

SEPTEMBER 1979

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TELEVISION

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BZV88 116V	0.25	BF155	0.70	SN76023N	2.00
BZV88 121V	0.25	BF156	0.40	SN76023ND	1.00
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BZV88 131V	0.25	BF158	0.60	SN76110N	2.00
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BZV88 316V	0.25	BF195	0.20	TDA1180	3.00
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BZV88 326V	0.25	BF197	0.20	TDA2002H	3.60
BZV88 331V	0.25	BF198	0.20	TDA2590Q	5.00
BZV88 336V	0.25	BF199	0.20	TDA2600	5.00
BZV88 341V	0.25	BF200	0.20	TDA2640	3.30
BZV88 346V	0.25	BF201	0.20	TDA3950	3.30
BZV88 351V	0.25	BF202	0.20	TAA621 AX1	3.00
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BZV88 361V	0.25	BF204	0.25	TCAS30S	2.00
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BZV88 371V	0.25	BF206	1.60		

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Philips G11 470 250	1.90
PYE 691 200 300/350	2.80
PYE 1000 1000 40	0.90
PYE 731 800 250	2.50
RRI 2500 2500 30	1.20
RRI 600/300	2.50
RRI 300 - 300/300	2.50
TCE 950 100 300 100 16	1.00
TCE 1400 150 100 100 150	3.70
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TCE 3000 3500 800 70	1.00
TCE 300 3500 6 100	0.70
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TCE 8000 8500 700 200	1.00
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TCE 9000 400 400	3.00
TCE 9500 220 400	2.20

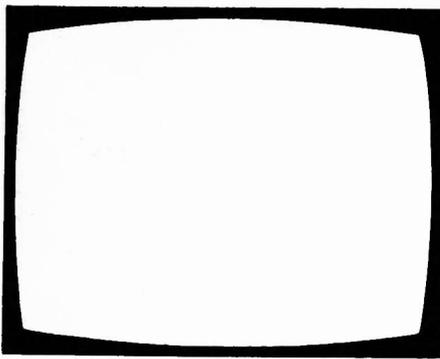
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TELEVISION

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QUERIES

We regret that we cannot answer technical queries over the telephone nor supply service sheets. We will endeavour to assist readers who have queries relating to articles published in *Television*, but we cannot offer advice on modifications to our published designs nor comment on alternative ways of using them. All correspondents expecting a reply should enclose a stamped addressed envelope.

Requests for advice in dealing with servicing problems should be directed to our Queries Service. For details see our regular feature "Your Problems Solved". Send to the address given above (see "correspondence").

this month

- 567 Leader**
- 568 Teletopics**
News, comment and developments.
- 570 Receiving French TV** *by Hugh Cocks*
In favourable locations along the south and east coasts French TV can be received on a permanent basis. Advice is given on transmitters to try for and the equipment required.
- 574 The V2000 VCR System**
Technical features of the new Philips/Grundig VCR system, which could become a new world standard.
- 576 No Clock Display** *by Steve Beeching, T.Eng. (C.E.I.)*
Another nasty VCR fault. This time a Sony Betamax VCR which wouldn't give a clock display.
- 577 All Slog and No Grog . . .** *by Les Lawry-Johns*
Part of this month's column is set to music. Whatever next? At least the Red Baron hasn't put in an appearance. Not yet.
- 579 Next Month in Television**
- 580 Restricted Brightness Range** *by George Wilding*
Quite a lot of things can be responsible for restricting the range of operation of a set's brightness control, and these depend on circuit design. A survey of possible causes is provided.
- 582 New Teletext Signal Panel** *by Alan Kitching*
This new signal panel has been designed as a direct replacement for the original one in the *Television* teletext decoder, using the same components. The use of an adaptive data slicer circuit gives improved performance under adverse signal conditions. The layout has been improved, and a sound i.f. preamplifier added.
- 586 Readers' PCB Service**
- 587 Servicing Pye Solid-State Colour Receivers, Part 1** *by Mike Phelan*
Dealing with faults on the Pye 713, 715, 717, 725, 731, 735, 737 and 741 chassis. This part covers the power supply and timebase circuits used in the larger-screen chassis.
- 592 Long-Distance Television** *by Roger Bunney*
Reports on DX reception and conditions, and news from abroad. Also the start of a new series giving advice to those thinking of making a start with experimental DX reception.
- 595 Tuners for DX Reception** *by Hugh Cocks*
A useful new v.h.f./u.h.f. tuner has become available on the surplus market.
- 596 TV Troubles** *by Robin D. Smith*
More notes on fault conditions. Also some of the problems that can arise when customers decide to have a go.
- 598 TV Servicing: Beginners Start Here . . . Part 24** *by S. Simon*
Now we really come to grips with colour! The basic colour mixing techniques are described, and things to look for listed when dealing with wrong colours or a poor grey scale on sets with colour-difference drive.
- 601 Letters**
- 602 Your Problems Solved**
- 604 Test Case 201**

OUR NEXT ISSUE DATED OCTOBER WILL BE
PUBLISHED ON SEPTEMBER 17

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PCL85	0.10	PCF808	0.25	EF80	0.10	PY800/1	0.10	30FL1/2	0.25	PL508	0.50
PCL86	0.10	PCF80	0.10	EF85	0.10	PL36	0.25	ECC82	0.10	PCH200	0.50
PFL200	0.10	PCC189	0.10	EF183	0.10	PL504	0.25	ECC81	0.10	PCF200	0.50
PCF801	0.10	PCC86	0.10	EF184	0.10	PL81	0.10	ECH81	0.10	CEY51	0.15
30C1	0.10	30C15	0.10	6BW7	0.10	6/30L2	0.10	ECL80	0.10		
30C17	0.10	30C18	0.25	ECC85	0.10	U26	0.10	ECL82	0.10		
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GEC/Sobell	6.50	7.50	—	—	—	6.50	—	—	—	7.50
Philips	6.50	9.50	—	—	—	7.50	—	—	—	6.50
Decca	6.50	9.00	9.00	—	—	6.50	2.00 (19" only)	8.00	—	6.00
Thorn 2000	5.00	5.00	5.00	6.50	6.50	6.00	—	6.50	10.00	6.50
Pye	7.50	7.50	9.50	—	—	6.50	—	—	—	7.50
Baird	6.50	8.50	7.00	—	—	6.50	—	—	—	6.00

Postage & Packing £1.25

S/STANDARD COLOUR SPARE PANELS

	IF	LUM	CHROMA	VIDEO	CON	POWER	L/TB	F/TB
Bush 184	7.50	—	12.00	—	8.00	6.00	12.00	—
GEC Hybrid	7.50	6.50	10.00	—	6.00	—	—	12.00
Philips G6 S/S	9.50	—	10.00	—	6.00	—	—	6.00
Thorn 3000	6.50	6.50	8.00	6.50	6.00	20.00	20.00	6.50
Pye 691/693	6.50	6.50	10.00	—	6.50	—	15.00	6.50
Thorn 3500	6.50	6.50	8.00	6.50	7.50	20.00	20.50	6.50

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AC113	0.17	AF172	0.20	BC173	0.12		0.37	BF262	0.28	OC48	0.35	1N4002	1500 18" 19" stick
AC115	0.17	AF178	0.49	BC177	0.12	BD225/T1P31A	0.39	BF263	0.25	OC70	0.22	1N4003	2.37
AC117	0.24	AF180	0.60	BC178	0.12		0.39	BF271	0.20	OC71	0.28	1N4004	1500 24" 5 stick 2.48
AC125	0.20	AF181	0.30	BC179	0.12	BD234	0.34	BF273	0.12	OC72	0.35	1N4005	Single stick Thorn TV
AC126	0.18	AF186	0.29	BC182L	0.09	BD222	0.73	BF336	0.28	OC74	0.35	1N4006	11.16K 70V
AC127	0.19	AF239	0.43	BC183L	0.09	BDX22	0.73	BF337	0.24	OC75	0.35	1N4007	TV20 2 MT
AC128	0.17	AU113	1.29	BC184L	0.09	BDX32	1.98	BF338	0.29	OC76	0.35	1N4148	TV20 16K 18V
AC131	0.13			BC186	0.18	BDY1B	0.75	BF342	0.26	OC77	0.50	1N4751A	
AC141	0.23	BA130	0.08	BC187	0.18	BDY60	0.80	BF434	0.24	OC78	0.13	1N5401	IC's
AC142	0.19	BA145	0.14	BC209	0.11	BF115	0.24	BFY43	0.27	OC81	0.20	1N5404	SN76013N 1.20
AC141K	0.29	BA148	0.17	BC212	0.09	BF121	0.21	BFX84	0.27	OC810	0.14	1N5406	SN76013ND 1.00
AC142K	0.29	BA155	0.08	BC213L	0.09	BF154	0.12	BFX85	0.27	OC82	0.20	1N5408	SN76023N 1.20
AC151	0.17	BA158	0.08	BC214L	0.09	BF158	0.19	BFX88	0.24	OC820	0.13		SN76023ND 1.00
AC165	0.16	BA165	0.08	BC237	0.07	BF159	0.24	BFY50	0.15	OC83	0.22		SN76226DN 1.50
AC166	0.16	BC107	0.10	BC240	0.31	BF160	0.23	BFY51	0.15	OC84	0.28		SN76227N 1.20
AC168	0.17	BC108	0.10	BC2B1	0.24	BF163	0.23	BFY52	0.15	OC85	0.13		TBA341 0.97
AC176	0.17	BC109	0.10	BC262	0.18	BF164	0.17	BFY53	0.27	OC123	0.20		TBA520Q 1.10
AC176K	0.28	BC113	0.09	BC263B	0.20	BF167	0.23	BFY55	0.27	OC169	0.20		TBA530Q 1.10
AC178	0.16	BC114	0.12	BC267	0.19	BF173	0.21	BHA0002	1.90	OC170	0.22		TBA540Q 1.45
AC186	0.26	BC115	0.10	BC301	0.22	BF177	0.26	BR100	0.20	OC171	0.27		TBA550Q 1.40
AC187	0.21	BC116	0.10	BC302	0.30	BF178	0.24	BSX20	0.23	QA91	0.05		TBA560CQ 1.50
AC188	0.20	BC117	0.11	BC307	0.10	BF179	0.28	BSX76	0.23	BRC4443	0.65		TBA570Q 1.00
AC187K	0.30	BC119	0.22	BC337	0.11	BF180	0.30	BSY84	0.36	R200BB	1.50		TBA800 1.00
AC188K	0.30	BC125	0.12	BC338	0.09	BF181	0.34	BT106	1.18	R2010B	1.50		TBA810 1.50
AD130	0.50	BC126	0.09	BC307A	0.10	BF182	0.30	BT108	1.23	R2305	0.38		TBA920Q 1.50
AD140	0.65	BC136	0.12	BC308A	0.12	BF183	0.29	BT109	1.09	R2305/BD222	0.37		TBA990Q 1.50
AD142	0.73	BC137	0.12	BC309	0.14	BF184	0.23	BT116	1.23	SCR957	0.65		TCA270SQ 1.45
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AD145	0.70	BC139	0.21	BC548	0.11	BF186	0.30	BU105/02	1.50	TIP32A	0.36		TCA1327B 1.00
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AD162	1.00	BC147	0.07	BD115	0.30	BF198	0.11	BY126	0.09				CS2030/2232/2630/
AF106	0.42	BC148	0.07	BD116	0.47	BF199	0.14	BY127	0.10				2632/2230/2233/
AF114	0.23	BC149	0.07	BD124	1.30	BF200	0.28						PL36 0.90
AF115	0.22	BC153	0.12	BD131	0.32	BF216	0.12						PL84 0.74
AF116	0.22	BC154	0.12	BD132	0.34	BF217	0.12						PL504 1.10
AF117	0.30	BC157	0.10	BD133	0.37	BF218	0.12						PL509 2.45
AF118	0.40	BC158	0.11	BD135	0.26	BF219	0.12						PL82 0.67
AF121	0.33	BC159	0.11	BD136	0.26	BF220	0.12						PCL84 0.75
AF124	0.33	BC160	0.22	BD137	0.26	BF222	0.12						PCL86 0.78
AF125	0.29	BC161	0.22	BD138	0.26	BF221	0.21						PCL805 0.75
AF126	0.29	BC167	0.09	BD139	0.40	BF224	0.12						PLF200 1.00
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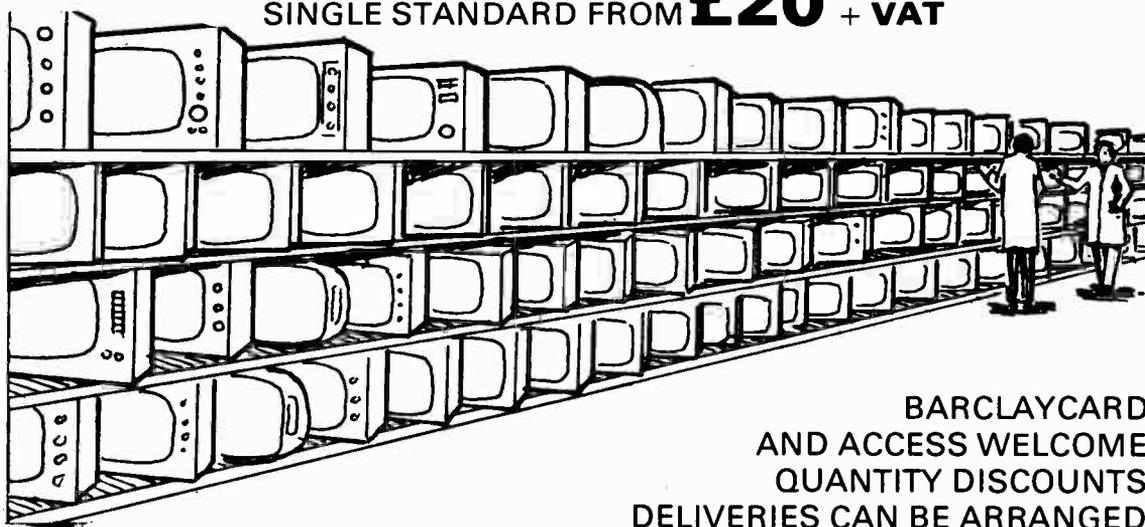
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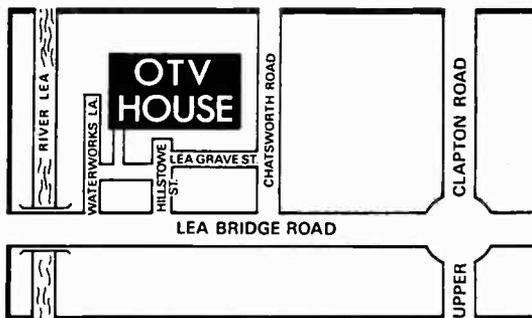
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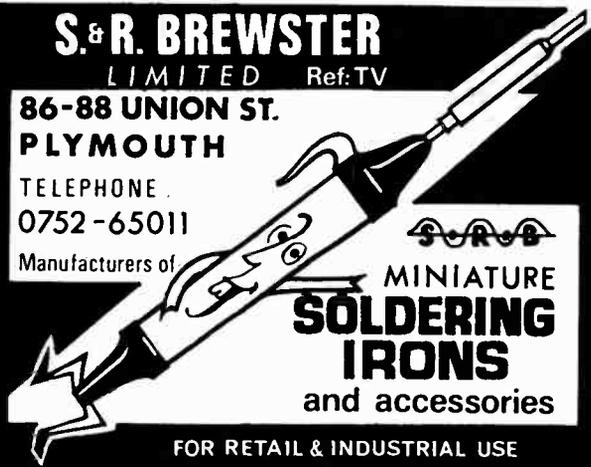
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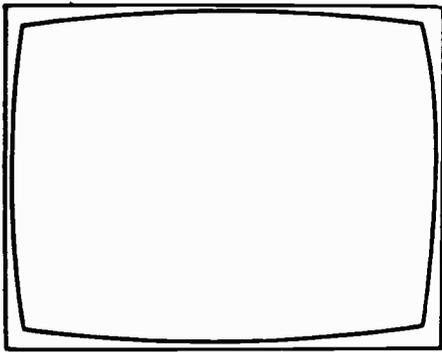
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AC117	0.38	AU107	2.75	BC204*	0.39	BC394	0.39	BD235	0.63	BF224 & J	0.22	BR101	0.83	MPSU06	0.76
AC126	0.48	AU110	2.40	BC205*	0.39	BC440	0.82	BD236	0.63	BF240	0.32	BR103	0.84	MPSU55	1.26
AC127	0.54	AU113	2.60	BC206*	0.37	BC441	0.59	BD237	0.66	BF241	0.31	BR303	1.06	MPSU56	1.32
AC128	0.46	BC107*	0.16	BC207*	0.39	BC461	0.78	BD238	0.66	BF244*	0.51	BR303	1.06	MPSU60	0.82
AC128K	0.55	BC108*	0.15	BC208*	0.37	BC477	0.30	BD253	1.58	BF245	0.43	BR339	0.80	MPCU131	10.59
AC141	0.55	BC109*	0.16	BC209*	0.39	BC478	0.25	BD410	1.65	BF254	0.48	BR356	10.44	OC26	1.90
AC141K	0.70	BC113	10.22	BC211*	0.36	BC479	0.33	BD433	0.65	BF255	0.58	BS527	0.92	OC28	1.49
AC142K	0.80	BC114	10.22	BC212*	0.17	BC547*	10.13	BD435	0.70	BF256*	0.49	BT106	1.90	OC29	1.80
AC151	0.31	BC116*	0.28	BC213*	0.17	BC548*	10.13	BD436	0.71	BF257	0.44	BT108	1.90	OC30	1.28
AC152	0.38	BC117	10.30	BC213*	0.16	BC549*	10.18	BD437	0.74	BF258	0.62	BT116	1.45	OC36	1.25
AC153	0.42	BC118	10.24	BC214*	0.18	BC550	10.24	BD438	0.76	BF259	0.62	BT119	5.18	OC42	0.90
AC153K	0.82	BC119	10.34	BC214*	0.18	BC556	10.23	BD519	0.88	BF262	0.73	BU102	2.85	OC44	0.68
AC154	0.41	BC125*	0.30	BC225	0.42	BC558*	0.17	BD520	0.88	BF263	0.88	BU105	11.80	OC45	0.63
AC176	0.45	BC126	10.30	BC237*	0.16	BC559*	0.18	BD599	0.87	BF270	0.47	BU105/02	11.85	OC70	0.66
AC178	0.51	BC132	10.20	BC238*	0.15	BCY10	0.30	BD600	1.23	BF271	0.42	BU108	12.98	OC71	0.75
AC179	0.85	BC134	10.22	BC239*	0.22	BCY30A	1.06	BD663BR	0.68	BF272A	0.80	BU126	12.91	OC72	0.73
AC187	0.56	BC135	10.21	BC251*	0.25	BCY32A	1.19	BDX18	1.58	BF273	0.33	BU204	12.90	OC81	0.83
AC187K	0.85	BC136	10.22	BC252*	0.26	BCY34A	1.02	BDX32	2.85	BF274	0.34	BU205	12.78	OC81D	0.85
AC188	0.52	BC137	10.30	BC253*	0.28	BCY34A	1.02	BDY16A	0.83	BF275	0.63	BU206	13.09	OC139	1.30
AC188K	0.81	BC138	10.35	BC253*	0.28	BCY34A	1.02	BDY18	1.58	BF337	0.65	BU208	13.09	OC140	1.35
AC193K	0.74	BC140	10.35	BC282A*	0.28	BD123	1.80	BDY20	2.25	BF338	0.65	BU407	11.38	OC170	0.80
AC194K	0.74	BC141	10.35	BC283*	0.28	BD124	1.85	BDY28	1.38	BF355	0.72	BU777	2.50	OC171	0.82
AC197	1.20	BC142	10.35	BC287*	0.20	BD124	1.85	BF115	0.48	BF362	0.49	C106D	0.80	OC200	3.90
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF117	0.45	BF363	0.49	C106F	0.43	OC201	3.95
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AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF123	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF124	0.48	BF367	0.29	C111E	10.46	OC205	3.95
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AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF127	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF128	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF129	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF130	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF131	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF132	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF133	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF134	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF135	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF136	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF137	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF138	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF139	0.48	BF367	0.29	C111E	10.46	OC205	3.95
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AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF163	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF164	0.48	BF367	0.29	C111E	10.46	OC205	3.95
AC197	0.95	BC143	10.38	BC288*	0.28	BD131	0.58	BF165	0.48	BF367	0.29	C111E	10.46	OC205	3.95
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A decade of the VCR

The 70s have seen the development of the domestic VCR from initial laboratory prototypes to an established consumer product. At the start of the decade, there were numerous intimations that a number of firms had development projects under way. There were also proposals for other domestic video systems, both disc (Teldec) and film (EVR), that subsequently fell by the wayside. The first domestic VCR system to appear, Cartrivision, was introduced in the USA in mid-1972. It was not a success. It appears to have lasted for about a year, by which time Ampex had also decided to drop its proposed Instavideo system. Though RCA continued work on various proposed systems, including discs and a holographic system using cheap plastic film, US firms then seem to have lost interest.

The main development was continued by Philips in Europe and various Japanese firms, in particular JVC and Sony. Philips were first to introduce a successful system in launching the N1500 on the European market in 1973. It gave an hours' recording/playback time. Up-dated versions were introduced in 1975 (N1501) and 1976 (N1502), and the N1700 with its two hours' (later two and a half hours') record/playback time was launched in late 1977. Philips never seem to have been keen to enter the US market with an NTSC version.

The Japanese video manufacturers battled it out over the years 1976-7 in their own and the US markets. Several systems came and went, and at the end of it all Sony's Beta II and JVC's VHS systems had become firmly established. During 1978, PAL versions were launched in the UK, giving three hours' playing time. Improved versions have already appeared, the main items receiving manufacturers' attention being timers with extended operating periods, facilities for locating particular parts of the recorded material quickly and easily, and the provision of pause controls.

There is no doubt that many leading international TV firms regard domestic video as the key to their future. The colour TV markets in the developed world have reached saturation point – the markets are now mainly first-time buyers and replacement ones – while it's likely that countries such as Korea, Taiwan and Singapore will scoop third world TV markets as they open up. So video is an obvious thing for Japanese and European TV firms to go for.

Seeing the growing dominance of the Japanese video firms, Grundig decided to develop a variant on the N1700 system with more sophisticated features such as search-

tuning. Its SVR system, giving four hours' playing time, was launched in 1978.

Which brings us close to the end of the decade and the recent announcement of the joint Philips/Grundig V2000 system. You might have thought that there were enough non-compatible VCR systems already. True enough, but if a major technical breakthrough has been achieved then yet another system is justified. All the systems so far use $\frac{1}{2}$ in. tape. What Philips and Grundig have succeeded in doing is to get up to eight hours' playing time (with a corresponding reduction in tape costs) from a cassette, by making use of the tape twice over. In fact it's a $\frac{1}{2}$ in. recording system on $\frac{1}{2}$ in. tape, the arrangement being similar to the standard audio cassette. This involves the use of some sophisticated techniques, in particular dynamic track following, in order to maintain correct head/track alignment. We shall have to wait to see whether the system is accepted in practice however. As they say, the proof of the pudding is in the eating. Philips and Grundig are nevertheless to be congratulated on their successful development of the new system, and it's refreshing to find that the European TV industry is not prepared to play second fiddle to you know who.

The situation is unlikely to end at this point however. Other systems are under development. Funai Electric of Japan for example intends to introduce a system using a $\frac{1}{2}$ in.-tape cassette, and there is some emphasis on the development of light-weight portable machines – the present generation of VCRs is hardly acceptable for portable use, being intended mainly as time-shift devices (seeing the programmes when you want to rather than when the broadcasting schedules dictate).

The intense competition in the video field has given the consumer the benefit of very reasonable VCR prices. Manufacturers can hardly have made much out of their VCR efforts to date. What are the prospects? We still incline towards pessimism. Do people have the time or inclination, even if they have the spare cash, to dabble with yet another piece of domestic technology? It's one thing to pick up the paper or switch on the radio or telly, another to organise yourself so that you can decide what you want to see and when a week or more in advance, and then arrange everything accordingly. And of course the marketing effort will be against a background of forecast deepening world economic recession.

Correction: The value of R9 in the class AB video circuit featured in the monochrome monitor conversion article last month should have been shown as 47k Ω , not 27k Ω .

Teletopics

TELETEXT TROUBLE

Setmakers, through BREMA, have expressed concern over the slow growth of the teletext service and are understood to be seeking government assistance. Production of teletext-equipped sets has failed to reach anything like the expected levels. The industry had originally hoped to sell about 40,000 teletext-equipped receivers by the end of 1977, but to date only some 20,000 sets have been sold. Production potential is said to be around 50,000 sets a year, but only half this number is at present being produced. The industry is blaming the price of teletext-equipped sets – around £700 for a 26in. model. It's felt that the public will begin to buy in large numbers only when teletext sets are available at an extra £60 to £70.

Apparently some i.c. manufacturers have encountered problems in getting the chips to operate at the frequencies involved. The price of sets of teletext i.c.s is certainly appreciable at present, accounting for much of the high price premium of teletext sets. Setmakers feel that a major breakthrough would occur if the price of the sets of chips could be brought down to around £10 to £15. This is one of those awkward chicken and egg problems however. Low production means high prices, and until volume production commences the prices will remain high.

With a saturated TV market, increased public demand for teletext sets will come mainly through replacement sales. Whilst replacement buyers frequently go up market, the present premium seems to be a deterrent to many purchasers.

DOMESTIC SATELLITE TV RECEPTION STARTS IN THE US

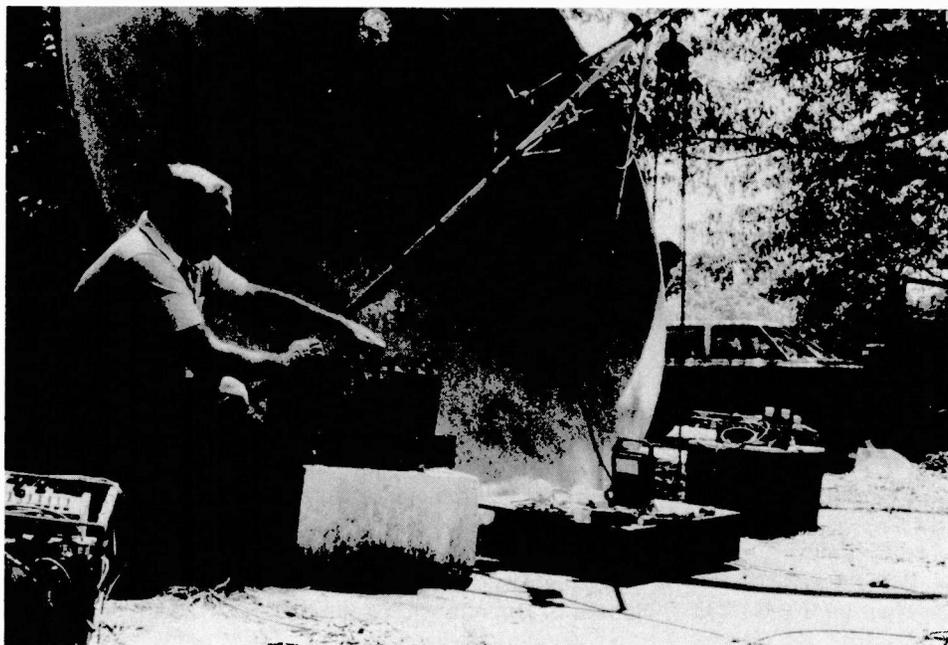
Satellites have been in use for some time now in the USA for coast-to-coast TV programme distribution, and have in particular benefited cable system operators in enabling them to increase substantially the number of channels

available to their subscribers. So why not set up your own backyard terminal, and link yourself to the satellite TV distribution system? Well cost for one thing. Until recently, it seems.

