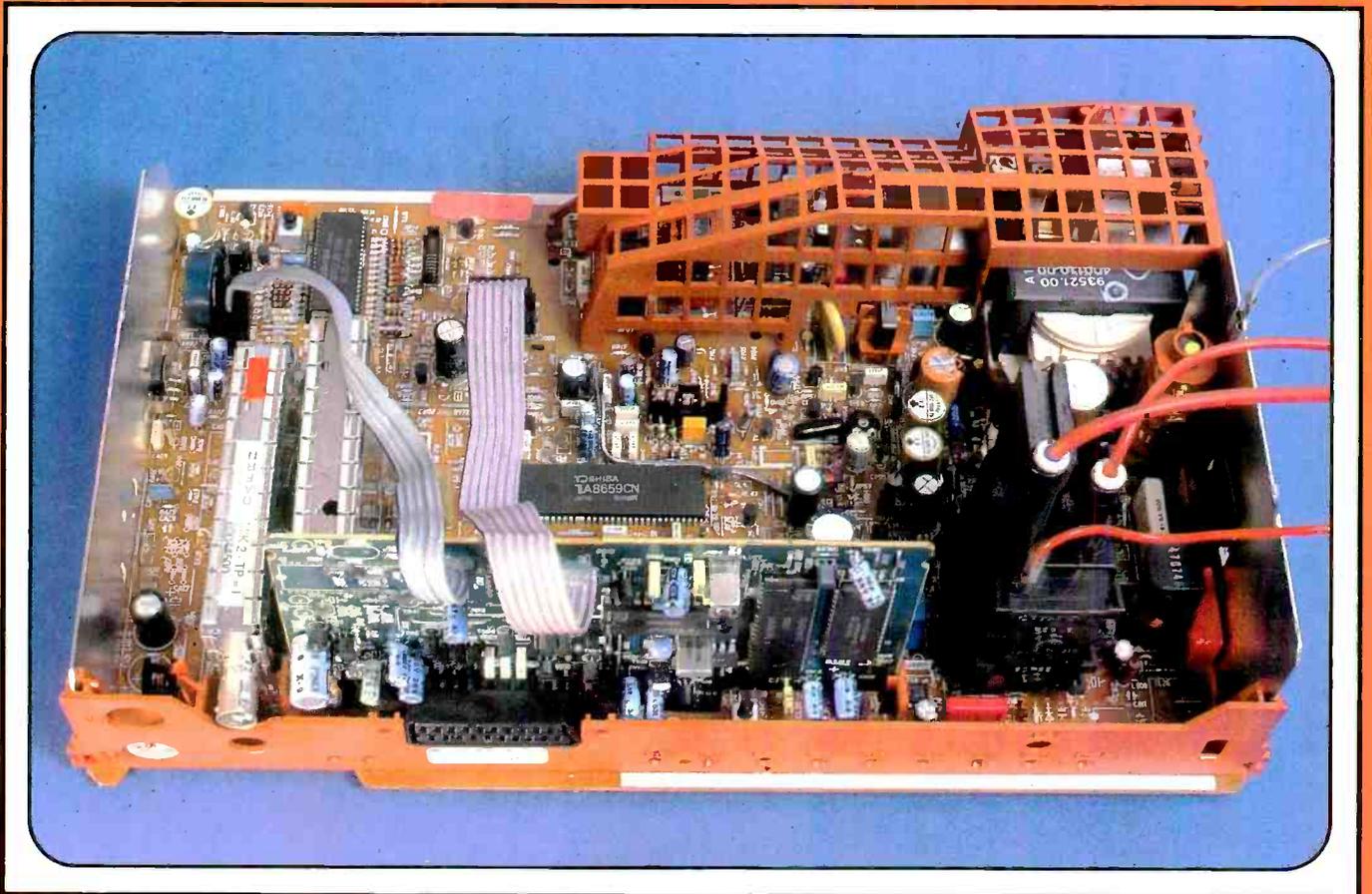


APRIL 1993

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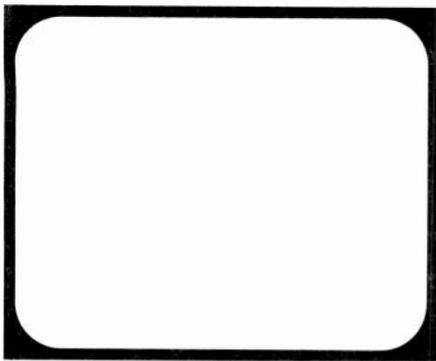


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APRIL
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Vol. 43, No.6
Issue 510

