59	-783.6	-362.6	1.3522
7	6.79	10.90	6.60	18.47	26.94	33.43	0.4916	0.0601	0.0133	1.3607	93.48	93.22	65.38	46.91	-812.3	-422.4	1.3607
8	6.99	10.95	5.61	17.54	26.85	33.65	0.4824	0.0669	0.0147	1.3636	92.50	92.19	66.21	48.67	-841.0	-451.5	1.3636
9	5.62	11.04	6.68	15.19	26.31	32.41	0.4879	0.1301	0.0274	1.3675	84.73	84.07	68.67	53.47	-926.6	-519.0	1.3675
10	9.77	11.06	6.31	14.14	26.06	31.10	0.5007	0.1644	0.0338	1.3661	80.68	79.84	69.45	55.31	-955.1	-535.4	1.3661
11	9.84	10.99	11.40	12.43	25.79	29.50	0.5104	0.1957	0.0385	1.3601	76.81	75.81	70.17	57.75	-983.6	-555.9	1.3601

TO/TU	PO/PU	EFF-AD	EFF-P	WCI/A1	TO2/T01	P02/P01	EFF-AD	EFF-P
INLET	INLET	%	INLET	LBM/SEC			%	INLET
1.1025	1.3648	90.69	91.06	25.46	1.1025	1.3648	90.69	91.06

STATOR 1

SL	EPSI-1		EPSI-2		V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	RUN NO 14, SPEED CLDE 70, POINT NO 3		T02/
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SIC	FT/SIC	FT/SIC	FT/SIC	FT/SIC	FT/SIC	DEGREE	DEGREE	DEGREE	DEGREE	PO/PU	TOT-INLET	TOT-INLET	TOT-INLET
1	16.072	14.765	725.4	476.0	421.0	471.3	590.7	-66.3	54.7	-7.9	0.6452	0.4136	1.3488	1.0986	1.3488	1.0986	1.0986
2	15.661	12.926	701.5	477.2	424.2	473.2	558.7	-61.4	52.9	-7.3	0.6225	0.4149	1.3525	1.0974	1.3525	1.0974	1.0974
3	13.446	11.212	679.0	478.3	424.6	474.5	529.9	-60.5	51.3	-7.2	0.6015	0.4162	1.3553	1.0964	1.3553	1.0964	1.0964
4	7.963	6.598	626.6	458.6	412.5	454.7	462.7	-59.2	47.6	-7.4	0.5525	0.3968	1.3438	1.0947	1.3438	1.0947	1.0947
5	1.840	0.932	563.1	427.5	379.6	431.6	415.7	-72.7	47.6	-9.5	0.4929	0.3797	1.3500	1.0977	1.3500	1.0977	1.0977
6	-0.926	-1.595	556.0	441.5	351.6	435.3	397.5	-72.8	45.4	-9.5	0.4678	0.3825	1.3315	1.0994	1.3315	1.0994	1.0994
7	-1.991	-2.622	561.4	448.2	410.4	443.4	383.1	-66.0	43.0	-8.5	0.4911	0.3887	1.3359	1.0988	1.3359	1.0988	1.0988
8	-2.903	-3.529	559.9	451.6	412.2	447.1	379.0	-65.3	42.6	-8.3	0.4693	0.3916	1.3384	1.1006	1.3384	1.1006	1.1006
9	-5.665	-6.175	555.9	448.6	399.7	443.5	386.4	-67.1	44.1	-8.6	0.4832	0.3868	1.3384	1.1111	1.3384	1.1111	1.1111
10	-6.708	-7.104	552.5	444.4	386.5	439.8	395.0	-63.5	45.7	-8.2	0.4789	0.3821	1.3365	1.1166	1.3365	1.1166	1.1166
11	-7.912	-8.106	542.4	431.2	366.9	426.2	395.6	-65.5	47.6	-8.8	0.4688	0.3697	1.3293	1.1212	1.3293	1.1212	1.1212

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	U-FAC	OMEGA-B	LOSS-P	P02/P01	ZEFF-P	ZEFF-A	B*-1	B*-2	V0*-1	V0*-2	PO/PU
DEGREE	DEGREE	DEGREE	DEGREE	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOT-STG	TOT-INLET	TOT-INLET	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	7.14	9.25	9.41	62.61	33.45	40.68	0.5227	0.1326	0.0269	0.9676	79.66	90.55	90.91	90.91	90.55	90.91	1.0986
2	7.04	9.45	8.90	60.22	34.05	40.98	0.5015	0.1116	0.0235	0.9743	81.75	92.54	92.82	92.54	92.82	92.54	1.0974
3	6.81	9.59	8.17	58.55	34.37	41.19	0.4820	0.0894	0.0196	0.9806	84.29	94.20	94.42	94.20	94.42	94.20	1.0964
4	5.57	9.29	6.86	54.90	34.84	39.48	0.4683	0.0973	0.0236	0.9818	81.09	93.09	93.34	93.09	93.34	93.09	1.0947
5	7.06	12.11	4.77	57.11	31.56	37.26	0.4584	0.0692	0.0187	0.9894	83.89	86.92	87.41	86.92	87.41	86.92	1.0977
6	5.41	11.03	4.67	54.92	32.79	37.51	0.4503	0.1050	0.0296	0.9842	74.22	85.83	86.36	85.83	86.36	85.83	1.0994
7	3.24	9.12	5.91	51.52	34.55	38.26	0.4352	0.1207	0.0349	0.9817	69.38	87.35	87.83	87.35	87.83	87.35	1.0988
8	3.02	9.17	6.11	50.95	34.74	38.55	0.4292	0.1223	0.0359	0.9815	67.75	86.39	86.91	86.39	86.91	86.39	1.1006
9	4.46	11.34	6.92	52.71	33.56	37.95	0.4465	0.1443	0.0445	0.9787	61.87	78.25	79.10	78.25	79.10	78.25	1.1111
10	5.77	12.82	8.53	53.95	32.31	37.46	0.4604	0.1508	0.0472	0.9781	60.68	74.14	75.15	74.14	75.15	74.14	1.1166
11	6.92	14.07	9.54	56.32	30.56	36.12	0.4820	0.1625	0.0514	0.9773	59.03	69.93	71.08	69.93	71.08	69.93	1.1212

NCURR	WCURR	TO/TU	PO/PU	EFF-AD	EFF-P	TO2/T01	P02/P01	EFF-AD	EFF-P
INLET	INLET	INLET	INLET	%	%			%	INLET
7482	11210	1.1025	1.3388	84.65	85.43	1.1025	0.9810	84.85	84.98

ROTOR 2

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, RUN NO 14, SPEED CODE 70, POINT NO 3, U-1, U-2, M-1, M-2, V-1, V-2. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHQVM-1, RHQVM-2, D-FAC, OMEGA-B, LOSS-P, PO2/ P01, XEFF-P, XEFF-A, B-1, B-2, VB-1, VB-2, PO/PO. Rows 1-11.

Summary table with columns: TO/TO, PD/PD, EFF-AD, EFF-P, MCI/A1, TO2/T01, P02/P01, EFF-AD, EFF-P. Rows 1-2.

STATOR 2

Table with columns: SL, EPSI-1, EPSI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, PD/PO, TO/TO, PO/PO, TO/TO, TO/TO, TO/TO, TO/TO, TO/TO, TO/TO. Rows 1-11.

Table with columns: SL, INCS, INCM, DEV, TURN, RHQVM-1, RHQVM-2, D-FAC, OMEGA-B, LOSS-P, PO2/ P01, XEFF-P, XEFF-A, XEFF-P, XEFF-P, XEFF-P, XEFF-P. Rows 1-11.

Summary table with columns: NCROR, MCROR, TO/TO, PD/PD, EFF-AD, EFF-P, TO2/T01, P02/P01, EFF-AD, EFF-P. Rows 1-2.

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APPENDIX E

TABLE XXXI (d) – OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

70% OF DESIGN SPEED
 STATOR 1 ($\beta^*_{des} - \beta^*_{act}$) = $+5^\circ$
 STATOR 2 ($\beta^*_{des} - \beta^*_{act}$) = 0°

U. S. CUSTOMARY UNITS

ROTOR 1

SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	U-1	U-2	M-1	M-2	V*-1	V*-2
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			FT/SEC	FT/SEC			FT/SEC	FT/SEC
1	16.343	18.067	317.3	715.3	317.3	385.3	0.0	602.7	0.0	57.4	0.2865	0.6356	438.4	507.5	0.4886	0.3527	541.2	396.9
2	13.535	15.516	323.5	688.9	323.5	393.5	0.0	565.4	0.0	55.1	0.2922	0.6108	472.7	552.1	0.5173	0.3501	572.8	394.9
3	10.962	13.182	329.1	644.5	329.1	387.1	0.0	540.1	0.0	54.3	0.2972	0.5877	506.4	556.6	0.5455	0.3427	603.9	347.5
4	4.749	7.102	340.3	612.1	340.3	380.1	0.0	479.8	0.0	51.6	0.3076	0.5384	602.9	630.3	0.6258	0.3556	692.3	408.9
5	-1.171	0.632	343.8	557.2	343.8	345.5	0.0	437.1	0.0	51.7	0.3108	0.4865	723.3	728.5	0.7240	0.3946	800.6	452.0
6	-3.555	-2.077	342.7	557.7	342.7	368.8	0.0	418.3	0.0	48.6	0.3098	0.4864	781.2	777.6	0.7712	0.4491	853.1	514.9
7	-5.068	-3.377	341.3	565.5	341.3	386.8	0.0	412.6	0.0	46.9	0.3085	0.4532	809.8	802.1	0.7544	0.4787	878.8	549.0
8	-6.808	-4.709	338.8	567.8	338.8	384.7	0.0	417.6	0.0	47.4	0.3062	0.4942	838.4	826.7	0.8173	0.4887	904.3	561.6
9	-11.357	-8.592	326.7	560.2	326.7	327.8	0.0	454.3	0.0	54.2	0.2921	0.4822	923.7	900.4	0.8850	0.4769	979.8	553.5
10	-12.145	-9.719	322.1	556.6	322.1	302.3	0.0	467.6	0.0	57.1	0.2909	0.4779	952.2	924.9	0.9077	0.4705	1005.2	548.2
11	-12.324	-10.739	318.1	555.3	318.1	289.1	0.0	474.2	0.0	58.6	0.2872	0.4753	980.6	949.5	0.9307	0.4762	1030.9	556.3

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	CMEGA-B	LOSS-P	P02/ P01	%EFF-P	%EFF-A	B*-1	B*-2	V0*-1	V0*-2	PO/PO
	DEGREE	DEGREE	DEGREE	DEGREE	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	TOT	TOT	TOT	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	7.45	12.06	14.08	67.72	23.30	30.86	0.5315	-0.0454	-0.0097	1.3972	102.04	102.16	53.84	-13.88	-438.4	95.2	1.3972
2	7.50	11.80	14.77	60.15	23.72	31.89	0.5541	-0.0477	-0.0109	1.3915	102.41	102.55	55.32	-4.84	-472.7	33.4	1.3915
3	7.69	11.80	13.96	54.27	24.09	31.63	0.5860	-0.0174	-0.0042	1.3847	100.95	101.03	56.70	2.43	-506.4	-16.5	1.3847
4	8.90	12.37	11.88	38.84	24.83	31.60	0.6019	0.0284	0.0070	1.3734	97.86	97.79	60.40	21.56	-602.4	-150.5	1.3734
5	10.04	12.74	9.86	24.44	25.06	28.95	0.6041	0.1192	0.0273	1.3556	89.33	88.89	64.57	40.13	-723.3	-291.4	1.3556
6	10.42	12.70	6.92	22.09	24.99	31.09	0.5549	0.1042	0.0236	1.3368	89.88	89.46	66.35	44.26	-781.2	-359.3	1.3368
7	10.63	12.73	4.91	21.98	24.90	32.69	0.5309	0.0948	0.0217	1.3766	90.45	90.04	67.21	45.23	-809.8	-384.6	1.3766
8	10.87	12.82	3.93	21.30	24.73	32.44	0.5351	0.1194	0.0272	1.3801	87.76	87.22	68.09	46.79	-838.4	-409.1	1.3801
9	11.64	13.06	6.92	16.58	23.93	27.23	0.6008	0.2517	0.0528	1.3773	74.22	73.06	70.69	53.71	-923.7	-446.1	1.3773
10	11.77	13.06	9.53	14.92	23.62	25.00	0.6229	0.2915	0.0582	1.3771	70.38	69.04	71.45	56.53	-952.2	-457.3	1.3771
11	11.75	12.50	12.29	13.45	23.35	23.87	0.6288	0.3135	0.0602	1.3800	68.16	66.72	72.09	58.64	-980.6	-475.3	1.3800

TO2/T01	P02/P01	EFF-AD	EFF-P	WCI/L1		TO2/T01	P02/P01	EFF-AD	EFF-P
1.1105	1.3752	86.27	86.84	23.53		1.1105	1.3752	86.27	86.84