As we go to press with this issue a Satellite Private Terminal Seminar (SPTS-79) is being held in Oklahoma City, co-ordinated by Bob Cooper who is well known for his DX-TV activities and as the former editor-in-chief of the CATJ magazine. Four years ago a satellite receiver terminal would cost you over \$100,000. The cost a year ago was \$25,000, and has now fallen to under \$8,000. If you have the knowledge to build and set up your own terminal however, the cost can be in the region of \$500 to \$1,000, depending on how much surplus equipment you can obtain to incorporate in the installation. Those attending the seminar were provided with two complete sets of plans for building a satellite terminal – the Coleman Conversion and the Howard Terminal.

EXTENDED PLAY VIDEODISCS

The battle of the VCR systems raged mainly around how many hours' playing time you could get out of the cassette. Now that Philips are test marketing their videodiscs in the USA (in Seattle and Atlanta initially) a similar contest seems to be looming up. The basic Philips videodisc, which we described in some detail in our June 1975 issue, has a playing time of an hour – half an hour per side. This is rather wasteful of disc space however if you think about it. The laser scans the disc from the centre outwards, each rotation of the disc giving a complete picture, i.e. two fields. This means that at the end of the disc (outer edge) a field takes up far more space than at the centre. Much more information could be crammed on the disc if the length of track occupied by a field was kept constant from the centre to the outer edge, with the disc speed being reduced accordingly as the scan proceeds. This is the proposal put



Robert Coleman of South Carolina with his \$200 satellite TV receiver terminal. Surplus equipment which Robert obtained over a six-month period enabled the cost to be kept to a minimum. Robert Coleman is believed to be the first individual working privately to design and bring into operation state-of-the-art gallium-arsenide f.e.t. low-noise amplifiers for this service. Coleman's receiver electronics cost him less than \$50 to assemble and put together: he was one of the programme instructors at the recent Satellite Private Terminal Seminar held in Oklahoma City.

forward by Philips for their Extended Play videodisc. There would be one complete picture per disc rotation at the centre, as with the Standard Play disc, and three complete pictures per rotation at the outer edge, the speed being progressively decreased from 1,800 r.p.m. at the centre to 600 r.p.m. at the outer edge.

Sony, who have also demonstrated a working optically-scanned videodisc system, have put forward an alternative suggestion – halving the disc speed to double the playing time.

TV4

The Government is to introduce a bill during the next parliamentary session extending the life of the IBA and giving it responsibility, "subject to strict safeguards", for the fourth TV programme. If all goes ahead as at present planned, TV4 is expected to open as a commercial network under IBA control in late 1982 or early 1983. The previous Government had authorised the IBA to commence engineering work for the new network.

MARKET FORECASTS

Mackintosh Consultants have issued a prediction that by 1982 72 per cent of Western European homes will have a colour receiver – this compares with 47 per cent last year. There is considerable variation between countries at present. Whilst the W. German, UK and Swedish markets are virtually saturated for example, only 15 per cent of Spanish homes have a colour receiver. The Spanish market is not likely to provide opportunities for hard-pressed German and UK setmakers however, since the Spanish TV industry enjoys a considerable measure of protection while per capita income is likely to prevent a rapid growth of sales.

As a result of excess production by W. German setmakers over a million sets are now estimated to be held in stock. Prices have fallen by a quarter, and some plants are working on short time.

The total European VCR market last year reached 225,000. BREMA figures suggest that UK imports had risen from 22,000 in 1977 to 95,000 last year. Mackintosh suggest that if the average VCR retail price falls below £600, European sales this year could reach 450,000.

The Henley Centre for Forecasting has also been looking at its crystal ball. Predictions here are that UK VCR sales could reach 150,000 this year, and that the market value of video systems will show an increase of over 1,000 per cent over the period 1978-84.

STATION OPENINGS

The following relay transmitters are now in operation:

Brushford (West Somerset) BBC-1 ch. 21, Westward Television ch. 24, BBC-2 ch. 27. Receiving aerial group A.

Claonaig (Kintyre) BBC-1 ch. 55, Scottish Television ch. 59, BBC-2 ch. 62. Receiving aerial group C/D.

Dowlais (Mid-Glamorgan) BBC-Wales ch. 58, HTV Wales ch. 61, BBC-2 ch. 64. Receiving aerial group C/D.

Faversham (Kent) BBC-1 ch. 22, Southern Television ch. 25, BBC-2 ch. 28. Receiving aerial group A.

Grantown-on-Spey (Highland) Grampian Television ch. 41, BBC-2 ch. 44, BBC-1 ch. 51. Receiving aerial group B.

Ireshopeburn (Co. Durham) BBC-1 ch. 55, Tyne Tees Television ch. 59, BBC-2 ch. 62. Receiving aerial group C/D.

Oban (Strathclyde) Scottish Television ch. 41, BBC-2 ch. 44, BBC-1 ch. 51. Receiving aerial group B.

Walthamstow (London) BBC-1 ch. 45, Thames/London

Weekend Television ch. 49, BBC-2 ch. 66. Receiving aerial group E.

All the above transmissions are vertically polarised.

The latest (May, 1979) issue of the IBA's invaluable pocket guide to transmitting stations has now been published. Copies can be obtained from the IBA Engineering Information Service, Crawley Court, Winchester, Hants, S021 2QA.

JAPANESE BUY UK CHIPS

Matsushita has placed an order with Plessey for 200,000 1GHz divide-by-256 CMOS i.c.s for use in a frequency synthesiser tuning system to be incorporated in up-market Panasonic TV receivers. The Plessey chip has been selected because it's the only 1GHz divider that can drive CMOS metal-gate logic directly without the need for low-power Schottky interfacing.

SUPERTITLING

Amongst the systems under development at the IBA's engineering headquarters is a new process called "Supertitles" to help the hard-of-hearing follow TV programmes. The system operates on the same principles as teletext, boxed captions appearing at the bottom of the screen. One problem is the fact that most people speak at a rate of around 160 words per minute, while few typists or machines can handle much over 80 words per minute. Southampton University is collaborating with the IBA on the project.

FLAT-SCREEN TV FROM SINCLAIR?

At a recent press conference Clive Sinclair announced that his company is in the final stages of developing a flat-screen TV receiver. The initial model would be a 3in. portable the size of a small paperback, but the principle can apparently also be used for large-screen models. What exactly the principle is remains something of a mystery, the only fact to emerge being that the screen is 3/8in. thick. Sinclair Radionics is unable to finance the establishment of a production line for the new development however, and is looking for a partner willing to provide the required investment. Meanwhile production of the present Microvision model is being moved from the company's St. Ives factory, where 160 redundancies have been announced, to a new and so far undisclosed location.

THE PYE STORY

A twenty page booklet marking the fiftieth anniversary of the formation of Pye Radio Limited is available to members of the public on application to Pye Ltd., Publications Department, 137 Ditton Walk, Cambridge. This fascinating little publication, entitled "*The Story of Pye Wireless*", traces the history of Pye receivers from the early twenties (the Pye Unit System of 1922) to the present day. TV sets, from 1936 on, naturally also feature in the story. Many of the early sets are illustrated.

An intriguing part of the story is the creation of Pye village industries throughout East Anglia during the 1939-45 war. The Government had suggested that Pye build a giant shadow factory. Instead however Pye took work to the villages in order to make use of the vast productivity potential of the area. By the end of the war the most complicated electronic equipment was being made in every corner of East Anglia, many people working at home. Pye had over 14,000 employees in village industries at the time.

Receiving French TV

Hugh Cocks

FRENCH TV can be received on a permanent or semi-permanent basis over quite a large area of England (apologies to those in Scotland, N. Ireland and Wales). Signals are present all the time along the entire south coast and a fair way up the east coast, and extend some way inland. During settled weather conditions, very strong signals are present over much of the country. There are three French TV networks, Television Francaise 1, Antenne 2, and France Regions 3. They can provide a refreshing change from our local programmes, especially the late night films! Language is not too great a problem: it's surprising how one tends to pick it up after watching for a while, though fast-spoken French in films can be a problem.

French TV System

As in the UK, all three networks use the same transmitter sites at u.h.f. The old 819-line system, used by TF-1 at v.h.f., is becoming obsolete and dates for the closedown of this service are being suggested, giving way to a new 625-line v.h.f. service (where have we heard that before?!).

The u.h.f. network uses system L. This has positive-going vision modulation, a.m. sound spaced 6.5MHz above the vision carrier, and SECAM colour with the subcarriers (two) at roughly the same frequency as our one subcarrier. Needless to say, a UK system I TV receiver won't think very much of the French transmissions, producing a somewhat jumbled negative picture with mostly buzzing from the loudspeaker. A system I set can be used to line up the aerials in the first place however, before you get too committed with system L receivers.

Which Transmitter?

The first thing to decide is which transmitter to try to receive. The map shown in Fig. 1 indicates the transmitters most favourably received in the UK. Those marked with an asterisk are lower powered ones, but can be well received under good conditions. A problem that has to be taken into account is UK transmitters on the same or adjacent channels. The channel groupings correspond to our own (the channel numbers are exactly the same) with the exception of Boulogne where a wideband aerial will be required.

As a very approximate guide to the "UK service area" of these transmitters, Lille is strongest up the east coast and inland areas; Boulogne in east Kent and south east Sussex; Caen from mid-Sussex to east Devon; Brest in the south west; and Rennes in the Channel Islands. Obviously the local terrain and UK relay transmitters may make the final selection of a transmitter somewhat different from this rough guide.

Care is required in receiving Caen in central southern England, as the aerial will be pointing more or less at Rowridge, Isle of Wight, which is only one channel away. Extra i.f. and aerial filters may be required therefore in order to get good results – to say nothing of high-gain aerials with a sharp forward pickup lobe. Sideways stacked aerials are

recommended, especially in this area, in order to narrow the forward pickup lobe – the problem in most locations will be not so much the strength of the received signal as the level of interference from UK transmitters.

Receivers

As regards receivers, there are several options open to the budding French TV viewer. The obvious one, though expensive, is a quick trip to Boulogne, where a set can be purchased at a price in excess of UK TV prices plus a large dose of French VAT (33%!) to say nothing of UK customs duty. Certain setmakers, notably the German ones, can supply SECAM sets in the UK. It's worth making enquiries.

Perhaps the easiest solution, to start off with anyway, is to convert a UK monochrome TV receiver. Late dual-standard sets are the best, in particular the Bush TV161 series. Modifications are relatively simple with a dual-standard set, as the French system L is a mixture of our 405- and 625-line systems. As a bonus, the set can still be kept dual-standard, switching between the UK and French u.h.f. systems.

Typical Conversion

As an example then we'll take the Bush TV161, though other dual-standard chassis will doubtless serve just as well.

First disconnect the switching linkage between the i.f. and timebase panels, and solder the timebase panel for operation on 625-lines only.

Connect switches 2S1a, b and c on the i.f. panel permanently in the 625-line position. This is best done at the rear of the panel, by breaking the "405" print to the switches and linking the "625" contacts together. To cater for the 6.5MHz spaced French sound, the old 405 sound i.f. needs to be moved from 38.15MHz to 33MHz. This is easily accomplished by increasing the value of C24 in the 2VT2 transistor can from 3.9pF to approximately 5.6pF,

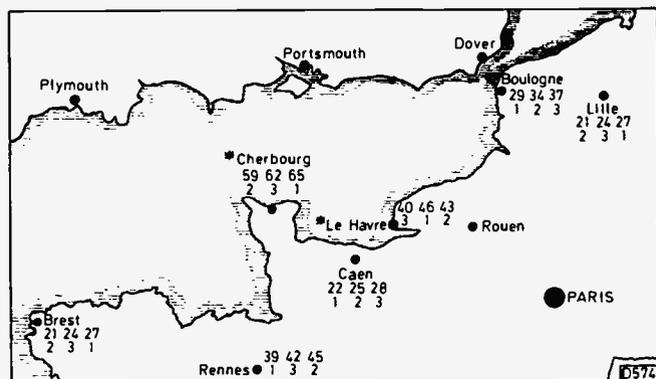
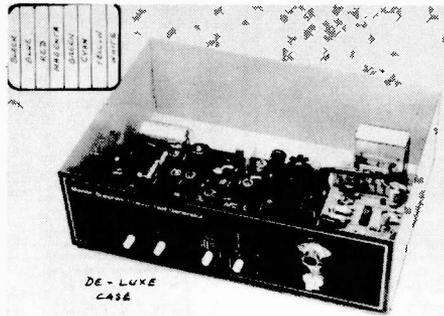


Fig. 1: French TV transmitters which can be received in the UK. Those marked with an asterisk provide a strong signal in good reception conditions only. Cherbourg, Le Havre and Boulogne have an e.r.p. of 100kW, all others an e.r.p. of 1MW. Rouen is also a 1MW transmitter, but the channels are the same as Crystal Palace. The network number is shown beneath the channel number.

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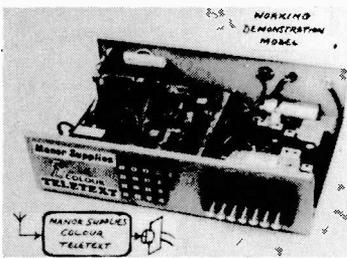
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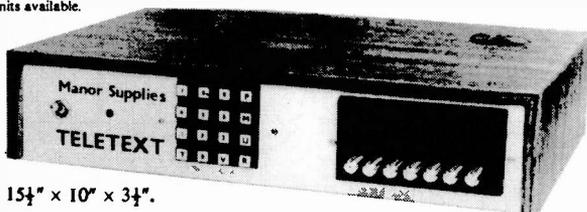
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M6

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M7

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M8

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M9

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M10

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M11

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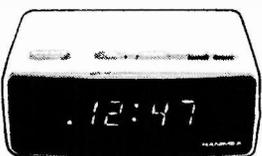
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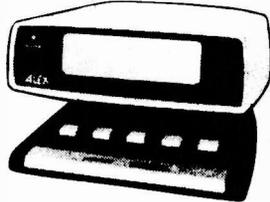
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M15

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LED CLOCK**



Automatic brightness control. Weekend alarm cancel.

Features and Specification:
Hour/minute display. Large LED display with p.m. and alarm on indicator. 24 Hours alarm with on/off control. Display flashing for power loss indicator. Repeatable 9-minute snooze. Automatic brightness control. Weekend alarm cancel.

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M16

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increasing the value of C54 in the 2VT5 transistor can from 47pF to 82pF, and increasing the value of C61 in the 2VT6 transistor can from 33pF to 47pF. In the 405-line position the i.f. panel switching now corresponds to the French system, while the 625-line position remains as required for UK reception.

Alignment

When it comes to alignment, no alteration to the UK side of things is required of course. Switch the i.f. strip to the French position, and tune in a French transmission. Sound of sorts should be heard immediately, probably accompanied by buzzing.

Starting with the sound take-off coil L11, adjust for maximum sound and least buzz. Then adjust the first and second sound i.f. coils L26 and L30 for the same results. Go back to L11, and repeat the procedure once or twice. This should produce buzz-free sound. Note that the contrast control (405/French) should not be over advanced, or sound-on-vision and vision-on-sound may result (the old 405-line system complaint!). When satisfied with the sound alignment, tweak L10 (2VT2 can) in the vision channel on test card (yes, the French radiate the PM5544 pattern all afternoon on the third channel!) for optimum frequency response. You should now have a highly sensitive French/UK TV receiver.

Single-standard Sets

Single-standard sets can also be modified, but require a great deal more work – not so much in providing for demodulation of the positive vision signal, but in arranging for the a.m. sound. An approach I've used is to employ the ubiquitous surplus Philips G8 gain and vision selectivity modules (see Fig. 2).

Three modules are required, two selectivity ones and a gain module. Insert one selectivity module immediately after the tuner, diplexing the output from this to the main i.f. strip and to the second selectivity module. The output from the latter goes to the gain module, whose video output pin provides the audio signal. By suitably aligning all the Philips cores, good sound can be obtained.

The correct vision signal sense can be obtained by using a phase-splitter stage in the main i.f. strip, following the vision detector diode. A suitable transistor is often present anyway as an emitter-follower, the simple course then being to take the signal from its collector. Beware of any d.c. coupling. If this is present, a.c. coupling will have to be introduced. You might think that simply reversing the detector diode would do the trick, but this will totally upset the a.g.c. circuit and any d.c. coupling present. No interaction occurs incidentally between the Philips units and the existing i.f. strip.

As it stands of course this results in a single-standard (French) TV receiver. By adding switching (a relay is best) however the sound and vision can be switched back to the UK standard: use the existing 6MHz feed for the sound, and tap the emitter of the phase-splitter transistor for the vision – also cut the supply voltage to the a.m. sound i.f. system.

Colour

The more adventurous reader may ask what scope there is for modifying a UK colour set for SECAM reception. Modifying an existing PAL only board would be a formidable task unfortunately. SECAM is a completely

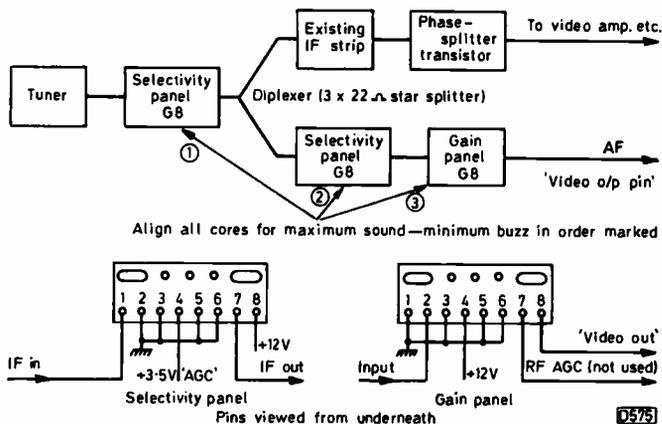


Fig. 2: Block diagram of a single-standard receiver converted for reception of French TV.

different system up to the matrixing of the luminance and colour-difference signals. One or two UK setmakers have produced export versions of their chassis, often with a PAL/SECAM decoder. The latter is a clever one with electronic switching between the two systems. I've seen such a board for the Thorn 3000 chassis. The situation with this is somewhat complicated by the fact that the board was made in Belgium and not by Thorn themselves, who cannot supply it.

Results

Providing there's a clear take-off in the French direction, and interfering signals are at a low level, signals of sorts should be seen at up to 150 miles from a 1MW French u.h.f. transmitter. Needless to say, high-gain aerials mounted as high as is practical should be used, particularly the farther inland one is. As mentioned earlier, the main problem will come from UK transmitters on the same or adjacent channels. If several French transmitters seem likely to be received, a wideband aerial on a rotator could be employed. During enhanced tropospheric conditions the signals become very strong indeed – often with stations from the south of France causing co-channel interference.

If you obtain a SECAM colour receiver, you'll obviously need a higher signal level than for monochrome reception. Below a certain signal level, colour noise increases rapidly with the SECAM system, due to the f.m. threshold effect. This happens only at quite low signal levels however, and in practice SECAM can provide a better signal-to-noise ratio than PAL under mediocre signal conditions. Noise tends to appear as long streaks with SECAM and can be irritating.

It would be possible to build a monochrome French to UK system converter. The French signal would have to be demodulated and then remodulated to the UK standard on a spare UK u.h.f. channel. I can somehow envisage a few G8 modules in the French i.f. strip!

One inconvenient point is that you can never be too sure what programmes are being shown on French TV until the day of the transmission. The French TV guide is published well in advance: it can be ordered through large newsagents.

It should be possible to obtain a teletext decoder or modify a UK one to receive the French Antiope system (different again, needless to say!) and have pages of French information in good signal areas.

Finally, my thanks to many friends in the south of the country who have helped with advice on suitable transmitters for different areas. And my apologies to anyone who is well and truly out of range of French TV... ■

The V2000 VCR System

THE new V2000 VCR system which has been jointly developed by Philips and Grundig represents a major advance in VCR technology. The compact cassette, roughly $7 \times 1 \times 4\frac{1}{4}$ in., is capable of providing up to eight hours' playing time. It achieves this by using a quarter-inch video recording system, i.e. there are two sets of video tracks (see Fig. 1) one above the other on the $\frac{1}{4}$ in. tape. The arrangement is the same as that used with audio cassettes: when one track length has been used, the cassette is withdrawn, turned over, and the second section of track is used. With each track section providing up to four hours' playing time, the total playing time is a maximum of eight hours.

The greatly extended playing time – and thus tape economy – has been achieved by cramming yet more information on to the tape. The speeds used are much the same as with other current machines, but the track width is the narrowest yet. As a comparison:

System	Tape Speed	Read/write speed*	Track Width
N1700	6.56cm/sec	8.1m/sec	84 μ m
SVR (Grundig)	3.95cm/sec	8.2m/sec	51 μ m
VHS	2.339cm/sec	4.83m/sec	49 μ m
Betamax	1.873cm/sec	6.6m/sec	30 μ m
V2000	2.44cm/sec	5.08m/sec	22.6 μ m

*Taking head and tape movement into account.

So the increased information packing density has been attained by using quarter-inch recording and very narrow tracks, laid down side by side. This implies the need for great accuracy in the head/track alignment, and for this purpose a new technique has been adopted – dynamic track following (DTF).

The video heads (see Fig. 3) are mounted on small plates of piezoelectric ceramic material which are in turn attached to the upper section of the head drum. Since piezoelectric material bends when a voltage is applied to it, this enables the heads to be moved vertically. The control voltage is obtained from the head as it follows the track, so that the alignment of the head with the track can be continuously maintained. The use of this technique has other advantages: interchangeability of cassettes between machines is guaranteed, while slow-motion, fast-motion and still-frames can be obtained with good picture quality and without interference.

The self-correcting video head system (dynamic track following) operates during both record and playback. The usual control track is dispensed with. As shown in Fig. 1 there are audio tracks at each side of the tape, both capable of stereophonic recording/reproduction, and cue tracks in the centre. These latter are not used in the initial production VCRs, but will be employed in later development of the system. For control purposes, DTF signals are laid down on the track during recording at frequencies below the 625kHz chrominance subcarrier (see Fig. 4). These vary between adjacent tracks, following the sequence (Fig. 5) 102kHz (f1), 117kHz (f2), 164kHz (f4), 149kHz (f3). Frequencies f1

and f4 are recorded by one head (K1), frequencies f2 and f3 by the other (K2).

Dynamic Track Following

During playback, the relevant video head scans the recorded tracks. In addition to the video signal and the track's DTF signal there will also be, due to crosstalk, difference frequencies is compared, to find out in which signal frequencies on adjacent tracks. Say head K1 is scanning a track with a 102kHz DTF signal (f1). Adjacent tracks will carry 117kHz (f2) and 149kHz (f3) signals. The two difference-frequency signals produced will thus be 15kHz and 47 kHz ($117 - 102\text{kHz} = 15\text{kHz}$, $149\text{kHz} - 102\text{kHz} = 47\text{kHz}$). The relative amplitude of these two difference-frequencies is compared, to find out in which direction the head is tending to move away from the correct track, and as a result a correction signal is obtained for application to the piezoelectric plate. This then pulls the head back into alignment with the track. The difference

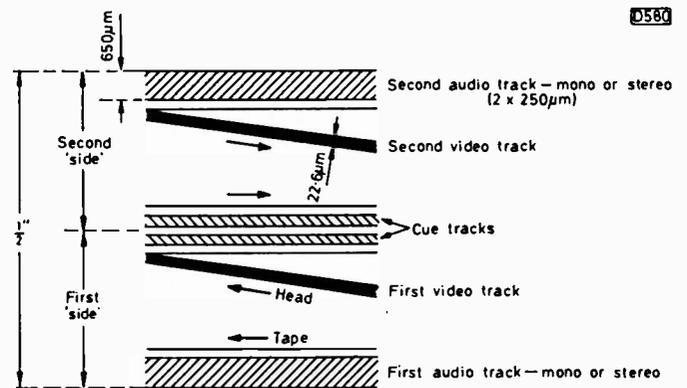


Fig. 1: Arrangement of the tracks on the tape.

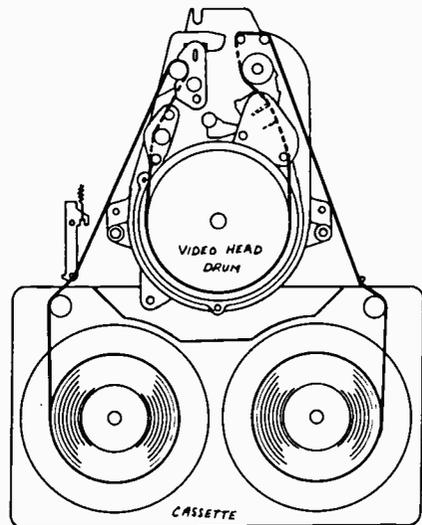


Fig. 2: The M-wrap tape path in the recorder.

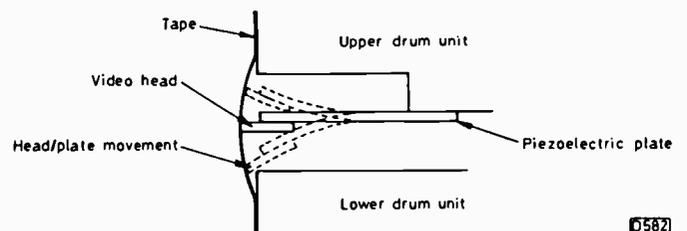


Fig. 3: The heads are mounted on servo-controlled piezoelectric elements to provide dynamic track following.

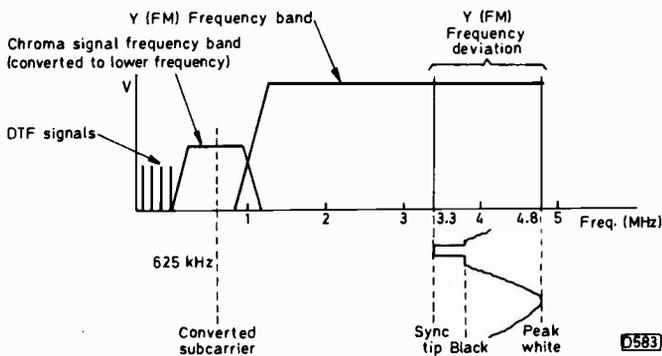


Fig. 4: The signal positions within the bandwidth.

frequencies are 15kHz and 47kHz whatever the track, as some addition and subtraction exercises will show.

During the period when a video head is not in contact with the tape, i.e. between fields, its piezoelectric carrying plate is restored to the position it had at the commencement of the previous track. When the head returns to contact with the tape therefore it's in the correct starting position.

The head drum is specially heated in order to reduce to a minimum the effect of any mechanical changes during the scanning of the tape. By keeping the drum at a constant temperature, its diameter hardly alters. Wear on the head and frictional losses due to the tape sticking to the drum are thus reduced to a minimum.

If the two heads show an equal deviation in the same direction during playback, the effect is remedied by moving the tape. For this action, the control voltage from the DTF discriminator is fed to the tape servo. The result is that the tape is moved relatively to the heads, restoring the correct alignment. This is termed automatic tracking (see later).

During recording, the heads must be lined up in exactly the correct position with respect to each other, since the video tracks are laid down side by side with no guard band. Due to tolerances however, for example the hysteresis characteristics of the piezoelectric head carrying plates, there is no permanent static condition. This means that dynamic control is necessary during recording as well as during playback.

This is done by placing one head in the nominal position and including the other in a control loop. An additional reference signal, at 223kHz, is recorded on the track for a one and a half line period during the field flyback. During the following one and a half lines, no signal is recorded on the track (see Fig. 6). This enables the signal on the adjacent track to be read in order to provide the required control voltage.