On sale March 17th

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BC108	8p	BD897	50p	R2010B	100p	2N6403	160p	EY87	70p	AN7146	210p	LA2101	270p	NE566	50p	STK4191	850p	STR44111	650p	TD62382	200p	TD43640	350p
BC109	8p	BD899	50p	S2800D	72p	3N143	65p	EY88	80p	AN7154	180p	LA2200	190p	NE565	110p	STK4192	800p	STR44115	650p	TD62506	200p	TD43651	200p
BC109C	10p	BD901	50p	S2800M	72p			PC91	100p	AN7156	240p	LA3160	120p	NE566	130p	STK4231H	950p	STR44117	700p	TD62705	250p	TD43652	500p
BC140	10p	BD912	50p	T2800T	72p			CC165	100p	AN7157	240p	LA3200	120p	NE567	130p	STK4231H	950p	STR44119	700p	TD62705	250p	TD43653	500p
BC141	20p	BDX32	100p	T2800M	72p			PCF80	100p	AN7178	270p	LA3210	65p	NE571	65p	STK4273	650p	STR50052	650p	TD6306P	350p	TD43654	150p
BC142	20p	BDX33	100p	TI29	15p			PCF801	110p	AN7222	180p	LA3220	100p	NE592	85p	STK4301	700p	STR50100	650p	TD6350P	500p	TD43710	320p
BC143	20p	BDX65	80p	TI29A	22p			PCF802	80p	AN7254	150p	LA3300	140p	NE532P	140p	STK4311	800p	STR5103A	300p	TD6359P	300p	TD43720	50p
BC147	20p	BDW23	50p	TI29B	25p			PCF803	150p	AN7255	150p	LA3301	140p	NE533	140p	STK4312	800p	STR5103B	300p	TD6360P	300p	TD43730	50p
BC148	8p	BDW24	55p	TI30	25p			PCH200	100p	AN7310	90p	LA3350	110p	SAA1005	400p	STK4352	640p	STR5011	650p	TD6A002	100p	TD43750	400p
BC149	8p	BDW93	50p	TI30C	30p			PCL81	65p	AN7311	90p	LA3361	100p	SAA1009	450p	STK4362	600p	STR51041	650p	TD6A003	100p	TD43760	470p
BC157	10p	BDW94	50p	TI31A	22p			PCL82	80p	AN7410	250p	LA3375	300p	SAA1010	450p	STK4372	570p	STR52041	650p	TD6A004	220p	TD43771	460p
BC159	30p	BF130	35p	TI31B	22p			PCL83	100p	AN7410	250p	LA3380	300p	SAA1011	450p	STK4373	570p	STR52042	650p	TD6A005	220p	TD43781	460p
BC160	30p	BF137	35p	TI32A	24p			PCL85	80p	AY3-1270	80p	LA4031	140p	SAA1025	500p	STK4432	600p	STR53041	650p	TD6A006	220p	TD43800	350p
BC171	10p	BF160	16p	TI32A	21p			PCL805	80p	AY3-1350	450p	LA4032	140p	SAA1961	400p	STK4733	900p	STR53043	650p	TD6A007	220p	TD43803A	500p
BC172	10p	BF180	16p	TI32B	21p			PFL200	110p	AY3-8910	360p	LA4051	160p	SAA1075	350p	STK4793	1100p	STR54041	400p	TD6A008	220p	TD43810	300p
BC177	14p	BF181	15p	TI32C	21p			PL30	120p	AY3-8912	400p	LA4100	85p	SAA1123	200p	STK4803	720p	STR55041	650p	TD6A009	220p	TD43820	300p
BC178	14p	BF183	20p	TI33C	60p			PL83	60p	BA3031	85p	LA4101	80p	SAA1123	400p	STK4813	450p	STR58041	400p	TD6A010	200p	TD43850	250p
BC179	14p	BF195	7p	TI33A	21p			PL84	80p	BA311	80p	LA4102	100p	SAA125	280p	STK4833	810p	STR59041	600p	TD6A011	200p	TD43860	400p
BC182	7p	BF199	8p	TI34C	60p			PL95	180p	BA313	60p	LA4110	120p	SAA1251	380p	STK4843	720p	STR6001	750p	TD6A012	350p	TD43870	250p
BC183	7p	BF203	15p	TI35A	25p			PL98	200p	BA315	100p	LA4112	120p	SAA127	280p	STK4853	720p	STR6002	750p	TD6A013	350p	TD43880	280p
BC183L	7p	BF225	30p	TI35C	65p			PL98	200p	BA302	150p	LA4120	270p	SAA1271	280p	STK4863	850p	STR6004	750p	TD6A014	350p	TD43890	280p
BC183L	7p	BF240	16p	TI41A	20p			PL99	220p	BA401	60p	LA4125	200p	SAA3004	400p	STK4873	900p	STRD1806	475p	TD6A015	320p	TD43920	400p
BC184	7p	BF245	25p	TI41B	22p			PV81	100p	BA402	60p	LA4126	240p	SAA5009	200p	STK4893	900p	STRD1816	475p	TD6A016	320p	TD43930	400p
BC184L	7p	BF254	25p	TI42A	22p			PV81	100p	BA403	60p	LA4127	240p	SAA5010	220p	STK4913	1180p	T2800	52p	TD6A017	320p	TD43940	350p
BC212	7p	BF255	12p	TI42C	22p			PV81	100p	BA404	60p	LA4130	200p	SAA5011	220p	STK4913	1180p	T2800	52p	TD6A018	320p	TD43950	350p
BC212L	7p	BF256	12p	TI47	40p			PV81	100p	BA405	60p	LA4131	200p	SAA5012	220p	STK4913	1180p	T2800	52p	TD6A019	320p	TD43960	350p
BC213	7p	BF257	12p	TI48	40p			QA30	10p	BA406	60p	LA4132	200p	SAA5013	220p	STK4913	1180p	T2800	52p	TD6A020	320p	TD43970	350p
BC213L	7p	BF258	12p	TI49	40p			QA91	10p	BA407	60p	LA4133	200p	SAA5014	220p	STK4913	1180p	T2800	52p	TD6A021	320p	TD43980	350p
BC214	7p	BF259	12p	TI50	40p			QA91	10p	BA408	60p	LA4134	200p	SAA5015	220p	STK4913	1180p	T2800	52p	TD6A022	320p	TD43990	350p
BC214L	7p	BF262	25p	TI52	120p			QA91	10p	BA409	60p	LA4135	200p	SAA5016	220p	STK4913	1180p	T2800	52p	TD6A023	320p	TD44000	350p
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BC238	7p	BF270	18p	TI54	140p			QA91	10p	BA411	60p	LA4137	200p	SAA5018	220p	STK4913	1180p	T2800	52p	TD6A025	320p	TD44020	350p
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BC300	20p	BF311	21p	TI106	65p			QA91	10p	BA413	60p	LA4139	200p	SAA5020	220p	STK4913	1180p	T2800	52p	TD6A027	320p	TD44040	350p
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BC302	20p	BF337	20p	TI110	40p			QA91	10p	BA415	60p	LA4141	200p	SAA5022	220p	STK4913	1180p	T2800	52p	TD6A029	320p	TD44060	350p
BC303	20p	BF338	20p	TI111	40p			QA91	10p	BA416	60p	LA4142	200p	SAA5023	220p	STK4913	1180p	T2800	52p	TD6A030	320p	TD44070	350p
BC304	20p	BF362	30p	TI112	40p			QA91	10p	BA417	60p	LA4143	200p	SAA5024	220p	STK4913	1180p	T2800	52p	TD6A031	320p	TD44080	350p
BC327	7p	BF367	13p	TI115	45p			QA91	10p	BA418	60p	LA4144	200p	SAA5025	220p	STK4913	1180p	T2800	52p	TD6A032	320p	TD44090	350p
BC328	7p	BF371	17p	TI116	45p			QA91	10p	BA419	60p	LA4145	200p	SAA5026	220p	STK4913	1180p	T2800	52p	TD6A033	320p	TD44100	350p
BC337	7p	BF381	17p	TI117	45p			QA91	10p	BA420	60p	LA4146	200p	SAA5027	220p	STK4913	1180p	T2800	52p	TD6A034	320p	TD44110	350p
BC338	7p	BF390	52p	TI120	37p			QA91	10p	BA421	60p	LA4147	200p	SAA5028	220p	STK4913	1180p	T2800	52p	TD6A035	320p	TD44120	350p
BC441	28p	BF491	99p	TI121	46p			QA91	10p	BA422	60p	LA4148	200p	SAA5029	220p	STK4913	1180p	T2800	52p	TD6A036	320p	TD44130	350p
BC446	8p	BF443	30p	TI122	47p			QA91	10p	BA423	60p	LA4149	200p	SAA5030	220p	STK4913	1180p	T2800	52p	TD6A037	320p	TD44140	350p
BC448	8p	BF452	30p	TI123	47p			QA91	10p	BA424	60p	LA4150	200p	SAA5031	220p	STK4913	1180p	T2800	52p	TD6A038	320p	TD44150	350p
BC461	28p	BF484	20p	TI126	56p			QA91	10p	BA425	60p	LA4151	200p	SAA5032	220p	STK4913	1180p	T2800	52p	TD6A039	320p	TD44160	350p
BC477	18p	BF485	20p	TI127	56p			QA91	10p	BA426	60p	LA4152	200p	SAA5033	220p	STK4913	1180p	T2800	52p	TD6A040	320p	TD44170	350p
BC478	18p	BF487	15p	TI130	30p			QA91	10p	BA427	60p	LA4153	200p	SAA5034	220p	STK4913	1180p	T2800	52p	TD6A041	320p	TD44180	350p
BC485	8p	BF490	15p	TI131	30p			QA91	10p	BA428	60p	LA4154	200p	SAA5035	220p	STK4913	1180p	T2800	52p	TD6A042	320p	TD44190	350p
BC537	25p	BF489	60p	TI141	90p			QA91	10p	BA429	60p	LA4155	200p	SAA5036	220p	STK4913	1180p	T2800	52p	TD6A043	320p	TD44200	350p
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UPC1377 200p	25A1210 120p	25C681 300p	25C1678 120p	25C2360 120p	25C2988 250p	25C3580 60p	25C3580 60p	25D 744 100p	25D 1409 170p	25K 234 350p	2772 150p	280ADMA 150p	280ADMA 150p
UPC1378 180p	25A1215 600p	25C683 120p	25C1683 100p	25C2361 150p	25C2996 60p	25C3586 100p	25C3586 100p	25D 745 100p	25D 1410 170p	25K 236 400p	2772 150p	280ADMA 150p	280ADMA 150p
UPC1382 110p	25A1216 100p	25C683 120p	25C1684 450p	25C2362 50p	25C2999 50p	25C3589 150p	25C3589 150p	25D 746 100p	25D 1411 170p	25K 238 130p	2772 150p	280ADMA 150p	280ADMA 150p
UPC1384 252p	25A1217 100p	25C710 200p	25C1685 60p	25C2365 50p	25C3001 1400p	25C3590 120p	25C3590 120p	25D 747 100p	25D 1412 350p	25K 240 100p	2772 150p	280ADMA 150p	280ADMA 150p
UPC1387 170p	25A1220 120p	25C711 50p	25C1729 90p	25C2366 6000p	25C3012 300p	25C3631 130p	25C3631 130p	25D 748 100p	25D 1413 360p	25K 242 300p	2772 150p	280ADMA 150p	280ADMA 150p