STATOR 1

SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	P0/PO	TO2/T01	PO/PO	TC2/ T01
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			INLET	INLET	INLET	STAGE
1	18.140	14.909	714.8	446.9	403.7	441.8	590.0	-67.0	55.8	-8.5	0.6351	0.3877	1.3473	1.0982	1.3473	1.0982
2	15.664	13.195	690.8	448.8	410.7	444.7	555.4	-60.9	53.6	-7.7	0.6126	0.3897	1.3518	1.0966	1.3518	1.0966
3	13.771	11.560	668.3	450.6	404.3	446.9	532.1	-57.3	52.8	-7.3	0.5912	0.3913	1.3533	1.0965	1.3533	1.0965
4	8.376	6.952	619.0	427.2	395.8	423.8	475.9	-54.0	50.3	-7.2	0.5448	0.3703	1.3445	1.0970	1.3445	1.0970
5	2.405	1.319	565.9	406.2	360.3	401.4	436.4	-62.3	50.4	-8.8	0.4945	0.3508	1.3339	1.1021	1.3339	1.1021
6	-0.129	-1.016	566.7	409.6	381.6	405.4	418.7	-58.4	47.6	-8.2	0.4946	0.3533	1.3366	1.1043	1.3366	1.1043
7	-1.911	-1.904	574.4	417.3	358.7	414.2	413.4	-50.9	46.0	-7.0	0.5012	0.3401	1.3417	1.1058	1.3417	1.1058
8	-1.816	-2.685	576.8	420.1	396.7	417.1	418.8	-49.8	46.6	-6.8	0.5024	0.3619	1.3444	1.1095	1.3444	1.1095
9	-4.710	-5.251	570.3	400.2	341.7	391.2	456.6	-84.5	53.2	-12.2	0.4918	0.3412	1.3379	1.1252	1.3379	1.1292
10	-6.102	-6.395	567.3	391.7	316.7	380.2	470.6	-94.0	56.1	-13.9	0.4873	0.3326	1.3349	1.1372	1.3349	1.1372
11	-7.675	-7.724	566.0	388.1	303.4	374.7	477.9	-101.0	57.7	-15.1	0.4849	0.3284	1.3344	1.1444	1.3344	1.1444

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	CMEGA-B	LOSS-P	P02/ P01	%EFF-P	%EFF-A	%EFF-P	%EFF-A	%EFF-P	%EFF-P
	DEGREE	DEGREE	DEGREE	DEGREE	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	P01	STAGC-ST	TOT-INLET	TOT-INLET	TOT-INLET	TOT-STG	TOT-STG
1	8.25	11.36	8.79	64.33	32.35	38.49	0.5569	0.1500	0.0303	0.9442	78.35	90.55	90.91	90.55	90.91	
2	7.79	10.19	6.49	61.38	33.26	38.90	0.5348	0.1278	0.0269	0.9713	80.50	93.17	93.42	93.17	93.42	
3	8.32	11.40	8.13	60.10	32.97	39.17	0.5161	0.1012	0.0221	0.9786	83.56	94.10	94.32	94.10	94.32	
4	8.26	11.57	7.04	57.49	32.79	37.12	0.5168	0.1157	0.0280	0.9788	80.06	91.02	91.36	91.02	91.36	
5	9.95	14.99	5.50	55.26	30.07	34.96	0.5222	0.1070	0.0276	0.9843	80.61	84.08	84.69	84.08	84.69	
6	7.63	13.23	6.16	55.84	32.07	35.28	0.5170	0.1370	0.0388	0.9789	73.43	82.89	83.55	82.89	83.55	
7	4.23	12.11	7.37	53.05	33.57	36.05	0.5081	0.1561	0.0452	0.9754	69.43	82.86	83.53	82.86	83.53	
8	6.95	13.10	7.61	53.37	33.32	36.23	0.5115	0.1629	0.0480	0.9742	68.03	80.72	81.49	80.72	81.49	
9	13.59	20.47	3.35	65.41	28.27	33.46	0.5934	0.1897	0.0579	0.9709	65.50	67.23	68.52	67.23	68.52	
10	16.16	23.21	2.86	70.01	26.08	32.31	0.6241	0.2014	0.0619	0.9697	64.22	62.75	64.21	62.75	64.21	
11	17.04	24.19	3.19	72.80	24.94	31.68	0.6445	0.2202	0.0681	0.9672	61.31	59.50	61.08	59.50	61.08	

NCORR	WCORR	TO2/T01	PO/PO	EFF-AD	EFF-P	TO2/T01	P02/P01	EFF-AD	EFF-P
INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET
RPM	LBM/SEC								
7459.	103.40	1.1105	1.3413	79.22	80.04	1.1105	0.9753	79.22	162.49

ROTOR 2

SL	EPI-S1-1		EPI-S2-2		V-1		V-2		VM-1		VM-2		VO-1		VO-2		B-1		B-2		M-1		M-2		U-1		U-2		M-1		M-1		V1-1	V1-2
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC		
1	11.358	10.952	470.3	817.1	465.8	541.8	-65.2	611.7	-7.9	48.3	0.4086	0.6909	581.6	610.0	0.6925	0.4581	797.0	541.8																
2	10.677	9.597	476.8	794.5	473.0	526.0	-59.6	595.9	-7.2	48.4	0.4147	0.6713	598.0	622.8	0.7046	0.4448	810.0	526.7																
3	9.882	8.353	482.1	777.0	479.4	523.9	-56.0	560.2	-6.7	46.8	0.4201	0.6472	615.0	636.0	0.7177	0.4467	824.6	529.4																
4	9.781	8.552	469.6	654.4	466.6	508.8	-53.3	473.2	-6.5	42.9	0.4082	0.5847	667.6	678.3	0.7405	0.4016	858.7	548.6																
5	0.177	0.113	450.5	596.9	446.2	459.4	-62.2	381.2	-7.9	39.7	0.3902	0.4987	760.1	739.7	0.7951	0.4868	918.8	582.7																
6	-2.612	-1.826	449.0	558.0	449.2	421.2	-58.5	366.6	-7.5	41.0	0.3885	0.4644	777.1	772.3	0.8191	0.4870	946.8	585.2																
7	3.399	-2.613	454.0	552.8	451.1	411.1	-51.1	369.5	-6.5	41.9	0.3926	0.4592	795.8	789.1	0.8298	0.4880	959.6	587.5																
8	-3.966	-3.305	456.7	553.1	454.0	411.8	-49.9	369.2	-6.3	41.8	0.3944	0.4584	814.5	806.3	0.8431	0.4977	976.4	600.5																
9	0.138	-3.712	447.0	544.6	438.9	430.1	-86.8	334.0	-10.9	37.7	0.3823	0.4463	871.6	859.7	0.9000	0.5566	1052.3	679.2																
10	-7.200	-6.877	442.0	531.6	431.7	427.7	-94.7	315.6	-12.3	36.3	0.3765	0.4337	890.8	878.0	0.9166	0.5764	1075.9	706.5																
11	-6.311	-6.241	440.4	515.8	428.4	423.3	-102.2	294.5	-13.4	34.7	0.3739	0.4191	910.0	896.7	0.9330	0.5981	1099.1	736.1																

SL	INCS DEGREE	INCM	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-8 TOTAL	LOSS-P TOTAL	PO2/P01	EFF-P TOT	EFF-A TOT	B-1 DEGREE	B-2 DEGREE	VB-1 FT/SEC	VB-2 FT/SEC	PC/PC INLET		
																	TOT	TOT	
1	4.09	9.00	20.22	24.35	40.25	51.50	0.5178	0.1557	0.0355	1.4251	89.17	88.63	54.17	-0.18	-0.66.7	1.7	1.9203		
2	4.29	8.74	16.73	51.33	40.98	50.39	0.5419	0.1747	0.0408	1.4104	87.32	86.72	54.24	2.91	-657.5	-26.9	1.9070		
3	4.11	8.69	15.74	46.25	41.55	50.58	0.5396	0.1656	0.0393	1.3920	87.16	86.57	54.46	8.21	-671.0	-75.8	1.8864		
4	5.36	10.15	12.39	35.16	40.29	50.00	0.5197	0.1826	0.0269	1.3657	89.90	89.46	57.11	21.95	-720.5	-205.2	1.8371		
5	7.45	12.03	9.74	22.55	38.32	45.24	0.5029	0.1270	0.0284	1.3164	85.97	85.44	60.92	31.56	-802.3	-338.4	1.7561		
6	7.58	11.91	7.73	18.00	38.24	41.30	0.5152	0.1749	0.0373	1.2883	79.60	78.89	61.95	43.94	-835.6	-406.3	1.7231		
7	7.07	11.15	6.29	14.46	38.80	40.23	0.5214	0.1949	0.0416	1.2817	77.03	76.23	61.94	45.34	-846.9	-419.6	1.7200		
8	6.88	10.69	4.33	15.41	38.97	40.17	0.5193	0.2041	0.0439	1.2810	75.31	74.87	62.26	46.64	-864.4	-437.1	1.7221		
9	8.44	11.12	3.47	14.45	37.02	41.26	0.4909	0.2123	0.0471	1.2845	73.31	72.38	65.25	50.56	-956.4	-525.7	1.7193		
10	9.04	11.22	5.91	13.65	36.15	40.74	0.4797	0.2098	0.0463	1.2805	72.75	71.80	66.24	52.59	-985.5	-562.4	1.7095		
11	9.45	11.14	9.09	12.21	35.66	40.07	0.4653	0.2055	0.0448	1.2724	72.10	71.16	66.96	54.75	-1012.2	-602.1	1.6978		

TO/TO INLET	PO/PO INLET	EFF-AD %	EFF-P INLET %	WCI/A1 LBM/SEC SQFT	TOT/TOT	PO2/P01	EFF-AD ROTOR %	EFF-P ROTOR %
1.2240	1.7749	79.42	80.99	29.11	1.1022	1.3233	81.30	82.01

STATOR 2

SL	EPI-S1-1		EPI-S2-2		V-1		V-2		VM-1		VM-2		VO-1		VO-2		B-1		B-2		M-1		M-2		U-1		U-2		V1-1	V1-2	
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC			FT/SEC
1	8.393	0.765	836.8	816.5	577.4	616.3	605.6	15.1	46.6	1.4	0.7092	0.5109	1.8371	1.2300	1.3637	1.1199															
2	7.466	0.579	813.8	823.4	559.5	623.3	590.9	5.7	46.8	0.5	0.6888	0.5175	1.8485	1.2274	1.3677	1.1193															
3	6.343	0.264	785.4	836.7	554.5	636.7	556.2	-1.2	45.2	-0.1	0.6641	0.5304	1.8679	1.2222	1.3782	1.1146															
4	3.596	-0.665	711.7	580.3	533.3	580.1	471.4	-16.3	41.5	-1.6	0.5999	0.4833	1.8143	1.2115	1.3497	1.1043															
5	-1.119	-0.976	612.5	487.7	479.7	487.1	380.9	-23.9	38.4	-2.8	0.5124	0.4041	1.7312	1.2074	1.2978	1.0955															
6	-0.168	-0.928	573.4	448.1	441.4	447.4	366.1	-24.7	39.6	-3.2	0.4777	0.3701	1.7002	1.2090	1.2720	1.0948															
7	-0.969	-0.911	568.1	442.2	431.2	441.5	369.9	-24.4	40.6	-3.2	0.4725	0.3647	1.6553	1.2116	1.2639	1.0959															
8	-1.833	-0.929	568.8	443.9	432.0	443.3	370.0	-23.2	40.5	-3.0	0.4720	0.3654	1.6953	1.2165	1.2609	1.0974															
9	-4.279	-1.141	564.2	473.1	453.5	472.7	335.7	-19.9	36.5	-2.4	0.4630	0.3859	1.7088	1.2426	1.2764	1.1022															
10	-5.049	-1.230	554.4	474.8	454.5	474.5	317.5	-15.9	35.0	-1.9	0.4530	0.3859	1.7067	1.2515	1.2784	1.1016															
11	-5.877	-1.216	543.2	454.3	455.0	454.2	296.7	-9.2	33.2	-1.2	0.4422	0.3677	1.6888	1.2586	1.2656	1.0998															

SL	INCS DEGREE	INCM	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	OMEGA-8 TOTAL	LOSS-P TOTAL	PO2/P01	EFF-P TOT	EFF-A TOT	B-1 DEGREE	B-2 DEGREE	VB-1 FT/SEC	VB-2 FT/SEC	PC/PC INLET	
																	TOT	TOT
1	-1.81	-0.25	13.21	45.24	34.25	61.99	0.4226	0.1531	0.0346	0.9562	71.70	82.42	83.84	77.12	78.08			
2	-0.65	1.37	11.77	46.25	53.02	63.01	0.4014	0.1162	0.0267	0.9681	76.56	84.29	85.56	78.30	79.22			
3	-1.40	1.11	10.74	45.35	53.00	64.90	0.3577	0.0411	0.0096	0.9894	89.89	87.88	88.88	83.55	84.26			
4	-4.03	-0.16	8.71	43.14	51.97	59.25	0.3560	0.0599	0.0149	0.9873	84.51	87.62	88.60	85.56	86.13			
5	-6.28	-0.97	7.50	41.23	46.94	49.27	0.3845	0.0942	0.0252	0.9844	76.88	81.77	83.10	80.80	81.47			
6	-4.76	1.03	7.07	43.78	43.01	44.97	0.4085	0.0963	0.0266	0.9860	77.30	78.28	79.82	74.93	75.74			
7	-3.64	2.35	7.01	43.74	41.94	44.24	0.4162	0.0997	0.0279	0.9859	76.52	76.86	78.49	71.99	72.87			
8	-3.50	2.70	7.12	43.54	41.89	44.23	0.4168	0.1089	0.0309	0.9846	74.16	75.13	76.88	70.13	71.06			
9	-7.27	-0.57	7.77	38.49	43.19	46.19	0.3481	0.0464	0.0136	0.9936	85.46	68.12	70.39	70.49	71.47			
10	-9.47	-2.59	8.86	36.90	42.93	45.98	0.3225	0.0125	0.0037	0.9984	95.37	65.54	71.31	72.27				
11	-12.54	-3.45	10.78	34.34	42.65	43.60	0.3324	0.0422	0.0126	0.9947	86.68	62.36	64.98	69.52	70.49			

NCDRR INLET RPM	HCDDRR INLET LBM/SEC	TO/TO INLET	PO/PO INLET	EFF-AD %	EFF-P INLET %	TOT/TOT	PO2/P01	EFF-AD ROTOR %	EFF-P ROTOR %
7459.	103.60	1.2240	1.7497	77.28	78.97	1.1022	0.9898	77.00	182.09