Servo Systems

The tape runs through the recorder at a constant speed of 2.44cm/sec. For this purpose the capstan is directly connected to the capstan motor spindle, on which a 216-pole tachogenerator is mounted. The motor speed is 116.4 r.p.m. Speed control during recording is achieved by comparing the phase of the signal from the tachogenerator with that of a fixed 419.376Hz signal produced by a crystal oscillator. During playback, the previously mentioned automatic tracking system is used to move the tape into the required position instead of using phase comparison.

The head drum is also directly driven, with the motor connected to a 125-pole tachogenerator. The speed of the head drum is 1,500 r.p.m. For phase comparison purposes a phototransistor, coupled to the head drum, produces one

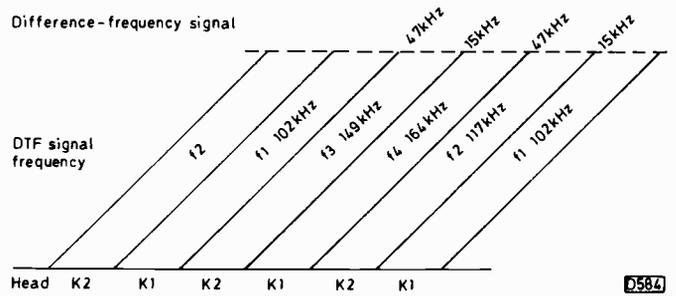


Fig. 5: The sequence of the dynamic track following signals. Read from the right, this is f1, f2, f4, f3.

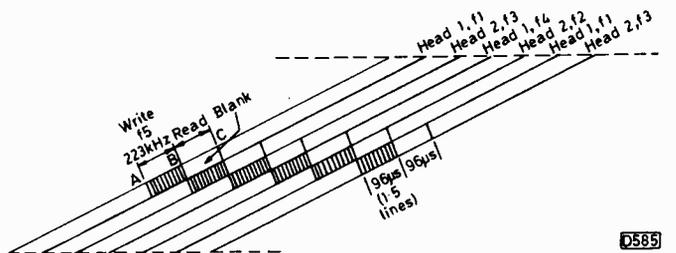


Fig. 6: For dynamic head position correction during recording, a signal is laid down during a 96µsec period while the field flyback is occurring. Recording ceases during the following 96µsec period, the head then reading the crosstalk signal from the previous track. The resultant signal initiates the servo control action.

pulse per revolution (25 pulses per second). These are compared to a 25Hz reference frequency. During recording the reference frequency is produced by division from the field frequency; during playback it's produced by a crystal oscillator.

The scanning unit, which consists of the microchassis and the integrated head drum motor/video head drum assembly, has been designed so that it can be automatically preadjusted in the factory. The scanning unit can be exchanged without difficulty in either the factory or the service department. The same interchangeability applies to the following parts of the scanning unit: the head drum motor (with or without head drum), the head drum, the audio head, and the erase head.

Signal Handling

As with the N1700 system, the slant-azimuth technique (the two heads are angled at +15° and -15° with respect to each other) is used to avoid luminance crosstalk between adjacent tracks. To avoid crosstalk between the lower frequency chrominance signals, a comb filter consisting of a 128µsec delay line and an adder circuit is used. This of course is a similar idea to the basic PAL arrangement. These techniques are said to ensure good picture quality during playback, while good sound quality is achieved by a new system developed by Philips - "dynamic noise suppression".

Operation

The VCR has been designed for simple, foolproof operation. Search tuning is employed, as in the Grundig SVR system (see *Television*, July). Once the search button has been pressed, the recorder automatically scans all the TV bands. Accurate, automatic tuning occurs immediately a station is found. The tuned-in frequency can then be stored in the memory, by operating the "store" command followed by a channel number chosen by the user. A maximum of 26 channels can be stored in the memory.

The Philips VR2020 VCR has five memory blocks for storing recording instructions. Each block stores the required starting time, stopping time, day of recording and the relevant channel number. Programming can be done up to 16 days in advance. Once the recorder has been programmed in this way, anyone using the recorder in between is warned by the indication "attention timer". The cassette lift opens if there is no cassette or a protected cassette in the machine, drawing the user's attention to the fact that he cannot record under these circumstances.

There's a separate switch, which can be set in either of two positions, for each side. In one position recording is possible: in the other, marked by a red indicator, recording and erasure are not possible. This provides protection against unintentional erasure.

If the auto-rewind button is pressed at the end of the pre-programmed recordings, the recorder automatically winds back to the beginning of the tape.

The VR2020 is equipped with a four-digit electronic tape counter. To go back to a certain tape position quickly, the go-to button is pressed and the required counter number is keyed in on the keyboard. The recorder then winds forward or backwards to the position requested. The counter is

automatically set to zero at the beginning of the tape. It can also be set to zero manually if required.

An infra-red remote control system provides remote channel selection and control of all the tape drive functions.

The use of an advanced microprocessor makes operation very simple. If any key is pressed at random, a check is first of all made by the microprocessor's programme to see whether the requested operation is permissible – for example in the case of recording with a protected cassette in the machine. The recorder is completely safeguarded against incorrect operation therefore.

As a result of using microprocessor control, it's possible to switch over directly from wind to play or from off to record for example: all the necessary intermediate steps are automatically carried out by the recorder.

If the electricity supply is interrupted, the channels stored in the memory are retained for about three months. Also, once the supply has been restored any interrupted operation continues.

The recorder contains a wideband aerial amplifier which passes the off-air or VCR signal to the TV set without loss. It's not necessary therefore to switch the recorder over between off-air and playback when the VCR and the TV set are used alongside. ■

No Clock Display

Steve Beeching, T.Eng. (C.E.I.)

THE problem with a Sony Betamax SL8000 VCR we had in recently was that on switching on the clock didn't show any digits. The first thing I did of course was to check that the supplies were reaching the timer board – these are 10V, -20V and 2.5V a.c. They all seemed to be o.k., making the checks with my oscilloscope since any further testing would probably require its use to check on the presence or absence of pulse waveforms. So on we went to check the waveforms around the timer i.c. IC3101. There seemed to be a general absence of pulses, except for pins 1 and 42 which had 400kHz pulses and pin 36 which had a 50Hz squarewave – at the correct levels.

There are five enable lines to the display board (four figures plus colon), on pins G1 to G5. Enable is 10V, otherwise the lines are biased to -20V via 100kΩ resistors. Each figure consists of a seven-segment arrangement, a to g, and each part of the colon has its own input. Without any input pulses there's no illumination – the digits are multiplexed, G1 to G5 being strobed in turn and each set of segments altered digit by digit at a fast rate to produce a constant display.

It seemed at the time a good idea to change the timer i.c., no mean feat since it has 42 soldered pins and is a CMOS

type at that. So the new one went in with me chained to earth. Switch on and . . . oh dear, no lights! Still no pulses anywhere either. My workshop has dents in the wall that match my forehead after previous VCR nasties, so I added a few more.

A closer look was needed since something had obviously been missed. Check i.c. pin voltages carefully. All correct except for pin 7, the reset pin, which is connected to the collector of Q3001 (see Fig. 1). This transistor should have been turned hard on, with its collector at 0V. Instead, it was at 7.5V. Drastic measures were called for, so I earthed the collector – and got lots of pretty green lights from the display. I then discovered that the 10V line was in fact also 7.5V.

Now Q3001 resets all the timer i.c. functions when the VCR is switched on, or in the event of a mains interruption, thus eliminating any false timer action. At switch on, Q3001 is biased off by the -20V rail. The 10V rail rises slowly, due to the large values of the decouplers and the action of C8104 (see Fig. 2) in the 10V regulator circuit. As the 10V rail rises, the voltage at the collector of Q3001 increases and, at a point just over 8V, the timer i.c. is powered but held reset. At about 8.2V, zener diode D3001 switches on, applying a positive voltage to the base of Q3001 which also switches on. Its collector voltage falls to 0V, thus removing the reset.

So if the 10V rail is lower than 8V, the i.c. is held reset and nothing happens. The fault was clearly in the power supply, and swapping the timer or display boards would have had no effect on the fault. The trouble was in fact due to an open-circuit joint on the 10V supply reservoir capacitor C8106. The effect of the rest of the circuit was to produce a well-smoothed 7.5V supply.

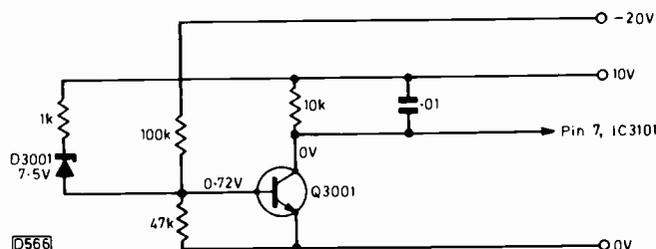


Fig. 1: Timer i.c. reset circuit.

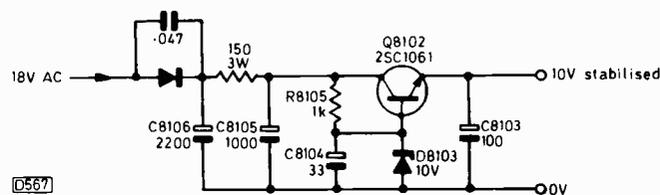


Fig. 2: 10V supply circuit.

All Slog and No Grog . . .

Les Lawry-Johns

THERE'S absolutely no rest for us busy boys lately. Even when we finish you can bet your life some joker will spoil your pint with "I don't want to bother you, but . . .". You escape from that and settle down at home with a bite to eat and a quick glimpse of the telly before bedtime and the thing changes channels all on its own. So you give up and go to bed and dream about sets that won't go right or women that won't go wrong or something. Look at yesterday for instance. It started with colourless sets.

First an 8500 (Ferguson) with the complaint that the colour had been intermittent but had now gone beyond recall.

Dealing with Lack of Colour

I suppose we all have our own pet ways of making a start when tackling faults that can have various possible causes. I always like to start on this one by proving the presence of timing pulses from the line output stage. These are applied to connection 3/2 on the decoder panel on the 8000 series chassis, and can be measured at TP9 in the burst gate circuit. Finding little activity here we nipped smartly over to the timebase panel and had a look at TP28, which again was lifeless. It was a short step from here to R404 (33k Ω) which was found to be open-circuit.

Nice going we thought. Keep it up and we might regain some of our lost confidence which has taken a bashing lately due to persistent wrong diagnoses, er diagnostics, er, jumping to the wrong conclusions, with the consequent hours lost plodding toward the right conclusions.

And the Next Gent Please

Of course the next case just had to be loss of colour again. Apparently Mr. Earlybirth had had a spot of trouble with his Philips G8 of late, and was dissatisfied with the service he had received from the original suppliers of the set. He produced massive repair bills to prove it. Horrific would perhaps be a better word. Since the last one was very recent and was incurred in the quest for lost colour, I suggested that he returned the set to the repairers for their approbation. "I'm too scared" he said. "It'll probably be a hundred quid this time." I couldn't quite see how this could happen, but as he was clearly adamant about not going back with it I didn't press the point further.

"O.K. Mr. Earlybirth, leave your phone number and we'll ring you when it's sorted out."

Clearly this was one to approach with caution. It was one of the separate panel type, and it was obvious that some work had been done on both the signal and the decoder panels.

So we decided to cut across the usual routine and fit a known good decoder panel which we just happened to have lying around. With this in there was still no colour, so we did something daft. We refitted the original panel and then checked for the positive and negative pulses at pins 8 and 1 respectively at the rear edge connector. The negative pulses were there but there was no joy at pin 8 (TP39). So over we went to the timebase (line scan) unit and checked at pin 1 of

plug U. Nothing here so follow the track along to R576 (4.7 Ω , or 4R7 if you like that better). It didn't look well, and indeed proved to be open-circuit. A replacement of the same small wattage did not overheat, and the positive pulses were now present on my little diode probe.

Sadly however there was still no colour (and I hadn't left the colour control turned down like I did on that one some time ago, chasing all over the place before I realized it).

So out came the decoder panel again and in went the test one. Full colour. Suspecting hanky-panky, we looked with care at the removed panel. The core of the reference oscillator coil looked decidedly out of place, whilst all the other cores were still sealed. So back went the panel and careful adjustment to the suspect core restored almost normal results except that the grey scale was out and the picture was too bright with the brightness right down.

Resetting the blue d.c. level control R297 restored normal brightness, and a touch up on the green and red level controls restored the grey scale to very nearly perfect. All that remained was to converge the set. This was easier said than done, since R1933 on the convergence panel had seen better days. A new 10 Ω potentiometer put this right, and we were quite pleased with the result.

"Mr. Earlybirth. Your set's ready. Bring a couple of hundred quid with you, ha, ha."

It was a bit premature really because I suddenly became aware that there was no sound when I turned it up to hear what the tennis scores were (I can't read).

The rear cover had to come off again, and the sound returned on its own. This proved to be nothing more than a poor contact on the audio plug, so we weren't all that upset.

Put the back on again, having wangled the control knobs through, and that was that. We didn't really sting him. He got change from three fivers, and was happy.

Only No Sound

"Not a lot wrong" he said. "Not a lot. Just no sound." As this was an ITT CVC5, it came as no surprise and of course we made straight for the PCL86. Giving it a quick clout with a screwdriver handle restored the sound with a sharp crack. In went a new valve and we waited for the sound to burst forth. It didn't. Applying the voltmeter, we found rather more h.t. than we expected. Not too much voltage you understand, but what there was was in too many places.

As usual, my mind went completely blank. I knew I should have h.t. on pin 6, the output pentode anode, but I couldn't remember what pin the screen grid voltage should be on. So we had 200V on pins 6, 8 and 3, and 100V on pin 9. Looking it up, we should have had 200V on pins 6 and 3, but pin 8 was the control grid. Not to be bothered with niceties, the valve was whipped out and the voltage on pin 8 vanished. Another duff new valve, but what had happened to the cathode bias resistor? Nothing apparently. It still read 120 Ω and the 50 μ F decoupler was also in one piece. Another new valve restored the sound.

"While you're at it" said Mr. Ratchet (christian name I presumed was Paul, as it said P on the job sheet), "you

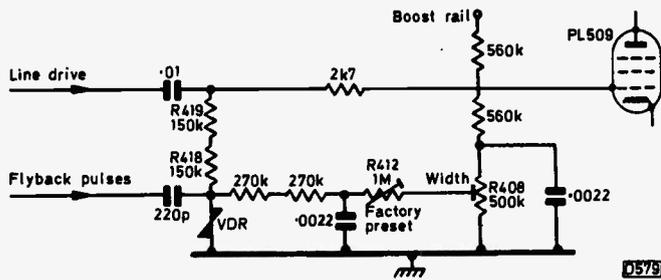


Fig. 1: The width control circuit used in the ITT CVC5 and subsequent hybrid colour chassis. The design is conventional, but care has been taken over its implementation. Pairs of resistors are used to reduce the voltage stress across the individual resistors, and the 0.0022 μ F decoupling capacitors are included to protect the factory and dealer preset width controls against high pulse voltages.

might have a quick look at the picture as there's a line down the left side." There was indeed. It looked like brushing of some sort, and the width only just made it. Just to put us on the wrong track (tracking?) there was a sharp crack of discharge from inside the line output section.

Off came the screening and we peered suspiciously at the tripler and focus assembly. Nothing seemed out of place, and the discharge did not recur. Bearing in mind Eugene's good advice from earlier in the year, we looked hard at the line output transformer subpanel for signs of dry-joints etc. Everything seemed in order.

Looking again at the picture, the line scan did not seem all that even. We concluded however that once the left side dribble was cured everything else would fall into line as it were. For want of something better to do, we changed the PL509. This made matters a damn sight worse, so we changed the PY500 as well. This didn't alter things at all.

Since the width was only just making it, we reset the "dealer width" control R408 (see Fig. 1) which didn't do anything. Neither did the "factory width" control R412, which seemed most peculiar. A meter applied to the PL509's control grid showed that there was adequate drive, and incidentally shot out the width. "Ah ha" we said (not being able to think of anything better).

So off went the supply and we got down to checking the resistors in the width circuit. All seemed in order until we came to the series resistors R418 and R419. They should have been something like 150k Ω each. R419 read o.k., but R418 didn't read at all. A new resistor in this position enabled us to set up the width correctly, with a nice even line scan and no dribble.

"Took a long time to find that, didn't it?" commented Mr. Ratchet. "My name's not Trundle" I protested (sorry Eugene). "My name is the one over the door and I am a well known ditherer. Always have been and it's a bit late to change now. If I was any good at this job I wouldn't be doing it." Now there's a profound thought. I must think about that.

So the Day Wore On

Just for a change we thought we'd have a go at a Ferguson audio effort. "Won't play the records it won't." This was a relief, as we'd had a bit of trouble of late with the cassette side of one of one of these and didn't relish another bout for a time. BSR deck, funny noise, and dead slow on 45 r.p.m.

Take off the turntable and clean up the centre post and bush. Rough up the idler wheel, and a drop of oil into the top motor bearing. Reassemble and check. Nice, quiet and

only slightly fast on the strobe (as usual). Switch to 33. Turntable stops. Do it again. O.K. on 45, stops on 33.

Take off turntable and check on idler wheel. Clunks nicely on to the drive spindle on 45, doesn't want to be pulled across fully on 33. Conclude that there's friction on swing spindle in the 33 position. Oil and try again. No better. Take out unit and check on nylon assembly and notice that swing arm has to come down a shade out of its true position which would make the idler contact the motor spindle. Why? Don't know.

Note that there's movement to spare on the assembly when in the 45 position, but none in the 33 position (determined by a nylon ratchet rotating the cog teeth of the nylon speed selector drum). Think. "If the ratchet is pushing the cog drum too far round, why not move it back one tooth?" Ease out the ratchet and allow the drum to advance one tooth. Instant success. Now plays 33 as well as 45.

Question: how did the ratchet and cog get out of sync in the first place? Never mind, plod on.

Think about calling it a day and cashing up. Not difficult as there is no cash in till other than that wrested from Mr. Earlybirth and Mr. Pawl, sorry Mr. Ratchet. Will have to reduce fluid intake until our monetary affairs improve.

Later

We had only a couple of halves, and that was spoilt by someone wanting to know something I didn't know anything about. And so to bed.

Funny it keeps changing channels like that. I'll have to see if it's the i.c. Never mind. Think about it tomorrow. Wonder what I can chat about in the next article? Twenty five years with the September issue, seems only yesterday.

Thirty years ago: wrestling with old prewar Cossor 1210 with the funny sync separator. Two top caps at 90 degrees, one for line, the other for frame (not field then). Bloody great 15in. tube.

Thirty five years, thirty six or so . . . I can still hear the boys singing Lily Marlene.

"There's a desert squadron
Somewhere in the blue,
No one there that matters
To tell 'em what to do.

About nine miles this side of Alexandria, well past the stinking tannery, is a small village called Fayid.

We had an airfield there, right on the Med, only the coast road between. Our main war effort was making sailing dinghies to play with out in the bay on our make and mends (afternoons off). Fleet requirement unit they called us, 775 squadron.

And so to Sleep

There was a panic on. The skipper was going barmy. He called Sub-Lt. Thompson in at the double.

"Listen Thompson. Something's up. Jerries are flying Ju 52s across to Benghazi carrying secret loads of I don't know what, but the army's going mad and the Admiral has been on the blower. He wants 'em shot down. Trouble is they're not ordinary Ju 52s, they're Ju 52Ms. The M is for metal. Bloody great lengths of corrugated iron right the way along 'em.

Machine guns are no good, 20mm. cannon shells are deflected back and shoot down or own Seafires - deflected back by the grooves of the corrugated iron. Only one thing to do. We've had a 70mm. gun mounted on a Hurricane and that'll knock a hole in anything. The recoil when the

thing goes off will knock you back a hundred knots, so you must go in at two hundred to avoid stalling.

We know your reputation for missing the target every time Thompson, but this time you mustn't miss. All the other pilots have shot themselves down."

Sub-Lt. Thompson,
Second in command,
Couldn't find the target,
Too much bloody sand.
He dropped all his bombs out in the blue,
Too bloody true, and so would you.
If you had seen Benghazi,
If you had seen B.G.

So off went our hero, out into the blue, flying the Hurricane burdened with the enormous gun.

Approaching Benghazi, he could see the distant speck of the three-engined Ju 52 out over the Med. He could see other flying things as well. Large birds called Shite Hawks, wheeling about the sky, hungry for prey. Peculiar birds. The only ones that fly in herds. Lots of cows and only one big bull. He was so wrapped up in what was before him that he didn't see what was behind. An Italian Macchi 42 was slowly coming up astern.

The Ju 52 came lumbering in over the coast line as our Subby closed in to attack. He could plainly see the corrugated side of the big jerry transport looming large.

Before he could get into the firing position, he saw the transport dropping its secret cargo. Hundreds of cones falling, each with their little parachute. Cornets from the toe of Italy. So that was it. Cornettoes. What a devilish scheme, seeing that allied troops held Benghazi at the moment.

They bomb Benghazi every night,
And when they're not,
They're getting tight.

He fired his mighty gun. Crash it went. Bash came the recoil, and the Hurricane practically stood still. Unfortunately, the Macchi had closed up for the kill and couldn't avoid hitting the Hurricane. Bang, they went.

The impact shot Subby Thompson clean out of his cockpit, and he'd forgotten his parachute. Whizz he went, through the crisp North African air. The big Shite Hawk saw his chance and moved in, grasping Subby firmly in his enormous talons. The 70mm. shell tore into the Ju 52 and down it went. Boom. The tangled mass of the Hurricane and the Macchi spiralled into the sea off the coast. Leaving our hero suspended as usual by Bull Shite.

Footnote to a Previous Epic

Footnote to the saga of Lt-Commander Pragham-Wright who attacked the whole Italian 7th fleet in the Straits of Messina (see July issue).

Nineteen ships were sunk that day by one torpedo. The twentieth ship was rammed by the lone Swordfish, whose pilot was heard to shout just before impact "one more for the pot."

We've had several enquiries, you see.

NEW TELEPART CATALOGUE

The new 152-page Telepart trade catalogue, listing over 5,000 items, is now available from Willow Vale Electronics Ltd., Old Hall Works, Arborfield Road, Shinfield, Reading, Berks. (Telephone: Reading (0734) 884444.)

next month in

TELEVISION

● COLOUR RECEIVER OPTIONS

Most constructors who embarked on the colour receiver project we started a year ago should by now either be receiving pictures on their set or be very close to finishing construction of the basic receiver.

Next month we start on the various options mentioned earlier in the series, starting with the addition of teletext reception facilities. For this purpose the Texas Instruments XM11 teletext decoder module is used, together with a very simple interface board and an inexpensive cable linked keypad. This approach provides the simplest possible solution to the provision of teletext, and the whole thing can be built and working within a matter of hours.

In subsequent issues we will describe how to add remote control to the basic receiver: this will be followed by the ultimate option, the addition of teletext and remote control – the remote control system operating both the receiver controls and the teletext functions. This last option will enable constructors to build a receiver which compares favourably with up-market commercial sets.

● SECAM COLOUR

Following our feature on receiving French TV this month, we thought it would be a good idea to take a look at the way in which the French colour system (SECAM) works. Keith Cummins describes the system, its pros and cons, and reports on his observations of the results off-screen.

● TACKLING MAINS/BATTERY PORTABLES

With their need to be able to operate from a 12V supply as well as the mains, portables present their own problems. A dead set can be a very dead one indeed – no signs of life at all. John Law describes how to tackle this sort of problem, with particular reference to the Thorn 1590/1591 chassis.

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Restricted Brightness Range

George Wilding

RESTRICTED brightness range, i.e. inability to black out the raster fully or, at the other extreme, to obtain peak white, is a common fault in sets of all types, though it's nowadays most often encountered in hybrid colour sets.

The brightness control arrangements used in monochrome sets are straightforward indeed, as the two examples shown in Fig. 1 bring out. Where d.c. coupling is used between the video output stage and the c.r.t. cathode however, as in Fig. 1(a), value change in quite a number of components can be responsible for the fault. The brightness control circuits used in colour sets vary so widely that again the causes of the trouble can be many and various. Assuming however that the c.r.t. first anode voltages are correct – a common cause of the fault on colour sets – the basic cause of the trouble is always the same, restricted or incorrect voltages between the cathode(s) and control grid(s) of the c.r.t. The c.r.t. gun has to be negatively biased of course, i.e. the grid made negative with respect to the cathode, though both electrodes may be at considerable positive voltages with respect to chassis.

As a typical example of d.c. coupling between the anode of the video output pentode and the c.r.t. cathode, Fig. 1(a) shows the circuit used in the Philips 300 chassis – the basic circuit is common to many earlier chassis from this setmaker. The d.c. voltage at the anode of the video output pentode is 142V, while the brightness control enables the c.r.t.'s control grid to be swung between 40-112V. The effective working c.r.t. bias can thus be varied between -30V, when the screen is at peak brightness, and -102V, which is more than ample to black out the raster.

Since a greater number of components affect the c.r.t.'s cathode voltage than its grid voltage in the circuit shown, there are more opportunities for brightness troubles to have their origin here rather than in the grid circuit. The possibilities are: a low-emission output valve; value change in the output pentode's cathode bias resistor, its screen grid feed resistor (if present) or, again if present, its bias stabilising resistor (between the h.t. line or the screen grid and cathode); leakage in the cathode decoupling capacitor; or value change in the anode load resistor.

If a component value change over biases the video output pentode, thus increasing its anode voltage and therefore the tube's cathode voltage (still assuming d.c. coupling), other faults will arise. The sync pulses and the darker picture tones will be amplified on the more curved portion of the valve's characteristic, i.e. towards valve cut-off. As a result, sync pulse amplification will be markedly reduced, often showing up as impaired field sync, while it will be almost impossible to separate the darkest two or three squares of the test card grey scale.

When a transistor is used to provide the video output, similar effects can occur due to an increased value emitter resistor or inadequate base bias. If the latter is provided by a d.c.-coupled emitter-follower driver stage, it may be necessary to check back to the conditions in that stage.