UPC1390 350p	25A1227A 300p	25C717 50p	25C1730 50p	25C2369 100p	25C3019 320p	25C3636 280p	25C3636 280p	25D 749 100p	25D 1414 360p	25K 244 400p	2772 150p	280ADMA 150p	280ADMA 150p
1403CA 650p	25A1241 200p	25C730 450p	25C1740 40p	25C2371 45p	25C3021 1250p	25C3641 600p	25C3641 600p	25D 750 100p	25D 1415 410p	25K 246 400p	2772 150p	280ADMA 150p	280ADMA 150p
1420CA 450p	25A1242 80p	25C732 70p	25C1741 45p	25C2373 210p	25C3025 50p	25C3657 400p	25C3657 400p	25D 751 100p	25D 1416 280p	25K 248 850p	2772 150p	280ADMA 150p	280ADMA 150p
1421CA 650p	25A1244 120p	25C733 25p	25C1742 45p	25C2375 70p	25C3026 550p	25C3669 600p	25C3669 600p	25D 752 100p	25D 1417 400p	25K 250 400p	2772 150p	280ADMA 150p	280ADMA 150p
1422CA 550p	25A1246 80p	25C735 40p	25C1743 45p	25C2379 45p	25C3030 750p	25C3688 120p	25C3688 120p	25D 753 100p	25D 1418 250p	25K 252 250p	2772 150p	280ADMA 150p	280ADMA 150p
UPC1504C 200p	25A1249 100p	25C736 40p	25C1744 45p	25C2381 110p	25C3039 140p	25C3699 200p	25C3699 200p	25D 754 100p	25D 1419 410p	25K 254 500p	2772 150p	280ADMA 150p	280ADMA 150p
UPC1505C 400p	25A1251 150p	25C739 150p	25C1745 45p	25C2383 120p	25C3048 120p	25C3718 280p	25C3718 280p	25D 755 100p	25D 1420 280p	25K 256 800p	2772 150p	280ADMA 150p	280ADMA 150p
1514CA 200p	25A1261 150p	25C739 150p	25C1746 40p	25C2385 40p	25C3059 110p	25C3739 150p	25C3739 150p	25D 756 100p	25D 1421 140p	25K 258 140p	2772 150p	280ADMA 150p	280ADMA 150p
1515CA 250p	25A1262 160p	25C741 200p	25C1747 40p	25C2387 50p	25C3071 250p	25C3769 200p	25C3769 200p	25D 757 100p	25D 1422 200p	25K 260 200p	2772 150p	280ADMA 150p	280ADMA 150p
UPC1520C 250p	25A1263 280p	25C742 150p	25C1748 1000p	25C2391 50p	25C3080 200p	25C3780 200p	25C3780 200p	25D 758 100p	25D 1423 300p	25K 262 300p	2772 150p	280ADMA 150p	280ADMA 150p
UPC1536C 500p	25A1264 200p	25C743 105p	25C1749 105p	25C2393 90p	25C3102 900p	25C3789 250p	25C3789 250p	25D 759 100p	25D 1424 200p	25K 264 200p	2772 150p	280ADMA 150p	280ADMA 150p
ZN473 100p	25A1265 280p	25C749 80p	25C1751 65p	25C2395 100p	25C3105 100p	25C3797 65p	25C3797 65p	25D 760 100p	25D 1425 140p	25K 266 120p	2772 150p	280ADMA 150p	280ADMA 150p
ZN474 100p	25A1283 60p	25C792 380p	25C1789 100p	25C2407 350p	25C3108 250p	25C3808 750p	25C3808 750p	25D 761 100p	25D 1426 60p	25K 268 450p	2772 150p	280ADMA 150p	280ADMA 150p
ZN475 250p	25A1284 60p	25C809 225p	25C1809 40p	25C2410 350p	25C3109 350p	25C3815 150p	25C3815 150p	25D 762 100p	25D 1427 450p	25K 270 50p	2772 150p	280ADMA 150p	280ADMA 150p
ZN476 560p	25A1285 60p	25C809 225p	25C1810 40p	25C2411 350p	25C3110 350p	25C3822 150p	25C3822 150p	25D 763 100p	25D 1428 450p	25K 272 400p	2772 150p	280ADMA 150p	280ADMA 150p
ZN477 250p	25A1286 60p	25C828 25p	25C1815 15p	25C2412 350p	25C3111 350p	25C3829 450p	25C3829 450p	25D 764 100p	25D 1429 410p	25K 274 400p	2772 150p	280ADMA 150p	280ADMA 150p
ZN478 510p	25A1287 60p	25C828 25p	25C1816 140p	25C2413 350p	25C3112 350p	25C3836 280p	25C3836 280p	25D 765 100p	25D 1430 280p	25K 276 400p	2772 150p	280ADMA 150p	280ADMA 150p
ZN479 190p	25A1288 60p	25C828 25p	25C1817 140p	25C2414 350p	25C3113 350p	25C3843 280p	25C3843 280p	25D 766 100p	25D 1431 200p	25K 278 400p	2772 150p	280ADMA 150p	280ADMA 150p
ZN480 640p	25A1289 60p	25C828 25p	25C1818 140p	25C2415 350p	25C3114 350p	25C3850 280p	25C3850 280p	25D 767 100p	25D 1432 200p	25K 280 400p	2772 150p	280ADMA 150p	280ADMA 150p
ZN481 2150p	25A1290 60p	25C828 25p	25C1819 140p	25C2416 350p	25C3115 350p	25C3857 280p	25C3857 280p	25D 768 100p	25D 1433 200p	25K 282 400p	2772 150p	280ADMA 150p	280ADMA 150p
ZN482 1250p	25A1291 60p	25C828 25p	25C1820 140p	25C2417 350p	25C3116 350p	25C3864 280p	25C3864 280p	25D 769 100p	25D 1434 200p	25K 284 400p	2772 150p	280ADMA 150p	280ADMA 150p
JAPANESE TRANSISTORS													
25A10F 35p	25A1353 100p	25C1001 950p	25C1821 210p	25C2418 100p	25C3117 120p	25C3871 80p	25C3871 80p	25D 770 100p	25D 1435 250p	25K 286 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10H 60p	25A1354 100p	25C1001 950p	25C1822 210p	25C2419 100p	25C3118 120p	25C3882 200p	25C3882 200p	25D 771 100p	25D 1436 250p	25K 288 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10J 120p	25A1355 130p	25C1010 225p	25C1904 125p	25C2420 100p	25C3119 100p	25C3891 220p	25C3891 220p	25D 772 100p	25D 1437 250p	25K 290 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10K 150p	25A1356 100p	25C1012 75p	25C1906 30p	25C2421 100p	25C3120 100p	25C3901 250p	25C3901 250p	25D 773 100p	25D 1438 250p	25K 292 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10L 150p	25A1357 100p	25C1013 170p	25C1907 75p	25C2422 100p	25C3121 100p	25C3908 250p	25C3908 250p	25D 774 100p	25D 1439 250p	25K 294 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10M 150p	25A1358 100p	25C1014 170p	25C1908 75p	25C2423 100p	25C3122 100p	25C3915 250p	25C3915 250p	25D 775 100p	25D 1440 250p	25K 296 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10N 150p	25A1359 100p	25C1015 170p	25C1909 75p	25C2424 100p	25C3123 100p	25C3922 250p	25C3922 250p	25D 776 100p	25D 1441 250p	25K 298 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10P 150p	25A1360 100p	25C1016 170p	25C1910 75p	25C2425 100p	25C3124 100p	25C3929 250p	25C3929 250p	25D 777 100p	25D 1442 250p	25K 300 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10Q 150p	25A1361 100p	25C1017 170p	25C1911 75p	25C2426 100p	25C3125 100p	25C3936 250p	25C3936 250p	25D 778 100p	25D 1443 250p	25K 302 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10R 150p	25A1362 100p	25C1018 170p	25C1912 60p	25C2427 100p	25C3126 100p	25C3943 250p	25C3943 250p	25D 779 100p	25D 1444 250p	25K 304 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10S 150p	25A1363 100p	25C1019 170p	25C1913 190p	25C2428 100p	25C3127 100p	25C3950 250p	25C3950 250p	25D 780 100p	25D 1445 250p	25K 306 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10T 150p	25A1364 100p	25C1020 170p	25C1914 190p	25C2429 100p	25C3128 100p	25C3957 250p	25C3957 250p	25D 781 100p	25D 1446 250p	25K 308 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10U 150p	25A1365 100p	25C1021 170p	25C1915 190p	25C2430 100p	25C3129 100p	25C3964 250p	25C3964 250p	25D 782 100p	25D 1447 250p	25K 310 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10V 150p	25A1366 100p	25C1022 170p	25C1916 190p	25C2431 100p	25C3130 100p	25C3971 250p	25C3971 250p	25D 783 100p	25D 1448 250p	25K 312 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10W 150p	25A1367 100p	25C1023 170p	25C1917 190p	25C2432 100p	25C3131 100p	25C3978 250p	25C3978 250p	25D 784 100p	25D 1449 250p	25K 314 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10X 150p	25A1368 100p	25C1024 170p	25C1918 190p	25C2433 100p	25C3132 100p	25C3985 250p	25C3985 250p	25D 785 100p	25D 1450 250p	25K 316 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10Y 150p	25A1369 100p	25C1025 170p	25C1919 190p	25C2434 100p	25C3133 100p	25C3992 250p	25C3992 250p	25D 786 100p	25D 1451 250p	25K 318 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A10Z 150p	25A1370 100p	25C1026 170p	25C1920 190p	25C2435 100p	25C3134 100p	25C3999 250p	25C3999 250p	25D 787 100p	25D 1452 250p	25K 320 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A11 150p	25A1371 100p	25C1027 170p	25C1921 60p	25C2436 100p	25C3135 100p	25C4006 100p	25C4006 100p	25D 788 100p	25D 1453 250p	25K 322 400p	2772 150p	280ADMA 150p	280ADMA 150p
25A11A 150p	25A1372 100p												