ORIGINAL PAGE IS
OF POOR QUALITY

APPENDIX E

TABLE XXXII (a) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

70% OF DESIGN SPEED

STATOR 1 (β^* des. - β^* act.) = +5^o

STATOR 2 (β^* des. - β^* act.) = +7.5^o

U. S. CUSTOMARY UNITS

ROTOR 1

SL	EFS1-1 DEGREE	EFS1-2 DEGREE	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	V0-1 FT/SEC	V0-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	M-1	M-2	RUN NO 20, SPEED CODE 70, POINT NO 1		V*-1 FT/SEC	V*-2 FT/SEC		
													U-1 FT/SEC	U-2 FT/SEC				
1	16.400	16.160	404.3	445.7	404.3	487.9	0.0	569.2	0.0	49.4	0.3668	0.6704	440.7	510.1	0.5426	0.4395	598.0	491.4
2	13.690	15.647	412.5	423.9	412.5	490.5	0.0	532.5	0.0	47.3	0.3745	0.6460	475.2	534.8	0.5713	0.4377	629.2	490.5
3	11.236	13.369	415.9	407.6	415.9	488.8	0.0	501.8	0.0	45.7	0.3814	0.6239	509.0	559.5	0.5994	0.4384	659.9	492.2
4	5.184	7.150	435.1	444.4	435.5	480.8	0.0	428.9	0.0	41.7	0.3960	0.5713	606.0	633.6	0.6787	0.4633	746.3	522.6
5	0.564	0.620	442.1	463.2	442.1	459.2	0.0	352.6	0.0	38.8	0.4022	0.4965	727.1	732.3	0.7742	0.5118	850.9	580.5
6	-2.234	-2.040	442.0	435.0	442.0	424.9	0.0	325.1	0.0	37.4	0.4021	0.4708	785.3	781.7	0.8199	0.5469	901.1	623.7
7	-3.156	-3.222	441.6	442.2	441.6	444.0	0.0	311.2	0.0	35.0	0.4018	0.4777	814.1	806.3	0.8426	0.5859	926.1	665.0
8	-4.281	-4.367	440.7	445.8	440.7	453.4	0.0	303.5	0.0	33.8	0.4009	0.4807	842.8	831.0	0.8652	0.6130	951.0	695.7
9	-4.234	-7.832	433.7	433.7	433.7	467.1	0.0	304.3	0.0	33.1	0.3943	0.4895	828.6	801.1	0.9219	0.6888	1024.8	781.0
10	-9.734	-9.665	429.5	424.5	429.5	473.2	0.0	307.7	0.0	33.0	0.3904	0.4955	857.2	824.8	0.9536	0.6862	1049.1	781.7
11	-11.133	-10.335	424.4	424.4	424.4	450.2	0.0	314.6	0.0	34.9	0.3857	0.4805	985.7	954.4	0.9752	0.6845	1073.2	782.4

SL	INCS DEGREE	INCH DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	CMEGA-B TOTAL	LOSS-P TOTAL	PO2/ PO1	%EFF-P TOT	%EFF-A TOT	B*-1 DEGREE	B*-2 DEGREE	V0*-1 FT/SEC	V0*-2 FT/SEC	PO/PO INLET
2	0.93	5.23	15.88	48.47	29.44	38.80	0.4304	-0.0822	-0.0189	1.3799	105.19	105.47	46.75	0.28	-475.2	-2.4	1.3799
3	1.24	5.30	18.25	43.46	25.89	38.95	0.4490	-0.0808	-0.0145	1.3701	104.26	104.48	40.20	6.72	-599.0	-57.7	1.3701
4	2.64	6.11	13.37	31.13	30.83	38.83	0.4608	-0.0141	-0.0035	1.3449	101.21	101.30	54.14	23.02	-666.0	-204.7	1.3449
5	4.17	6.86	10.56	17.65	31.22	35.61	0.4459	0.0599	0.0136	1.2951	92.78	92.54	58.69	40.84	-727.1	-379.7	1.2951
6	4.71	6.59	9.73	13.57	31.21	34.53	0.4232	0.0734	0.0158	1.2810	90.26	89.95	80.84	47.07	-789.3	-436.6	1.2810
7	4.95	7.08	7.82	13.46	31.19	36.26	0.3909	0.0434	0.0094	1.2901	93.96	93.77	61.93	48.14	-814.1	-495.1	1.2901
8	5.19	7.14	6.48	13.07	31.14	37.13	0.3738	0.0335	0.0073	1.2959	95.10	95.01	62.41	49.34	-842.8	-527.6	1.2959
9	5.32	7.34	5.31	12.86	30.72	38.26	0.3613	0.0585	0.0127	1.3106	91.24	90.93	64.56	52.10	-828.6	-600.8	1.3106
10	6.15	7.44	5.68	13.15	30.47	38.71	0.3597	0.0701	0.0154	1.3165	89.47	89.08	65.83	52.68	-957.2	-622.1	1.3165
11	6.55	7.51	6.43	11.91	30.16	36.58	0.3776	0.1166	0.0248	1.3042	82.48	81.84	66.69	54.78	-985.7	-639.9	1.3042

TOT/TOT	PO/PC	EFF-AD	EFF-P	MC1/A1	TOT/TOT	PC2/PO1	EFF-AD	EFF-P
INLET	INLET	INLET	INLET	LBM/SEC	STAGE	ROTOR	ROTOR	
1.0E71	1.3201	94.86	95.03	29.64	1.0871	1.3201	94.86	95.03

STATOR 1

SL	EFS1-1 DEGREE	EFS1-2 DEGREE	V-1 FT/SEC	V-2 FT/SEC	VM-1 FT/SEC	VM-2 FT/SEC	V0-1 FT/SEC	V0-2 FT/SEC	B-1 DEGREE	B-2 DEGREE	M-1	M-2	RUN NO 20, SPEED CODE 70, POINT NO 1		V*-1 FT/SEC	V*-2 FT/SEC	TOZ/ TOI
													U-1 FT/SEC	U-2 FT/SEC			
1	16.115	14.788	456.3	405.0	414.4	603.5	557.2	-41.8	47.5	-3.9	0.6788	0.5327	1.3525	1.0932	1.3525	1.0932	
2	15.732	12.926	435.2	555.9	516.7	598.4	523.0	-40.1	45.5	-3.8	0.6570	0.5285	1.3527	1.0914	1.3527	1.0914	
3	13.522	11.142	413.7	595.5	514.9	594.3	494.3	-37.6	43.9	-3.6	0.6366	0.5247	1.3516	1.0901	1.3516	1.0901	
4	7.768	6.164	660.2	574.1	504.9	572.2	425.4	-46.5	40.1	-4.6	0.5863	0.5056	1.3335	1.0871	1.3335	1.0871	
5	1.414	0.184	575.7	530.7	460.6	528.1	352.0	-52.4	37.4	-5.7	0.5118	0.4666	1.2915	1.0828	1.2915	1.0828	
6	-1.473	-2.426	552.0	512.2	446.0	509.0	325.2	-57.7	36.1	-6.5	0.4865	0.4500	1.2741	1.0813	1.2741	1.0813	
7	-2.678	-3.494	558.5	516.8	463.4	513.7	311.8	-57.0	34.0	-6.3	0.4928	0.4544	1.2743	1.0806	1.2743	1.0806	
8	-3.492	-4.416	561.9	524.1	472.2	522.0	304.6	-53.7	32.9	-5.9	0.4958	0.4614	1.2816	1.0813	1.2816	1.0813	
9	-6.401	-6.940	574.8	544.2	486.4	542.0	306.2	-48.9	32.3	-5.2	0.5059	0.4777	1.2945	1.0887	1.2945	1.0887	
10	-7.242	-7.710	582.1	549.4	452.8	547.3	309.8	-50.1	32.3	-5.3	0.5119	0.4818	1.3012	1.0921	1.3012	1.0921	
11	-6.165	-8.458	568.3	522.0	471.7	530.0	317.0	-46.5	34.0	-5.0	0.4980	0.4644	1.2879	1.0964	1.2879	1.0964	

SL	INCS DEGREE	INCM DEGREE	DEV DEGREE	TURN DEGREE	RHOVM-1	RHOVM-2	D-FAC	CMEGA-B TOTAL	LOSS-P TOTAL	PO2/ PO1	%EFF-P TOT	%EFF-A TOT	B*-1 DEGREE	B*-2 DEGREE	V0*-1 FT/SEC	V0*-2 FT/SEC	TOZ- STG
2	-0.39	2.01	12.42	45.26	40.62	49.53	0.3405	0.0770	0.0163	0.9806	80.29	98.73	98.73	98.73	98.76		
3	-0.60	2.14	11.80	41.48	40.72	49.29	0.3242	0.0543	0.0120	0.9870	84.53	95.85	95.83	95.85	95.83		
4	-1.93	1.79	9.44	44.70	40.44	47.39	0.2996	0.0343	0.0083	0.9928	87.60	98.44	98.44	98.44	98.49		
5	-3.14	1.90	8.65	43.62	37.07	43.30	0.2706	0.0099	0.0027	0.9985	93.68	91.63	91.63	91.63	91.63		
6	-3.91	1.70	7.89	42.58	35.95	41.53	0.2717	0.0463	0.0132	0.9930	71.00	88.16	88.16	88.16	88.59		
7	-5.23	0.04	8.04	40.32	37.58	41.93	0.2683	0.0755	0.0219	0.9884	52.64	85.61	85.61	85.61	85.93		
8	-6.73	0.59	8.54	36.76	38.40	42.63	0.2572	0.0750	0.0221	0.9884	47.42	90.40	90.40	90.40	90.70		
9	-7.34	0.46	10.37	31.46	39.54	44.17	0.2480	0.0673	0.0209	0.9892	42.17	87.03	87.03	87.03	87.47		
10	-7.68	0.63	11.52	31.51	39.99	44.52	0.2525	0.0683	0.0215	0.9889	42.32	84.95	84.95	84.95	85.47		
11	-6.60	0.55	13.27	39.67	38.01	42.83	0.2703	0.0799	0.0255	0.9875	41.25	77.82	77.82	77.82	78.56		

MCPRK	MCPRK	TOZ/TOI	PO/PC	EFF-AD	EFF-P	TOZ/TOI	PC2/PO1	EFF-AD	EFF-P
INLET	INLET	INLET	INLET	INLET	INLET	STAGE	ROTOR	ROTOR	
7456	130.50	1.0E71	1.3068	91.26	91.55	1.0871	0.9899	91.26	92.62

ROTOR 2

SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	U-1	U-2	M-1	M-2	PC/PC	TC2/
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	CEGPR	CEGPR	CEGPR	CEGPR	CEGPR	CEGPR	CEGPR	CEGPR	TOTAL	TOTAL
1	11.582	11.182	658.3	661.8	657.0	751.4	-40.6	632.0	-3.5	40.0	0.5827	0.48501	584.6	613.2	0.8029	0.6508	907.0	751.6
2	10.737	9.955	659.9	673.4	658.7	754.2	-39.2	615.3	-3.4	39.1	0.5847	0.48428	601.2	624.0	0.8140	0.6531	918.0	754.3
3	9.694	8.828	661.8	665.2	660.8	768.2	-36.8	584.4	-3.2	37.2	0.5869	0.48368	618.2	639.4	0.8251	0.6677	930.4	770.1
4	8.655	8.353	651.8	661.4	650.0	743.7	-46.1	434.6	-4.1	30.3	0.5781	0.47451	671.1	661.9	0.8587	0.6779	967.9	783.7
5	7.613	8.212	602.2	685.5	599.9	629.7	-52.6	281.9	-5.0	24.1	0.5228	0.45931	744.0	743.5	0.8823	0.6712	997.2	780.7
6	6.567	7.251	577.5	599.6	574.6	559.2	-57.9	217.1	-5.8	21.2	0.5102	0.5142	781.2	776.3	0.8584	0.6780	1017.0	790.9
7	5.567	6.211	579.2	565.0	576.4	552.0	-57.1	193.7	-5.7	19.3	0.5119	0.5020	799.9	793.3	0.9129	0.6994	1032.4	815.0
8	4.597	5.036	585.6	603.5	563.1	576.9	-54.0	177.2	-5.3	17.0	0.5177	0.5194	818.8	810.6	0.9129	0.7373	1049.7	856.7
9	3.720	4.255	604.2	635.1	602.2	615.3	-49.5	157.5	-4.7	14.3	0.5331	0.5470	876.2	864.2	0.9744	0.8071	1104.3	937.1
10	3.244	3.519	606.5	636.7	604.8	618.2	-50.6	152.1	-4.8	13.8	0.5348	0.5476	895.5	882.6	0.9494	0.8231	1122.9	957.9
11	2.016	2.755	588.4	587.6	588.5	570.9	-47.1	139.0	-4.6	13.6	0.5165	0.5030	914.8	901.4	0.9890	0.8153	1126.6	952.5

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P	PO2/	%EFF-P	%EFF-A	B-1	B-2	V0-1	V0-2	PC/PC
DEGREE	DEGREE	DEGREE	DEGREE							TOTAL	TOTAL	TOTAL	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	-2.97	-1.66	18.57	44.43	52.75	62.45	0.3436	0.2196	0.0560	1.3795	80.57	79.69	43.50	-1.42	-625.2	18.8	1.8658
2	-5.76	-1.36	14.63	43.36	52.92	63.56	0.3479	0.1927	0.0450	1.3886	82.59	81.78	44.17	0.81	-640.3	-10.7	1.8784
3	-5.59	-1.01	11.61	40.66	53.04	65.84	0.3340	0.1366	0.0326	1.4007	87.18	86.58	44.76	4.08	-655.0	-55.0	1.8931
4	-3.92	0.88	8.83	29.44	51.86	65.41	0.3178	0.0830	0.0195	1.3398	90.44	90.07	47.83	18.35	-717.2	-247.3	1.7858
5	-0.45	4.12	8.02	16.17	47.64	55.28	0.3112	0.1076	0.0246	1.2286	82.10	81.62	53.02	36.25	-796.6	-461.6	1.5844
6	1.22	5.56	8.77	10.62	45.61	48.74	0.3031	0.1380	0.0290	1.1703	72.75	72.19	55.60	44.98	-839.1	-559.3	1.4912
7	1.44	5.27	8.66	16.17	47.64	48.18	0.2854	0.1287	0.0266	1.1571	72.64	72.12	56.07	47.32	-857.1	-599.6	1.4774
8	0.85	4.66	5.28	8.43	46.39	50.61	0.2528	0.0849	0.0179	1.1653	80.58	80.20	56.23	47.60	-872.8	-633.4	1.4937
9	0.09	2.77	1.74	8.06	47.78	53.91	0.2164	0.0408	0.0112	1.1710	87.43	87.20	56.40	46.84	-925.7	-706.8	1.5187
10	0.15	2.33	2.96	7.71	47.94	53.92	0.2129	0.0558	0.0131	1.1660	85.19	84.92	57.35	49.64	-946.1	-730.5	1.5170
11	1.04	2.74	7.41	5.46	46.26	49.23	0.2168	0.0788	0.0179	1.1397	77.57	77.20	58.55	53.07	-961.9	-762.4	1.4676