Where a.c. coupling is used between the video output stage and the c.r.t. cathode, as in most mains/battery portables, the d.c. working conditions of the video output stage are divorced (or should be, unless the coupling capacitor is leaky) from the tube's cathode. The most likely cause of the trouble in this case is a fault in the brightness

control circuit. The control is usually connected across the h.t. supply, generally with series resistors between the control and h.t. and the control and chassis to set the range of operation. If a resistor on the h.t. side of the control increases in value, the brightness range will be restricted,

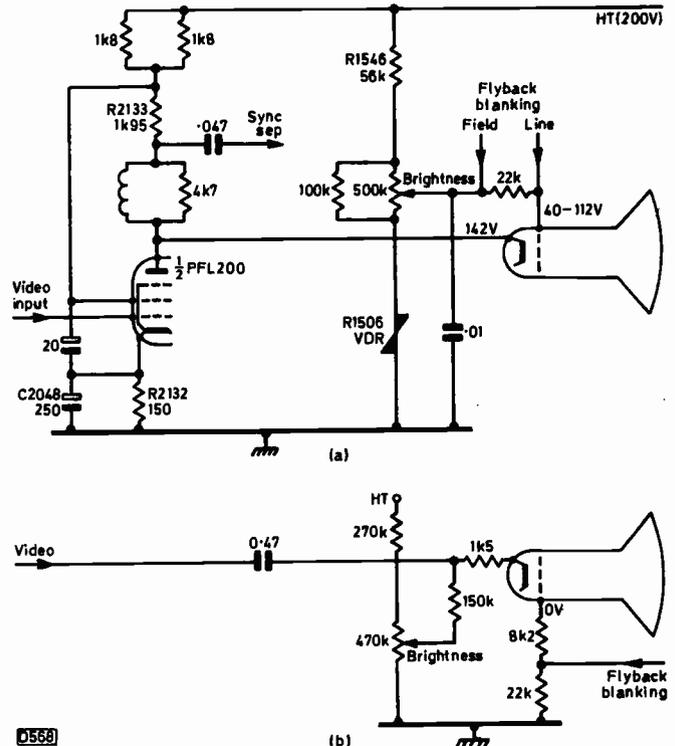


Fig. 1: Contrasting monochrome receiver c.r.t. biasing arrangements. (a) D.C. coupling between the anode of the video output pentode and the c.r.t. cathode, with the brightness control setting the tube's grid voltage. This particular circuit is based on that used in many Philips monochrome receivers. With d.c. coupling, changes in the d.c. conditions in the video output stage will directly affect the tube biasing. Thus changes in the value of quite a number of components, or a low-emission output pentode, will affect the brightness. The VDR R1506 is included to provide switch-off spot protection. When the voltage across a VDR falls, its resistance increases. The effect here is to hold the grid positive with respect to the cathode on switching the set off, thus rapidly discharging the e.h.t. and preventing the appearance of a switch-off spot. (b) A.C. coupling between the output valve/transistor and the cathode of the c.r.t., with the brightness control setting the d.c. voltage at the c.r.t. cathode and the grid returned to chassis. Component values as used in the Thorn 1500 chassis. Provided the coupling capacitor is not leaky, there's little to cause brightness troubles in this type of circuit. The usual cause of such trouble here is change of value of a resistor in series with the brightness control. This type of circuit is very common in transistor portables. Where the resistor between the h.t. rail and the brightness control increases in value, the brightness will increase – because the c.r.t.'s cathode voltage will be reduced. On some monochrome sets with a.c. coupling the brightness control is included in the c.r.t.'s grid circuit, a fixed potential divider being used to set the c.r.t.'s cathode voltage. Obviously a changed value resistor in the potential divider network will alter the brightness level.

while if a resistor on the chassis side increases in value it may become impossible to black out the screen — assuming that the brightness control is in the c.r.t.'s grid circuit.

Fig. 1(b) shows the brightness control arrangement used, with a.c. video coupling, in the Thorn 1500 chassis. In this example the control grid is taken to chassis and is thus at 0V d.c., serving simply as a suitable point at which to apply the negative-going flyback blanking pulses. The brightness control sets the positive d.c. voltage at the cathode — range from 0 to about 90V. This is equivalent to varying the control grid between 0 and -90V of course.

If in doubt as to whether advancing the setting of the brightness control reduces the tube bias sufficiently, a simple test is to momentarily short the grid and cathode together. This should not significantly increase the brightness of the raster with the brightness control well advanced. If it does, either the c.r.t.'s cathode voltage is too high or its grid voltage too low.

On occasion, you might find that as the brightness control is advanced to increase the c.r.t. grid voltage, so the cathode voltage tends to follow suit. This is a sure indication of grid-cathode leakage in the tube. It can sometimes be cured by flashing techniques, but usually means that a replacement tube will be needed.

Hybrid Colour Sets

When we come to hybrid colour sets using colour-difference drive, we find a very similar situation to monochrome receivers using d.c. coupling. The luminance output pentode is d.c. coupled to the three c.r.t. cathodes, and all the considerations of changed value screen grid and cathode resistors etc. still apply. In addition however it will be found that brightness control is effected by varying the output pentode's negative control grid bias, while this bias may also be affected by the action of the beam limiter circuit. When operating correctly, excessive e.h.t. current will result in the beam limiter increasing the bias on the luminance output pentode. A fault in the beam limiter circuit may change the bias in either direction however. In total therefore many components could be responsible if you find that the luminance output pentode's anode voltage cannot be swung between the normal limits.

An interesting example of such a fault came our way recently, the set being an Ekco one fitted with the Pye hybrid chassis. Although the tube was undoubtedly of low emission, appraisal of the test card showed that all three darkest sections of the grey scale were at about the same darkness level, and couldn't be separated by juggling with the contrast and brightness controls. Probably the most common cause of excessive luminance output pentode anode voltage (lack of brightness) and thus high tube cathode voltage is a low-emission PL802 luminance output valve. A replacement brought no improvement this time however. The beam limiter threshold control RV16 was found to have no effect, while the tube's first anode preset controls were as near maximum as possible consistent with obtaining a relatively untinted raster.

The brightness control circuit used in this chassis is shown in Fig. 2. It acts in conjunction with the d.c. restorer diode D39 which conducts on the tips of the negative-going sync pulse tips. When this happens, C39 is charged to the voltage at the slider of the brightness control, which is connected between 20V and -20V rails via R213, R212 and R202. The brightness control thus sets the d.c. level at the control grid of the PL802 luminance output valve, providing a smooth transition from minimum to maximum brightness. It also provides a means for the beam limiter to act — when the beam limiter transistor VT35 conducts, at

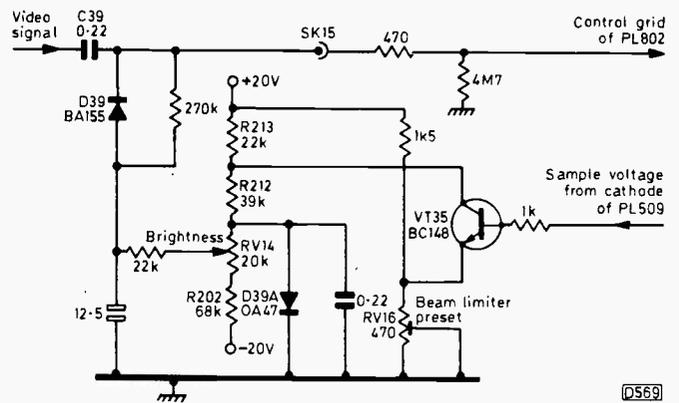


Fig. 2: Brightness control circuit used in Pye hybrid colour receivers. The d.c. restorer diode D39 conducts on the tips of the negative-going sync pulses, returning the coupling capacitor C39 to the d.c. voltage set by the brightness control. The beam limiter also acts on this circuit. With excessive beam current, the line output valve's cathode voltage increases and the beam limiter transistor VT35 switches on. Its collector current, flowing through R213, alters the voltages along the resistive chain R213/R212/RV14/R202. The voltage at the slider of the brightness control is thus pulled back, and the beam current reduced to a safe level.

maximum beam current, the voltage at the junction of R212/R213 is reduced.

Withdrawing the small white plug from socket 15 on the colour-difference amplifier panel removes both the luminance signal feed and the control bias from the control grid of the PL802. When this was done, with the brightness control at maximum, there was an immediate and most pronounced increase in brightness level. Clearly then the brightness control was failing to reduce the bias on the PL802 sufficiently, and on making voltage checks along the resistor network R213, R212 etc. R212 was found to be open-circuit. Replacing R212 also restored normal beam limiter action.

Restricted brightness control range on hybrid colour sets using colour-difference tube drive can also of course be caused by incorrect tube control grid voltages. The colour-difference signals are a.c. coupled to the grids, with clamps to establish the correct d.c. conditions. These are usually driven by line-frequency pulses, so absence of the pulses will remove the clamp action. This is quite rare however: more common is drift or variation in the d.c. level from one gun to another due to a component value change. With the Pye hybrid chassis however the tube will be completely or almost completely biased off should either R389 or R393 on the CDA panel go open-circuit. The effect of this is to remove the clamp voltage, so that the voltages at the anodes of the clamp triodes fall to a very low figure instead of the correct 100V or so.

The diversity of brightness control arrangements used in receivers using RGB drive is such that we can't go into them here. Fortunately they don't in practice give much trouble.

Preset Controls

Often the trouble is simply an incorrectly adjusted preset control. Preset brightness controls are to be found in sets of all types, and operate in a variety of ways. In the GEC hybrid chassis there's a background control which sets the colour-difference signal clamping level. In addition you'll often find in a colour set a beam limiter threshold control. It's vital that all controls that affect the brightness level of the picture are correctly set up. This is especially so when the tube is ageing, since wrongly adjusted presets accentuate the effects of low tube emission. ■

New Teletext Signal Panel

Alan Kitching

SOMETIME ago I built up the original version of the *Television* teletext decoder. I found however that under certain signal conditions an unusually high number of errors was present on the display. These could usually be eliminated by adjusting the slice level, the tuning and the clock frequency slightly, but the main difficulty seemed to lie in the critical nature of the data recovery section used in the original design. To overcome this problem, a new signal panel was designed. This uses the original i.f. strip along with a new adaptive data recovery section which is able to cope with quite large variations in signal strength and noise levels. Improvements were also made to the i.f. strip earthing arrangements, to overcome certain problems with the original.

The circuit of the new section of the board is shown in Fig. 1. The video input is taken from the positive-going video output of the TDA440 i.c. (pin 12). The new section also includes a 6MHz sound preamplifier as some problems were experienced in the original design at low sound modulation levels.

Buffer Stage

The positive-going video output from pin 12 (which was left disconnected in the original design) of the TDA440, at about 3V peak-to-peak, is a.c. coupled to the base of the emitter-follower Tr1. This provides a low-impedance source to drive the sync and data separator circuits. A parallel tuned

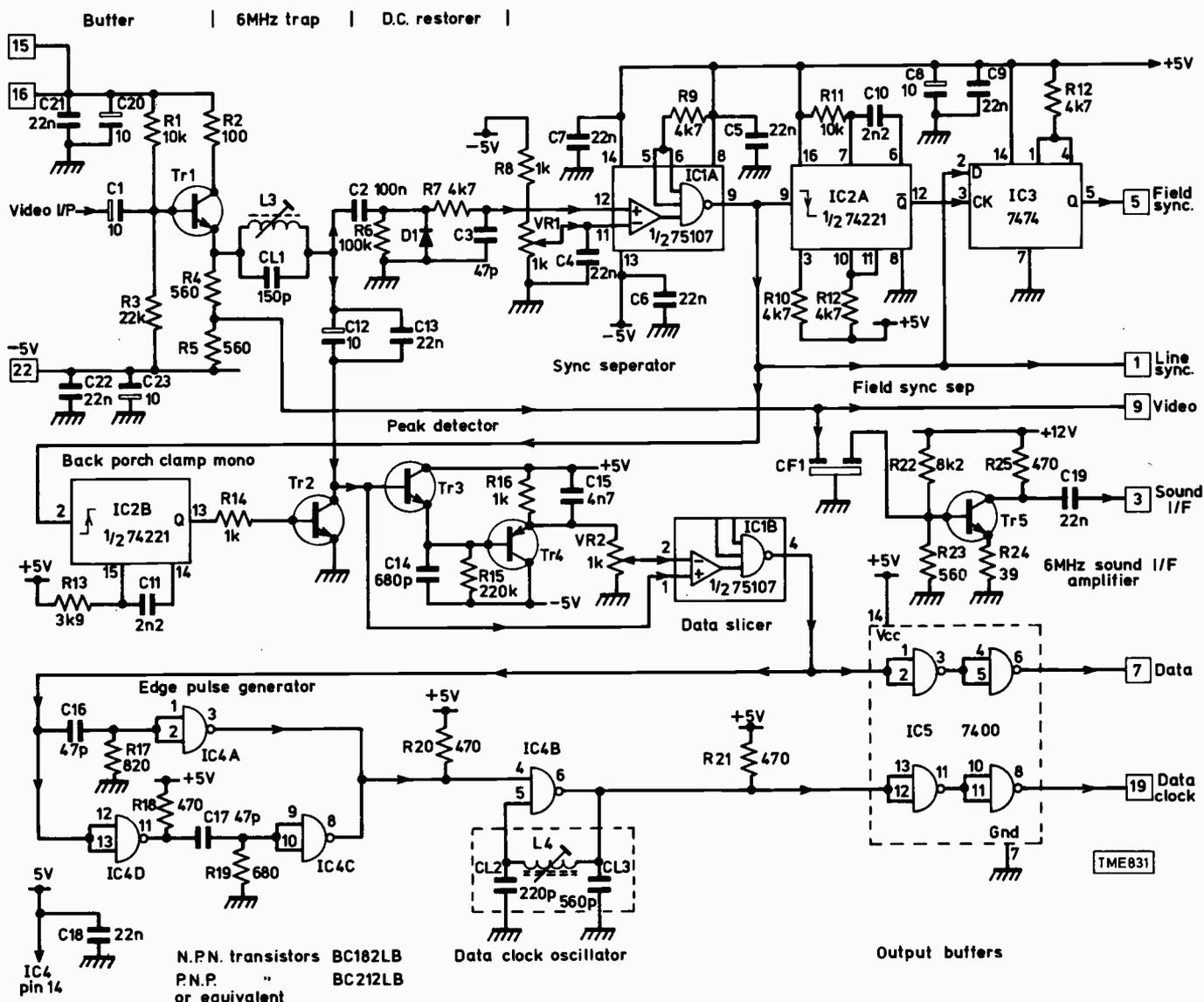


Fig. 1: Circuit diagram of the revised data recovery section. The i.f. section remains unchanged. R12 shown twice in error.

circuit (L3/CL1) removes the 6MHz intercarrier sound signal, which would otherwise upset the operation of the data clock – this is very close to 6MHz.

Tr1 has a split emitter-load resistor (R4/R5), so that a high-amplitude video signal is available to drive the sync and data separators and a low-amplitude video output is available to drive the modulator and the sound i.f. preamplifier Tr5. This split emitter load also provides isolation between the external circuit connected to the video output edge connector pin 9 and the internal data separation circuitry, thus reducing the number of errors caused by locally generated interference.

Sync Separator

We will deal first with the sync separator section of the circuit. The composite video at the emitter of Tr1 is a.c. coupled via C2, with D1 providing d.c. restoration, clamping the sync pulses at about $-0.6V$. R7 and C3 form an h.f. filter, removing the chroma information and the remaining video signal from the feed to the positive input (pin 12) of the comparator IC1a. The negative input (pin 11) of the comparator is connected to a voltage between $-5V$ and $0V$: this sets the level at which the composite video is sliced. The level is set to approximately half-way through the sync pulse portion of the waveform. TTL mixed sync appears at the output pin 9.

The negative-going leading edges of the sync pulses trigger the monostable IC2a, which switches state for $18\mu\text{sec}$. The Q output then returns to logic 1. This rising edge clocks the D-type flip-flop IC3, the Q output of which takes up the state of the D input which, during the field sync period, is at logic 0. We thus have negative-going field sync pulses at the Q output of IC3. These are taken out to edge connector pin 5, while the line sync pulses are brought out to pin 1, maintaining compatibility with the original board.

Adaptive Data Slicer

Turning now to the data separation section of the circuit, the positive-going trailing edges of the sync pulses trigger monostable IC2b. This produces a short, positive-going pulse of about $2\mu\text{sec}$ duration during the back porch period. The pulse switches Tr2 on, clamping the black level of the video signal, which is a.c. coupled via C12/C13, at approximately $0V$ regardless of the average level of the signal. The slice level is set by using a peak detector to detect the data amplitude. The resultant information is used to set the slice level midway between the positive data peaks and black level. Let's see how this operates.

Tr3 and C14 form the positive data peak-detection circuit, with R15 providing the time-constant to set the decay time. The time-constant is fairly long compared to the data bytes, to prevent too much decay during the worst-case condition of fourteen consecutive zeros. Tr4 offsets the base-emitter voltage drop of Tr3, while the shorter time-constant of C15, R16 increases the rise time of the peak-detector circuit to reduce the effect of large noise spikes.

The slice level can be adjusted by means of VR2 over the range from $0V$ to the positive data-peak level. The voltage from the slider of VR2 is applied to the negative input (pin 2) of the second comparator IC1b, the video signal being fed directly to its positive input (pin 1). The output, at pin 4, is a TTL signal representing the sliced serial data. This is buffered by half the 7400 i.c. IC5.

Data Clock

The serial data from pin 4 of the data slicer i.c. is also fed to the clock generator section. The differentiating network C16, R17 produces a positive-going output to turn on gate IC4a, forcing its output to the low state coincident with the positive-going edge of the data bits. IC4d inverts the serial

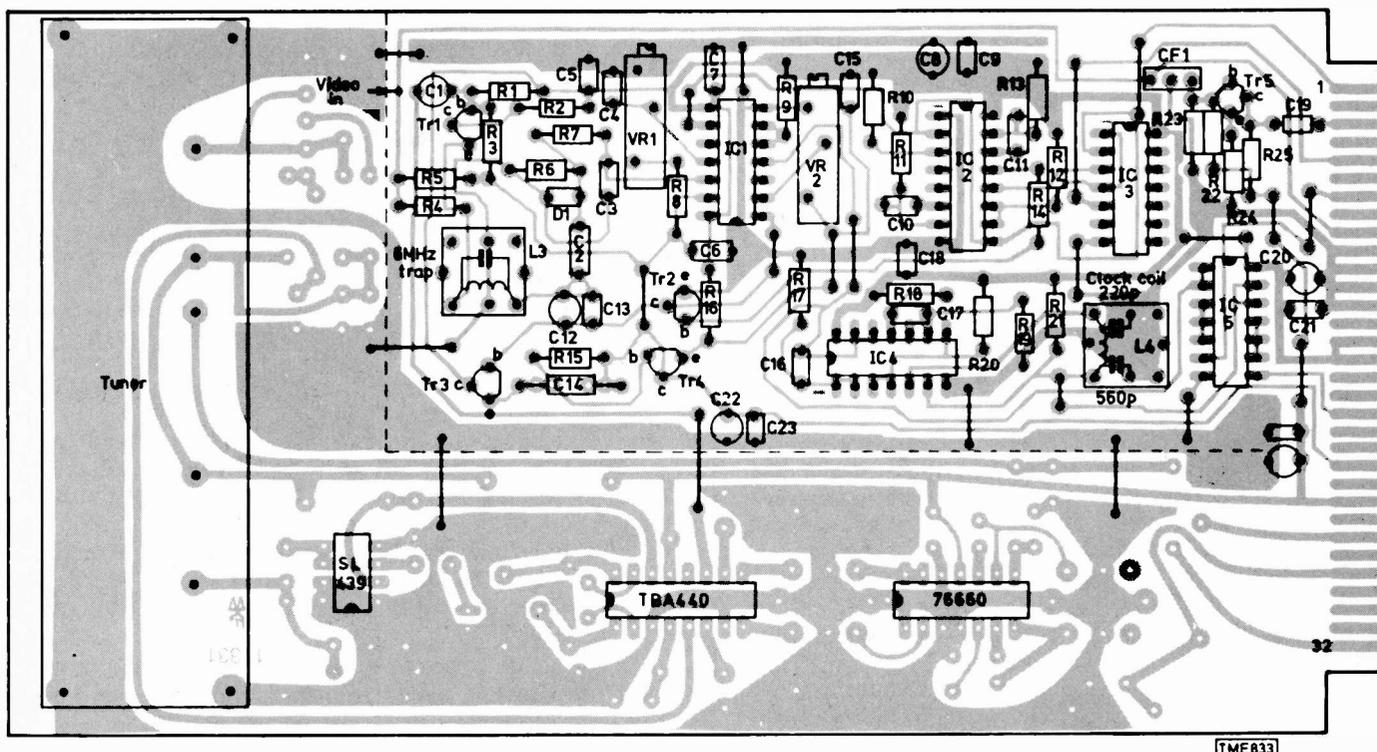


Fig. 2: Component location diagram of the new signal board. The component location diagram for the i.f. section is given in the October 1977 issue.

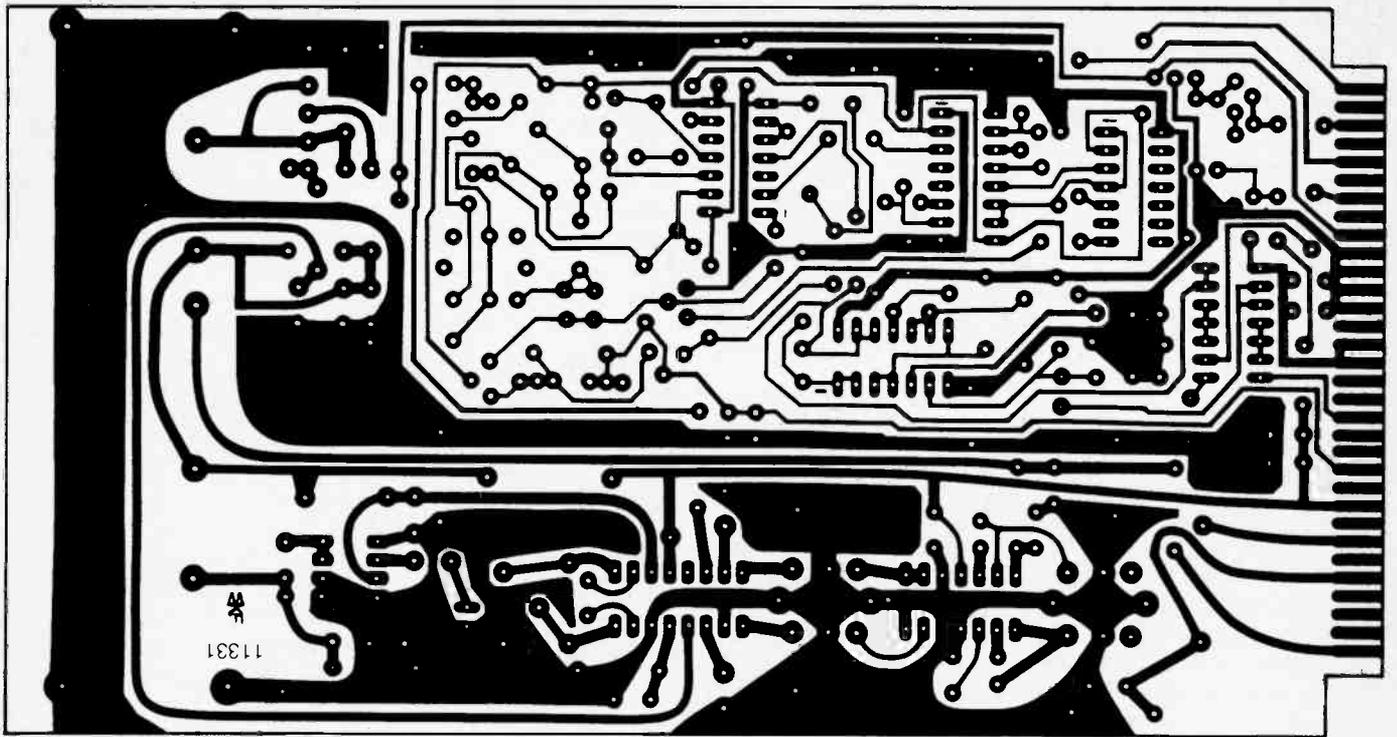


Fig. 3: Copper pattern of the new signal board. The board is available from our Readers PCB Services, reference 11331. Note that the actual size of the board is 386mm x 205mm.

★ components list
(new data recovery section only)

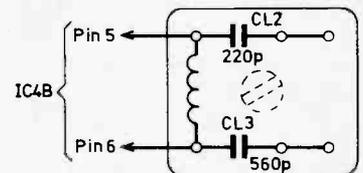
Resistors:

R1	10k
R2	100Ω
R3	22k
R4	560Ω
R5	560Ω
R6	100k
R7	4k7
R8	1k
R9	4k7
R10	4k7
R11	10k
R12	4k7
R13	3k9
R14	1k
R15	220k
R16	1k
R17	820Ω
R18	470Ω
R19	680Ω
R20	470Ω
R21	470Ω
R22	8k2
R23	560Ω
R24	39Ω
R25	470Ω
All ¼W 5% carbon film	
VR1	1k
VR2	1k
½in. cermet multiterm	
Semiconductors:	
IC1	75107
IC2	74221
IC3	7474
IC4	7403
IC5	7400
D1	1N4148
Tr1	BC182L
Tr2	BC182L

Capacitors:

C1	10μF 25V
C2	100n
C3	47p
C4	22n
C5	22n
C6	22n
C7	22n
C8	10μF 10V
C9	22n
C10	2n2
C11	2n2
C12	10μF 10V
C13	22n
C14	680p
C15	4n7
C16	47p
C17	47p
C18	22n
C19	22n
C20	10μF 10V
C21	22n
C22	22n
C23	10μF 10V
CL1	150p polystyrene
CL2	220p polystyrene
CL3	560p polystyrene
All electrolytics tantalum bead.	
All capacitors not otherwise specified ceramic plate.	
Tr3	BC182L
Tr4	BC212L
Tr5	BC182L
Coils etc:	
L3	25 turns
L4	30 turns
both 36swg, ecw on 4mm formers with cores and screens.	
CF1	SFE6.0MB Murata

Fig. 4: Constructional details of coil L4.



data and drives another differentiating network C17, R19. This, with IC4c, operates in the same way as IC4a/C16/R17, producing a short negative-going pulse coincident with the negative-going edge of the data bits. The outputs from IC4a and IC4c are connected in the wired-or mode, with R20 forming a common load resistor. Consequently a series of short, negative-going pulses coincident with the positive- and negative-going data transitions is fed into one input of the data clock oscillator formed by IC4b with L4 and the associated tuning capacitors. The pulses serve to lock the oscillator in the correct phase and frequency as the incoming data. The free-running frequency of the oscillator is set by the core in L4 to the data clock frequency (6.9MHz).

The data clock output is buffered by half the 7400 i.c. IC5 and is then brought out to edge connector pin 19.

Construction

If the new signals board is to be constructed using components from the original board, these can be transferred on a one-to-one basis – the component layout is identical. If the circuit is to be built from scratch however the constructional details given in the October 1977 issue should be followed and alignment carried out as described in the November 1977 issue.

Construction of the new section of the board is straightforward, following the component layout shown in Fig. 2. The only component requiring any special consideration is the clock coil L4, which differs slightly from the original. It can be wound on the same former however after removing the old winding (see details in components list). Take care to

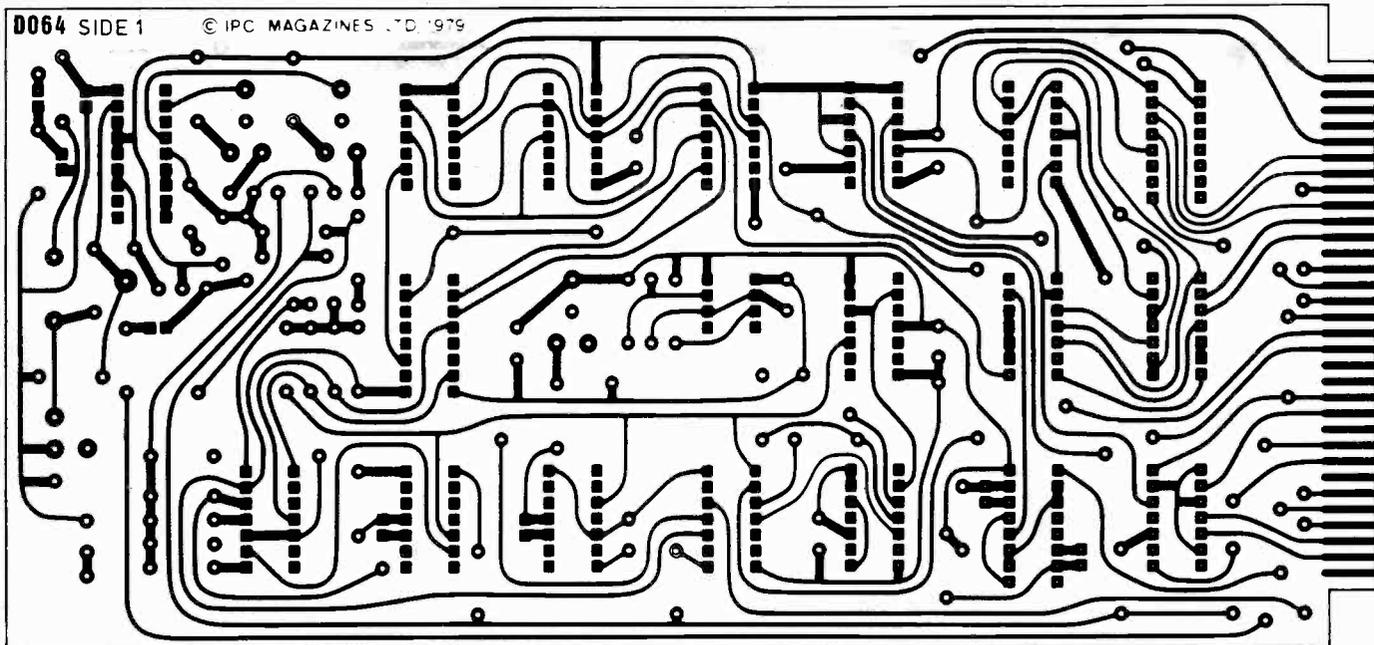


Fig. 5: Underside copper pattern for the teletext options card (see last month), ref. D064.