SONY FLYBACK TRANSFORMERS

Table with columns: Part No, Models, Price. Lists various Sony flyback transformer models and their prices.

FLYBACK TRANSFORMERS

Table with columns: Model, Price. Lists various flyback transformer models and their prices.

GRUNDIG

Table with columns: Model, Price. Lists Grundig transformer models and prices.

PHILIPS

Table with columns: Model, Price. Lists Philips transformer models and prices.

ITT

Table with columns: Model, Price. Lists ITT transformer models and prices.

HITACHI

Table with columns: Model, Price. Lists Hitachi transformer models and prices.

OUTPUT TV MODULE

Table with columns: Model, Price. Lists output TV module models and prices.

IDLERS & PULLEYS REPLACEMENTS

Table with columns: Model, Price. Lists various idler and pulley replacement parts and their prices.

AMSTRAD

Table with columns: Model, Price. Lists Amstrad transformer models and prices.

FERGUSON

Table with columns: Model, Price. Lists Ferguson transformer models and prices.

FISHER

Table with columns: Model, Price. Lists Fisher transformer models and prices.

GOLDSTAR

Table with columns: Model, Price. Lists Goldstar transformer models and prices.

HINARI

Table with columns: Model, Price. Lists Hinari transformer models and prices.

HITACHI

Table with columns: Model, Price. Lists Hitachi transformer models and prices.

HITACHI TV

Table with columns: Model, Price. Lists Hitachi TV transformer models and prices.

JVC

Table with columns: Model, Price. Lists JVC transformer models and prices.

MATSU

Table with columns: Model, Price. Lists Matsushita transformer models and prices.

MITSUBISHI

Table with columns: Model, Price. Lists Mitsubishi transformer models and prices.

MITSUBISHI Cont.

Table with columns: Model, Price. Lists Mitsubishi transformer models and prices.

NEC

Table with columns: Model, Price. Lists NEC transformer models and prices.

NATIONAL

Table with columns: Model, Price. Lists National transformer models and prices.

ORION

Table with columns: Model, Price. Lists Orion transformer models and prices.

SAISHO

Table with columns: Model, Price. Lists Saisho transformer models and prices.

SANYO

Table with columns: Model, Price. Lists Sanyo transformer models and prices.

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Table with columns: Model, Price. Lists Sharp transformer models and prices.

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HR0455/HR0725
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HR0170/180/210/230/300/320/370/400/430/530/700/750
HR55000
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HR7200/7300/7350
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HRD110/111/120/121/225
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HR7600/7610/7650/7655
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HRD110/111/120/121/225
Contents
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Order Code: SK35 £10.50

Economy Kit Contents
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3V29/3V30
HR7200/7300/7350
Contents
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Order Code: SK31 £11.50

Economy Kit Contents
BELT SET, T/U REEL IDLER TYRE, SUPPLY REEL TABLE TYRE, PINCH ROLLER, REEL IDLER TYRE, T/U IDLER TYRE, T/U CLUTCH
Order Code: SK32 £5.60

3V44/45/48/53/54/55/57
HRP50/HRD140/150/158/160
HRD250/257/565/566/755
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FISHER

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Economy Kit Contents
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Order Code: SK58 £5.00

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Economy Kit Contents
BELT SET, PINCH ROLLER, IDLER TYRE
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HITACHI

VT11/VT33
Contents
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VT11/33
Contents
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Order Code: SK45 £15.00

Economy Kit Contents
BELT SET, PINCH ROLLER, FF/REW IDLER TYRE, T/U REEL TABLE TYRE, SUPPLY REEL TABLE TYRE
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VIDEO SERVICE KITS (Cont.)

HITACHI

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Economy Kit Contents
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Order Code: SK50 £3.25

VT400/405/410/13/14/15/18/420/25/26/28/430/31/35/38/450/498/510/520/225/26/530/35/36/540/545/46/48/570/75/576/580/85/88
Contents
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Order Code: SK52 £11.50

VT100/110/111/113/115/118/120/125/128/130/135/138/145/150/175/220/225/250/255/258/260/VT130
Contents
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PANASONIC

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Contents
BELT SET, PINCH ROLLER, TENSION BAND, IDLER TYRES
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Economy Kit Contents
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Economy Kit Contents
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NVG7/NVG9/NVG10/NVG11/NVG12/NVG14/NVG15/NVG16/NVG18/NVG30/NVG120/NVG130/NVG400/NVH65 (PK/AC)/AG1810 (PK/K)
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Order Code: SK27 £9.50

Economy Kit Contents
LOADING BELT, CAPSTAN, BELT, PINCH ROLLER, IDLER TYRE
Order Code: SK28 £4.50

NV332
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Order Code: SK29 £13.00

Economy Kit Contents
BELT SET, PINCH ROLLER, PLAY IDLER TYRE, FF/REW IDLER TYRE
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NV230/250/260/280/430/450/460/470/650/810/89C
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Economy Kit Contents
BELT SET, PINCH ROLLER, IDLER TYRE
Order Code: SK18 £4.00

VIDEO SERVICE KITS (Cont.)

SHARP

VC381
Contents
BELT SET, PINCH ROLLER, REEL IDLER, TENSION BAND, VIDEO LAMP
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STK7358	£4.40		

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HR7300, HR7600, HR7610,
HR7650, HR7655

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340, 503, 640, 5030

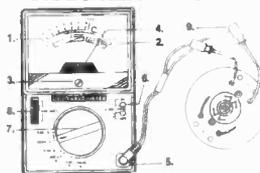
MITSUBISHI VIDEO HEAD £18.00
HS303, 304, 320, 700
HS306, 318, 710
HS300, 301, 302, 310 £17.00
HS337, 347 £20.00

PHILIPS

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6470, 6561, 6670, 6760, 6761, 6870, 6970

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VR6291, VR6293, VR6362, VR6367, VR6390, VR6391,
VR6393, VR6467, VR6468, VR6470, VR6561, VR6570,
VR6571, VR6670, VR6671, VR6760, VR6761, VR6762,
VR6870, VR6970, VR6975, VR8681, 63S87, 68S84,
71S87, 72S88, 92S831

VIDEO HEAD TESTER



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- Pointer Adjusting Screw
- Pointer
- Measuring Socket
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NATIONAL NV8050, NV8051	2800P
N.E.C. DX2000 DS6000	3400P 3500P
SAMSUNG VM1560, VN1561	2200P
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IC TRANSISTORS