TO/TO	PO/PC	EFF-AD	EFF-P	WCI/41	T02/T01	P02/P01	EFF-AD	EFF-P
INLET	INLET	INLET	INLET	LBM/SEC	INLET	INLET	%	%
		%	%	SQFT				
1.1655	1.6276	88.04	88.82	37.24	1.0758	1.2455	85.28	85.70

STATOR 2

SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	PC/PC	TO/TO	PC/PC	TC2/
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	CEGPR	CEGPR	CEGPR	CEGPR	CEGPR	TOTAL	TOTAL	TOTAL
1	8.611	0.743	1027.5	955.2	815.0	949.4	625.7	-136.4	37.8	-8.2	0.8958	0.8276	1.7325	1.2252	1.2809	1.1205
2	7.559	0.584	1016.4	961.0	812.8	955.9	610.2	-99.1	37.1	-5.9	0.8856	0.8303	1.7449	1.2231	1.2899	1.1204
3	6.623	0.409	1005.7	970.5	821.2	964.2	580.6	-109.8	35.4	-6.5	0.8771	0.8414	1.7715	1.2184	1.3103	1.1176
4	4.468	-0.172	899.4	935.7	787.4	924.7	434.5	-142.6	29.0	-8.8	0.7817	0.8163	1.7448	1.1944	1.3067	1.0985
5	1.757	-0.904	727.0	802.3	669.7	791.1	283.0	-150.8	22.9	-10.8	0.6273	0.7006	1.5781	1.1642	1.2213	1.0752
6	0.003	-1.240	637.3	723.2	558.9	708.4	217.8	-145.4	20.0	-11.6	0.5481	0.6271	1.4834	1.1507	1.1643	1.0642
7	-1.066	-1.370	620.6	657.5	585.5	683.1	194.1	-142.9	18.2	-11.8	0.5343	0.6052	1.4568	1.1450	1.1414	1.0595
8	-2.004	-1.420	637.6	693.5	612.4	679.1	177.6	-140.8	16.2	-11.7	0.5505	0.6021	1.4516	1.1417	1.1327	1.0558
9	-4.017	-1.364	672.2	725.7	653.3	714.5	158.3	-126.8	13.6	-10.0	0.5810	0.6308	1.4771	1.1462	1.1390	1.0528
10	-4.698	-1.325	678.6	727.6	661.1	717.7	153.1	-119.6	13.1	-9.4	0.5860	0.6316	1.4745	1.1457	1.1335	1.0526
11	-5.508	-1.231	636.9	682.0	623.3	673.3	140.0	-108.6	12.7	-9.1	0.5494	0.5840	1.4226	1.1504	1.1107	1.0492

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P	PO2/	%EFF-P	%EFF-A	B-1	B-2	V0-1	V0-2	PC/PC
DEGREE	DEGREE	DEGREE	DEGREE							TOTAL	TOTAL	TOTAL	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	-3.17	-1.61	11.16	45.94	65.43	74.48	0.2341	0.1745	0.0390	0.9291	-1.63	75.42	77.22	80.69	62.01	62.01	1.1205
2	-2.81	-0.79	12.84	43.02	66.33	75.51	0.2159	0.1743	0.0399	0.9302	-23.03	77.21	78.89	62.53	63.82	63.82	1.1204
3	-3.71	-1.21	11.85	41.52	68.29	77.01	0.1990	0.1611	0.0375	0.9363	-70.25	81.22	82.04	68.16	69.32	69.32	1.1176
4	-9.10	-5.23	9.05	37.73	67.62	75.55	0.1312	0.0866	0.0217	0.9698	237.64	88.61	89.45	80.56	81.26	81.26	1.0985
5	-14.31	-5.00	7.02	33.66	57.73	64.84	0.0668	0.0499	0.0131	0.9881	121.48	84.61	85.54	77.82	78.39	78.39	1.0752
6	-16.93	-11.15	6.13	31.55	51.35	57.78	0.0317	0.0484	0.0131	0.9909	115.77	79.08	80.19	69.02	69.63	69.63	1.0642
7	-18.52	-12.53	5.66	30.01	50.63	55.69	0.0262	0.0707	0.0194	0.9873	127.75	78.28	79.38	64.62	65.23	65.23	1.0595
8	-20.40	-14.19	5.51	27.85	52.88	55.43	0.0535	0.1455	0.0416	0.9722	171.01	74.33	80.36	64.96	65.53	65.53	1.0528
9	-22.67	-15.98	7.62	23.67	56.21	58.15	0.0446	0.1339	0.0387	0.9726	169.84	80.66	81.67	71.63	72.10	72.10	1.0526
10	-23.91	-17.03	8.83	22.50	56.50	58.11	0.0469	0.1353	0.0395	0.9720	178.36	78.42	79.54	68.98	69.47	69.47	1.0492
11	-25.54	-18.44	10.21	21.84	52.53	53.84	0.0484	0.1657	0.0488	0.9693	205.21	70.45	71.65	58.53	59.06	59.06	1.0492

WCI/41	WCI/PC	TO/TO	PO/PC	EFF-AD	EFF-P	T02/T01	P02/P01	EFF-AD	EFF-P
INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET	STAGE	T01-STG
RPM	LBM/SEC			%	%			%	%
7458	130.50	1.1655	1.5771	81.98	83.08	1.0758	0.9690	72.72	-373.66

TABLE XXXII (b) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

70% OF DESIGN SPEED

STATOR 1 ($\beta^*_{des.} - \beta^*_{act.}$) = +5°
 STATOR 2 ($\beta^*_{des.} - \beta^*_{act.}$) = +7.5°

U. S. CUSTOMARY UNITS

ROTOR 1

SL	EFSI-1		EFSI-2		V-1		V-2		VM-1		VM-2		V0-1		V0-2		B-1		B-2		M-1		M-2		U-1		U-2		M+1		M+2		V1-1		V1-2		
DEGREE	DEGREE		FT/SEC		FT/SEC		FT/SEC		FT/SEC		FT/SEC		FT/SEC		DEGREE		DEGREE		FT/SEC		FT/SEC		FT/SEC		FT/SEC		FT/SEC		FT/SEC		FT/SEC		FT/SEC		FT/SEC		
1	16.436	18.134	365.5	739.7	365.5	439.5	0.0	594.9	0.0	0.0	54.5	0.3309	0.6595	438.7	507.9	0.5169	0.3995	571.0	448.1																		
2	15.766	15.621	372.5	711.9	372.5	439.2	0.0	560.3	0.0	0.0	51.9	0.3373	0.6331	473.0	532.4	0.5452	0.3913	602.1	440.1																		
3	11.357	13.308	378.8	687.5	378.8	439.4	0.0	528.7	0.0	0.0	50.2	0.3432	0.6100	506.7	557.0	0.5732	0.3908	632.7	440.4																		
4	5.239	7.327	391.9	632.9	391.9	429.7	0.0	464.7	0.0	0.0	47.2	0.3554	0.5586	403.3	630.8	0.6523	0.4066	719.4	460.7																		
5	-0.183	0.953	397.0	561.5	397.0	389.5	0.0	404.5	0.0	0.0	46.1	0.3600	0.4922	723.8	729.0	0.7487	0.4443	825.5	506.9																		
6	-2.031	-1.667	396.9	546.8	396.9	394.0	0.0	379.1	0.0	0.0	43.9	0.3600	0.4786	781.8	778.2	0.7952	0.4909	876.8	560.8																		
7	-3.145	-2.883	396.5	550.2	396.5	412.2	0.0	364.4	0.0	0.0	41.5	0.3596	0.4819	810.4	802.7	0.8183	0.5270	902.2	601.6																		
8	-4.442	-4.076	395.5	549.9	395.5	414.6	0.0	361.2	0.0	0.0	41.1	0.3586	0.4812	839.0	827.3	0.8412	0.5659	927.5	623.8																		
9	-8.567	-7.722	388.0	558.4	388.0	420.5	0.0	367.5	0.0	0.0	41.1	0.3517	0.4866	924.4	901.0	0.9088	0.5920	1002.5	679.3																		
10	-10.031	-9.007	384.1	562.5	384.1	418.2	0.0	376.3	0.0	0.0	41.9	0.3481	0.4891	952.9	925.6	0.9310	0.6003	1027.3	690.4																		
11	-11.302	-10.311	379.5	548.7	379.5	394.5	0.0	381.3	0.0	0.0	43.9	0.3438	0.4755	981.3	950.2	0.9532	0.6000	1052.1	692.3																		

SL	INCS	INCH	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-S	LOSS-P	P02/	%EFF-P	%EFF-A	B*-1	B*-2	V0*-1	V0*-2	P0/P0	
DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	P01	TOT	TOT	DEGREE	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	3.56	8.16	16.75	61.15	26.48	34.55	0.4635	-0.0299	-0.0065	1.3893	101.49	101.59	49.94	-11.21	-438.7	87.1	1.3893	
2	3.69	7.98	15.98	55.12	26.93	34.89	0.4988	-0.0132	-0.0020	1.3804	100.74	100.80	51.50	-3.62	-473.0	27.8	1.3804	
3	3.95	8.06	15.21	49.28	27.33	35.21	0.5168	-0.0026	-0.0006	1.3724	100.15	100.19	52.96	3.68	-506.7	-28.3	1.3724	
4	5.34	8.81	11.41	35.75	28.16	34.99	0.5389	0.0416	0.0103	1.3554	96.63	96.51	56.84	21.10	-603.3	-166.1	1.3554	
5	6.73	9.41	9.52	21.45	28.48	31.97	0.5356	0.1157	0.0267	1.3227	88.36	87.93	61.25	39.80	-723.8	-324.5	1.3227	
6	7.16	9.44	8.03	17.72	28.47	32.55	0.4974	0.1060	0.0236	1.3227	88.33	87.89	63.09	45.37	-781.8	-399.1	1.3227	
7	7.36	9.46	6.46	17.17	28.45	34.22	0.4636	0.0784	0.0174	1.3306	90.93	90.58	63.94	46.77	-810.4	-438.3	1.3306	
8	7.56	9.51	5.49	16.43	28.38	34.48	0.4560	0.0841	0.0186	1.3345	90.01	89.62	64.78	48.35	-839.0	-466.1	1.3345	
9	8.20	9.62	4.92	15.52	27.91	34.94	0.4511	0.1230	0.0270	1.3497	84.84	84.21	67.24	51.72	-924.4	-533.5	1.3497	
10	8.38	9.67	5.66	15.40	27.66	34.67	0.4591	0.1477	0.0324	1.3546	81.84	81.08	68.06	52.66	-952.9	-569.3	1.3546	
11	8.52	9.67	8.82	13.69	27.38	32.55	0.4740	0.1854	0.0391	1.3452	77.02	76.07	68.85	55.16	-981.3	-568.8	1.3452	

TO/TO	P0/P0	EFF-AD	EFF-P	WC1/A1	TO2/TO1	P02/P01	EFF-AD	EFF-P
INLET	INLET	INLET	INLET	LBM/SEC	%	%	ROTOR	ROTOR
%	%	%	%	SCFT			%	%
1.0993	1.3466	89.40	89.81	26.98	1.0993	1.3466	89.40	89.81

STATOR 1

SL	EFSI-1		EFSI-2		V-1		V-2		VM-1		VM-2		V0-1		V0-2		B-1		B-2		M-1		M-2		PO/P0		TO/TO		PO/P0		TO2/TO1						
DEGREE	DEGREE		FT/SEC		FT/SEC		FT/SEC		FT/SEC		FT/SEC		FT/SEC		DEGREE		DEGREE		FT/SEC		FT/SEC		FT/SEC		INLET		INLET		STAGE		STAGE						
1	16.150	14.849	743.1	514.1	461.6	512.3	582.4	-43.1	51.8	-4.8	0.6628	0.4484	1.3429	1.0970	1.3429	1.0970																					
2	15.806	13.062	717.9	512.7	461.1	511.3	550.3	-37.6	50.2	-4.2	0.6389	0.4474	1.3456	1.0958	1.3456	1.0958																					
3	13.643	11.362	695.4	512.3	460.9	511.1	520.8	-35.3	48.5	-3.9	0.6177	0.4473	1.3478	1.0945	1.3478	1.0945																					
4	8.100	6.613	644.0	496.3	449.7	494.8	460.9	-38.3	45.7	-4.4	0.5690	0.4328	1.3382	1.0941	1.3382	1.0941																					
5	1.760	0.726	574.2	463.8	408.2	460.6	403.8	-54.2	44.7	-6.7	0.5038	0.4034	1.3132	1.0947	1.3132	1.0947																					
6	-1.025	-1.815	559.9	459.2	411.8	456.1	379.4	-52.5	42.7	-6.6	0.4907	0.3993	1.3085	1.0946	1.3085	1.0946																					
7	-2.152	-2.855	563.2	468.2	428.6	465.4	365.3	-50.3	40.5	-6.2	0.4939	0.4075	1.3141	1.0941	1.3141	1.0941																					
8	-3.141	-3.782	563.2	473.4	431.0	470.8	362.5	-49.9	40.1	-6.1	0.4934	0.4118	1.3177	1.0961	1.3177	1.0961																					
9	-5.980	-6.401	572.8	489.2	427.6	487.6	369.7	-40.0	40.3	-4.7	0.4998	0.4240	1.3301	1.1062	1.3301	1.1062																					
10	-6.932	-7.256	577.5	493.1	436.0	491.8	378.8	-34.5	41.1	-4.0	0.5028	0.4264	1.3335	1.1117	1.3335	1.1117																					
11	-8.013	-8.172	564.8	474.0	413.9	472.2	384.3	-40.8	43.0	-5.0	0.4902	0.4085	1.3215	1.1163	1.3215	1.1163																					