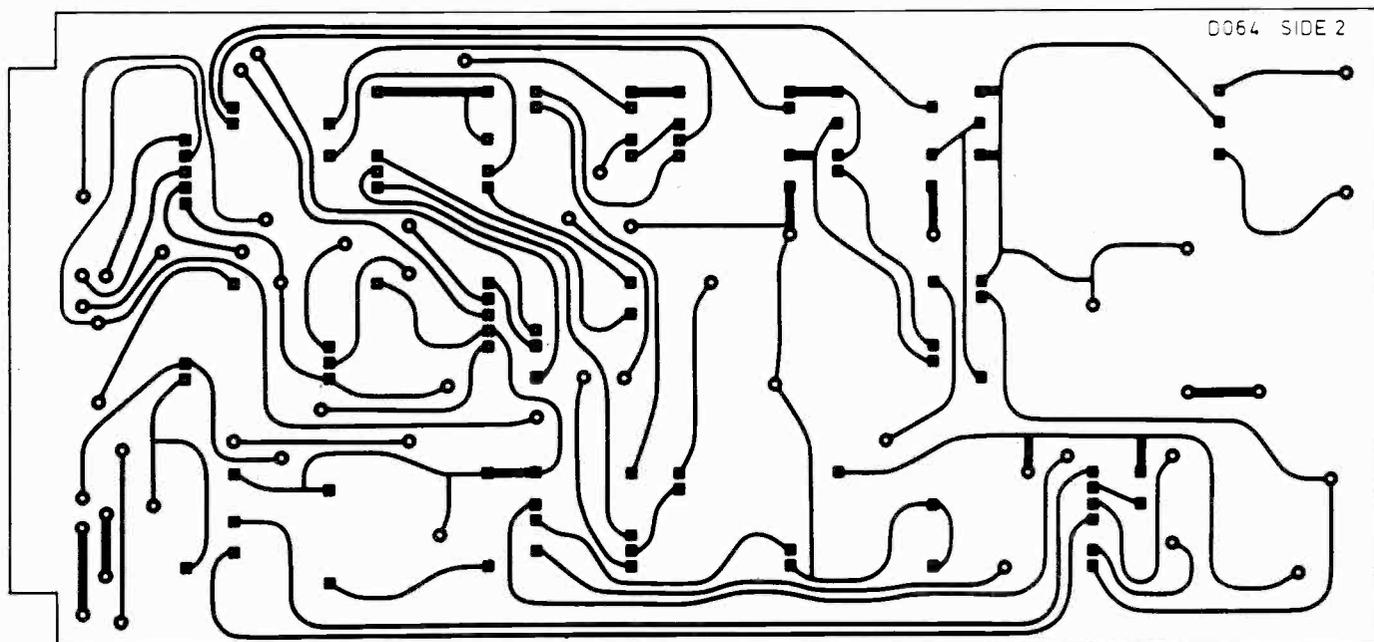


Fig. 6: Topside copper track of the options card D064. Note that the actual board size is 438mm x 205mm.

connect the decoupling electrolytics on the negative supply rail the correct way round, i.e. positive to chassis.

Alignment

Assuming that the alignment and the 6MHz sound trap have been set up in accordance with the instructions given in the November 1977 issue, and that a good picture which includes a teletext transmission is being received, the new data recovery section should be set up as follows. Switch to the text mode and connect a scope to pin 9 of IC1a. Adjust VR1 to produce TTL composite sync at this point. Check that TTL field sync pulses are present at pin 5 of IC3: if not, check the timing components and connections around IC2a and IC3.

Select the page roll mode and whilst watching the screen adjust VR2 for the most rapidly changing display of characters. When this point has been reached, adjust L2

slowly until the text is as free of errors as possible and complete pages are seen to roll through. Repeat these last two steps if necessary.

Finally switch off page roll and select the clock-cracker page. Adjust L4 a quarter of a turn at a time until complete pages of error-free text are produced. Check on all the other channels. ■

MONOCHROME MONITOR CONVERSION

One of the fundamental requirements for a monitor is that it is isolated from the mains. We neglected to mention this point in our article last month, and it's important that constructors incorporate a mains isolating transformer adequately rated for the set being converted. A suitable transformer is the RS Components type 207-469 which is rated at 500VA. Where the power consumption does not exceed about 150W, the 200VA type 207-021 can be used.

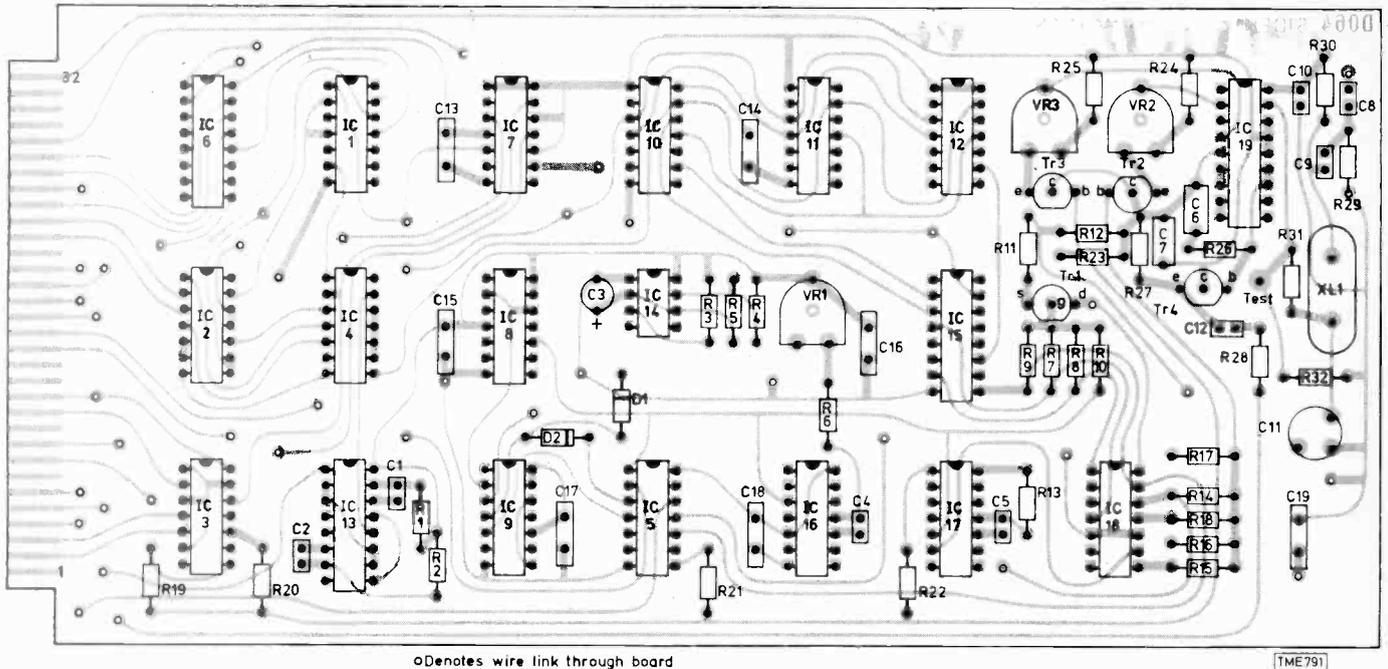
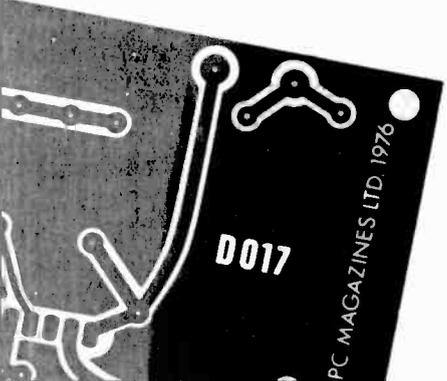


Fig. 7: Component location diagram for the options board.



All boards are epoxy glassfibre and are supplied ready drilled and roller-tinned.
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<p>Issue November 1976 December 1976 March 1977 May 1977 May 1977 June 1977 June 1977 July/Aug 1977 August 1977 September 1977 September 1977 October 1977 Feb/March 1978 April/May 1978 May/June 1978 Aug/Sept 1978 October 1978 January 1979 February 1979 March 1979 July 1979 September 1979 August 1979 August 1979 September 1979</p>	<p>Project Ultrasonic Remote Control IC Sound Circuits for the Constructor Teletext Decoder Power Supply Teletext Decoder Input Logic Single-chip SPG Wideband Signal Injector Teletext Decoder Memory Teletext Decoder Display Logic State Checker Teletext Decoder Switch Board Teletext Decoder Mother Board Teletext Decoder IF Board On-Screen Clock CRT Rejuvenator Test-Pattern Generator Diagnostic Pattern Generator Colour Receiver PSU Board Colour Receiver Signals Board Commander-8 Remote Control System Colour Receiver Timebase Board Colour Pattern Generator Teletext Decoder Options Board Teletext Decoder New Mother Board Simple Sync Pulse Generator New Teletext Signal Panel</p>	<p>Ref. no. D007/D008 D009 D017 D022 D011 D030 D031 D012 D013 D038 D021 D027 D041 D045 D046 D048 D051 D052 D053 D054/S D049 D062 D063 D064 D065 D067 11331</p>	<p>Price £3.24 per set £1.44 £1.44 £3.24 £10.53 £3.30 £0.79 £8.51 £8.62 £1.70 £1.43 £4.36 £6.50 £7.03 £2.76 £9.15 £8.62 £3.83 £10.75 £5.43 per set £17.13 £13.50 £9.15 £8.50 £5.00 £4.00 £8.00</p>
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Servicing Pye Solid-State Colour Receivers

The 713, 715, 717, 725, 731, 735, 737 and 741 Chassis

Part 1

Mike Phelan

THIS series of articles will cover all the Pye solid-state colour chassis produced up to, but excluding, those sets using the G11 chassis. First we shall deal with the large-screen models. The 18 and 20in. sets used a chassis with certain similarities but a completely different layout: these (the 713, 715 and 717) will be discussed later.

Chassis Numbering

Now to sort out the confusing mixture of chassis numbers. The original was the 731 chassis, using a 26in. tube and an SN76544 combined line and field oscillator i.c. To make the sets VCR compatible, the i.c. was altered to a TBA920 with the field oscillator redesigned using discrete components: the chassis number became 737. Putting the tuning controls in a drawer separate from the push-buttons changed the number to 735! Later models using an A66-410X quick-heat tube had their chassis designated 741; and a "pruned" version fitted with a 20 or 22in. 90° tube was numbered 725.

Despite this complicated system of numbering, most of the panels are interchangeable; the exceptions of course are the line timebase and convergence panels, which differ for 90° and 110° models; the field timebase panel (which can be changed if three components are altered); the c.r.t. base panel; and finally power supplies coded 4A4 cannot be changed for different types.

Accessibility and Layout

Accessibility is quite good, most of the panels being held in three vertical plastic frames which slide on runners, two on the left of the c.r.t. looking from the back and one on the right. The latter holds the convergence, power supply and field timebase panels; for access, lift the plastic latch at the bottom rear corner, draw the panel to the rear until it clicks, then swing it out and lock it in position with the plastic peg at the top. In this position, the convergence controls are accessible from the front of the set. For greater access push the panel, while it's still at an angle, back into the cabinet to free it from the runners. The top runner can be freed from its guide with a strong pull, allowing the panel to be laid on its back.

The extreme left-hand frame carries the chroma panel (top) and a bottom panel containing the tuner, i.f. module, vision detector and sound stages. This frame can be pulled along its runners after the top and bottom latches have been released. When in the nearest position, the panels swing out to the left. The frame on the left nearest the c.r.t. contains one large board with the line timebase and raster correction circuitry on it, and is attached to the cabinet in the same way as the right hand frame – it's necessary to swing out the chroma/i.f. panel however before removing or turning the line timebase. The plastic moulding on the large i.f. can is to prevent shorts to the line timebase print when

both panels are out, but beware of the i.f. panel shorting against a metal aerial plug (I found this out the hard way!).

Power Supply Circuit

Starting with the power supply, a blown mains fuse will in most cases mean either that the mains rectifier thyristor D888 is short-circuit or that the mains filter capacitor C915 (0.22 μ F) is short-circuit. If C915 has shorted it will usually have blown one of its ends off. It should be replaced by a component rated at 1kV working. Early power supplies used a 16472 thyristor, later ones a 2N4444 or BT106. Beware of devices coded TV106 – an OT112 seems to be about the most reliable replacement.

The thyristor can suffer from leakage as an alternative to going completely short-circuit: this causes the h.t. flutter familiar to most of us (though this symptom can have other causes as well). First try setting up the h.t. Adjust RV916 (h.t. fine) to mid-position, and RV917 (h.t. coarse) fully anti-clockwise. With the meter on the dropper tag marked "185V", adjust RV917 for 195V, then adjust RV879 (overvolts) until the picture *just* starts to pulsate. Finally adjust RV917 for 185V.

Another cause of h.t. flutter is a faulty diac, particularly if of the black plastic D3202Y type. A BR100 is a suitable replacement, but in an emergency reversing the diac sometimes works. Often this device will go open-circuit, sometimes intermittently, but an intermittent diac can usually be persuaded to give up the ghost altogether when sprayed with freezer.

Early panels had a diac/thyristor arrangement for overvoltage protection: this was later altered to a more conventional circuit using a transistor – similar to that in the Philips G8 chassis. As mentioned before, the earlier and later panels are interchangeable – unless the board is a very early one coded 4A4.

A fairly common fault on this set, as in the G8 chassis, is a dry-joint on the mains filter choke L909. Those of us used to the G8 may think that a quick clean-up and re-solder will get the set going again within minutes. But no – the beast will usually be found to be very dead on switching on again. The reason is that the tag on the choke burns quite a hole in the print before the receiver packs up altogether, and the heat produced destroys D884 (7.5V zener) in the overvoltage circuit.

Measuring the voltages on the diac can be revealing in cases where a.c. is reaching the thyristor but nothing is coming out. First however make sure nothing is on the cathode: a very low a.c. reading means that the power supply is working but R978 (3.3 Ω) is open-circuit. Confusing, but quite logical – if the thyristor's cathode is not connected to the rest of the set, it will follow the gate via R885, and the gating pulse must be between gate and cathode.

Back to the diac: there should be 11.5V positive on one

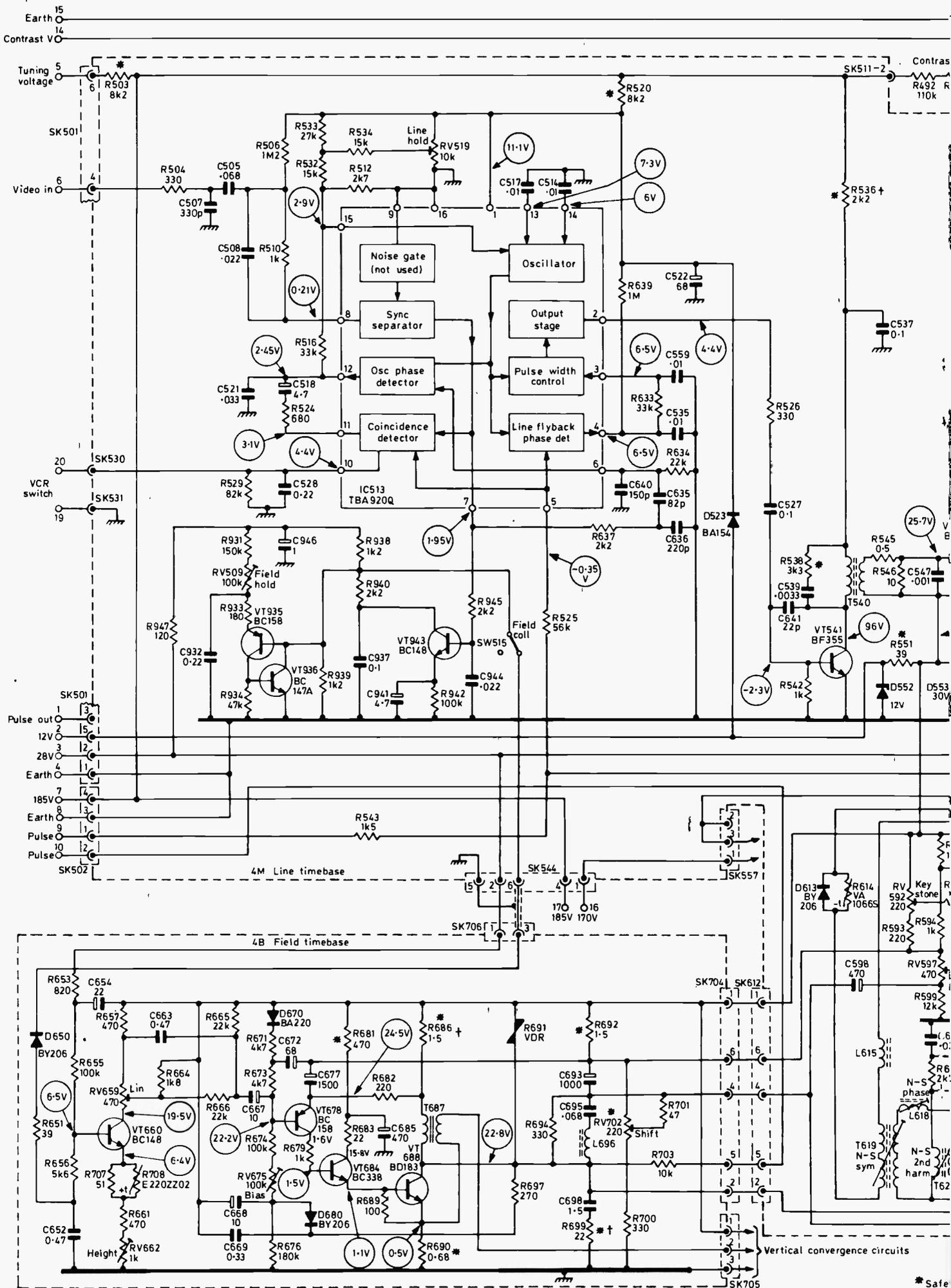
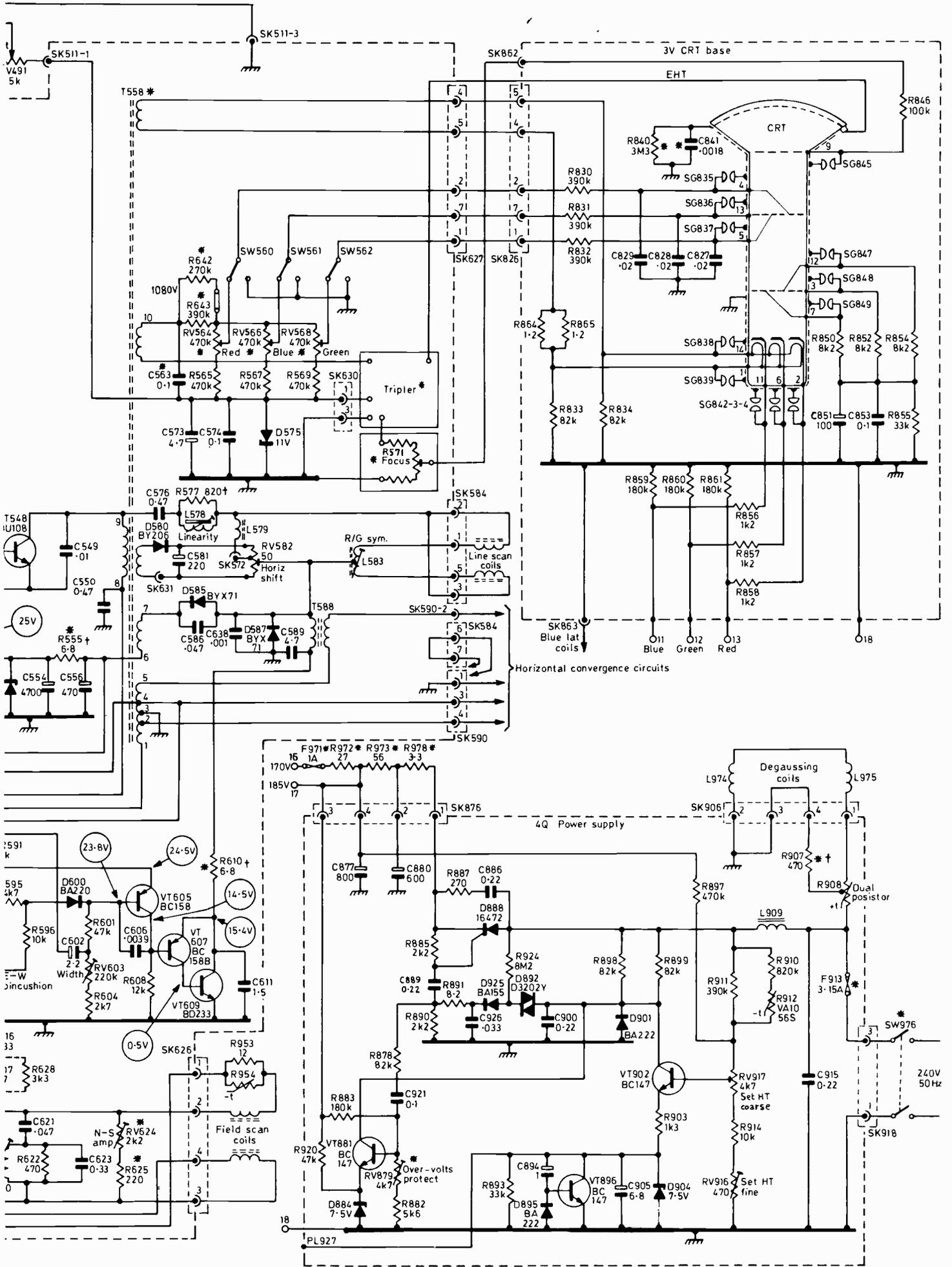


Fig. 1: The timebase, c.r.t. and power supply circuitry used in the 737 chassis. In earlier versions a gating pulse at pin 3 of SK501 is obtained



† component to be replaced only by same type or manufacturers approved alternative. † Fusible

connected from pin 2 of the line output transformer, via an 18kΩ resistor (R632), and is used for a.g.c. gating in the TCA270Q i.c. in the i.f. strip.

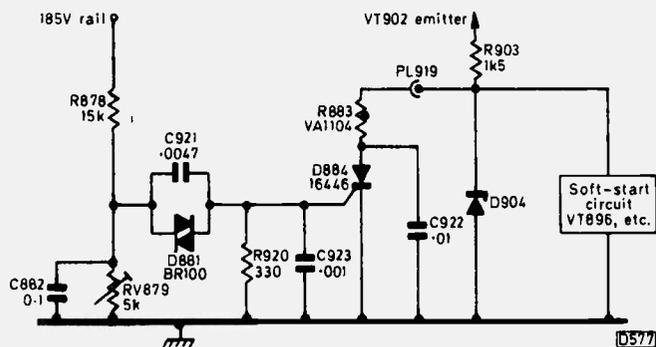


Fig. 2: The over-voltage protection circuit used in early models. On very early versions, PL919 is taken to the cathode of the mains rectifier thyristor: this gives a crowbar action, blowing the mains fuse in the event of excessive h.t. voltage.

side and 8V negative on the other – no positive voltage means either a fault in the overvoltage protection circuit or D901 (BA222) short-circuit; a very low voltage means VT896 (BC147), VT902 (BC147) or D904 (7.5V zener) short-circuit, or possibly C905 defective (can result in a very low h.t. rail if leaky). VT881 and VT896 can be temporarily removed just to check, but remove the h.t. fuse first (situated bottom centre). Lack of negative voltage normally means a defective diac.

Up to now the dropper has behaved itself, apart from the aforementioned R978, which may either be part of the dropper or a separate resistor mounted above. If of the latter type, the correct replacement must be used otherwise mysterious hum bars may be produced. Dry-joints on C880 and C877 (h.t. reservoir/smoothing) can also be the cause of hum bars. As yet we haven't had to replace either of these capacitors, but sooner or later they will begin drying up to cause low h.t.

R911 can change value to cause low h.t. As with other solid-state chassis, it's advisable to check that the h.t. is correctly adjusted whenever one of these sets is serviced.

The Line Timebase

The line timebase is fairly conventional, using a BU108 output transistor. A feature to note is the method of deriving the boost voltage for the tube first anodes. The e.h.t. tripler contains the now usual clipper diode to remove the rings on the input pulse and improve the e.h.t. regulation. If the overwinding is not connected to anything else d.c.-wise, it assumes a potential of about 1kV above chassis. The "bottom" end is decoupled by C563 (0.1 μ F), and supplies the first anodes. C563 in fact is the bête noire of this chassis. When it goes short-circuit it gives the symptoms of a faulty tripler – disconnect the tripler, and the line timebase starts up. Later sets use an 0.22 μ F, 1.25kV working capacitor. If the set is left on in this condition, the demise of the tripler, sometimes followed by the BU108 and the line output transformer, can result before the h.t. fuse blows. Where the h.t. fuse F971 has blown, C563 should be the first check therefore. C563 should also be checked whenever the tripler fails.

The 90° and 110° transformers are not interchangeable, the 90° one having more tags. Also, later replacement transformers from the manufacturer have the shift winding incorporated in the primary bobbin instead of being wound externally on to the core: a slight modification is needed on fitting, but full details are supplied with each transformer – a 2.7 Ω resistor is required in series with the cathode of D580.

The next most common fault must be failure of C514, the line oscillator timing capacitor (with the TBA920 i.c.). The

result is a dead set, which often springs to life if any voltage measurements are taken round the line driver stage, leaving doubt as to the cause of the fault. If the set manages to stay off, it will be found that the collector of the driver transistor VT541 is at h.t., with no negative voltage at its base. Another prod with the AVO shows that the voltage at pin 2 of the TBA920 is approximately correct – so we jump to the wrong conclusion and replace the BF355. After this disturbance the set may work, but sooner or later will fail again when C514 goes open-circuit and the line oscillator tries to run at about 3MHz. Replace with a polyester – not ceramic – type. Twice we have replaced C514 and the fault recurred a few weeks later due to the driver transistor developing an open-circuit base-emitter junction. The policy therefore is to replace both components at the same time.

C586 in the EW modulator circuit can be responsible for lack of width. Again a polyester type must be used. The focus unit can go up in smoke, but that's an obvious one.