M491BB1	500P
SAAS243PE	800P
TIP112H	50P
UPC1488H	150P
STR4090A	650P

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AKAI RC-V10A RCV37B V25A	1000P 1000P 1000P
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DECCA RC70	850P
FISHER RC905B	1000P
GRANADA/REDIFFUSION UNIVERSAL, 79500C, 986700	850P
SATELLITE MK4 TEXT, 70115G, 70133G, 70357E MK4A TEXT, 70375C 95288E 94490D	1000P 850P 850P 1000P 1000P

GRUNDIG TP160E TP200, TP300 TP400 TP590-600 TP390, TP610 TP621 TP630, TP650 TP660 TP661	1050P 1000P 850P 1050P 1050P 1050P 1000P 1050P 1050P
HITACHI CLE800-CLE830 A617402/655602 A512120/230 A514790 A5088470 A518612 SCL002 C2096 A511940 655602H	900P 1000P 1000P 1000P 1000P 1000P 1000P 1000P 1000P
ITT IFB13, 14, 15 FS4 RG305 RG306 FS9/1-10/1 VS5 RUK VS4-1 MULTICONTROL (17C20)	900P 850P 900P 900P 900P 900P 900P 1000P
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SABA T6772 TC319-320 TC356 TC358 TC360 TC365	1000P 1050P 1050P 1050P 1000P 1000P
SALORA SERIES L 86173	1000P 1000P
SANYO RC218, RC222, RC228, RC238 JXGE JXDE VHR2300 RC628	900P 1000P 1000P 1000P 1000P

SHARP G0121CESA, 123CESA, 204, 251	900P
SIEMENS FC616 FC631 FC742	1000P 1000P 1000P
SONY RM604, RM605, RM606 32 CHANNEL RM613 RM632, RM636	900P 900P 900P 900P
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SL1430	1.95
SL1431	2.50
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STK4332	5.95
STK5331	4.50
STK5332	4.50
STK5333	4.50
STK5421	4.50
STK5422	4.95
STK5467	12.50
STK5471	8.75
STK5481	5.95
STK5482	4.95
STK5490	7.95
STK5730	4.95
STK7308	5.50
STR4211	5.50
STR5412	4.95
STR4090	8.95
STR50020	7.95
STR5103A	5.50
STR54041	9.95
STR55041	6.95
STR58041	6.95
STR59041	8.50
STR6020 (KIT)	5.95
TDA1035T	2.50
TDA1044	1.95
TDA1170S	1.95
TDA1510	1.95
TDA1515	3.50
TDA1670A	3.95
TDA1770A	3.95

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FERGUSON TX90 14"	23.95
FERGUSON TX90 20"	17.50
FERGUSON TX95	22.95
FERGUSON TX100 90D	18.95
FERGUSON TX100 110D	17.25
FERGUSON TX100 FST	20.75
FIDELITY ZX2000 + MOD	15.50
FIDELITY ZX3000	14.95
FIDELITY ZX 22"/26"	18.95
FINLUX 1000 SERIES	19.95
HINARI CT4/5	18.25
HITACHI CPT1174	18.95
HITACHI CPT1446/2028	19.25
HITACHI CPT2174/78/78	18.95
ITT COMPACT FS1	20.50
ITT CV1100	19.20
ITT CV1200/1	19.95
ITT MONOPRINT A	18.25
ITT MONOPRINT B	23.85
MATSUI 1410/20/40	18.95
MATSUI C1480A	24.95
MATSUI CF1	23.50
PHILIPS CP90	22.95
PHILIPS CTX14"/20"	21.50
PHILIPS K40	23.75
PHILIPS 2A	23.50
SAISHO CT141R/RA	18.50
SHARP CT1410	24.95

SERVICE MANUALS

AMSTRAD 4600	9.95
AMSTRAD 6000	9.95
FERGUSON TX65	9.95
FERGUSON 3V55	11.95
FERGUSON 3V58	11.95
FERGUSON 3V59	11.95
FERGUSON 3V65	11.95
FERGUSON FV11	9.95
FERGUSON FV12	9.95
FERGUSON FV20	9.95
FERGUSON FV32	9.95
FIDELITY AVS1600	7.95
FIDELITY AVS2000	14.95
FIDELITY CTV14R	7.95
PANASONIC NV370	14.95
PANASONIC NV300	24.50
PANASONIC NV870	25.95
PANASONIC NVGT	24.95
PANASONIC NVG10	24.95
PANASONIC NVG12	17.50
PANASONIC NVG40	17.95
PANASONIC NVL25	16.95
PANASONIC TX1	9.95
PANASONIC TX3	9.95
PANASONIC TX24A1	9.95
PHILIPS KT4/40	9.95

TX90/100 STANDARD

TX90/100 STANDARD	1.50
TX90/100 REMOTE	1.75

EXTENDED RANGE OF VIDEO & AUDIO HEADS RING OR WRITE FOR DETAIL

TRANSISTORS

BC307	10
BC327	10
BC337	10
BC547	10
BC548	10
BC639	20
BC640	20
BD238	40
BF458	35
BF460	35
BF461	35
BU208A	70
BU208	1.45
BU208D	1.95
BU280	3.30
BU246A	1.45
BU250A	2.00
BU508A	1.50
BU508AF	1.95
BU508D	1.95
BU508DF	2.50
BU509V	2.75
BU526	1.95
BU536	2.25
BU807	1.75
BU908	2.95
BUK44/5008	3.30
BU11AF	2.75
BU112A	1.50
BU156A	2.75
BUX84	80
R4050	2.95
R4051	2.50
T9053V	3.50
T9054V	3.95
T9064V	3.95
TIP22E (TO189V)	75
TIP42C	50
TIP42C	50
TIP12H (TO167V)	1.95
TIP1791A	7.95
KT3 REMOTE	1.75
KT4/CTX REMOTE	1.75
SAISHO FST2130	9.95
SOLARA PCB REMOTE	9.95
SONY KV1612 REMOTE	3.95
SONY KV2022 REMOTE	5.95
TATUNG 140	2.50
TATUNG 161	1.50
TATUNG 165 REMOTE	1.75
THORN UNIVERSAL	1.00
TX910 STANDARD	1.00
TX910 REMOTE	1.75

WE ALSO SUPPLY
MANUALS FOR:
NEC, NIKKAI, SAISHO &
SHARP
PLEASE RING FOR
PRICES

SWITCHES

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FIDELITY CTV140	1.50
FIDELITY CTV14R	3.95
FIDELITY CTV14S	3.95
GRUNDIG CUC731	3.50
G11 STANDARD	1.35
G11 REMOTE	1.75
ITT TX SERIES	4.95
MATSUI 2190	5.95
KT3 REMOTE	1.75
KT4/CTX REMOTE	1.75
SAISHO FST2130	9.95
SOLARA PCB REMOTE	9.95
SONY KV1612 REMOTE	3.95
SONY KV2022 REMOTE	5.95
TATUNG 140	2.50
TATUNG 161	1.50
TATUNG 165 REMOTE	1.75
THORN UNIVERSAL	1.00
TX910 STANDARD	1.00
TX910 REMOTE	1.75

GENUINE PANASONIC L.O.P.T'S

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PANASONIC TC2031	53.50
PANASONIC TC2033	53.50
PANASONIC TC2051	43.50
PANASONIC TC2061	43.50
PANASONIC TC2243	53.50
PANASONIC TC2263	43.50
PANASONIC TX1642	53.50
PANASONIC TX1752	43.50
PANASONIC TX2034	53.50
PANASONIC TX2044	53.50
PANASONIC TX2122	43.50
PANASONIC TX2162	43.50
PANASONIC TX2461	39.50
PANASONIC TX3	43.50
PANASONIC TX3000	53.50
PANASONIC TXC22	43.50

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SONY & SHARP LOPTS
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EXTENSIVE RANGE OF
NEW
MICROPROCESSORS
NOW AVAILABLE
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DETAILS

AKAI VIDEO SPARES

VS1/5	
BELT KIT	1.95
PINCH ROLLER	3.95
REEL IDLER UNIT	6.95
TAKE UP CLUTCH	8.95
TENSION BAND	2.95
VIDEO HEAD VS1/5	17.95
VIDEO HEAD VS4	34.50