SL	INCS	INCH	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-S	LOSS-P	P02/	%EFF-P	%EFF-A	B*-1	B*-2	V0*-1	V0*-2	P0/P0
DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	TOTAL	TOTAL	TOTAL	TOTAL	TOTAL	P01	STATC-ST	TOT-INLET	TOT-INLET	TOT-STG	TOT-STG	TOT-STG	TOT-STG
1	4.23	6.34	12.57	56.54	36.22	43.46	0.4741	0.1306	0.0266	0.9666	78.36	90.66	91.01	90.66	91.01	90.66	
2	4.32	6.72	12.06	54.33	36.50	42.53	0.4541	0.1048	0.0222	0.9748	81.41	92.47	92.75	92.47	92.75	92.47	
3	4.02	6.61	11.46	52.48	36.77	43.63	0.4347	0.0784	0.0173	0.9822	84.98	94.24	94.45	94.24	94.45	94.24	
4	3.69	7.41	9.86	50.10	36.41	42.21	0.4154	0.0629	0.0153	0.9876	86.19	92.29	92.57	92.29	92.57	92.29	
5	4.17	9.21	7.61	51.36	33.32	39.00	0.4087	0.0494	0.0123	0.9928	87.93	85.56	86.07	85.56	86.07	85.56	
6	2.64	8.25	7.74	45.22	33.83	38.55	0.4007	0.0742	0.0211								

ROTOR 2

SL	EPSI-1		EPSI-2		V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	RUN NO 20, SPEED CODE 70, POINT NO 3		M'-1	M'-I	V'-1	V'-2
	DEGREE	DEGREE	FT/SEC	FT/SEC											FT/SEC	FT/SEC				
1	11.603	11.016	554.4	875.7	552.8	615.8	-41.9	622.6	-4.3	45.2	0.4851	0.7468	582.0	610.4	0.7294	0.5252	833.6	615.9		
2	10.767	9.690	558.3	859.5	557.1	611.1	-36.7	604.4	-3.8	44.6	0.4890	0.7326	598.5	623.2	0.7399	0.5211	844.9	611.4		
3	9.752	8.432	562.6	836.8	561.6	614.2	-34.6	588.3	-3.5	42.7	0.4933	0.7132	615.4	636.5	0.7521	0.5267	859.0	618.0		
4	5.914	4.900	556.3	755.5	555.0	596.0	-37.8	464.3	-3.9	37.9	0.4876	0.6420	668.1	678.8	0.7870	0.5383	898.0	633.4		
5	0.059	0.343	522.3	634.9	519.5	525.2	-54.0	356.7	-5.9	34.2	0.4563	0.5357	740.7	740.2	0.8295	0.5487	944.5	650.3		
6	-2.390	-1.669	512.3	578.2	509.6	479.6	-52.5	323.1	-5.9	33.9	0.4472	0.4865	777.7	772.9	0.8504	0.5532	974.1	657.5		
7	-3.291	-2.514	518.2	566.6	515.7	476.9	-50.6	305.9	-5.6	32.6	0.4527	0.4769	796.3	789.9	0.8663	0.5718	991.6	679.3		
8	-4.134	-3.250	522.6	568.0	520.2	491.2	-50.1	285.3	-5.5	30.1	0.4562	0.4785	815.1	806.9	0.8814	0.6035	1009.6	716.5		
9	-6.823	-6.196	538.9	585.2	537.4	513.2	-40.4	281.2	-4.3	28.6	0.4689	0.4910	872.3	860.4	0.9216	0.6493	1059.2	773.8		
10	-7.657	-7.224	543.0	585.5	541.9	512.6	-34.9	283.0	-3.7	28.8	0.4714	0.4900	891.4	878.7	0.9317	0.6577	1073.2	785.9		
11	-8.480	-8.385	525.7	572.7	524.1	503.3	-41.3	273.2	-4.5	28.4	0.4548	0.4775	910.7	897.3	0.9401	0.6685	1086.7	801.7		

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P	PO2/	%EFF-P	%EFF-A	B'-1	B'-2	VM'-1	VM'-2	PO/PO
DEGREE	DEGREE	DEGREE	DEGREE	DEGREE				TOTAL	TOTAL	P01	TOT	TOT	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	-1.10	3.22	19.27	49.51	46.13	56.30	0.4467	0.1317	0.0300	1.4224	89.94	89.44	48.38	-1.13	-673.9	12.2	1.9101
2	-1.23	3.22	15.80	46.97	46.55	56.46	0.4566	0.1237	0.0285	1.4175	90.22	89.74	48.73	1.76	-635.2	-18.8	1.9074
3	-1.16	3.41	13.85	42.87	46.96	57.40	0.4509	0.1014	0.0241	1.4064	91.45	91.05	49.19	6.32	-650.0	-68.2	1.8955
4	0.10	4.90	10.23	32.07	46.22	56.91	0.4392	0.0568	0.0138	1.3695	94.31	94.07	51.85	19.79	-705.9	-214.6	1.8323
5	3.36	7.93	7.92	20.89	43.03	50.38	0.4377	0.0775	0.0178	1.3105	90.32	89.97	56.83	36.14	-794.7	-383.5	1.7203
6	4.08	8.42	6.93	15.31	42.24	45.92	0.4401	0.1118	0.0242	1.2750	84.84	84.34	58.45	43.14	-830.2	-449.8	1.6693
7	3.77	7.85	6.11	13.27	42.85	45.76	0.4246	0.1106	0.0237	1.2640	84.22	83.72	58.64	45.37	-846.9	-483.8	1.6613
8	3.57	7.38	4.34	12.30	43.18	47.26	0.3940	0.0830	0.0178	1.2634	87.41	87.01	58.95	46.66	-865.2	-521.6	1.6648
9	2.62	5.30	1.24	11.10	44.38	49.13	0.3745	0.0828	0.0192	1.2654	86.77	86.35	59.43	48.33	-912.7	-579.2	1.6826
10	2.37	4.55	2.48	10.42	44.59	48.85	0.3740	0.0898	0.0213	1.2612	85.41	84.95	59.57	49.15	-926.3	-595.7	1.6828
11	3.55	5.25	5.33	10.07	42.87	47.66	0.3705	0.0883	0.0210	1.2639	85.59	85.13	61.06	50.99	-957.0	-624.1	1.6707

TC/TO	PD/PO	EFF-AD	EFF-P	WCI/A1	TC2/TO1	PO2/PO1	EFF-AD	EFF-P
INLET	INLET	%	%	LBM/SEC	STAGE	STAGE	%	%
1.1993	1.7456	86.52	87.51	33.57	1.0909	1.3154	89.43	89.81

STATOR 2

SL	EPSI-1		EPSI-2		V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	RUN NO 20, SPEED CODE 70, POINT NO 3			
	DEGREE	DEGREE	FT/SEC	FT/SEC											FT/SEC	FT/SEC	FT/SEC	FT/SEC
1	8.462	0.616	503.4	748.7	660.4	744.2	616.5	-81.7	43.3	-6.3	0.7732	0.6291	1.8572	1.2267	1.3830	1.1182		
2	7.258	0.330	666.0	746.9	652.6	741.6	599.2	-88.7	42.8	-6.8	0.7576	0.6283	1.8603	1.2237	1.3826	1.1167		
3	6.144	0.020	862.2	744.4	652.0	738.2	564.1	-95.8	41.0	-7.4	0.7371	0.6278	1.8632	1.2174	1.3823	1.1122		
4	3.460	-0.761	778.8	693.8	626.6	688.3	462.4	-101.6	36.5	-8.4	0.6635	0.5858	1.8083	1.2034	1.3515	1.0992		
5	0.692	-1.369	657.0	602.3	551.9	593.0	356.4	-105.3	32.8	-10.1	0.5555	0.5067	1.7099	1.1923	1.3025	1.0891		
6	-0.883	-1.556	600.6	550.2	506.2	539.4	323.2	-108.6	32.5	-11.4	0.5062	0.4619	1.6595	1.1876	1.2675	1.0851		
7	-1.730	-1.579	588.9	537.5	503.1	525.0	306.1	-115.6	31.3	-12.4	0.4966	0.4514	1.6478	1.1845	1.2537	1.0825		
8	-2.475	-1.533	590.3	527.9	516.5	524.6	285.9	-119.1	29.0	-12.8	0.4981	0.4521	1.6472	1.1830	1.2500	1.0793		
9	-4.376	-1.364	611.2	563.6	542.0	558.5	282.7	-75.6	27.6	-7.7	0.5140	0.4721	1.6616	1.1949	1.2494	1.0804		
10	-5.086	-1.329	614.8	568.6	545.0	564.3	284.6	-69.9	27.6	-7.1	0.5158	0.4752	1.6622	1.2010	1.2460	1.0805		
11	-5.895	-1.233	607.4	551.7	541.5	547.5	275.2	-68.0	27.0	-7.1	0.5080	0.4593	1.6428	1.2069	1.2430	1.0811		

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P	PO2/	%EFF-P	%EFF-A	%EFF-P	%EFF-A	%EFF-P	%EFF-A
DEGREE	DEGREE	DEGREE	DEGREE	DEGREE				TOTAL	TOTAL	P01	STAGE-ST	TOT-INLET	TOT-INLET	TOT-STG	TOT-STG	TOT-STG
1	2.34	3.90	13.06	49.54	59.20	71.22	0.3454	0.0850	0.0191	0.9722	78.10	85.27	86.47	81.96	82.75	
2	2.84	4.86	11.94	49.57	59.29	71.30	0.3357	0.0783	0.0179	0.9752	78.12	86.67	87.76	82.94	83.68	
3	1.87	4.37	10.96	48.40	59.99	71.47	0.3164	0.0571	0.0133	0.9826	81.78	89.41	90.28	86.16	86.76	
4	-1.58	2.28	9.39	44.90	59.08	66.81	0.2895	0.0519	0.0127	0.9867	78.77	90.61	91.34	89.88	90.28	
5	-4.38	0.93	7.74	42.89	52.42	57.37	0.2730	0.0346	0.0091	0.9934	81.04	86.08	87.07	87.00	88.22	
6	-4.37	1.42	6.35	43.90	48.01	51.92	0.2832	0.0370	0.0100	0.9941	79.24	82.94	84.09	82.21	82.77	
7	-5.44	0.55	5.26	43.70	47.84	50.54	0.2886	0.0523	0.0143	0.9919	71.61	83.09	84.22	80.74	81.32	
8	-7.40	-1.39	4.84	41.72	49.24	50.52	0.2839	0.0681	0.0189	0.9894	63.43	83.70	84.78	82.92	83.42	
9	-8.73	-2.04	9.97	35.27	51.32	53.25	0.2505	0.0765	0.0222	0.9874	53.89	80.07	81.42	81.54	82.09	
10	-9.34	-2.46	11.22	34.67	51.30	53.48	0.2462	0.0731	0.0215	0.9879	54.35	77.67	79.18	80.35	80.92	
11	-11.22	-4.12	12.37	34.08	50.55	51.39	0.2610	0.1027	0.0304	0.9834	46.80	73.61	75.36	78.86	79.48	

NCORR	WCDRR	TD/TO	PD/PO	EFF-AD	EFF-P	TC2/TO1	PO2/PO1	EFF-AD	EFF-P
INLET	INLET	INLET	INLET	%	%	STAGE	STAGE	%	%
7464.	118.80	1.1993	1.7230	84.33	85.46	1.0909	0.9870	85.00	86.47

TABLE XXXII (c) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

70% OF DESIGN SPEED

STATOR 1 (beta*_des. - beta*_act.) = +5 degrees
STATOR 2 (beta*_des. - beta*_act.) = +7.5 degrees

U. S. CUSTOMARY UNITS

ROTOR 1

Table with columns: SL, EPI-1, EPI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, U-1, U-2, M1-1, M1-2, V1-1, V1-2. Headers include RUN NO 20, SPEED CODE 70, POINT NO 13. Rows 1-11 show performance data.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, CMEGA-B, LOSS-P, PO2, WEFF-P, WEFF-A, B*-1, B*-2, VB*-1, VB*-2, PO/PQ. Rows 1-11 show detailed performance metrics.

Summary table with columns: TO/TO, PO/PD, EFF-AD, EFF-P, WCI/A1, TO2/TO1, PO2/PO1, EFF-AD, EFF-P. Includes inlet and rotor rotor values.

STATOR 1

Table with columns: SL, EPI-1, EPI-2, V-1, V-2, VM-1, VM-2, V0-1, V0-2, B-1, B-2, M-1, M-2, PO/PD, TO/TO, INLET, STAGE, TO2/. Headers include RUN NO 20, SPEED CODE 70, POINT NO 13. Rows 1-11 show performance data.

Table with columns: SL, INCS, INCM, DEV, TURN, RHOVM-1, RHOVM-2, D-FAC, CMEGA-B, LOSS-P, PO2, WEFF-P, WEFF-A, WEFF-P, WEFF-A, WEFF-P. Rows 1-11 show detailed performance metrics.

Summary table with columns: NCORR, WCORR, TO/TO, PO/PD, EFF-AD, EFF-P, TO2/TO1, PO2/PO1, EFF-AD, EFF-P. Includes inlet and stator-stg values.