The c.r.t. first anode preset controls used in these sets are prone to alteration in value, giving changes in grey scale. The series resistors R565, R567 and R569 (470k Ω) are also suspect for this. What seems to happen is that the presets fall in value while the series resistors go high, until a situation is reached where it is impossible to turn the presets down sufficiently. Sometimes it's necessary to replace R642 (270k Ω) and R643 (390k Ω) which feed the first anode potentiometers from the boost rail. They tend to go high resistance, causing a dark picture, though they can also fall in value, giving excessive brightness. The grey-scale setting up procedure will be given later, as it's necessary to adjust the d.c. levels on the decoder first.

The rest of the line timebase has proved quite reliable. One fault we've encountered once or twice on the 110° chassis has been intermittent droop at the top of the raster, caused by a bad spot on the track of RV624 (NS amplitude). The early 110° panel with the SN76544 has the latter and its associated components mounted on a small subpanel.

The Field Timebase

The field timebase uses a single-ended class A output stage with choke loading, similar to the Thorn 3500 chassis. The field oscillator, except on the early 731 chassis which uses part of the SN76544 for the purpose, employs a complementary pair of transistors on the line timebase panel. These are connected as a silicon controlled switch which gives an output consisting of negative-going pulses that forward bias D650 to produce the flyback. This discharges the field charging capacitor C652, which during the forward scan charges from the unstabilised 28V rail via R653, R655 and R656. VT660 amplifies the waveform produced by C652, its gain being variable for control of height by varying the emitter resistor's value. VT660's collector waveform is integrated by C663 and R665, R664, R666 and the linearity control RV659. The remainder of the timebase consists of three d.c.-coupled transistors, VT678, VT684 and VT688, the latter being mounted on a large heatsink. The choke load T687 is actually a transformer, but the secondary supplies a convergence waveform only.

This panel seems to be reasonably reliable, most cases of intermittent field collapse being due to faulty plugs and sockets – either SK704 near the output choke, or one of the plugs at the top of the line timebase. Attention should be directed to these when the field timebase has been proved working – either by a measurable a.c. voltage on the output transistor's collector or an audible buzz from T687.

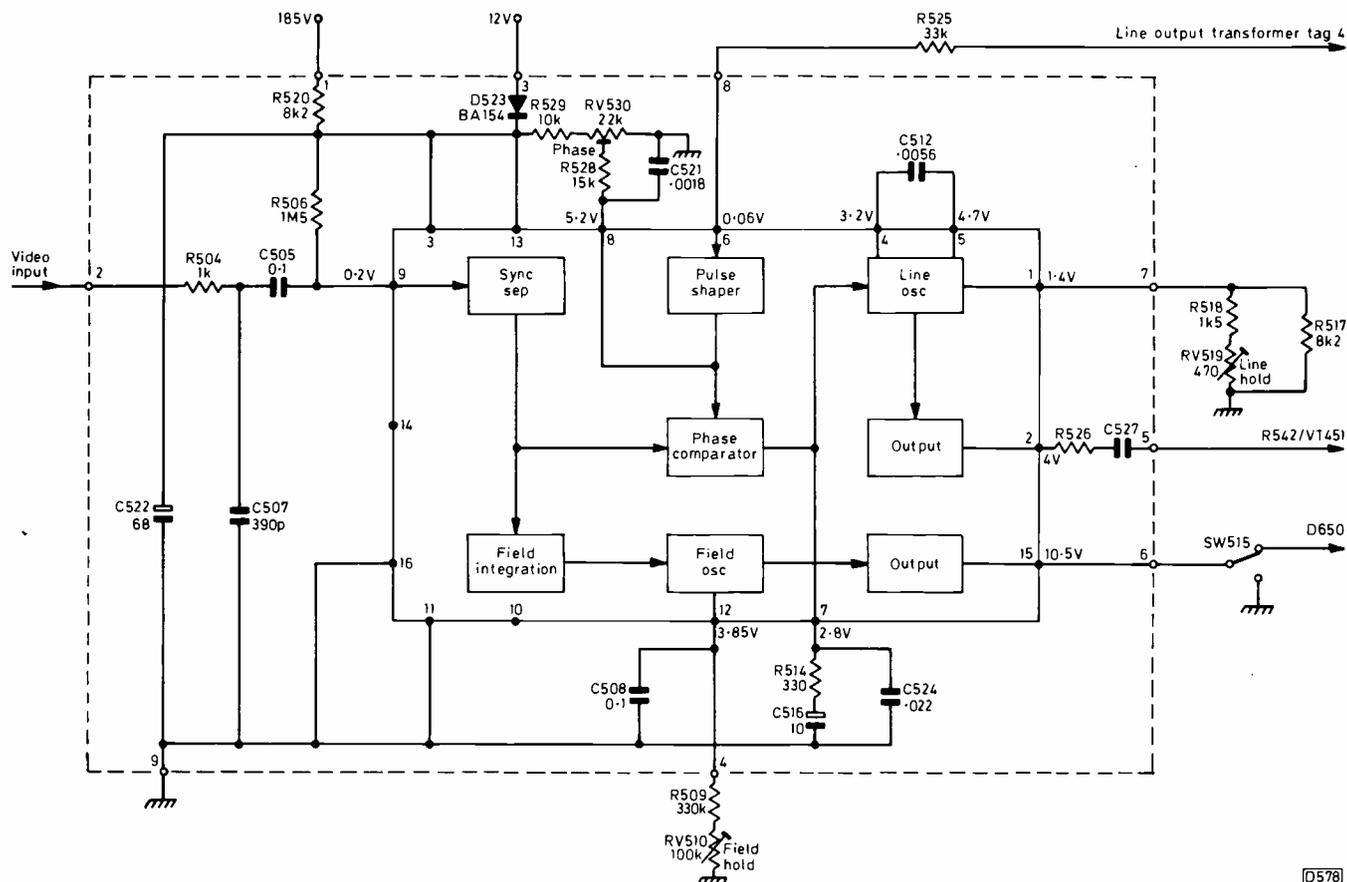


Fig. 3: The 731 chassis uses an SN76544N07 i.c. as the sync separator and line and field oscillator. It's mounted, along with certain associated components, on a subpanel, as shown above. R526 and C527 values as in Fig. 1.

A 3in. high scan with no video has nothing to do with the timebases but is caused by R555 (25V supply filter resistor) springing open. Why did it spring open? H.T. too high, probably because the thyristor in the power supply was leaky.

Both VT678 and VT684 (BC158 and BC338 respectively) can be responsible for field collapse, sometimes intermittent. The output transistor VT688 can be replaced by a 2N3055. It doesn't fail often, but can go leaky causing a progressive reduction in height as it warms up. Always check the setting of RV675 (bias) after any replacements in the field timebase. Start with the control fully clockwise, and turn anticlockwise until the slight compression about a third of the way down the raster disappears and VT688's emitter voltage is no more than 0.5V.

The various electrolytics in the field timebase cause different fault symptoms. Up to now most failures have been due to leakage, but no doubt as these sets age more of the electrolytics will have to be replaced because they've dried up. By far the most common electrolytic to give trouble is C672, in which slight leakage gives reduction of height, but still with a linear scan. C668 gives lack of height, with a band of compression at the centre of scan. We have had to replace a dried up C693 (1,000 μ F) once or twice, as it was giving severe lack of height with cramping at centre and bottom of the scan. Leakage in C941 causes weak field sync, which can also be caused by C194 (tuner a.g.c. smoothing) on the signals panel.

The 90° and 110° panels are interchangeable, provided three components are changed in value as follows: R661 is 1k Ω for 90°, 470 Ω for 110°; R703 is 1.5k Ω for 90°, 10k Ω for 110°; C663 is 0.68 μ F for 90°, 0.47 μ F for 110°. Failure to carry out these changes will result in excessive

height if a panel from a 110° set is fitted to a 90° chassis. The converse applies if the field timebase from a 725 chassis is fitted to a 110° set.

Convergence Circuitry

The convergence circuitry in both the 90° and 110° chassis has been quite free of trouble. This is in no small measure due to the good design, avoiding controls with low values and high dissipation (which inevitably become noisy and intermittent). The field convergence circuit is driven from the aforementioned secondary winding on the output transformer T687, and is of the active variety, using four transistors in a waveform amplifying and shaping circuit. These occasionally go faulty, usually with open-circuit emitter-base junctions – maybe intermittently. The result depends on which transistor is faulty, but you'll usually find gross convergence errors, the static convergence being so far out that purity is also affected. As a quick check, pull the plugs off the convergence yoke and switch on: though there will obviously be no dynamic convergence, the static convergence should be reasonable.

Other convergence faults have been few and far between, and mostly of the type that respond to tapping – for example an intermittent contact on one of the plugs, or a coil leadout wire dry-jointed.

When adjusting the convergence on the 110° sets, don't forget that there are two three-position switches which can be adjusted in conjunction with the R/G tilt and blue tilt controls. The centre positions give nil correction. As well as this, the blue lateral coil has four tappings on to which the flying lead can be plugged.

CONTINUED NEXT MONTH

Long-distance Television

Roger Bunney

THE Sporadic E season continued into June, with signals at fair levels, and many enthusiasts have remarked on the quite dramatic signals received from Scandinavia — Norway (NRK) in particular. Since NRK includes the transmitter identification on the PM5544 test pattern, establishing the exact transmitter received when the signal is clear enough is relatively easy. With conditions as they have been however, at least two NRK patterns may be received simultaneously on each channel, making identification difficult. Iceland has also been received at good strength on chs. E3 and E4: following recent advice, one DXer tried RUV reception very late — and succeeded in noting system M signals from the NW. These must obviously have originated from somewhere in the Americas!

My own log for the month has been pretty full, though there was no really dramatic reception. The following loggings were all via SpE.

- 2/6/79 TSS (USSR) chs. R1, 2; NRK E2, 3 and 4 (two on each channel); SR (Sweden) E2, 4. This developed into an all-day opening that jammed Band I.
- 3/6/79 NRK E3, 4; SR E3; DR (Denmark) E3, 4; also unidentified signals.
- 4/6/79 RAI (Italy) IA (twice), IB; TVP (Poland) R1; CST (Czechoslovakia) R1; MTV (Hungary) R1; TSS R1, 2.
- 5/6/79 DFF (East Germany) E4.
- 6/6/79 SR E2, 3; RAI IA; plus many unidentified R1, 2 signals.
- 8/6/79 TSS R1, 2.
- 10/6/79 TSS R1.
- 16/6/79 NRK E2, 3; unidentified R1, 2 signals.
- 17/6/79 TSS R1 twice; RAI IA.
- 19/6/79 TSS R1, 2; RAI IA.
- 21/6/79 RAI IA; TSS R1, 2; unidentified R1, 2, 3 signals; plus a mystery signal at 0800 consisting of a pulse and bar pattern followed by a non-identified FUBK test card, weak from the SE, between the E2, R1 carriers.
- 22/6/79 SR E2, 3, 4; CST R1, 2; TSS R2; unidentified signals.
- 25/6/79 TVP R1, 2; unidentified R1, 2 signals.
- 26/6/79 RAI IB; RTP (Portugal) E2.

One point is clear: signals from RTVE (Spain) have been lacking this season. There was an improvement in tropospheric reception during the 18-20th — even W. Germany at u.h.f. was noted!

Hugh Cocks (E. Sussex) reports reception of "JTV AMMAN" (identification on PM5544 test pattern) on Sunday the 10th at 1620. There have been several reports that the RAI PM5544 pattern has been seen with the identification "RAY 1" instead of the usual "RAI 1". Mike Allmark (Leeds) received the Tele Oristano (Sardinia) ch. IB electronic test pattern on the 1st — it resembles the W. German circular type pattern of the late 1960s, with the identification "Teleor Can B UHF". Kevin Jackson (Leeds)

and Hugh Cocks report reception of another ch. E3 Italian "free" station early in the period, with the "NCT" caption. Gwelo, Rhodesia ch. E2 was received at good strength on May 29th. Geoff Perrin (Dubai) also reports good SpE conditions — he received Pakistan ch. E4 using the PM5544 pattern with the identification "Pakistan" at the top and "Television" at the bottom.

During the early hours of June 12th, Cyril Willis (Cambridge) attempted to receive RUV (Iceland). Starting at 0115, he received for twenty minutes rolling pictures that were out of both field and line sync. This suggests a system M signal. Cyril reports that the signals were "in the middle of the tuner, at around ch. E3", i.e. ch. A2. No sound was present unfortunately, so the origin of the signals will never be known. I feel that they are most likely to have come from the eastern seaboard, since they were picked up from a westerly direction.

A correction to the July column incidentally. On page 475 the Lopik channel should have been given as E4, not E3.

News Items

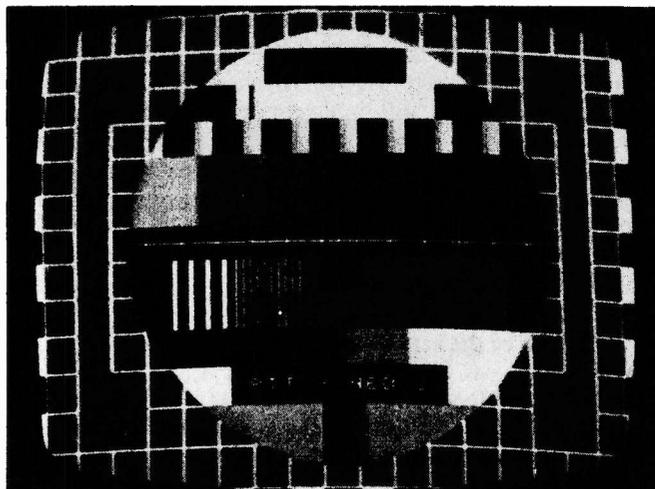
Luxembourg: CLT is using a 1,000kW transmitter at Dudelange to facilitate reception in Belgium and W. Germany. It's the first time that the same programmes have been transmitted on different standards from co-sited transmitters.

Albania: A new transmitter in Tirana is operating on ch. E10, providing a superior signal to the ch. C outlet.

Eire: New EBU listings: Cork ch. IG 100/50kW vertical; Sligo ch. IG 100/10kW horizontal; Gort ch. IH 100/50kW vertical; Kilkenny ch. IJ 100/50kW vertical — all RTE-2. Three Rocks RTE-1 ch. 29, 25kW horizontal. The Dublin ch. B3 and B7 and Sligo ch. B11 transmitters have now closed down.

The 30-50MHz Band

With the exception of ch. B1 and TV from ch. E2 upwards, the band 30-50MHz is empty in the UK — apart from i.f. radiation of course. In other parts this spectrum is used for medium-haul ground-wave communications, and of course for forward-scatter communications in Eastern Europe. When F2 propagation is increasing, this band can be used to advantage to see how high the maximum usable frequency has reached. Signals you may receive can come from Indian- or African mobile radio transmitters, Russian communications, or US Highway Patrol and paging



The NOS (Holland) PM5544 test pattern, received by Gareth Price (Lowestoft) on ch. 27.

stations. Short-wave radio harmonics abound of course.

Covering this spectrum is a problem unfortunately, since apart from specialised communications receivers (the Eddystone 770R etc.) there's little equipment available. I've approached the problem in various ways over the years, and do at present have a means of covering this spectrum accurately.

During the last sunspot cycle I modified the coils of a government surplus RF26 unit, feeding its i.f. output into a short-wave receiver. The next approach was to use a home-built tunable converter, covering 25-55MHz, using EF80/ECF80/EF80 valves and Denco coils. The Denco range of v.h.f. coils, reaching to about 80MHz, is still available and could probably be used with f.e.t. circuitry. Subsequently I obtained through *Practical Wireless's* VHF Bands columnist Ron Ham an historical (circa 1939) Hallicrafters S21 receiver covering 25-66MHz. Later types, including the S36, cover 26-150MHz and are available at low cost. Unfortunately, impressive though these receivers look they use elderly valves which by today's standards have low gain and poor noise performance. For the wealthy in our midst, Eddystone manufacture both v.h.f. and u.h.f. radio units (990 series).

Perhaps the easiest and cheapest way of covering the spectrum, assuming that you have a short-wave receiver covering 10-7MHz, is to use the tuner head available from Ambit International (Brentwood, Essex). Their 5402 varicap tuned head unit is available covering 30-50MHz and features a BF256 f.e.t. input amplifier driving a TFK1062 v.h.f. i.c. with an output at 10-7MHz. There's a pin diode a.g.c. system, but the only voltage requirements are a 12V supply and the tuning voltage. The cost (early June) is £14.75 plus VAT, and delivery approximately four weeks.

Coverage of 30-50MHz can also be obtained by using imported transistor radio receivers intended for the American market and for police monitoring. They are imported by Allan Electronics, 21 Ocean View, Whitley Bay, Tyne and Wear, NE26 1AL, and several models are available. I invested in the cheapest one, which is a Radioshak model with the Realistic emblem, made in Taiwan for export to Tandy in Canada. The "Patrolman 50" I'm using covers 30-50MHz, 108-174MHz and 450-512MHz with f.m. demodulation and squelch provision, and the broadcast bands 88-108MHz and MW. The electronics, including the miniature u.h.f. tuner, are mounted on a single board. Switching from band to band connects the aerial to the appropriate tuner, separate tuners being provided for each band with a common ganged tuning capacitor. The gain is good and the overall quality better than expected. Being intended for the American market, the mains transformer is for 120V a.c. input, though the importers say that 240V adaptors are available.

The set I ordered came via a Canadian air cargo flight and was held for a considerable time by the customs at Heathrow. Apparently there are now ample stocks however. Unfortunately, recent price and VAT increases have made this a less attractive proposition than last winter, but it does provide the quickest way of monitoring the required band with minimum effort. In its original form (120V a.c. and 6V battery operation) the Patrolman 50 costs £80.44, or £85 with 240V in-line adaptor, inclusive of postage and VAT.

Any other ideas from readers on covering the 30-50MHz band would be welcome.

F2 Propagation

Ian Roberts (South Africa) reports that an s.s.b. two-way

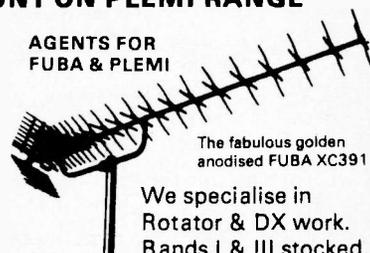
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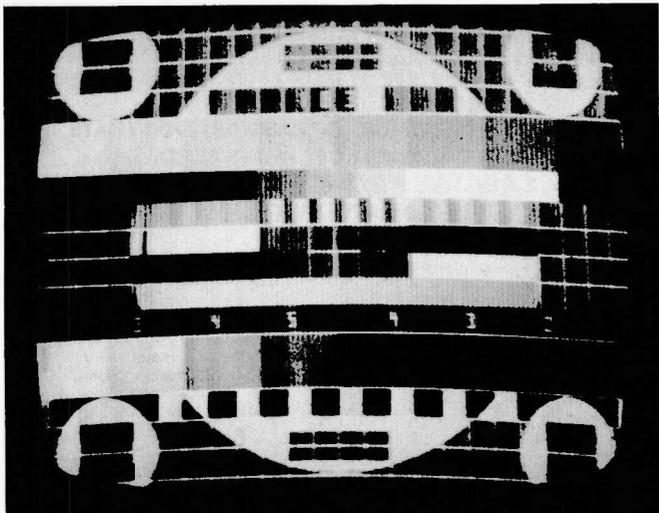
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The Russian electronic test pattern received on ch. R2 via SpE by Gareth Price.

contact has taken place at 144MHz between Italy and Luderitz (S.W. Africa), setting a new world record. Texas TV DXer Pat Dyers received ch. A2 (at up to 58MHz) from Venezuela on April 17th, the first time in this cycle. Jerry Pulice (Staten Island, USA) reports that during good F2 conditions in February the UK ch. B2 could be received at high levels, though with no sign of ch. B1 at 45MHz. On other days during February ch. B1 was generally very, very strong!

From our Correspondents . . .

The many letters I've received this month indicate that SpE reception has been experienced throughout the country. Mike Gaskin (Croydon) has been using a JVC 3050 portable TV set with excellent results, despite being only two miles from Crystal Palace. His loggings include Denmark chs. E3 and E4 via a very short skip path, and a 200W 88MHz RUV (Iceland) f.m. station.

Frank Jimenez (Clapham) has logged SR, NRK and RUV with only a small aerial sticking out of the window. He too has received short-skip signals from Denmark. John Lees (Cheltenham) has noted the RAI test card with "RAY 1" identification, and two West German transmitters at Ochsenkopf and Kreuzberg, using an indoor aerial. Gareth Price (Lowestoft) has sent us an excellent photograph of the Russian electronic test pattern, received on ch. R2.

Long-distance TV for the Beginner

The Long-distance Television column and its predecessor DX-TV have been running monthly in this magazine since the early 1960s. There have been many changes over the years: colour is now often a feature of long-distance (DX) reception; there has been a vast increase in the number of transmitters (all seemingly using that plague – for identification purposes – the PM5544 test pattern); but perhaps the change that has become the greatest problem is the increase in the number of programme hours, with the corresponding reduction in test card transmission time, making station identification increasingly difficult. The technology has also changed: u.h.f. DX-TV reception is now firmly established, while some enthusiasts have already sampled the delights of satellite TV. And with advances in tuner and aerial technology, it's possible to achieve reception at very low signal levels. To cater for newcomers, it's necessary from time to time to go over the basic techniques of DX-TV reception, so here we go again. My



An example of reception during a period of enhanced tropospheric propagation – photo by Gareth Price.

apologies to those who already know it all: I'm sure they will understand.

Perhaps most viewer's first introduction to DX-TV reception comes when they find on their screen a signal that hasn't come from one of the local transmitters. This may happen while tuning between the usual stations, and may lead to an exploration over the whole u.h.f. TV band. This will probably reveal further unexpected signals.

The quality of distant TV signals varies from day to day, and the signals may last for a few hours or less. Warm, settled weather is best. There may in some locations be distant signals of sorts present every day, stronger on some days than on others. U.H.F. signals are particularly dependent on weather conditions. Remember the "old 405-line days" however, when the BBC signal would sometimes be upset during the summer months by weird patterning and Spanish voices, leading to the familiar "foreign interference" announcements. That's another form of DX-TV reception, but at distances of 500 miles or more, actual signal strength being very strong and receivable even on an indoor aerial.

The potential DX-TV enthusiast will obviously wish to minimise his initial expenditure until he can assess the possibilities that expensive aerials and ancillary equipment might bring at his location. Fortunately it's possible to use a standard u.h.f. TV receiver (preferably one with full dial tuning rather than push-buttons for channel selection) for both v.h.f. and u.h.f. DX reception – more on that next month.

Considering first long-distance u.h.f. reception, we've already pointed out that the number of transmitters that can be received and the quality of the signals is related to the weather. This is determined by the conditions in the troposphere – the region from the Earth's surface upwards to some 25,000ft. (8,000m.). For obvious reasons, this type of reception is called tropospheric reception. Pointers to the likelihood of such reception are the slow-moving high-pressure systems that give us our sunny, cloudless summer days, with a rapid fall in temperature at night due to the clear skies. This results in the signals improving during the evening, falling off next morning as the Sun heats the Earth's atmosphere again. Fog is another effect that's often present during such conditions, and during the autumn you'll often find that remarkable tropospheric reception is possible during foggy conditions. Sometimes, when a moving weather system produces abrupt pressure changes along the isobars, a form of signal ducting occurs – *along*

the line of the isobar. So it pays to keep an eye on the weather maps.

You don't need a vast or complicated installation to start experimenting with DX u.h.f. reception. Obviously an aerial is required, and a basic rule of aerials is the larger the system the higher the gain, i.e. a big aerial captures more signal. Fortunately however the advent of low-noise aerial preamplifiers has made it possible to achieve reasonable DX reception using a compact array.

The bandwidth of u.h.f. aerials (and preamplifiers) varies. Most aerials sold for normal domestic reception of local transmissions are grouped, i.e. designed to receive particular groups of channels - group A, channels 21-34; group B channels 39-53; group C/D channels 48-68. There are also wideband u.h.f. aerials - for channels 39-68 (group E); channels 21-48 (usually suffixed K); and the /W type which covers the entire u.h.f. bandwidth (channels 21-68). To minimise outlay, a single /W aerial is a sensible purchase. Since gain falls with increase in bandwidth however, improved results will be obtained by employing a group A and group E aerial or by employing three aerials (group A, B and C/D) to cover the bandwidth. For a given type of aerial, the greater the number of elements the higher the gain and the more directional the response (assuming that the system is correctly designed of course).

Gain is specified in decibels (dBs), the basic half-wave dipole being assumed to have zero gain. Add a reflector rod and perhaps a couple of director rods and the aerial gain is increased, at the same time making the system more directional, i.e. restricting the forward pickup angle (helpful in reducing interference from unwanted signals). An aerial with a 3dB gain has twice the signal output of a single half-wave dipole, i.e. there's a power gain. A four times increase is 6dB, an eight times increase 9dB, a sixteen times increase 12dB - in fact a 3dB power gain every time the output doubles. If you want to go into aerial theory in greater depth, it would be worth consulting Gordon J. King's "Practical Aerial Manual", 2nd edition, published by Newnes-Butterworths. If I may include a commercial break at this point, you'll also find much information on aerials in my own book "Long-Distance Television (DX-TV) for the Enthusiast", published by Babani Publishing at £1.45. There's far more information there than I can include here.

So you buy your aerial, and we'll assume you don't live within five miles or so of a high-power transmitter (if you do, you've got problems!). The next thing is where to point it, since there are signals in all directions. It's obviously best to be able to rotate the aerial. Aerial rotators are available, but again this involves expense. If you have access to a wall and ground however you can erect the aerial on a scaffold pole mounted on a large ball bearing. Support the pole with wall brackets and thrust/ballrace/bearings - so long as the friction is low and the aerial clears the roof, it can be turned by hand (for further details see the article by Keith Hamer and Gary Smith in the March 1978 issue of *Television*).

An aerial preamplifier is helpful - essential in some locations, but occasionally a problem (less than five miles from a local transmitter). It can be used indoors where the feeder run is very short (say less than 30ft.) and very low-loss, high-quality coaxial cable is used. If a long length of cable is necessary however the preamplifier must be mounted at the aerial end. Select a medium- to high-gain preamplifier, with low noise and good cross-modulation performance, i.e. it can withstand a high-level local signal without overloading (producing interference on other channels). Wideband preamplifiers can be obtained with noise figures of less than 3dB and gains of 22dB minimum (voltage gain, not power gain) over the entire bandwidth.

It's worth taking a look at the Labgear and Wolsey ranges.

Turning to aerials again, if minimum outlay is essential I'd suggest giving thought to a stacked bowtie system, such as the Wolsey Colour King and other variants, or a multiple Yagi aerial such as the /W versions in the Antiference XG range. Fuba also have a range of wideband aerials with a high reputation.

If interference from a local channel is a problem, a simple filter can be made to attenuate such channel(s). If preamplifier overloading is taking place however the filtering will have to be done prior to the preamplifier. Hugh Cocks covered the whole subject of filtering in the November 1977 issue of *Television*.

Tropospheric signal propagation can result in u.h.f. reception over many hundreds of miles, at high signal levels. In the eastern coastal areas of the UK, signals have been received from as far away as Poland, the USSR, Sweden, Czechoslovakia, Austria and Switzerland. On a more local note, in most areas a good aerial installation should provide at least one additional IBA channel.

Tuners for DX-TV

Hugh Cocks

For some time the ELC2000 tuner has been much sought after by DXers. This tuner covers the v.h.f. and u.h.f. bands, with the advantage of an extended low-band coverage (Bands I and II) up to approximately 90MHz, enabling the OIRT and Italian/Albanian Band II channels to be received. The disadvantage of the tuner is its price, also its availability, though the latter has improved recently.