ALBA VIDEO SPARES

VCR4000	
BELT KIT	1.95
CAPACITOR BACK-UP	1.85
PINCH ROLLER	3.95
REEL IDLER	3.95
REEL PULLEY	1.95
REPAIR KIT	11.50
TENSION BAND	2.50
VIDEO HEAD	16.95
VCR5000	
BELT KIT	1.95
PINCH ROLLER	3.95
REEL IDLER	3.95
REEL PULLEY	1.95
TENSION BAND	2.50
VIDEO HEAD	16.95
VCR6000	
BELT KIT	1.95
CLUTCH ASSEMBLY	4.50
PINCH ROLLER	3.95
REEL IDLER	4.50
REPAIR KIT	12.95
TENSION BAND	2.50
VIDEO HEAD	17.95

AMSTRAD VIDEO SPARES

VCR4500	
BELT KIT	1.95
GEAR ASSEMBLY	9.95
MODIFICATION KIT	6.50
PINCH ROLLER	3.50
VIDEO HEAD	14.95
VCR4600BELT KIT	1.95
GEAR ASSEMBLY	9.95
MODIFICATION KIT	6.50
PINCH ROLLER	3.50
VIDEO HEAD	14.50
VCR7000	
BELT KIT	1.95
LAMP	95
PINCH ROLLER	3.95
REEL IDLER	3.95
REEL MOTOR	14.95
VIDEO HEAD	15.25
VCR6000	
BELT KIT	1.95
PINCH ROLLER	3.95
VIDEO HEAD	17.95

FERGUSON VIDEO SPARES

3V29/30	
BELT KIT	1.95
CAPSTAN MOTOR	32.50
CASSETTE LAMP	70
LOADING BELTS (5)	1.95
PINCH ROLLER	3.95
REPAIR KIT	12.95
REEL IDLER	12.95
TAKE UP CLUTCH	2.95
TAKE UP IDLER	1.95
VIDEO HEAD	8.75
3V35/39	
BELT KIT	1.95
CAPSTAN MOTOR	31.95
CASSETTE HOUSING	25.95
LOADING BELTS (5)	1.95
MAINS TRANSFORMER	23.95
PINCH ROLLER	3.95
REEL IDLER	3.95
REPAIR KIT	12.95
TAKE UP IDLER	1.95
TAKE UP CLUTCH	2.95
VIDEO HEAD	8.75
3V44/45	
BELT KIT	1.50
CASSETTE HOUSING	25.95
PINCH ROLLER	3.95
REPAIR KIT	15.95
VIDEO HEAD	19.50
3V65/FV11	
BELT KIT	1.75
CAPSTAN MOTOR	27.50
CASSETTE HOUSING	29.95
PINCH ROLLER	3.95
REEL IDLER	2.75
REPAIR KIT	11.95
VIDEO HEAD	17.95

FISHER VIDEO SPARES

FVH5000	
BELT KIT	2.20
REEL IDLER	5.50
PINCH ROLLER	3.50
TENSION BAND	2.60
VIDEO HEAD	24.50
FVH615/720	
BELT KIT	1.95
CLUTCH ASSEMBLY	5.95
PINCH ROLLER	4.50
REEL IDLER	5.95
VIDEO HEAD	15.95
FVH905/910	
BELT KIT	1.95
CLUTCH ASSEMBLY	19.95
REEL IDLER	5.95
VIDEO HEAD	15.95

HITACHI VIDEO SPARES

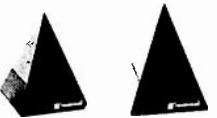
VT8000/8700E	
BELT KIT	1.95
CAPSTAN MOTOR	38.50
FF/REW IDLER	2.95
FF/REW PULLEY	95
PINCH ROLLER	3.95
PLAY IDLER	3.95
REEL IDLER	3.95
TENSION BAND	3.95
VIDEO HEAD	15.70
VT9300/9700E	
BELT KIT	1.95
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FF/REW PULLEY	95
PINCH ROLLER	3.95
PLAY IDLER	3.95
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TENSION BAND	1.95
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AUDIO HEAD VT33E	14.95
BELT KIT	1.95
CAPSTAN MOTOR VT11E	23.95
CAPSTAN MOTOR VT33E	23.95
CASSETTE HOUSING	16.50
CLUTCH ASSEMBLY	7.95
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PINCH ROLLER	3.95
REPAIR KIT	15.95
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TENSION BAND	2.95
VIDEO HEAD	15.70
VT63/64E	
BELT KIT	1.95
CAPSTAN MOTOR	27.50
CASSETTE HOUSING	14.70
CLUTCH ASSEMBLY	7.95
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PINCH ROLLER	3.95
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TENSION BAND	2.50
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VIDEO HEAD VT65	28.50
VT120/130E	
BELT KIT	1.95



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PREPROGRAMMED REMOTE CONTROLS 5 INDIVIDUAL APPLIANCES TV, VCR & SATELLITE ETC. 24.95



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CREDIT CARD SIZE 9.95
WORKS MOST PHILIPS SETS
BASIC FUNCTIONS
ENGINEERS MUST



POWERMID
NO WIRES, JUST PLUG IN AND TRANSMIT BY YOUR REMOTE CONTROL TO ANY ROOM IN YOUR HOUSE! 44.95

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FERGUSON T789.....	13.95
FAST TEXT.....	13.95