ROTOR 2

RUN NO 20, SPEED CODE 70, POINT NO 13																				
SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	U-1	U-2	M-1	M-1	V-1	V-2		
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			FT/SEC	FT/SEC			FT/SEC	FT/SEC	FT/SEC	FT/SEC
1	11.599	10.568	511.5	86C.1	510.0	578.3	-40.0	636.6	-4.5	47.6	0.4460	0.7312	581.6	61C.0	C.7010	0.4922	804.0	578.9		
2	10.756	9.606	516.0	843.3	514.8	570.0	-35.0	621.5	-3.9	47.4	0.4504	0.7164	598.0	622.8	0.7122	0.4842	816.0	570.0		
3	9.732	8.323	521.5	820.2	520.4	577.4	-33.5	582.5	-3.7	45.2	0.4555	0.6967	615.0	636.1	C.7263	0.4926	831.5	579.9		
4	5.826	4.750	517.2	738.5	516.2	556.8	-33.3	485.2	-3.7	41.0	0.4516	0.6251	667.6	678.4	0.7600	0.4988	870.5	589.4		
5	-0.014	0.234	489.6	632.8	487.3	502.3	-47.9	384.8	-5.6	37.5	0.4261	0.5319	740.2	739.7	C.8064	0.5170	926.6	615.0		
6	-2.576	-1.837	483.8	585.6	481.6	463.7	-45.4	357.7	-5.4	37.6	0.4209	0.4910	777.1	772.3	0.8294	0.5215	953.2	622.0		
7	-3.497	-2.682	491.3	575.4	489.7	456.4	-39.8	350.4	-4.6	37.5	0.4278	0.4822	795.8	789.1	0.8432	0.5306	968.5	633.1		
8	-4.269	-3.468	497.6	577.7	456.2	465.7	-37.0	341.8	-4.3	36.2	0.4330	0.4840	814.6	806.4	C.8576	0.5511	985.6	657.8		
9	-6.800	-6.179	501.7	588.5	500.4	486.7	-36.4	330.7	-4.1	34.1	0.4341	0.4900	871.6	859.8	C.8969	0.5986	1036.8	718.9		
10	-7.699	-7.268	497.6	584.8	456.5	477.5	-33.0	337.7	-3.8	35.1	0.4290	0.4848	890.8	878.1	0.9043	0.5977	1048.8	721.1		
11	-8.548	-8.448	482.1	562.8	481.7	463.7	-36.5	319.0	-4.3	34.4	0.4149	0.4649	910.0	896.7	0.9122	0.6119	1062.0	740.7		

SL	INCS	INCM	DEV	TURN	RMDVM-1	RMDVM-2	D-FAC	CMEGA-B	LOSS-P	PO2/	%EFF-P	%EFF-A	B-1	B-2	V0-1	V0-2	PO/PC
DEGREE	DEGREE	DEGREE	DEGREE					TOTAL	TOTAL	PO1	TOT	TOT	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	1.08	5.40	17.78	53.16	43.13	53.28	0.4760	0.1520	0.0346	1.4267	89.26	88.72	50.56	-2.62	-621.6	26.6	1.9091
2	0.91	5.36	13.95	56.73	43.63	53.04	0.4928	0.1531	0.0358	1.4207	88.80	88.25	50.86	0.13	-633.1	-1.3	1.9056
3	0.92	5.49	12.81	45.59	44.12	54.32	0.4827	0.1267	0.0302	1.4085	90.08	89.60	51.27	5.28	-648.5	-53.5	1.8931
4	1.91	6.70	9.56	34.54	43.61	53.42	0.4773	0.0922	0.0224	1.3686	91.37	91.00	53.66	19.12	-701.0	-193.2	1.8295
5	4.80	9.38	7.02	23.03	40.94	48.48	0.4690	0.1025	0.0237	1.3190	88.28	87.83	56.27	36.24	-788.1	-356.5	1.7388
6	5.28	9.61	5.57	17.86	40.54	44.72	0.4735	0.1380	0.0305	1.2881	82.98	82.39	59.65	41.78	-822.6	-416.6	1.6981
7	4.74	8.82	4.58	15.78	41.32	44.05	0.4694	0.1499	0.0330	1.2768	80.86	80.22	59.61	43.83	-835.6	-438.8	1.6911
8	4.36	8.17	2.55	14.87	41.85	44.98	0.4528	0.1421	0.0315	1.2756	81.27	80.64	59.74	44.87	-851.6	-464.6	1.6955
9	4.25	8.93	0.16	13.81	41.80	46.64	0.4292	0.1354	0.0321	1.2825	81.34	80.69	61.06	47.26	-908.0	-529.1	1.7091
10	4.46	6.63	1.72	13.26	41.23	45.40	0.4396	0.1511	0.0364	1.2818	79.32	78.60	61.66	48.40	-923.9	-540.4	1.7055
11	5.42	7.12	5.47	11.81	39.75	43.83	0.4278	0.1417	0.0336	1.2762	79.88	79.20	62.93	51.13	-946.5	-577.7	1.6881

TO/TO PO/PC EFF-AD EFF-P WCI/A1 T02/T01 P02/P01 EFF-AD EFF-P
INLET INLET INLET INLET LBM/SEC ROTOR ROTOR ROTOR ROTOR
1.2101 1.7608 83.38 84.63 31.74 1.0975 1.3239 85.44 85.99

STATOR 2

RUN NO 20, SPEED CODE 70, POINT NO 13																			
SL	EPSI-1	EPSI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	PO/PO	TO/TO	PO/PO	ICQ7			
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			INLET	INLET	STAGE	TO1			
1	8.463	0.643	883.0	667.3	618.3	684.4	630.3	-63.0	45.8	-5.3	0.7528	0.5734	1.8453	1.2293	1.3792	1.1202			
2	7.243	0.362	865.2	689.1	667.5	686.0	616.2	-65.3	45.6	-5.4	0.7370	0.5757	1.8521	1.2266	1.3811	1.1195			
3	6.105	0.031	841.3	652.7	611.2	687.9	578.2	-81.0	43.6	-6.7	0.7164	0.5803	1.8617	1.2207	1.3852	1.1146			
4	3.425	-0.771	758.1	639.3	584.2	633.4	483.1	-87.0	39.6	-7.8	0.6429	0.5359	1.8071	1.2082	1.3516	1.1028			
5	0.651	-1.338	651.2	558.2	525.7	550.2	384.4	-94.3	36.2	-9.7	0.5483	0.4663	1.7261	1.2003	1.3093	1.0935			
6	-0.748	-1.455	604.1	511.7	466.7	506.5	357.9	-97.0	36.3	-10.8	0.5073	0.4301	1.6878	1.1968	1.2805	1.0909			
7	-1.533	-1.471	594.0	503.6	479.3	494.3	350.8	-97.1	36.2	-11.1	0.4986	0.4200	1.6773	1.1959	1.2665	1.0900			
8	-2.280	-1.443	596.4	501.2	488.2	493.9	342.5	-96.4	35.0	-11.0	0.5004	0.4193	1.6755	1.1971	1.2606	1.0891			
9	-4.184	-1.279	611.0	523.8	512.6	517.2	332.4	-82.4	33.0	-9.0	0.5097	0.4340	1.6850	1.2130	1.2644	1.0911			
10	-4.885	-1.251	610.6	526.8	507.4	522.2	339.7	-69.8	33.8	-7.6	0.5073	0.4348	1.6838	1.2229	1.2654	1.0933			
11	-5.763	-1.191	593.8	508.2	499.3	506.3	321.3	-62.9	32.8	-7.1	0.4917	0.4182	1.6655	1.2270	1.2606	1.0909			

SL	INCS	INCM	DEV	TURN	RMDVM-1	RMDVM-2	D-FAC	CMEGA-B	LOSS-P	PO2/	%EFF-P	%EFF-A	%EFF-P	%EFF-A	%EFF-P
DEGREE	DEGREE	DEGREE	DEGREE					TOTAL	TOTAL	PO1	STATC-ST	TO1-INLET	TO1-INLET	TO1-STG	TO1-STG
1	4.86	6.42	14.06	51.06	56.15	67.01	0.3984	0.1066	0.0240	0.9666	77.75	83.35	84.70	79.87	80.75
2	5.69	7.71	13.32	51.64	55.76	67.48	0.3868	0.0925	0.0212	0.9719	79.21	84.91	86.14	80.73	81.57
3	4.41	6.92	11.63	50.21	56.77	68.17	0.3606	0.0575	0.0134	0.9833	85.21	87.96	88.95	84.99	85.64
4	1.58	5.45	10.00	47.46	55.46	63.00	0.3435	0.0513	0.0126	0.9876	84.69	88.40	89.30	87.21	87.73
5	-1.05	4.25	8.08	45.67	50.31	54.38	0.3409	0.0410	0.0108	0.9924	86.16	84.18	85.33	85.39	85.91
6	-0.60	5.19	6.89	47.12	46.58	49.88	0.3555	0.0385	0.0105	0.9938	87.07	81.89	83.16	80.37	81.01
7	-0.56	5.43	6.56	47.27	45.91	48.62	0.3639	0.0519	0.0143	0.9919	83.12	81.22	82.52	77.44	78.16
8	-1.52	4.69	6.58	46.06	44.79	48.49	0.3658	0.0749	0.0209	0.9882	76.23	80.58	81.91	76.59	77.32
9	-3.32	3.37	8.63	42.01	48.66	50.09	0.3424	0.0871	0.0253	0.9858	70.04	75.42	77.13	75.97	76.73
10	-3.11	3.76	10.68	41.44	47.74	50.11	0.3366	0.0796	0.0233	0.9872	71.66	71.95	73.50	74.38	75.19
11	-5.39	1.71	12.33	35.94	46.63	48.03	0.3379	0.0801	0.0237	0.9878	72.49	69.06	71.16	75.08	75.86

NCORR WCORR TO/TO PO/PC EFF-AD EFF-P T02/T01 P02/P01 EFF-AD EFF-P
INLET INLET INLET INLET INLET INLET ROTOR ROTOR ROTOR ROTOR
7459. 112.40 1.2101 1.7368 81.24 82.62 1.0975 0.9866 81.19 263.61

ORIGINAL PAGE IS
OF POOR QUALITY

APPENDIX E

TABLE XXXII (d) - OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

70% OF DESIGN SPEED

$$\text{STATOR 1 } (\beta^*_{\text{des.}} - \beta^*_{\text{act.}}) = +5.0^\circ$$

$$\text{STATOR 2 } (\beta^*_{\text{des.}} - \beta^*_{\text{act.}}) = +7.5^\circ$$

U. S. CUSTOMARY UNITS

ROTOR 1

SL	EPSI-1		EPSI-2		V-1		V-2		VM-1		VM-2		V0-1		V0-2		B-1		B-2		M-1		M-2		POINT NO 4		
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC
1	16.288	18.167	324.2	706.3	324.2	403.0	0.0	580.0	0.0	55.2	0.2928	0.6279	440.3	505.8	0.4939	0.3637	546.8	409.1									
2	13.408	15.650	330.7	681.4	330.7	401.7	0.0	550.4	0.0	53.9	0.2987	0.6043	474.8	534.5	0.5227	0.2565	578.0	402.0									
3	10.955	13.408	336.5	657.5	336.5	393.3	0.0	526.9	0.0	53.2	0.3041	0.5816	508.7	559.1	0.5511	0.3441	609.9	394.6									
4	4.854	7.413	347.6	609.4	347.6	386.9	0.0	471.4	0.0	50.6	0.3143	0.5366	605.6	633.2	0.6314	0.3690	698.3	419.3									
5	-0.897	0.921	351.3	552.2	351.3	352.4	0.0	425.1	0.0	50.3	0.3177	0.4822	726.6	731.8	0.7299	0.4082	807.0	467.7									
6	-3.143	-1.832	350.0	550.5	350.0	367.6	0.0	409.8	0.0	48.1	0.3165	0.4803	784.7	781.1	0.7771	0.4558	859.3	522.5									
7	-4.475	-3.133	348.7	562.9	348.7	383.8	0.0	411.8	0.0	47.0	0.3154	0.4907	813.5	805.8	0.8004	0.4795	885.1	550.0									
8	-6.031	-4.450	346.7	564.1	346.7	394.3	0.0	403.4	0.0	45.7	0.3135	0.4916	842.2	830.4	0.8235	0.5065	910.7	581.3									
9	-10.621	-8.351	335.5	557.4	335.5	353.6	0.0	430.8	0.0	50.6	0.3032	0.4814	927.4	904.4	0.8916	0.5105	986.7	591.0									
10	-11.664	-9.544	331.0	552.5	331.0	326.6	0.0	445.6	0.0	53.7	0.2950	0.4783	956.5	929.1	0.9144	0.5020	1012.1	583.5									
11	-12.136	-10.646	326.8	552.7	326.8	305.4	0.0	460.6	0.0	56.4	0.2951	0.4737	985.0	953.8	0.9374	0.4971	1037.8	580.0									