I recently came across a cheaper solution which also has a marginally improved frequency coverage - the ELC2060 tuner. This is physically identical to the ELC2000, the difference in coverage being that the low band extends to over 100MHz, enabling channel R5 to be received (not possible with the ELC2000). The ELC2060 is intended for use in sets destined for the Australian market, which accounts for the extended frequency range.

A minor advantage of this tuner is that on Band III it's aligned down to 138MHz, the Australian channel 5A. Coverage in practice extends well below this, down to about 110MHz, making possible reception of a multitude of non-TV signals. The ELC2000 also has this band coverage, but the tuned circuits are aligned only as far as the bottom of the European Band III (approximately 175MHz).

The ELC2060's u.h.f. coverage is good - from below channel 21 to well above channel 68.

The tuner is available from Sendz Components, 2 Woodrange Close, Thorpe Bay, Essex. The price at the time of writing is £4.50, including VAT and postage.

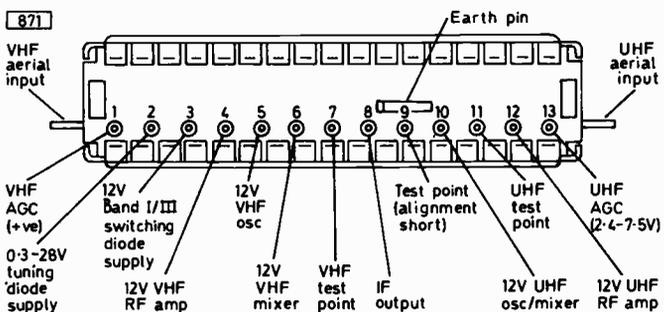


Fig. 1: ELC2000/ELC2060 u.h.f./v.h.f. varicap tuner pin connections. The output from the u.h.f. section of the tuner is coupled to the v.h.f. mixer.

TV Troubles

Robin D. Smith

Rank A823 Chassis

A six year old set fitted with the Rank A823 chassis was in need of a general overhaul. It came in initially because the customer complained of a "ticking" noise which we never heard. We decided to fit a new tube and while the chassis was out had a good look around. The h.t. reservoir/smoothing capacitors 8C9/10 had leaked badly over the chassis, so had to be replaced, but we doubted whether this could have had anything to do with the "ticking". Close inspection in the e.h.t. compartment then revealed that the focus stick 6VDR1 had crumbled badly, so we assumed that this was the cause of the complaint.

With the new tube fitted and the e.h.t. set up correctly there was a reasonable picture but not one of the quality that should have been present with a new tube in the set. Attention was turned to the two-chip decoder therefore, and the U reference signal at 3TP7 adjusted for 600mV by means of the preset colour control 2RV6 (see my notes in the July 1978 issue, page 465). The general colour still appeared to be desaturated however. A new decoder panel produced the results we were after, so we realigned the original following the instructions in the manual. We found that by setting up the matrix amplitude control 3RV3, the V reference phase coil 3L5, the U reference phase coil 3L10 and the matrix phase coil 3L7 our troubles were completely cured.

We've since had several of these decoders in with similar alignment errors.

The customer himself had had a go on one of the later A823B versions of this chassis. Finding the l.t. voltages to the decoder and i.f. unit low, he'd decided to check the smoothing electrolytics 8C3/4 in the power supply. He came to the conclusion that they were both leaky, but as he didn't have a replacement he decided to refit the panel while obtaining a new can. He forgot to refit the screws securing the panel to the chassis however, and on switching the set on there was a loud bang. When he'd sorted that out, he discovered he'd got no picture. This is where we came on the scene.

The l.t. was low but e.h.t. was present. We then advanced the c.r.t.'s first anode controls to maximum, obtaining a negative picture. It's my experience that this is generally due to the SL901B i.c. on the decoder panel, so I came to the conclusion that he'd destroyed it when the power supply earthing had been incorrect. I decided to leave this however until the l.t. supply was correct. It was about 3V down, with hum at minimum volume and a hum bar. 8C3/4 were checked but seemed to be all right, so the other two electrolytics 8C1/2 came under suspicion. Muck had started to leak out, but a replacement block still didn't cure any of the faults.

So if the power supply panel and 8C1/2 weren't the cause of the trouble, what was? I remembered a similar fault that took me an age to find many years ago. There's a tagstrip near 8C1/2/9/10, secured to chassis by two screws which provide the necessary earth connections for the components

mounted on the strip. On examination, one of these screws was found to be very loose. It was tightened, with a little difficulty, the chassis assembled and the set switched on. L.T. now correct, no zero volume hum, no hum bar. Replace the SL901B, reset the chroma reference signal level, generally converge and the results were excellent.

Intermittent Signals

The trouble on an ITT colour set fitted with the CVC9 chassis was intermittent loss of sound and picture – the sound and vision would cut out, leaving just a snowy raster. This suggested a fault in the i.f. strip, not uncommon on these sets. We noticed however that the picture geometry was not quite correct when the fault appeared, and felt that maybe the fault was in the line output stage. Now the small panel on the line output transformer is prone to dry-joints, so instinct told us to look there first. Luckily we found the fault quickly – at the pulse winding earth pin 3 – and resoldering cleared the trouble. Why did this remove the signals? Well the 75V pulse from pin 4 of this winding is used to gate the a.g.c. circuit. With no pulse present, there's no a.g.c. action and the first two i.f. transistors are driven into saturation, removing the signals.

Signal Cramping

A customer brought in a Bush monochrome set (TV161 series) with the fault weak field lock. He'd been having a go himself, having fitted a regunned c.r.t. and checked the field timebase thoroughly. On switching on I noticed that the picture was not as good as it should have been with a replacement tube, indicating a fault in the video circuitry. The voltages around the PFL200 video output/sync valve were all correct, so I moved back to the video phase-splitter transistor 2VT4. The collector was at the l.t. rail voltage, while both the base and emitter read 0.7V. Clearly the transistor was short-circuit base-to-emitter, and a replacement gave a sharp picture with good field lock. From experience, I've found that tube flashover is usually the cause of the failure of this transistor – remember that a new tube had been fitted.

2VT4 acts as an emitter-follower on 625-lines incidentally, with no gain but a high input and low output impedance. The short-circuit would load the detector circuit therefore, clipping the sync and video information.

Terrible Striations

The same customer, a bit of a TV cowboy, subsequently brought in a Philips dual-standard monochrome set (210 chassis) with the worst vertical striations I'd ever seen – alternate black and white bars, about 2in. wide, right across the screen. This time he'd fitted a new line output transformer – and after some time spent checking the connections, we found he'd got them wrong. The moral here is always to make a drawing before removing any part which has multiple connections, in particular noting the destinations of any wires with the same colour coding.

Line Drive Trouble

Back in February I described an awkward fault on a Decca Bradford chassis – the picture getting darker after the set had been on for a while. The trouble then was due to the feedback capacitor (C427) in the line oscillator stage being of the wrong value, as a result of which the line drive

waveform was incorrect. The set was back with us recently with similar trouble – low amplitude line drive, as a result of which the line output valve was overheating, eventually blowing the 500mA h.t. fuse. Checking the voltages in the line oscillator circuit didn't reveal any major errors, but then meters aren't always that accurate when it comes to oscillator stages. This time the fault was traced to the pentode's anode load resistor R444, which had changed value from 33k Ω to something more like 3.3k Ω .

Yet More Cowboys

The 'phone rang one morning recently. "Have you a 13A to 15A fuse for a colour TV set?" "There's no such thing" we replied. "Well the one fitted was 13A, and a 13A mains fuse blows." So we had the set in and duly noted a 13A fuse in the mains fuse holder. It turned out to be a Bush set, fitted with the A823A chassis. Checks revealed that the thyristor rectifier was short-circuit, the series thermistor shattered, and the associated print blown apart. After making the necessary repairs, fitting the correct fuses (none of them correct) and setting up we awaited the return of this other cowboy. When he came in we asked him what made him think the fuse was rated at 13A? "Well the old one was marked T3-15A" he said, "and I took this to mean 13-15A."

Another A823A chassis had received the attentions of the son of the house. He'd started a job in electronics and, after four months, thought he could repair colour television sets. He'd apparently found the l.t. fuse blown, due he discovered to a short-circuit l.t. rectifier, but on replacing these still had no picture. We first checked the h.t., which was found to be high at 240V. This indicated the reason for the absence of e.h.t. – the over-voltage protection circuit had tripped, stopping the line oscillator. So we turned the set e.h.t./h.t. control 8RV1 to minimum, then advanced it to read 200V at the h.t. fuse 8F3. Still no picture, because the tube heaters were not alight, but a healthy oscillation could be heard and the hairs on the back of a hand placed close to the tube face confirmed the presence of e.h.t. The absence of the heater supply was simply a plug-and-socket fault, soon put right.

It's very easy to move 8RV1 accidentally when working on the power supply panel, which was presumably why the h.t. was high and the over-voltage trip had operated. We always turn it to minimum before switching on after carrying out any repairs in this area.

Anyway, we now had a picture – but it was negative, with flyback lines. From experience we concluded that the SL901B demodulator/matrixing i.c. on the decoder panel was faulty, and a replacement produced a normal picture.

We gave the budding apprentice a short talk, and I expect he got a thick ear when his father received our bill for £17. Shame!

A Pye Hybrid Colour Set

We were caught again the other day by a stock fault on the Pye hybrid colour chassis – lines across the top of the picture due to a defective pincushion correction potentiometer, RV41 – though the fault had taken eight years to put in an appearance. The cause of the trouble was a dead spot on the wirewound track – the fault disappeared when the preset was moved. Cleaning and refitting the control cleared the problem. Another fault on the set was that the green first anode control couldn't be adjusted, due to its series 1.5M Ω resistor R465 being open-circuit.

While setting the receiver up, R389 (3.3k Ω) on the CDA panel started to glow like a bulb. This resistor supplies the

screen grids of the PCL84 colour-difference output valves, also the tuning voltage for the varicap tuner. It's decoupled by a 4 μ F electrolytic, which was our first suspect, but the trouble turned out to be due to a screen grid-cathode short in one of the PCL84 valves.

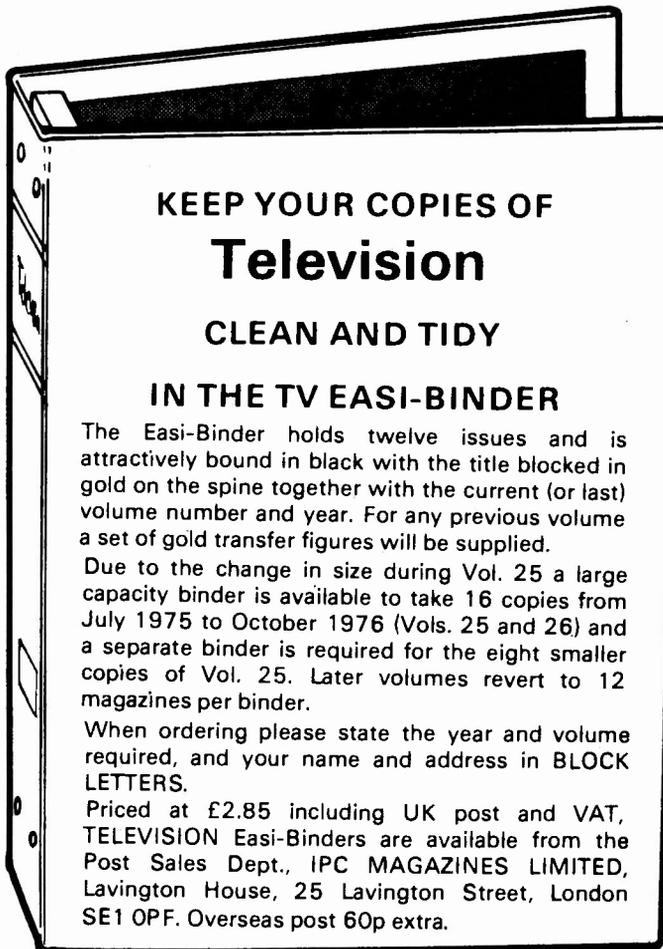
On making some further adjustments we had the set working very well for its age.

20AX Tube Fault

The complaint on a set fitted with the ITT CVC32 chassis was lack of brightness. The set was only four weeks old, so we thought that adjusting a preset was probably all that would be required. On inspecting the test card however we found that the focus and convergence were very poor at the edges – in fact the picture was poor generally. It turned out to be a faulty tube – our first defective 20AX type. Very easy to change and set up on this chassis.

All Part of the Service . . .

The customer complained that the sound on his GEC C2110 series receiver cut out after a couple of hours. Fitting a replacement sound panel cured the problem – these panels are not worth repairing by us – but a week or so later the customer phoned to say that the trouble had returned, along with varying brightness. On examination, we found the set to be thoroughly wet, with the e.h.t. sparking away. We brought it into the workshop to dry it out, after which it performed correctly. All this had to be done free of charge, since the set was under guarantee. All we could do was to give some advice on heating and hope for the best.



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TV Servicing: Beginners Start Here . . .

Part 24

S. Simon

LAST month we tiptoed into the shallow end of colour receiver servicing, and found that the power supply and line timebase sections of a hybrid colour set present little in the way of problems that we've not already met in dealing with monochrome receivers. We must now wade into slightly deeper water.

The next part of the set – sticking with Pye hybrid chassis – we're going to look at is the CDA panel – CDA standing for colour-difference amplifier. Why colour-difference? Well, remember first that there are three beams in a colour tube, to activate the red, green and blue phosphors, and that the luminance signal will drive the colour tube to produce a monochrome display just as with a monochrome set – in fact the luminance signal in a colour set is exactly the same as the video signal that drives the c.r.t. in a monochrome set. Clearly then to get colour on our colour tube we require something in addition to the luminance signal. That something consists of three colour-difference signals, one each for the three primary colours, red, green and blue. They may be positive- or negative-going, so as to add to or subtract from the luminance signal applied to each gun. Say we want to turn our display from monochrome to red. Obviously we have to turn up the red beam, but at the same time we have to turn down the blue and green beams, in order to preserve the correct brightness level. This is what the colour-difference signals do.

Colour Mixing

This is obviously a mixing process. We mix the luminance signal (Y) with the colour-difference signals (B – Y, R – Y and G – Y) in order to get the correct colour in the display. Now this mixing can be done in several ways. It can be done by a simple resistor network before application of the signals to the c.r.t., or as in most recent chassis in an i.c., or alternatively, as in many hybrid chassis including the Pye ones, by feeding the Y signals to the c.r.t. cathodes and the colour-difference signals to the tube's control grids (see Fig. 1). This latter technique is for obvious reasons called colour-difference tube drive; the alternative arrangement, in which the tube is driven (almost always at its cathodes) by RGB signals, is for equally obvious reasons called RGB tube drive. Note that for a monochrome display the colour-difference signals simply disappear, the tube being driven by the luminance signal only.

Grey Scale

As you'd expect, there are some complications. Since the human eye has an uneven colour response, the signal levels have to be adjusted to take this into account. The correction required is done at the transmitter. To take into account receiver circuit tolerances, and differences between the characteristics of different tubes, highlight presets are incorporated in the tube drive circuits while the tube's first

anodes are provided with low-light presets that set the cut-off levels of the three guns (since the PIL type of tube has a common first anode structure, the low-light presets with this type of c.r.t. must act on the tube's biasing). When everything is set up correctly, we should have a tint-free grey scale from bright white through to dark grey.

This is all very nice, but alas tubes age and the emission of the three guns tends to vary over a period of time, with the result that the displayed picture may show decided colour tints at different brightness levels. Assuming that the tube's emission is good however, the grey scale should not be too difficult to set up, if indeed this is necessary at all. The point to bear in mind is that if a good black-and-white picture cannot be resolved with the colour off, it will be impossible to obtain correct colours when colour is restored to the display. You have the first basic rule of colour receiver servicing therefore: first get it right in black and white.

CDA Circuitry

RGB drive to the tube's cathodes is the more efficient system, since the cathodes are being swung with respect to steady voltages on the first anodes and control grids, i.e. if the cathode is driven negatively, this is the same as both the control grid and the first anode being driven positively, whereas when a colour-difference signal is applied to the grid the voltage difference between the cathode and the first

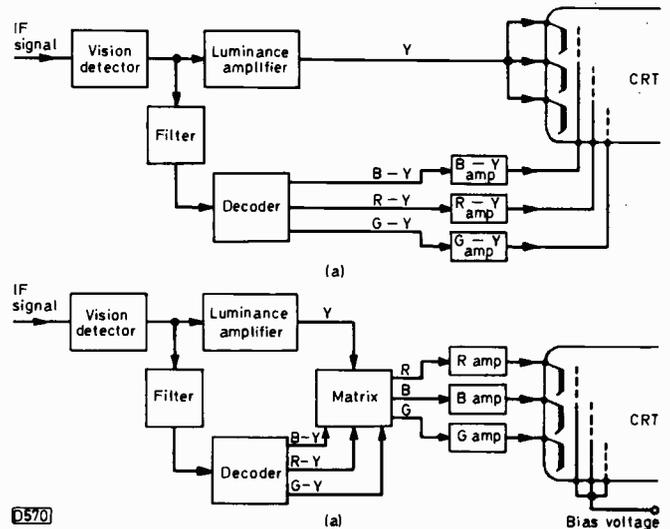


Fig. 1: Methods of driving a colour tube. (a) Colour-difference drive, with the luminance signal (Y) applied to the three cathodes and the three colour-difference signals applied to the grids. The tube then carries out the RGB matrixing, the phosphor screen being activated by the three primary-colour signals. (b) RGB drive. In this case matrixing is carried out prior to the tube, the RGB signals being applied (almost always) to the three cathodes.

anode remains the same, so that a larger signal swing is required. This large signal swing requirement persuaded most designers of early sets to opt for valve colour-difference amplifiers. If the signal voltage swing required to drive a beam from full on to full off is 150V, this must be developed across a resistor of some 10kΩ from a supply line of over 200V. A valve with a fairly good mutual conductance figure (change of anode current with change of grid voltage) is required to provide the current necessary to produce this swing across the 10kΩ load resistor. So it's quite common to find three colour-difference amplifier valves of the PCL84 type driving the three tube control grids, while a PL802 luminance output pentode drives the three tube cathodes. This valve line-up is not universal however: in the Philips G6 chassis for example you'll find a PFL200 used as the luminance output valve and three PCF200 valves as the colour-difference amplifiers.

The PCL84 and PCF200 valves are triode-pentodes, the pentode sections being the high-gain amplifiers which drive the c.r.t. grids, while the triodes are used as clamps to keep the d.c. conditions at the tube grids correct (because the pentodes are a.c. coupled to the grids). The basic idea is shown in Fig. 2. The drive signal developed across R1 is coupled via C1 to the c.r.t. grid. The triode clamp is driven hard on at the end of each line by a pulse derived from the line output stage. As a result, the junction of C1 and R2 is restored once each line to the voltage set by the potential divider R3/R4, thus stabilising the d.c. conditions.

The clamp triode's anode resistor is of a high value, typically 10MΩ, and it's not uncommon to find one of these (remember that three such circuits are required, one for each c.r.t. control grid) open-circuit or very high in value, thus allowing the relevant tube grid to drift, rendering the grey scale quite wrong. Note that as a result of the a.c. coupling a faulty pentode anode load resistor (R1) will not affect the grey scale (there's no colour signal swing) but will really upset the colour rendering.

Poor Grey Scale

Inability to obtain a good grey-scale with a tube that's known to be good must direct attention to the tube base voltages, checking that the first anode voltages are roughly equal (say 450V at each first anode pin), that the cathodes are at whatever is stated in the service data for the set (say 220V) while the grids are at around 80-100V (assuming colour-difference tube drive). If the application of the voltmeter to one cathode drastically changes the colour, check the preset drive control associated with that cathode (see Fig. 3). If the grid voltages are not roughly the same, check the clamp triode and its associated components, particularly the high-value anode resistor. Also remember this: the grids of the three clamp triodes are connected together, so that a fault in one triode will affect the others. PCL84 valves are particularly prone to developing faults in their triode sections, and one faulty one will affect the other two.

The Pye hybrid sets are also particularly prone to developing troubles on the CDA panel itself, due mainly to decomposition of the plastic panel material (the heat from the four valves being conducted down on to it by the base contacts). Thus incorrect colours may well be due to cracks in the panel, leakage through the panel material, and poor earthing to the rear clips. The earthing is made by spring wires which pass through loops of metal, and it's the loops that are soldered to the panel earth. Poor contact between the wire and the loop therefore will result in a poor earth connection to the main frame. This is one cause of colour

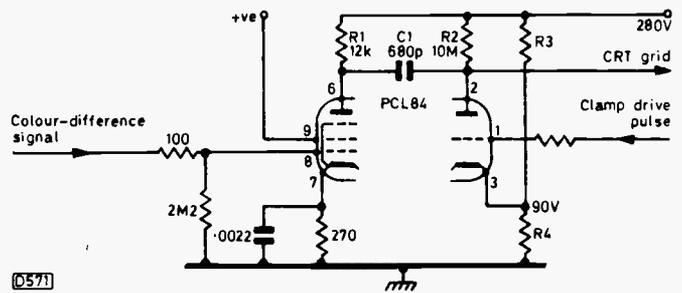


Fig. 2: A typical colour-difference output stage, with triode clamp. C1 couples the signal to the c.r.t.'s grid, with the triode setting the d.c. conditions at the grid. The black level is set by the potential divider R3/R4.

shading from the left to the right of the screen (say green to the right and blue to the left). The remedy is to solder the wires to the loops, or connect a flying lead from the panel earth to a screwed earth on the main frame. Speaking generally, many strange effects can be displayed on almost any make of colour set as a result of poor earthing, and the connection of a lead from the main frame to the various panel earths can be a rewarding exercise.

Signals in a Colour Set

Now let's just briefly consider the various signals we're concerned with in a colour set. There are three colour-difference signals plus the luminance signal, and when these are mixed, either before the c.r.t. or by application to the c.r.t. electrodes, we get R, G and B primary-colour signals to activate the colour phosphors on the screen. The luminance signal is the same as the video signal in a monochrome set, and has the full video bandwidth, i.e. the picture detail is contributed by the luminance (Y) signal, exactly as in a monochrome receiver. In addition, two colour-difference signals are transmitted. Only two, you may ask? Yes, because if you look at the mathematical relationships between the two transmitted colour-difference signals (R - Y and B - Y) and the luminance signal (Y), i.e. their relative amplitudes, you'll find that the third colour-difference signal (G - Y) can be obtained quite simply in the receiver by adding together certain preset proportions of B - Y and R - Y. This is done in the G - Y matrix, which may consist of a couple of resistors or be something that in more recent sets goes on within an i.c. The two transmitted colour-difference signals have a much narrower bandwidth than the luminance signal, since the human eye is not sensitive to colour detail, and are carried on a common subcarrier which fits within the channel bandwidth. The various signals are separated out in the receiver by filters, and sent to the appropriate parts of the set.

The chrominance signal, as the transmitted colour-difference signals when modulated on to their subcarrier is called, passes from the video detector (or a separate detector) to the colour decoder, whose function is to process and demodulate the chrominance signal and present to the video output circuits either RGB signals or the luminance and three colour-difference signals depending on receiver design. The colour-difference signals are adjusted in amplitude at the studio to correspond with the sensitivity of the human eye, and are further weighted to avoid overloading the transmitter. The latter is corrected in the receiver simply by presetting the relative gains of the R - Y and B - Y amplifiers. The PAL system introduces some clever twists to overcome the effects of signal distortion in the transmission process - but we'll have to leave a look at that side of things until we come to the decoder. Our main

since, as we've already mentioned, deterioration of the panel occurs: as a result, the fact that the h.t. is present at the panel input point does not mean that it gets to where it's supposed to be. Cracks in the tracks you see, something to bear in mind.

Later versions (693, 697) of the Pye hybrid chassis employ a varicap tuner which requires a stabilised 30V tuning line. This is obtained from the h.t. line through a resistor or resistors on the tuner panel. The h.t. is not taken direct from the power supply however, but is derived from a point on the CDA panel. Deterioration of the panel can thus result in the absence of the tuning voltage, with the result that the tuner cannot select any signals and simply produces noise. The tuning voltage also disappears when R389 goes open-circuit, but as this also removes the supply to the

c.r.t.'s control grid clamp circuits the result is no or very little screen illumination and no sound signals of course. The trick is to know what voltage to expect and where to expect it. Almost back where we started, aren't we?

Summarising

In conclusion this time we'd mention that whilst the colour decoder, which we've yet to consider, is far more complex than the colour tube's drive circuitry (the luminance and colour-difference amplifiers), the fact is that the vast majority of colour faults are due to something amiss in the c.r.t. drive/biasing arrangements. There are also convergence and purity to consider, though the results of faults here are mainly self-evident.

Letters

EW TINTING

I've read with interest the comments in *Television* on EW tinting with the Pye hybrid colour chassis. The fault has come my way only once, and what I can't understand is how switching the c.r.t. first anodes on and off could have cured it, even temporarily.

I arrived at the cause of the trouble after giving it some thought. What was obviously happening was that one of the guns was being turned on progressively harder as its beam scanned across the screen. This was verified by using the scope to monitor the c.r.t. cathode waveforms and also by observing the three rasters separately. This threw suspicion on the colour-difference output/clamp circuits, and the 12k Ω pentode anode load resistor was found to be open-circuit (R391 in the G - Y channel in this case). I've since been told that the fault is quite common on these chassis. The sure-fire way of checking this is to disconnect the lead supplying the 47V pulses to the clamps: this stops the clamp action, and if the tint disappears the pentode anode load resistor is the cause of the trouble.

I'd also like to take this opportunity to agree with your contributors who have commented on the low standards of performance most people are prepared to accept from their TV sets, even when new.

Gerald Messent, North Cornelly, Bridgend, Glamorgan.

Editorial comment: Since the pentode anode load resistors sometimes go open-circuit intermittently, it would seem that the first anode switching business is coincidental.

BIONIC PYES

We read with interest the article entitled *Bionic Pyes* in your June issue, covering certain of our products specifically designed as replacement units for use in Pye hybrid colour receivers. We appreciate the fair presentation and recommendations, but would like to add a few comments.

First the CDA panel on which your tests were made was an early production one. Although many thousands of these are now in use, the only modification we have found to be desirable is to change the colour-difference output transistors from type BF259 to type BF459 so that we can use a different type of heatsink. There is nothing wrong with the BF259 as such, but the tall heatsink we used with it makes it top heavy and vulnerable to damage, especially

when sent through the post. Rough handling could result in the transistor leads being pulled out of the board, and this could have been the cause of the dry-joint trouble referred to in your article. There have been very few cases of this reported to us, but we decided to prevent it by changing to the BF459 with its lighter heatsink - this was some eight months ago.

The audio module, like the CDA panel, has also been very successful and well received by users. We have found however that the supply of the SN76013ND i.c. in production quantities is too erratic, though it is readily available for replacement purposes. Being unable to find a suitable alternative i.c., we decided to redesign the module using discrete components which we can get in sufficient quantities to maintain production. The new module is still a direct replacement for the LP1162, and of course we've used silicon transistors which make it more reliable than the original Mullard LP1162 unit.

Your readers may be interested in our new 915 module, which has been designed as a direct replacement for the i.f. selectivity/gain unit used in the Pye 713, 725, 731, 735, 737 and 741 chassis and the Philips 570 chassis. The original units have proved troublesome due mainly to the use of a number of through board connections and double-sided print. Our replacement unit uses a SAWF to provide the bandpass response and an i.c. to provide the gain, and as a result we've managed to achieve a single-sided print layout.
W. Kennedy, LEDCo, Thornton Heath, Surrey.