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FERGUSON 3V55.....	15.30
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FIDELITY CT V22T.....	14.95
FIDELITY CT V2210.....	12.95
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FISHER FTS 6310TX.....	22.95
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PANASONIC TX2482/92.....	21.50
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PANASONIC NV430.....	31.50
GENUINE.....	31.50
PANASONIC NV730.....	15.25
PANASONIC NV870.....	28.95
GENUINE.....	28.95
PANASONIC NVG10.....	28.95
GENUINE.....	28.95
PANASONIC NVG12.....	26.95
GENUINE.....	26.95
PANASONIC NVG16.....	31.50
GENUINE.....	23.45
PANASONIC NVG21.....	23.45
GENUINE.....	23.45
PANASONIC NVG40.....	29.95
GENUINE.....	29.95
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PANASONIC NV230.....	17.50
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PANASONIC NV366.....	19.95
PANASONIC NV370.....	9.95
PANASONIC NV430.....	14.25
PANASONIC NV688.....	27.70
PANASONIC NV730.....	18.95
PANASONIC NV777.....	18.95
PANASONIC NV788.....	25.95
PANASONIC NV870.....	37.30
PANASONIC NV2000/7000.....	8.95
PANASONIC NVG7.9.....	17.30
PANASONIC NVG10/12.....	17.30
PANASONIC NVG18.....	28.70
PANASONIC NVG20/21.....	24.95
PANASONIC NVG30/40.....	24.50
PANASONIC NVG45.....	34.50
PANASONIC NVL25.....	38.50
PHILIPS VR6185.....	42.50
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PHILIPS 6760 GENUINE.....	41.70
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PYE DV468.....	40.70
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SAISHO VR6367.....	17.50
SAISHO VR3600.....	19.50
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SENTRA 8400.....	16.95
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SHARP VC9300/381/481.....	14.75
SHARP VC581/681.....	14.75
SHARP VC787.....	32.50
SHARP VCA140.....	14.75
SOLAVOX 1000.....	16.95
SONY C5/7.....	14.95
SONY SL630.....	21.50
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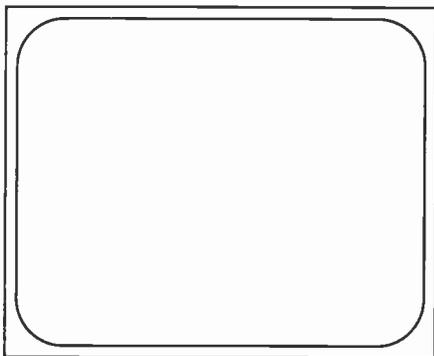
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2SC 1921	0.18	2SC 2366	51.42	2SC 2824	0.35	2SC 3277	1.65	2SC 3675	0.75	2SC 4137	0.36	2SD 1046	1.05	2SD 1438	0.82	2SD-1883	1.50	2SD-1725	3.75	2SD-177	3.75	2SK-555	3.53
2SC 1928	0.11	2SC 2371	0.25	2SC 2827	1.32	2SC 3279	0.23	2SC 3676	1.02	2SC 4138	2.18	2SD 1051	0.42	2SD 1442	1.13	2SD-1886	3.45	2SD 731	2.10	2SD-182L	1.04	2SK-556	3.84
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2SC 1941	0.30	2SC 2396	0.20	2SC 2837	2.78	2SC 3296	0.67	2SC 3686	3.68	2SC 4159	2.83	2SD 1071	2.70	2SD 1453	0.35	2SD-1933	1.35	2SD 756	0.27	2SD-182L	1.04	2SK-562	3.00
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2SC 1944	2.58	2SC 2408	0.56	2SC 2840	0.08	2SC 3298A	0.90	2SC 3688	5.99	2SC 4230	3.29	2SD 1088	1.49	2SD 1455	2.78	2SD-1941	4.18	2SD 757	0.41	2SD-182L	1.04	2SK-564	0.52
2SC 1945	1.14	2SC 241X	0.18	2SC 2851	1.20	2SC 3299	0.67	2SC 3689	4.93	2SC 4207	0.15	2SD 1111	2.25	2SD 1457	1.34	2SD-1944	0.38	2SD 758	0.56	2SD-182L	1.04	2SK-565	0.27
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2SC 1962	1.50	2SC 2443	14.75	2SC 2878	0.12	2SC 3310	1.13	2SC 3694	1.28	2SC 4236	6.00	2SD 1142	2.78	2SD 1494	2.32	2SD-2000	1.90	2SD 774	2.84	2SD-182L	1.04	2SK-727	5.25
2SC 1966	9.77	2SC 2440	2.03	2SC 2898	2.69	2SC 3311	0.08	2SC 3705	0.30	2SC 4237	6.38	2SD 1145	0.18	2SD 1496	2.99	2SD-2011	1.79	2SD 784	3.00	2SD-182L	1.04	2SK-738	0.87
2SC 1967	12.78	2SC 2442	0.25	2SC 2900	0.25	2SC 3312	0.15	2SC 3707	0.60	2SC 4242	1.78	2SD 1146	0.83	2SD 1497	0.06	2SD-2012	1.42	2SD 786	0.23	2SD-182L	1.04	2SK-738	4.62
2SC 1969	1.64	2SC 2459	0.11	2SC 2908	1.30	2SC 3316	1.90	2SC 3715	3.45	2SC 4273	1.44	2SD 1148	1.43	2SD 1504	0.17	2SD-2018	0.75	2SD 786S	0.23	2SD-182L	1.04	2SK-758	2.25
2SC 1970	1.17	2SC 2461	2.60	2SC 2909	0.25	2SC 3317	2.18	2SC 3716	2.63	2SC 4288	10.77	2SD 1153	2.27	2SD 1505	0.38	2SD-2019	0.75	2SD 787	0.23	2SD-182L	1.04	2SK-769L	10.50
2SC 1971	2.63	2SC 2471	0.18	2SC 2910	0.17	2SC 3318	2.32	2SC 3717	3.00	2SC 4289A	11.51	2SD 1160	0.72	2SD 1506	0.52	2SD-2046	0.38	2SD 789C	0.21	2SD-182L	1.04	2SK-791	5.82
2SC 1973	0.60	2SC 2481	0.48	2SC 2911	0.39	2SC 3320	4.61	2SC 3719	0.72	2SC 4290	12.67	2SD 1161	1.43	2SD 1507	0.52	2SD-2046	0.38	2SD 789C	0.21	2SD-182L	1.04	2SK-791	5.82
2SC 1975	0.98	2SC 2483	0.23	2SC 2912	0.45	2SC 3321	0.18	2SC 3720	0.25	2SC 4291	2.25	2SD 1162	0.98	2SD 1508	0.72	2SD-2125	4.13	2SD 789E	0.21	2SD-182L	1.04	2SK-791	1.52
2SC 1983	0.90	2SC 2491	1.28	2SC 2922	4.38	2SC 3330	0.15	2SC 3738	5.69	2SC 4295	1.18	2SD 1163A	0.67	2SD 1510	0.20	2SD-2151	1.88	2SD 792	4.25	2SD-182L	1.04	2SK-792	2.25
2SC 1984	0.78	2SC 2495	17.15	2SC 2923	0.67	2SC 3331	0.08	2SC 3740	0.23	2SC 4301	4.13	2SD 1164K	0.67	2SD 1511	1.72	2SD-2251	1.01	2SD 793	0.38	2SD-182L	1.04	2SK-793	4.43
2SC 1985	0.67	2SC 2497	0.75	2SC 2925	0.38	2SC 3333	0.33	2SC 3743	2.10	2SC 4304	1.89	2SD 1167	0.67	2SD 1512	0.45	2SD-2259	0.90	2SD 794	0.35	2SD-182L	1.04	2SK-794	4.13
2SC 1986	0.90	2SC 2498	0.12	2SC 2926	0.23	2SC 3335	1.04	2SC 3746	0.69	2SC 4305	5.22	2SD 1168	0.98	2SD 1513	0.57	2SD-2470	0.57	2SD 795	0.48	2SD-182L	1.04	2SK-795	4.80
2SC 2002	0.18	2SC 2500	0.25	2SC 2929	1.44	2SC 3346	1.13	2SC 3747	0.72	2SC 4310	5.90	2SD 1169	1.43	2SD 1514	0.21	2SD-2470	0.57	2SD 796	0.48	2SD-182L	1.04	2SK-796	4.80
2SC 2003	0.23	2SC 2512	0.17	2SC 2937	1.41	2SC 3345	2.47	2SC 3752	1.33	2SC 4312	6.78	2SD 1171	0.67	2SD 1515	0.38	2SD-2527	1.51	2SD 797	0.57	2SD-182L	1.04	2SK-797	4.80
2SC 2004	0.18	2SC 2516	0.84	2SC 2938	2.39	2SC 3355	0.41	2SC 3753	1.50	2SC 4313	8.52	2SD 1172	1.43	2SD 1516	0.38	2SD-2527	1.51	2SD 798	0.57	2SD-182L	1.04	2SK-798	4.80
2SC 2009	0.30	2SC 2519	0.12	2SC 2944	4.44	2SC 3356	0.48	2SC 3750	0.15	2SC 4314	11.25	2SD 1173	0.67	2SD 1517	1.28	2SD-2565	0.75	2SD 800	0.38	2SD-182L	1.04	2SK-822	0.60
2SC 2021	0.11	2SC 2523	4.93	2SC 2952	0.90	2SC 3357	0.36	2SC 3778	0.23	2SC 4327	2.55	2SD 1174	1.43	2SD 1518	0.57	2SD-2565	0.75	2SD 801	0.38	2SD-182L	1.04	2SK-822	0.60
2SC 2022	1.10	2SC 2526	6.52	2SC 2954	0.90	2SC 3359	0.30	2SC 3779	0.20	2SC 4351	9.93	2SD 1175	0.67	2SD 1519	0.57	2SD-2565	0.75	2SD 802	0.38	2SD-182L	1.04	2SK-822	0.60
2SC 2023	2.00	2SC 2527	2.03	2SC 2958	0.27	2SC 3376	1.76	2SC 3781	1.13	2SC 4367	0.78	2SD 1176	0.67	2SD 1520	0.57	2SD-2565	0.75	2SD 803	0.38	2SD-182L	1.04	2SK-822	0.60
2SC 2026	0.38	2SC 2530	1.32	2SC 2960	4.45	2SC 3377	1.15	2SC 3783	0.45	2SC 4382	3.00	2SD 1177	0.67	2SD 1521	0.57	2SD-2565	0.75	2SD 804	0.38	2SD-182L	1.04	2SK-822	0.60
2SC 2027	2.25	2SC 2534	1.02	2SC 2962	5.54	2SC 3378	0.33	2SC 3785	0.33	2SC 4383	2.30	2SD 1178	0.67	2SD 1522	0.57	2SD-2565	0.75	2SD 805	0.38	2SD-182L	1.04	2SK-822	0.60
2SC 2028	0.99	2SC 2535	1.62	2SC 2979	2.10	2SC 3391	1.50	2SC 3786	0.36	2SC 4386	2.63	2SD 1179	0.67	2SD 1523	0.57	2SD-2565	0.75	2SD 806	0.38	2SD-182L	1.04	2SK-822	0.60
2SC 2053	0.45	2SC 2538	0.72	2SC 2983	0.65	2SC 3383	0.30	2SC 3787	0.44	2SC 4388	4.50	2SD 1180	0.67	2SD 1524	0.57	2SD-2565	0.75	2SD 807	0.38	2SD-182L	1.04	2SK-822	0.60
2SC 2056	1.84	2SC 2539	9.52	2SC 2987	2.03	2SC 3387	3.30	2SC 3788	0.60	2SC 4408	0.38	2SD 1181	0.67	2SD 1525	0.57	2SD-2565	0.75	2SD 808	0.38	2SD-182L	1.04	2SK-822	0.60
2SC 2058	3.12	2SC 2542	16.88	2SC 2987A	2.03	2SC 3388	0.20	2SC 3789	0.60	2SC 4409	0.38	2SD 1182	0.67	2SD 1526	0.57	2SD-2565	0.75	2SD 809	0.38	2SD-182L	1.04	2SK-822	0.60
2SC 2059	0.45	2SC 2543	1.62	2SC 2988	1.08	2SC 3395	1.08	2SC 3790	0.33	2SC 4410	0.38	2SD 1183	0.67	2SD 1527	0.57	2SD-2565	0.75	2SD 810	0.38	2SD-182L	1.04	2SK-822	0.60
2SC 2060	0.21	2SC 2545	0.23	2SC 2995	0.15	2SC 3396	0.15	2SC 3793	1.50	2SC 4490	0.38	2SD 1184	0.67	2SD 1528	0.57	2SD-2565	0.75	2SD 811	0.38	2SD-182L	1.04	2SK-822	0.60
2SC 2068	0.45	2SC 2546	0.33	2SC 2999	0.12	2SC 3399	0.15	2SC 3795	1.16	2SC 454	0.11	2SD 1185	0.67	2SD 1529	0.57	2SD-2565	0.75	2SD 812	0.38	2SD-182L	1.04	2SK-822	0.60
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2SC 2072	0.72	2SC 2547E	0.21	2SC 3011	0.65	2SC 3401	0.12	2SC 3801	0.11	2SC 458	0.08	2SD 1187	0.67	2SD 1531	0.57	2SD-2565	0.75	2SD 814	0.38	2SD-182L	1.04	2SK-822	0.60
2SC 2075	1.13	2SC 2551	0.20	2SC 3012	1.88	2SC 3402	0.11	2SC 3802	0.52	2SC 464A	0.11	2SD 1188	0.67	2SD 1532	0.57	2SD-2565	0.75	2SD 815	0.38	2SD-182L	1.04	2SK-822	0.60
2SC 2078	0.52	2SC 2552	0.52	2SC 3013	1.08	2SC 3405	0.13	2SC 3803	0.52	2SC 464B	0.11	2SD 1189	0.67	2SD 1533	0.57	2SD-2565	0.75	2SD 816	0.38	2SD-182L	1.04	2SK-822	0.60