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	CMGA-B	LOSS-P	PQ2/		EFF-P	EFF-A	B*-1	B*-2	VB*-1	VB*-2	PO/PO
	DEGREE	DEGREE	DEGREE	DEGREE						TOTAL	TOTAL	TOT	DEGREE	DEGREE	FT/SEC	FT/SEC		INLET
1	6.98	11.59	18.07	63.25	23.76	32.13	0.9049	-0.0323	-0.0070	1.3801	101.52	101.62	53.37	-9.89	-440.3	70.2	1.3801	INLET
2	7.04	11.32	17.33	57.12	24.19	32.33	0.9406	-0.0129	-0.0030	1.3742	100.65	100.71	54.84	-2.28	-474.8	14.0	1.3742	INLET
3	7.22	11.33	16.20	51.56	24.58	31.88	0.9733	0.0205	0.0049	1.3666	98.77	98.74	56.23	4.67	-508.7	-32.2	1.3666	INLET
4	8.49	11.95	12.97	37.33	25.31	31.85	0.9871	0.0613	0.0151	1.3570	95.34	95.17	59.99	22.66	-605.6	-161.7	1.3570	INLET
5	9.67	12.36	10.75	23.17	25.55	29.21	0.9834	0.1415	0.0320	1.3356	86.87	86.36	64.13	41.02	-726.6	-306.7	1.3356	INLET
6	10.06	12.34	7.55	20.70	25.47	30.60	0.9449	0.1368	0.0304	1.3437	86.32	85.76	65.99	45.29	-784.7	-371.3	1.3437	INLET
7	10.26	12.36	5.45	21.67	25.39	32.00	0.9317	0.1358	0.0307	1.3572	86.23	85.45	64.84	45.76	-813.5	-394.0	1.3572	INLET
8	10.47	12.43	4.44	20.39	25.25	32.93	0.9107	0.1294	0.0292	1.3608	86.28	85.70	67.69	47.30	-842.2	-427.0	1.3608	INLET
9	11.20	12.62	0.46	16.59	24.52	29.15	0.9569	0.2387	0.0506	1.3585	74.34	73.24	70.24	53.26	-927.9	-473.6	1.3585	INLET
10	11.34	12.63	8.54	15.08	24.21	26.77	0.9825	0.2829	0.0573	1.3563	69.88	68.59	71.02	55.94	-956.5	-483.5	1.3563	INLET
11	11.36	12.51	11.82	13.53	23.93	24.93	0.6036	0.3195	0.0622	1.3591	66.44	64.99	71.69	58.17	-982.0	-493.1	1.3591	INLET

TO/TO	PO/PO	EFF-AD	EFF-P	WCI/A1	TO2/TO1	PQ2/PO1	EFF-AD	EFF-P
INLET	INLET	INLET	INLET	LBM/SEC				
				% SQFT				
1.1175	1.3563	84.32	84.95	24.03	1.1079	1.3563	84.32	84.95

STATOR 1

SL	EPSI-1		EPSI-2		V-1		V-2		VM-1		VM-2		V0-1		V0-2		B-1		B-2		M-1		M-2		POINT NO 4			
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	
1	18.342	15.051	707.7	440.5	422.5	439.0	567.8	-36.9	53.6	-4.8	0.6293	0.3826	1.3285	1.0950	1.3285	1.0950	1.3285	1.0950	1.3285	1.0950	INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET
2	16.177	13.428	685.1	443.5	420.8	442.7	540.7	-32.1	52.3	-4.1	0.6078	0.3856	1.3338	1.0942	1.3338	1.0942	1.3338	1.0942	1.3338	1.0942	INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET
3	14.116	11.841	662.9	446.4	412.4	445.3	519.1	-32.2	51.7	-4.1	0.5867	0.3879	1.3378	1.0945	1.3378	1.0945	1.3378	1.0945	1.3378	1.0945	INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET
4	8.707	7.287	618.3	431.2	404.4	429.8	467.6	-34.5	49.2	-4.6	0.5444	0.3741	1.3315	1.0937	1.3315	1.0937	1.3315	1.0937	1.3315	1.0937	INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET
5	2.626	1.557	562.2	408.2	368.7	406.0	424.4	-41.6	49.0	-5.8	0.4916	0.3529	1.3184	1.0928	1.3184	1.0928	1.3184	1.0928	1.3184	1.0928	INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET
6	-0.001	-1.000	560.6	411.1	382.1	409.5	410.2	-36.5	47.0	-5.1	0.4895	0.3552	1.3200	1.1018	1.3200	1.1018	1.3200	1.1018	1.3200	1.1018	INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET
7	-1.076	-2.048	572.8	429.7	357.3	429.0	412.6	-24.2	46.1	-3.2	0.4947	0.3709	1.3306	1.1067	1.3306	1.1067	1.3306	1.1067	1.3306	1.1067	INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET
8	-2.005	-2.961	574.0	432.9	407.2	432.3	404.6	-21.4	44.8	-2.8	0.5006	0.3737	1.3332	1.1082	1.3332	1.1082	1.3332	1.1082	1.3332	1.1082	INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET
9	-4.656	-5.621	568.1	426.0	367.6	424.4	433.1	-36.1	49.7	-4.9	0.4911	0.3647	1.3324	1.1235	1.3324	1.1235	1.3324	1.1235	1.3324	1.1235	INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET
10	-6.121	-6.675	563.3	408.9	341.2	406.0	448.3	-48.6	52.8	-6.8	0.4851	0.3486	1.3241	1.1306	1.3241	1.1306	1.3241	1.1306	1.3241	1.1306	INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET
11	-7.622	-7.880	563.6	410.4	319.9	407.0	464.2	-52.7	55.5	-7.4	0.4836	0.3483	1.3258	1.1410	1.3258	1.1410	1.3258	1.1410	1.3258	1.1410	INLET	INLET	INLET	INLET	INLET	INLET	INLET	INLET

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	CMGA-B	LOSS-P	PQ2/		EFF-P	EFF-A	B*-1	B*-2	VB*-1	VB*-2	PO/PO
	DEGREE	DEGREE	DEGREE	DEGREE						TOTAL	TOTAL	TOT	DEGREE	DEGREE	FT/SEC	FT/SEC		INLET
1	6.01	8.12	12.57	58.32	33.66	37.90	0.9466	0.1598	0.0326	0.9624	77.03	89.08	89.48	91.21	90.88	91.21	91.21	91.21
2	6.43	8.83	12.11	56.39	33.80	38.34	0.9252	0.1344	0.0285	0.9701	79.59	90.88	91.21	91.21	90.88	91.21	91.21	91.21
3	7.15	9.91	11.28	55.77	33.33	38.65	0.9062	0.1024	0.0225	0.9786	83.39	91.77	92.07	91.77	92.07	92.07	92.07	92.07
4	7.17	10.85	9.69	33.76	33.16	37.28	0.9492	0.1044	0.0254	0.9808	81.71	89.11	89.11	89.11	89.11	89.11	89.11	89.11
5	8.51	13.26	8.46	54.66	30.42	35.00	0.9000	0.0836	0.0227	0.9872	83.75	82.38	82.38	82.38	82.38	82.38	82.38	82.38
6	7.01	12.63	9.26	52.13	31.67	35.25	0.9493	0.1046	0.0298	0.9843	78.82	81.14	81.14	81.14	81.14	81.14	81.14	81.14
7	6.24	12.16	11.16	45.32	32.98	36.86	0.9730	0.1209	0.0352	0.9810	74.59	79.71	79.71	79.71	79.71	79.71	79.71	79.71
8	5.22	11.37	11.59	47.67	33.85	37.18	0.9653	0.1280	0.0380	0.9798	72.15	80.48	80.48	80.48	80.48	80.48	80.48	80.48
9	10.04	16.96	10.69	54.57	30.17	36.05	0.9085	0.1311	0.0408	0.9799	72.64	69.29	70.48	69.29	70.48	70.48	70.48	70.48
10	12.83																	

ROTOR 2

RUN NO 20, SPEED CODE 70, POINT NO 4

SL	EPSTI-1	EPSTI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	0-1	0-2	M-1	M-2	U-1	U-2	M'-1	M'-2	V'-1	V'-2
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			FT/SEC	FT/SEC			FT/SEC	FT/SEC
1	11.707	10.981	472.8	434.8	471.4	528.9	-35.9	645.8	-4.4	50.5	0.4115	0.7078	584.2	612.8	0.6780	0.4499	779.0	530.0
2	10.957	9.635	486.8	820.5	475.8	528.1	-31.3	628.0	-3.7	49.8	0.4188	0.6951	600.7	625.6	0.6912	0.4474	793.5	528.1
3	10.003	8.372	487.9	800.9	486.9	538.2	-31.3	593.0	-3.7	47.7	0.4252	0.6782	617.8	638.5	0.7071	0.4575	811.4	540.2
4	8.237	4.823	481.7	716.0	480.5	517.2	-34.0	495.2	-4.1	43.7	0.4193	0.6038	670.6	681.4	0.7425	0.4636	852.9	549.8
5	0.388	0.270	458.4	623.7	456.5	475.5	-41.5	403.6	-5.2	40.3	0.3976	0.5226	743.5	743.0	0.7877	0.4895	908.1	584.2
6	-2.380	-1.922	455.4	586.4	453.9	446.2	-36.6	380.5	-4.6	40.4	0.3946	0.4897	780.6	775.8	0.8100	0.4978	934.8	596.1
7	-3.456	-2.848	469.4	515.5	468.8	438.7	-24.3	372.5	-3.0	40.3	0.4062	0.4800	799.4	792.7	0.8201	0.5066	947.7	607.4
8	-4.265	-3.650	470.2	514.1	469.7	430.5	-21.5	379.9	-2.6	41.5	0.4069	0.4780	818.2	810.0	0.8327	0.5086	962.1	608.2
9	-6.478	-6.063	468.8	577.5	485.4	445.0	-35.9	368.2	-4.4	39.5	0.4008	0.4762	835.6	863.6	0.8787	0.5491	1023.4	665.9
10	-7.437	-7.143	452.7	588.8	490.1	446.3	-49.0	352.6	-6.2	38.2	0.3871	0.4669	894.8	882.0	0.8940	0.5884	1045.7	692.4
11	-8.440	-8.449	455.4	593.4	492.2	443.3	-53.4	331.4	-6.7	36.7	0.3875	0.4521	914.1	900.7	0.9089	0.5989	1068.0	721.3

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	MEGA-B	LOSS-P	P02	%EFF-P	%EFF-A	B-1	B-2	V0-1	V0-2	PC/PO
DEGREE	DEGREE	DEGREE	DEGREE	DEGREE			TOTAL	TOTAL		P01	TOT	TOT	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	3.22	7.53	16.84	96.28	40.24	49.34	0.5235	0.1674	0.0381	1.4320	88.95	88.39	52.70	-3.56	-620.2	33.1	1.9024
2	2.84	7.29	13.96	93.06	41.02	49.74	0.5321	0.1691	0.0374	1.4264	88.96	88.41	52.80	-4.26	-632.0	2.4	1.9025
3	2.80	7.38	12.39	46.30	41.65	51.21	0.5211	0.1358	0.0324	1.4165	89.99	89.50	53.16	4.86	-649.0	-45.9	1.8950
4	4.01	8.60	10.23	35.97	45.96	50.09	0.5159	0.1086	0.0263	1.3741	90.43	90.01	55.76	19.19	-704.7	-186.3	1.8295
5	6.35	10.93	7.29	24.31	38.71	46.36	0.4962	0.1043	0.0241	1.3321	88.64	88.45	59.82	35.52	-783.0	-339.4	1.7501
6	6.57	10.91	5.31	19.42	38.52	43.41	0.4949	0.1317	0.0293	1.3051	84.81	84.25	60.94	41.52	-817.2	-395.3	1.7251
7	5.47	9.54	4.48	14.61	39.74	42.62	0.4869	0.1384	0.0305	1.2897	83.27	82.68	60.94	43.73	-823.7	-420.2	1.7165
8	5.37	9.18	2.60	14.83	39.85	41.72	0.4986	0.1680	0.0368	1.2876	80.02	79.32	60.75	44.92	-839.7	-430.1	1.7167
9	0.05	8.73	0.85	14.52	39.02	42.53	0.4852	0.1840	0.0430	1.2927	77.17	76.35	62.86	47.94	-911.5	-495.5	1.7236
10	7.21	9.39	3.05	14.68	37.45	42.37	0.4756	0.1799	0.0422	1.2969	77.33	76.51	64.41	49.73	-943.8	-529.4	1.7170
11	7.34	9.04	6.32	12.88	37.32	41.74	0.4594	0.1733	0.0403	1.2857	76.97	76.16	64.85	51.98	-967.9	-569.3	1.7042

IO/IO PO/PC EFF-AD EFF-P WGL/A1 T02/T01 P02/P01 EFF-AD EFF-P
INLET INLET INLET INLET LBM/SEC ROTOR ROTOR
% %
1.2204 1.7720 80.50 81.98 29.98 1.1015 1.3331 84.30 84.91

STATOR 2

RUN NO 20, SPEED CODE 70, POINT NO 4

SL	EPSTI-1	EPSTI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	0-1	0-2	M-1	M-2	U-1	U-2	M'-1	M'-2	V'-1	V'-2
DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			FT/SEC	FT/SEC			FT/SEC	FT/SEC
1	8.466	0.665	853.0	633.2	564.6	630.4	639.4	-59.0	48.8	-5.3	0.7248	0.5258	1.8328	1.2285	1.3799	1.1220	1.1220	1.1220
2	7.273	0.419	836.0	646.2	560.9	634.3	622.6	-86.6	48.2	-7.8	0.7114	0.5324	1.8446	1.2266	1.3832	1.1207	1.1168	1.1168
3	6.174	0.121	811.8	652.6	567.7	647.3	588.6	-82.8	46.2	-7.3	0.6939	0.5443	1.8631	1.2224	1.3925	1.1168	1.1055	1.1055
4	3.559	0.632	732.2	592.7	541.2	587.2	493.2	-80.9	42.4	-7.8	0.6185	0.4942	1.8047	1.2114	1.3553	1.1055	1.0964	1.0964
5	0.966	-1.073	639.4	514.8	456.3	507.4	403.2	-86.7	39.1	-9.7	0.5365	0.4276	1.7333	1.2059	1.3147	1.0964	1.0943	1.0943
6	-0.237	-1.101	602.6	480.1	487.1	472.2	380.8	-86.5	39.1	-10.4	0.5040	0.3979	1.7047	1.2059	1.2911	1.0943	1.0905	1.0905
7	-0.932	-1.085	592.0	469.8	459.8	462.0	372.9	-84.8	39.0	-10.4	0.4944	0.3889	1.6964	1.2070	1.2750	1.0905	1.0894	1.0894
8	-1.726	-1.685	581.1	472.2	452.2	464.6	380.7	-84.4	40.1	-10.3	0.4927	0.3904	1.6974	1.2102	1.2732	1.0894	1.0894	1.0894
9	-4.255	-1.272	598.3	447.3	470.2	481.4	370.0	-75.9	38.2	-8.9	0.4941	0.3993	1.7020	1.2343	1.2762	1.0894	1.1004	1.1004
10	-5.043	-1.295	592.6	484.4	474.8	479.1	354.7	-72.7	36.8	-8.6	0.4874	0.3954	1.6965	1.2434	1.2814	1.1004	1.0975	1.0975
11	-5.841	-1.223	582.1	467.5	476.9	464.5	333.8	-53.4	35.1	-8.6	0.4765	0.3797	1.6805	1.2522	1.2677	1.0975	1.0975	1.0975