LEDCo CDA PANEL

Having been plagued for some time by drifting grey-scale and other problems in an ageing Pye hybrid colour set (697 chassis), I decided some while ago to fit the LEDCo CDA panel reviewed in your June issue. For nine months or so the board has performed admirably in eliminating these defects, and looks like adding several years to the life of the set. I was surprised however that you omitted to mention a rather obvious shortcoming in the design of the solid-state circuit. This is that the components which bias the base of the luminance input transistor (VT701) upset the action of the d.c. restorer D39, causing the black level to float up and down with the picture content as if the luminance was a.c. coupled. I must say however that this is far less annoying than the effects of tired valves.

Alan Pemberton, Sheffield.

P.S. Poor field lock on this set turned out to be the field sync pulse integrating capacitor C41 (0.0047 μ F) open-circuit, replacement curing the trouble. I've not seen this one mentioned in your columns before. It's mounted on the i.f. panel, along with the sync separator.

Your PROBLEMS solved

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TELEFUNKEN 709 CHASSIS

The set will work perfectly all evening provided the channel is not changed. If another channel is selected after the set has been on for some time, it's impossible to obtain a picture. The situation is the same on all channels. The set works normally when first switched on from cold.

The tuning voltage stabiliser diode GR971 (ZTK33) has a tendency to cause slight tuning drift when warm, since it then stabilises at a slightly different voltage. This effect is often sufficient to throw the set off tune when a different channel is selected. Another area that gives trouble on this chassis is the gated a.g.c. circuit. This is on the main signal board, alongside the i.f. unit. Operation of the circuit can become very critical when, as the set warms up, either of the transistors T171 (BC237A) or T172 (also BC237A) starts to break down, reducing the voltage at pin 3 of the i.f. strip so that overloading occurs. Under these conditions it's extremely difficult to tune the receiver to any station at all.

GEC C2002H

There's a dynamic convergence problem with this set. The colours are correct at the centre of the screen. The top left-hand side is all green however and the bottom red, the right-hand side being the same but with the colours reversed. The colouring tends to vary with the brightness.

The most likely cause of this would seem to be a defect associated with the horizontal R/G symmetry coil L905 on the convergence panel. There must be d.c. continuity, since the line scan current flows through this coil. Try setting it up, and if this fails fit a replacement.

THORN 3500 CHASSIS

The set will work perfectly for perhaps a few hours, then the cutout will operate. If this is reset, the set will again work satisfactory for a while but will eventually trip. This can happen several times in the course of an evening. A possible clue is that R609, which is in series with the chopper transistor, tends to burn out. The tripping continues after replacing this resistor. The cutout itself has been replaced, and everything else appears to be in order.

The cutout operates when the crowbar thyristor W621 fires, shorting R609 to chassis in the process. It seems therefore that there is repeated crowbar action. Suspects in this area are the crowbar thyristor W621, the sensing zener diode W617, and C618 (100 μ F) which is present in this circuit to suppress transients. Alternatively, the h.t. supply could be rising so that the trip operates. Disconnect the feedback amplifier by removing R621: this should give a

small picture, with the h.t. supply falling to about 30V. If the trip still operates, the chopper transistor is probably faulty. If the h.t. is rising due to the monostable being held on too long, check W615. Make sure the print around W621 is clean – the electrolytics tend to leak.

DECCA 30 SERIES

This Decca 30 series chassis is actually in a Telefunken model. The picture is very good once the set settles down after the first few minutes, but some odd things occur initially. After switching on, one usually gets to start with a very dark, diffused picture, mainly in blues and greens. Then the screen becomes almost entirely white, with very pale colours here and there. Eventually a vague picture is seen, then a hissing noise occurs accompanied by dark lines across the screen. Then the picture comes up much clearer.

It seems to us that the most likely cause of these symptoms is simply that either the PL509 or PY500 line output stage valve is lazy. Alternatively, it could be that the c.r.t. is loading the e.h.t. generator due to its being driven hard as a result of a fault on the decoder panel. This would show up as an abnormally low voltage on all three cathodes, and could be due to a faulty MC1327P demodulator/matrixing i.c. or a fault in the luminance emitter-follower (TR204) circuit.

CHECKING CAPACITORS

Reference is often made in your magazine to leaky capacitors. Can you advise on the equipment and method of checking this? What I do is to use a scope to trace the signal, then use a multimeter to check for open- and short-circuit capacitors when the scope indicates that a fault is present. Some capacitors check out o.k. however, though replacement produces an improvement. Other capacitors look as if they're defective but perform satisfactorily.

We cannot suggest any improvement upon your method of checking suspect capacitors. The only additional factor we tend to rely on is that some types of capacitor are more prone to failure than others. Other than this if in doubt, chuck it out.

ITT CVC8 CHASSIS

The trouble with this set is loss of colour. I managed to restore the colour by replacing the delay line driver transistor T29, using a BC107, but the colour went again after a couple of days. Using the correct BC171B transistor produced no results. The voltages seem to be correct, except for those at the output pins 1, 2 and 4 of the MC1327 i.c. These are 7.5-8V instead of 6V. I've changed the varicap diodes in the saturation control circuit, also C161 which couples the signal to the base of T29.

First check that the bistable transistors are working – the collector voltages of the two transistors (T36/37) should be 9-10V with a colour signal. Then check C165 which decouples the emitter of T29 and C162 which smooths its base bias. These are both 4.7 μ R tantalum electrolytics. There are three other capacitors of this type in the chroma amplifier circuit, C155, C153 and C151. All may need to be checked – observe correct polarity if any need to be replaced. The chroma amplifier transistors T27 and T28 are also suspect. Loss of colour is commonly due to faults in the burst/reference oscillator section, such as oscillator drift, but this would be betrayed by a rainbow pattern as the fault comes and goes. If necessary, check that the output from the ident stage is adequate – there should be 11V across C218 with a colour signal.

THORN 1500 CHASSIS

The problem with this set is wavy verticals, from the bottom to the top of the screen, slightly more noticeable on the right-hand side. There is no buzz on sound however.

In spite of the absence of hum, the main electrolytic block C88/91/101 could be faulty. Check its connections to the printed board before condemning it. A more likely suspect however is C102 which smooths the h.t. rail used by the line generator and sync circuits. Other suspects are C98 which decouples the line output valve's screen grid, C32 which smooths the video driver transistor's base bias, C56 and C58 which smooth the l.t. supplies, or possibly heater-cathode leakage in the PY801 boost diode.

TELEFUNKEN 634E

Recently, after the set has been switched on the picture appears first as a slot across the centre of the screen. The picture then "flicks", and during the next couple of minutes expands vertically. It never quite reaches the top and bottom of the screen however.

This set is in fact fitted with the Decca hybrid colour chassis, and consequently the same fault-finding approach is required. The most common culprit causing sluggish opening out of the field scan is simply the PL508 field output valve, which may be taking rather a long time to reach full emission. When this valve starts to fail, its cathode bias resistor R413 (560Ω) and screen grid feed resistor R415 (3.9kΩ) tend to cook, so these should also be checked. The PCF80 (triode section) which forms part of the field oscillator is usually reliable, though it's emission has been known to fall, giving similar results. Lack of height is commonly due to the resistors in the height control circuit changing value. Check R402 (820kΩ) and R405 (270kΩ).

PYE 691 CHASSIS

A band, approximately 1½ in. wide, passes through the picture. It varies in speed and direction, sometimes going from the top of the screen to the bottom, then changing direction. At other times it's almost stationary. The main smoothing block C306/315 has been changed and other capacitors in the smoothing section checked by substitution. Voltage checks show a slight variation in the voltage at the collector of the field output transistor VT27, in sympathy with the band. The verticals in the band bend to the left, but there's no change of colour. Both the line and field locking are good.

It could be tricky trying to find the source of this hum problem. As a start we suggest you double check the smoothing electrolytics, especially the 1,250μF ones (C307/313/308/309). If these are satisfactory, the inter-connecting plugs and the chassis bonding connections will have to be checked. Remember that the i.f. strip's l.t. smoothing capacitors are on the top of the i.f. panel itself.

THORN 1500 CHASSIS

The trouble is that the field hold cannot be held for any length of time before it drifts away again. I've tried a new PCL805 field timebase valve without success.

This sort of trouble is often due to the circuit between the anode of the output pentode section of the valve and the triode grid. There are two resistors (R101 and R102) that tend to change value. Check that they are still 18kΩ. If it's necessary to replace them, use 1W types. Then check the associated capacitors, particularly C75, since these can become leaky. Also check the sync separator's screen grid feed resistor R44 (47kΩ), again replacing if necessary with a 1W type.

BUSH TV300

When the set has not been in use for a while, a normal picture is obtained after switching on. This lasts for half an hour to an hour, then the white parts of the picture begin to streak to the right and eventually, even with the contrast control at minimum, the picture goes almost totally white. Try the set within three days and the streaking is still pretty bad: leave it a week or so and a normal picture is obtained again. The resistors and electrolytics in the video output and contrast control circuits have been checked, and the video output transistor TR10 changed, but the trouble persists. The voltage at the collector of the video output transistor is very low with the fault present.

The low collector voltage on TR10 is the key factor. The supply comes from the line output stage, and is smoothed by C519 and C520 (both 1μF). Every time we've come across these symptoms, one or other of these electrolytics has turned out to be responsible. It's possible that the rectifier concerned (D505), the filter resistor R515, or the discharge resistor R234 could be at fault however.

TELETON VX1110

The raster collapses, as though the set has been switched off, reappearing a few seconds later. This can happen two or three times, then the set will settle down with no further trouble. There's also intermittent loss of field hold, and poor field linearity (top elongated).

For the loss of e.h.t. (picture collapse), open the right side compartment flap to expose the 3AT2 e.h.t. rectifier and check with a neon tester — the neon should light up when brought near (not touching) the valve. You should also be able to see the glow of this valve's heater. If the neon remains alight when the picture goes off, see if the heater fades out. If it does, make sure that the e.h.t. is discharged and then remove the valve base to check the heater contacts and the 2.2Ω series resistor. If the neon goes out, check the line timebase valves and voltages. The line output valve is a 31JS6A and the boost diode a 17DW4A. The field trouble should respond to a new 17JZ8 field output valve. If necessary, check its cathode bias components and those in the linearity network.

PHILIPS 210 SERIES

There's an odd sound fault on this set. After switching on, the sound comes on at full volume, with a trace of hum, even with the volume control at minimum. After about half an hour however the conditions stabilise and the volume control operates normally.

The volume control is returned to chassis via a 2.5μF electrolytic capacitor (C1503). Either the volume control itself is defective, the capacitor is defective or improperly connected, or the earthing is not being made to chassis. Note that the positive side of C1503 goes to chassis, the negative side to the volume control.

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TELEVISION SEPT. 1979

TANDBERG CTV2

The original fault with this set was loss of raster, with the power supply module going into its "purring" mode. The cause was found to be a defective horizontal shift choke (L752), and replacing this restored the sound and picture. There are still a couple of faults however. First the picture is of reduced width, the width control R860 (in the EW modulator circuit) having no effect at all. The voltage at the supply end reads 30V instead of 25V. Secondly, although the 6.8V reference zener diode D975 in the switch-mode power supply control circuit has been changed (to cure picture size variations) the h.t. supply cannot be set any higher than 150V (should be 160V). The set h.t. control R976 can be used to reduce the h.t. below 150V however. Whilst checking around the circuit I noticed that the EW modulator diodes D750 and D751 seem to have been running hot, as the board is slightly scorched in the vicinity.

All your problems are likely to be resolved by replacing

the EW modulator diodes, plus the EW modulator output transistors Q853/852 if necessary. Also check whether the horizontal shift control R772 is burnt.

THORN 980 CHASSIS

The trouble with this set is very critical line hold, which has to be constantly adjusted – every three to four minutes. A new line oscillator valve has been tried but has not improved matters.

The fault could be in the flywheel line sync circuit, where the discriminator diodes W3/4 are the first suspects. A very likely possibility however is a fault in the video output stage. You will find a bias stabilising resistor (R26, 39k Ω , 1W) connected between the screen grid and the cathode of V5. This commonly falls in value, upsetting the bias conditions in the stage and therefore severely clipping the sync pulses. The sync separator's screen grid and anode load resistors would also be worth checking.

TEST CASE

201

Each month we provide an interesting case of television servicing to exercise your ingenuity. These are not trick questions but are based on actual practical faults.

An ASA Model CT6000 colour receiver had been working satisfactory for at least four years – with good sound and bright pictures – at a site within six miles visible range of a low-power transmitter. Being a worker with "unsociable hours", the owner decided to try out a video cassette recorder, and for the first week or so was happy with the results. The pictures were crisp and the colours accurate, both off-air (through the machine's "monitor" mode) and off-tape.

As the days went by however, the early morning viewer of the previous night's programmes became less enchanted. He found the recorded pictures getting less sharp, though the colour accuracy was unaffected. The distaff side started to complain that it was necessary to turn down the brightness and sometimes the contrast, and to darken the room, in order to achieve acceptable viewing from the set. It was discovered that the pictures could be improved by altering the position of the set-top aerial so that it was broadside on to the distant, though visible, transmitting aerial, whereas previously the best pictures had been obtained with the aerial pointing at the transmitter.

Since the colours remained accurate, the technician investigating the problem concluded that the e.h.t. tripler was at fault, especially after one or two measurements revealed that the focus potential at pin 1 of the tube was lower than normal even with the focus preset at maximum setting.

Unfortunately, tripler replacement failed to solve the

problem. The picture was still weak and not properly in focus at any point on the range of the preset focus control, though at full brightness setting the overall screen illumination was quite reasonable. Replacing the focus preset gave no improvement, and it was then concluded that video crushing was responsible. Detailed tests in the colour-difference and video amplifier stages failed to shed any light on the problem however.

What was the most likely cause of the trouble, and why was the fault seemingly aggravated by the use of a VCR? See next month for the solution and for a further item in the series.

SOLUTION TO TEST CASE 200

– page 550 last month –

It will be recalled that the Decca CTV25 mentioned in last month's test case was suffering from two faults, weak field sync and slight variations in height accompanied by an audible sizzle. The weak field sync was not a difficult problem to solve. The field sync pulses are applied to one of the control grids of the ECC82 cathode-coupled field multivibrator via an OA81 interlace diode (D301) whose cathode is biased by a potential divider consisting of a 3.3M Ω resistor (R302) connected to the h.t. rail and a 150k Ω resistor (R303) to chassis. With age, the higher-value resistor in the network tends to rise considerably in value, and the fault was completely cleared by replacing R302.

The field amplitude jitter was located less scientifically! Had it not been for the "reflected spark", diagnosis would have been more protracted. In the event, it was discovered that the spark was concentrated around the positive tag of the 400 μ F h.t. reservoir capacitor C2705 in the power pack. The tag had developed a high-resistance contact to its termination, and the result was a tendency to spark across due to the heavy ripple current. C2705 was still providing capacitance, but the ripple discharge was affecting the field scan more dramatically than any of the other sections of the receiver fed from the h.t. rail.

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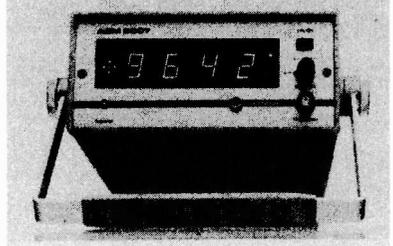
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AF117	28	BC107	11	BC149	11	BC238	11	BD115	36	BD234	45	BF183	28	BF274	13	BF490	20	MJE2955	76	TIP31	32	ZTX500	60
AF118	68	BC108	10	BC153	11	BC239	10	BD116	55	BD237	50	BF184	27	BF274	40	BF491	20	MJE3055	71	TIP32	36	ZTX500	10
AF125	36	BC109	11	BC154	11	BC237	12	BD131	37	BD238	50	BF185	27	BF276	27	BF492	20	OC28	2.10	TIP33	54	ZTX500	10
AF126	37	BC113	13	BC157	10	BC237	12	BD132	43	BD435	65	BF194	10	BF337	27	BF490	90	OC35	1.40	TIP34	58	ZTX500	10
AF127	37	BC114	13	BC158	09	BC237	12	BD133	39	BD437	45	BF195	09	BF338	27	BF490	33	OC36	1.16	TIP41	36	ZTX500	10
AF139	48	BC115	14	BC159	11	BC238	12	BD135	36	BD509	55	BF196	09	BF355	40	BF490	40	OC44	39	TIP42	37	ZTX500	11
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AF180	1.58	BC117	11	BC170B	70	BC461	27	BD140	39	BDX32	1.70	BF198	17	BF363	40	BU105/02	1.46	OC71	40	TIP112	85	ZTX500	53
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AA116	14	BA145	16	BY206	15
AA117	13	BA155	11	BY207	20
AA119	06	BA156	09	BY210/400	21
AA143	10	BA202	09	BY210/800	29
AA144	07	BA219	08	BY227	28
AY102	1.54	BA316	20	BY251	20
AY106	1.41	BA317	20	BY255	24
BA102	33	BAX13	04	BY298	40
				BY299	40

ZENER DIODES

part	price	part	price
IN4007	0.7	IN4148	0.3
IN4148	0.3	IN4448	1.7
IN4001	0.5	IN5401	1.3
IN4002	0.5	IN5404	1.5
IN4003	0.5	IN5408	1.6
IN4004	0.6	IT144	0.4
IN4005	0.7	ITT2002	1.3
IN4006	0.7		

INTEGRATED CIRCUITS

part	price	part	price	part	price
BRCM200	3.34	SN72733L	1.68	TBA651	2.97
BRCM300	3.42	SN76003N	1.40	TBA673	2.10
BRC1330	80	SN76013N	1.10	TBA690	2.80
BT1782	5.21	SN76013ND	1.05	TBA700	1.60
BT17810B	1.97	SN76023N	1.10	TBA720A	2.40
CS500	2.67	SN76023ND	1.05	TBA750	1.39
CA270AE	2.85	SN76033N	1.40	TBA800	1.06
CA270BI	2.70	SN76110N	1.60	TBA810A	1.38
CA505	1.30	SN76226ND	1.79	TBA810S	2.22
CA758E	3.40	SN76227N	1.08	TBA820	95
CA920AE	1.96	SN76228N	1.86	TBA890	1.94
CA2121	1.80	SN76530P	1.47	TBA920	2.20
CA3099E	3.40	SN76532N	1.38	TBA940	3.09
CA3090D	1.45	SN76533N	1.50	TBA950A	3.07
ET15016	2.10	SN76544N	1.40	TBA970	2.94
ET15016B	2.10	SN76546N	2.89	TBA990	1.65
LM1351	1.58	SN7666E	1.27	TBA1440C	3.33
LM1370	1.78	TA450A	1.89	TBA1441	3.33
MC1307P	1.69	TA450B	2.7	TC4270	1.95
MC1310P	1.11	TA450C	2.7	TC4270S	2.24
MC1527A	2.67	TA450D	2.7	TC4290A	3.23
MC1527P	1.20	TA4570	1.80	TC4420A	2.04
MC1330P	66	TA4591	1.98	TC4440	1.98
MC1349P	1.99	TA4618	2.48	TC4640	2.97
MC1351P	1.20	TA4619	3.40	TC4650	3.42
MC1352P	1.20	TA4618B	1.80	TC4730	3.32
MC1358P	1.20	TA4700	2.00	TC4950	2.43
MC1724CP	1.36	TBA231	1.29	TCA80K	2.20
ML237B	1.97	TBA240A	4.60	TCA820	2.27
SA4570	1.98	TBA325	1.57	TCA830S	2.13
SA4700	3.91	TBA395	1.85	TCA900	1.48
SA5605	1.75	TBA396	1.60	TCA910	1.48
SA5570S	1.75	TBA440C	3.33	TCA940	1.80
SA5580	2.25	TBA440N	3.33	TCE100P	3.54
SA5590	2.45	TBA480	1.10	TDA440	3.30
SA5660	3.41	TBA500	1.65	TDA440N	3.39
SA5670	3.41	TBA510	1.65	TDA1170	3.81
SC9503P	1.00	TBA520	1.95	TDA1142	1.10
SC9504P	1.45	TBA530	1.23	TDA2522	2.66
SC9506P	2.69	TBA540	1.40	TDA2530	2.20
SL437F	5.99	TBA550	1.80	TDA2560	2.15
SL9018	4.60	TBA560C	2.00	TDA2590	2.68
SL917B	5.95	TBA570	1.50	TDA2600	2.74
SL918A	4.56	TBA571A	1.65	TDA3950	2.57
SN16848N	1.99	TBA571B	2.70	TMS3889NC	4.37
SN16851N	1.99	TBA618X1	2.95	ZTK33A	72

EHT MULTIPLIER TRAYS

part	price	part	price	part	price
TCE1400 (5 Stick)	3.08	TCE3000 3500	5.55		
TCE1500 (3 Stick)	2.47	TCE4000	5.20		
TCE1500 (5 Stick)	3.08	TCE8000	2.76		
ITT CVC 5.7 B & 9	4.80	TCE9000	5.50		
ITT CVC 20.30	5.40	TCE9000	6.35		
GEC 2028 1040	4.80	RR1 Dual Standard CTV	6.50		
GEC 2110	4.80	RR1 A823	5.70		
GEC 2100	5.95	RR1 A823B	4.85		
GEC 2200	4.				

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5200pF	40p	8200pF	50p

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800mfd 300v.	GEC	175p
800mfd 300v.	A823	162p
800mfd 300v.	Z179	160p
800mfd 300v.	G9	160p
400mfd 350v.	8000	154p
470mfd 250v.	G11	132p
800mfd 250v.	G9	167p
200 + 300mfd 350v.	891	205p
300 + 300mfd 300v.	A640	190p
400 + 400mfd 350v.	Decca	280p
150 + 150 + 100mfd 300v.	1500	160p
175 + 100 + 100mfd 400/350v.	3500	204p
200 + 400 + 50mfd 325v.	A816	230p
200 + 200 + 150 + 50mfd 300v.	GEC	200p
300 + 300 + 100 + 32 + 32mfd 300v.	Z148	243p
300 + 300 + 300 + 150 + 100 + 50mfd 325v.	GEC	300p
1000mfd 63v.	3500	62p
2200mfd 63v.	G9	95p
1250mfd 50v.	169	60p
4700mfd 25v.	1590	73p
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A44-120W.....	18.75	2.19
A50-120W.....	18.75	2.34
A59-23W.....	17.95	2.24
A61-120W.....	18.95	2.37

U.S.A./JAP. TYPE Nos.

9AGP4.....	19.50	2.44
190AB4/C4.....	17.50	2.19
230ADB4.....	28.50	3.56
230DB4/CT468.....	24.00	3.00
240AB4A.....	17.95	2.24
CT507.....	17.95	2.24
CT512.....	27.50	3.44
310DGB4/DMB4.....	23.00	2.88
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A47-343X.....	69.50	8.89
A49-191X.....	59.50	7.44
A51-220X.....	64.00	8.00
A56-120X.....	69.50	8.89
A63-120X.....	69.50	8.89
A66-120X.....	75.00	9.37
A66-140X/410X.....	70.50	8.81
A67-120X.....	82.00	10.25
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LISTS S.A.E.

QUOTED PRICES INCLUDING 0% ALLOWANCE IN LIEU OF GUARANTEE ON EVA VALVES

IMMEDIATE POSTAL DESPATCH		LISTS S.A.E.		QUOTED PRICES INCLUDING 0% ALLOWANCE IN LIEU OF GUARANTEE ON EVA VALVES	
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DY86/7 78p	GY501 £1.68	PCF805 £1.83	PL84 63p	30P15 P.O.A.	
DY802 84p	PC86 99p	PCF808 £1.83	PL504 £1.57	6F23 63p	30PL14 £1.26
ECC81 78p	PC88 99p	PCH200 £1.31	PL508 £1.62	6F28 £1.05	30PL15 £1.15
ECC82/3 78p	PC97 84p	PCL82 £1.05	PL509 £3.15	20P4 73p	Also 3AT2,
ECL80 75p	PCC84 36p	PCL83 POA	PL802 £3.05	30C1 94p	17DW4A & 40KD6
EF80 69p	PCC89 78p	PCL84 £1.05	PY81/83 94p	30C17 78p	12HG7, 31JS6A
EF183 84p	PCC189 78p	PCL85 } £1.20	PY800 94p	30FL1 } £1.20	BY 100/127 etc.
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Production 30PL1 discontinued

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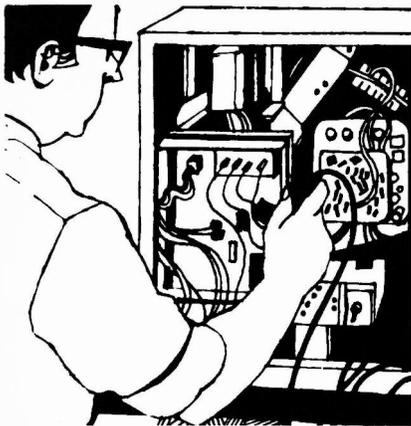
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19" £29.50 MONO 20" £30.50
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ANY 1-20p, 5-80p, 10-£1.25, 50-£5.50

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S/S Colour £30, Mono Push Button £3. Plus VAT. Phone Southend 559895. Any time.

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20AX and P.I.L. tube prices available on application.

Mono	Price
20"	£11.00
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Prices are based on a sound tube for tube exchange.

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Under five valves postage 6p each

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EB91	12p	PCC84	8p	PL36	20p
ECC82	10p	PCC85	20p	PL504	25p
ECL80	8p	PCC89	8p	PY32/33	15p
EF80	8p	PCC189	8p	PY81/800	15p
EF85	8p	PC805	15p	PY801	20p
EF183	10p	PCF80	8p	U191	15p
EF184	10p	PCF86	15p	6F23	15p
EH90	13p	PCF805	20p	6/30L2	15p
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 12 months guarantee
 Colour tubes supplied on a 'glass for glass' basis
 Callers ring to arrange to bring your glass for on the spot exchange from our stocks
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 Carriage costs per tube: Portable £1.00; Mono £3.00; Colour £4.00; incl. VAT

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A28-14W 11" (Pencil) £14	22" £28
A31-410W 12" £14	25" 28" £30
A31-120W 12" (Pencil) £14	26" 110" £34
A31-18W 12" £14	
A34-100W 14" (Pencil) £14	
A38-180W 15" (Pencil) £14	NEW MONO
A44-120WR 17" £14	A31/510 12" £17
A58-23W 23" £14	Replaces A31/120 Mullard
A50-120WR 20" £11	A31/410 2 year warranty
A61-120WR 24" £11	A34/510 14" £18.50
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 All tube prices subject to 15% VAT

No minimum order limit - you may order as you please
 Cash with order please - any excess refunded
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 SAE of enquiries please
 Immediate despatch
 Many more "V" series valves in stock
NEW VALVES

Type	Price	Type	Price	Type	Price
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DX802	85p	GH90	77p	PCC89	87p
OY88/7	80p	E124	61.84	PCC189	87p
PC84	53p	E184	62p	PCF80	85p
ECC82/2	85p	EY88/7	82p	PCF86	87p
ECC85	51p	EY80DA	£1.83	PCF200	£1.63
ECC88	74p	EZ80	61p	PCF802	85p
ECF80	87p	EZ81	61p	PCF805	£1.08
ECF82	87p	EZ80	61p	PCF806	71p
ECF84	51p	EZ81	61p	PCF808	£1.74
ECF88	74p	EY80DA	£1.83	PCF809	£1.83
ECL80	62p	KT86	£3.58	PCF809	£1.83
ECL82	62p	KT86	£3.58	PCF809	£1.83
ECL86	77p	PC86	77p	PL82	75p
ECF88	85p	PC88	77p	PL84	75p
EF80	41p	PC92	86p	PCL85/85	87p
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