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	MEGA-B	LOSS-P	P02	%EFF-P	%EFF-A	B-1	B-2	V0-1	V0-2	PC/PO
DEGREE	DEGREE	DEGREE	DEGREE	DEGREE			TOTAL	TOTAL		P01	STAGE-ST	STAGE-A	STAGE	STAGE	FT/SEC	FT/SEC	INLET
1	7.86	9.42	13.98	54.15	52.09	62.87	0.4421	0.1236	0.0278	0.9635	76.92	82.60	84.28	85.56	80.29	81.15	79.74
2	8.28	10.28	10.99	52.52	52.28	62.55	0.4311	0.1064	0.0243	0.9694	78.62	84.28	85.56	80.29	81.15	79.74	79.74
3	7.05	9.55	11.06	53.48	53.48	65.33	0.3954	0.0829	0.0146	0.9826	85.46	87.40	88.43	86.84	84.76	85.44	85.44
4	4.34	8.20	9.98	50.24	51.98	59.37	0.3865	0.0618	0.0152	0.9860	84.43	86.84	87.87	85.81	86.39	86.39	86.39
5	1.86	7.17	8.10	48.77	48.02	50.98	0.4024	0.0780	0.0206	0.9861	80.15	82.59	83.86	84.16	84.73	84.73	84.73
6	2.26	6.04	7.35	45.52	45.14	47.22	0.4204	0.0796	0.0216	0.9873	80.24	79.89	81.31	80.16	80.82	80.82	80.82
7	2.27	8.26	7.28	46.39	44.37	46.10	0.4231	0.0763	0.0210	0.9883	81.05	78.70	80.20	79.24	79.92	79.92	79.92
8	3.51	5.71	7.33	50.33	43.54	46.23	0.4248	0.0720	0.0201	0.9890	81.85	77.60	79.18	75.85	76.63	76.63	76.63
9	1.92	4.62	8.72	47.17	44.57	46.93	0.4051	0.0828	0.0240	0.9873	77.31	69.98	72.10	72.41	73.32	73.32	73.32
10	-0.15	6.73	9.66	45.43	44.65	46.28	0.3962	0.0789	0.0231	0.9882	77.99	66.92	65.24	72.87	73.79	73.79	73.79
11	-3.16	1.94	12.88	41.43	44.42	44.90	0.3961	0.0796	0.0206	0.9861	74.72	63.21	65.84	71.71	72.62	72.62	72.62

W CORR W CORR TO/TO PO/PO EFF-AD EFF-P
INLET INLET INLET INLET INLET INLET

7492. 105.80 1.2204 1.7448 78.15 79.76 1.1015 0.9847 75.60 214.09

ORIGINAL PAGE IS
OF POOR QUALITY

TABLE XXXIII (a) — OVERALL PERFORMANCE AND BLADE-ELEMENT DATA

70% OF DESIGN SPEED

STATOR 1 ($\beta^*_{des.} - \beta^*_{act.}$) = +5°
 STATOR 2 ($\beta^*_{des.} - \beta^*_{act.}$) = -5°

U. S. CUSTOMARY UNITS

ROTOR 1

																RUN NO 21, SPEED CODE 70, POINT NO 4			
SL	EPISI-1	EPISI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	U-1	U-2	M*-1	M*-2	V*-1	V*-2	
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			FT/SEC	FT/SEC			FT/SEC	FT/SEC	
1	16.425	18.089	321.0	698.0	521.0	397.4	0.0	573.8	0.0	55.3	0.2899	0.6204	439.1	508.3	0.4911	0.3580	543.9	402.8	
2	13.714	15.567	326.3	672.5	328.3	394.4	0.0	544.7	0.0	54.0	0.2966	0.5962	473.5	532.9	0.5205	0.3499	576.2	394.6	
3	11.324	13.254	335.0	647.6	335.0	385.2	0.0	520.6	0.0	53.4	0.3027	0.5727	507.2	557.5	0.5493	0.3422	607.9	386.9	
4	5.179	7.262	349.0	601.7	349.0	386.5	0.0	461.1	0.0	50.0	0.3156	0.5296	603.9	631.3	0.6307	0.3717	697.5	422.3	
5	-0.750	0.931	353.6	541.7	353.6	349.9	0.0	413.5	0.0	49.8	0.3199	0.4735	724.5	729.7	0.7292	0.4123	806.2	471.6	
6	-2.976	-1.715	352.8	533.6	352.8	366.0	0.0	388.3	0.0	46.7	0.3191	0.4661	782.5	778.9	0.7764	0.4675	858.3	535.2	
7	-4.374	-2.998	351.7	541.4	351.7	384.0	0.0	381.7	0.0	44.8	0.3181	0.4729	811.1	803.5	0.7996	0.4982	884.1	570.3	
8	-6.036	-4.316	349.6	549.7	349.6	392.8	0.0	384.6	0.0	44.4	0.3162	0.4797	839.8	828.1	0.8226	0.5169	909.6	592.4	
9	-10.640	-8.292	338.6	545.8	338.6	353.2	0.0	416.1	0.0	49.7	0.3060	0.4720	925.2	901.8	0.8905	0.5193	985.2	600.5	
10	-11.634	-9.512	334.2	541.5	334.2	329.1	0.0	430.1	0.0	52.6	0.3019	0.4665	953.7	926.4	0.9131	0.5131	1010.6	595.5	
11	-12.105	-10.627	330.2	538.0	330.2	310.2	0.0	439.6	0.0	54.7	0.2983	0.4620	982.2	951.0	0.9361	0.5137	1036.2	598.2	

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P	P02/	%EFF-P	%EFF-A	B*-1	B*-2	V0*-1	V0*-2	PO/PO
	DEGREE	DEGREE	DEGREE	DEGREE	TOTAL	TOTAL		TOTAL		P01	TOT	TOT	DEGREE	DEGREE	FT/SEC	FT/SEC	INLET
1	7.19	11.80	16.60	62.93	23.55	31.89	0.5112	-0.0668	-0.0145	1.3814	103.15	103.33	53.58	-9.35	-439.1	65.5	1.3814
2	7.17	11.46	17.90	56.69	24.04	31.96	0.5489	-0.0396	-0.0091	1.3748	102.08	102.20	54.99	-1.71	-473.5	11.8	1.3748
3	7.30	11.40	16.99	50.85	24.48	31.41	0.5817	-0.0024	-0.0006	1.3664	100.12	100.16	56.30	5.45	-507.2	-36.9	1.3664
4	8.33	11.80	14.05	36.10	25.41	32.04	0.5781	0.0238	0.0058	1.3591	98.13	98.07	59.83	23.73	-603.9	-170.2	1.3591
5	9.46	12.14	11.82	21.88	25.71	29.23	0.5727	0.1083	0.0241	1.3370	89.76	89.36	63.98	42.09	-826.5	-316.2	1.3370
6	9.82	12.10	9.53	18.88	25.65	30.76	0.5214	0.0907	0.0196	1.3413	90.56	90.19	65.76	46.87	-782.5	-390.6	1.3413
7	10.02	12.12	7.38	18.91	25.58	32.38	0.4967	0.0779	0.0170	1.3512	91.60	91.26	66.60	47.69	-811.1	-421.7	1.3512
8	10.25	12.20	5.62	18.98	25.44	33.12	0.4907	0.0876	0.0193	1.3600	90.38	89.98	67.46	48.48	-839.8	-443.5	1.3600
9	10.98	12.40	7.18	16.05	24.72	29.39	0.5414	0.2061	0.0430	1.3598	77.28	76.31	70.03	53.98	-925.2	-485.7	1.3598
10	11.12	12.41	9.44	14.36	24.43	27.23	0.5646	0.2500	0.0500	1.3580	72.71	71.54	70.80	56.44	-953.7	-496.4	1.3580
11	11.13	12.28	12.35	12.77	24.16	25.58	0.5781	0.2813	0.0539	1.3579	69.41	68.10	71.46	58.69	-982.2	-511.4	1.3579

TO/T0	PO/PO	EFF-AD	EFF-P	MC1/A1	T02/T01	P02/P01	EFF-AD	EFF-P
INLET	INLET	%	%	LBM/SEC			%	%
1.1040	1.3565	87.53	88.03	24.14	1.1040	1.3565	87.53	88.03

STATOR 1

																RUN NO 21, SPEED CODE 70, POINT NO 4			
SL	EPISI-1	EPISI-2	V-1	V-2	VM-1	VM-2	V0-1	V0-2	B-1	B-2	M-1	M-2	PO/PO	TO/TO	TO2/TO1	TO2/			
	DEGREE	DEGREE	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	FT/SEC	DEGREE	DEGREE			INLET	INLET	STAGE	T01			
1	18.286	14.956	698.8	444.1	415.7	442.5	561.7	-37.5	53.7	-4.8	0.6211	0.3860	1.3292	1.0937	1.3292	1.0937			
2	16.070	13.249	675.6	447.8	412.5	446.6	535.0	-33.1	52.5	-4.2	0.5992	0.3894	1.3347	1.0932	1.3347	1.0932			
3	13.931	11.580	652.6	450.9	403.6	449.6	512.9	-33.6	51.9	-4.2	0.5774	0.3922	1.3390	1.0932	1.3390	1.0932			
4	8.364	6.932	610.1	437.1	403.6	436.0	457.4	-30.9	48.6	-4.0	0.5374	0.3798	1.3331	1.0934	1.3331	1.0934			
5	2.236	-1.412	552.0	414.7	366.4	412.6	412.8	-42.2	48.4	-5.8	0.4829	0.3592	1.3198	1.0969	1.3198	1.0969			
6	-0.392	-0.985	544.2	412.5	380.9	410.5	388.7	-40.6	45.6	-5.6	0.4758	0.3572	1.3186	1.0971	1.3186	1.0971			
7	-1.370	-1.957	552.0	419.8	398.0	418.6	382.5	-32.0	43.9	-4.4	0.4826	0.3635	1.3231	1.0982	1.3231	1.0982			
8	-2.201	-2.813	560.3	428.6	406.3	427.7	285.7	-27.9	43.5	-3.7	0.4893	0.3708	1.3288	1.1014	1.3288	1.1014			
9	-4.984	-5.482	557.1	421.6	367.9	419.9	418.3	-38.2	48.7	-5.2	0.4822	0.3617	1.3281	1.1189	1.3281	1.1189			
10	-6.263	-6.572	553.0	411.8	344.3	409.6	432.8	-42.8	51.5	-6.0	0.4769	0.3518	1.3237	1.1265	1.3237	1.1265			
11	-7.726	-7.816	549.8	402.1	325.6	399.6	443.0	-52.8	53.8	-7.5	0.4726	0.3430	1.3199	1.1342	1.3199	1.1342			

SL	INCS	INCM	DEV	TURN	RHOVM-1	RHOVM-2	D-FAC	OMEGA-B	LOSS-P	P02/	%EFF-P	%EFF-A	%EFF-P	%EFF-A	%EFF-P	%EFF-A
	DEGREE	DEGREE	DEGREE	DEGREE	TOTAL	TOTAL		TOTAL		P01	STAGE-ST	TDT-INLET	TDT-INLET	TDT-STG	TDT-STG	TDT-STG
1	6.15	8.26	12.53	58.50	33.34	38.21	0.5341	0.1652	0.0337	0.9620	75.52	90.48	90.48	90.48	90.83	90.83
2	6.67	9.08	12.02	56.72	33.36	38.70	0.5112	0.1365	0.0289	0.9704	78.50	92.32	92.60	92.60	92.60	92.60
3	7.37	10.15	11.15	56.14	32.82	39.05	0.4898	0.0997	0.0219	0.9797	83.04	93.41	93.65	93.65	93.65	93.65
4	6.57	10.29	10.23	52.62	33.33	37.86	0.4767	0.1078	0.0263	0.9807	79.99	91.68	91.98	91.98	91.98	91.98
5	7.89	12.93	8.47	54.23	30.47	35.62	0.4734	0.0868	0.0236	0.9872	81.64	85.22	85.76	85.76	85.76	85.76
6	5.55	11.17	8.71	51.22	31.88	35.43	0.4673	0.1156	0.0329	0.9834	74.84	84.78	85.33	85.33	85.33	85.33
7	4.07	9.95	10.02	48.24	33.41	36.13	0.4573	0.1361	0.0396	0.9800	69.96	84.85	85.41	85.41	85.41	85.41
8	3.92	10.06	10.70	47.25	34.11	36.87	0.4533	0.1503	0.0445	0.9773	66.52	83.56	84.17	84.17	84.17	84.17
9	9.07	15.95	10.34	52.90	30.48	35.73	0.4986	0.1605	0.0499	0.9763	65.37	71.12	72.22	72.22	72.22	72.22
10	11.60	18.65	10.79	57.53	28.36	34.62	0.5279	0.1746	0.0550	0.9748	63.69	66.00	67.29	67.29	67.29	67.29
11	13.15	20.30	10.76	61.33	26.72	33.55	0.5585	0.1967	0.0625	0.9721	60.40	61.54	62.98	62.98	62.98	62.98

NCORR	WCORR	TO/T0	PO/PO	EFF-AD	EFF-P	T02/T01	P02/P01	EFF-AD	EFF-P
INLET	INLET	INLET	INLET	%	%			%	%
7471.	106.30	1.1040	1.3272	81.01	81.72	1.1040	0.9784	81.01	167.84

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