TELEVISION

Channels Galore

One increasingly wonders why so much political effort was put into keeping alive the MAC approach to the development of TV transmission when the digital approach was advancing at such a rate. Philips and Thomson, who have a great deal of influence with the European Commission, had of course invested heavily in MAC – and saw it as a way of halting the advance of Far Eastern consumer electronics manufacturers in the European market. But they've not been idle with respect to digital TV, which has everything going for it – including the prospect of an internationally accepted standard.

The aspect of digital TV that has been much in the news of late is the prospect of vastly increasing the number of channels in the bandwidth available through the use of signal compression. BBC and BT engineers demonstrated at the recent ISO/MPEG (the Moving Pictures Expert Group of the International Standards Organisation) meeting in London a video coding system that compresses a standard-definition TV signal to a data rate of 6Mbits/sec rather than 216Mbits/sec. Of particular interest technically is the fact that this system has a 'two-layer' capability, providing standard or HDTV pictures in either of two modes, simulcast or compatible. In the former the SDTV and HDTV images are coded independently while in the latter the SDTV signal is used as one prediction option for the HDTV encoder. Digital compression systems reduce the demand on spectrum space by selecting for transmission only the differences between successive fields rather than sending complete fields. The receiver's decoder uses a field store to hold the field, the incoming data being used to update it.

Thus digital signal processing enables us to cram more channels into a given bandwidth and/or provide higher-definition pictures. At the recent *Financial Times* Cable and Satellite conference Celso Azevedo, technical director of Societe Europeenne des Satellites (SES) which runs the Astra system, announced that by building digital capability into its new satellites the Astra system would be able to provide 180 channels in two years' time. This could be doubled to 360 channels by launching a further satellite. The digital compression system to be used squeezes ten standard channels into the space now occupied by one.

From the broadcasting viewpoint the economics are interesting. A single-channel transponder at present costs £4m a year to lease. If it carries ten digitally compressed channels the rent per channel could fall proportionally, introducing all sorts of possibilities. It seems however that the main use envisaged – who could provide 180 channels of separate programming? – is as a means of making feature films available to the viewer at a reasonable cost. Six channels could, it was suggested, be devoted to one film, with staggered start times so that the wait for the start of a particular film would not be more than about twenty minutes.

Digital compression enables the data rate for digital TV signals to be reduced by a factor of about fifty without any noticeable impairment of picture quality. It can be used for satellite, terrestrial or cable TV channels – and other services of course. Added complexity is required in the receiver, but with modern chip technology this shouldn't translate into any dramatic price increase. If we accept SCS's forecasting, and it has proved to be reliable in the past, this massive increase in the number of channels could be available within two-three years.

It is particularly gratifying that the UK continues to play a major role in the development of digital TV. The original impetus for its development came from the need for standards conversion. By early 1973 a field-rate standards converter developed by the IBA was in regular use. DICE (digital intercontinental conversion equipment) as it was known was an outstanding engineering achievement, the fastest computer in the world at the time. By the early Eighties compression techniques that enabled the bandwidth required to be halved had been developed. Along the way came teletext, Nicam and other developments. The UK has all along been in the forefront in digital signal processing.

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COVER PHOTO

This month's cover photograph shows the Ferguson IKC2 chassis – see article on pages 416-9



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Importance of Dish Size with Astra Reception

Ian Martin

Some time back in these pages I wrote about the installation of my own Amstrad SRX200 Astra system and, subsequently, my Philips STU902 BSB system. Like many in the industry, I have since then bolted a lot of satellite dishes to a lot of walls and found several factors that commonly affect system performance.

Sparklies

The most common complaint with existing installations is of sparklies. This is usually because the signal's carrier-to-noise (C/N) ratio is too low. In most cases the cure is to realign the dish carefully, using a signal-strength meter, and perhaps add a little mechanical skew to the LNB with the voltage-switched type. Sometimes you find that the gain of an LNB or a receiver is lower on one or more channels than the others. In such cases changing a head-end component or using an LNB with a lower noise figure can give improved results. Whilst changing any head-end component, check for ingress of moisture or spiders. Where the cause of the problem is a mismatch in the cable, shortening or even lengthening it can just occasionally help. Unfortunately it's not easy to check on such deficiencies, let alone remedy them, in the limited time available when attending a simple Astra installation – and the problem always becomes worse as time passes or as soon as the installer goes away!

Even when all the above points have been checked and corrected it's still possible to have signal problems on a few channels.

This is especially so when a 60cm dish is used in a "fringe" area such as Wales, the South West or anywhere north of the M62. The problem is usually experienced first with some of the vertically polarised German mode 2 channels via Astra 1A – their signal strength becomes weaker as one travels westwards and northwards. It's accentuated when the receiver has a poor threshold and the LNB has a not-so-low noise figure. Wet weather worsens the situation by attenuating the signal from – and sometimes to – the satellite.

Dish Size

One solution, local planning regulations permitting, could be to use a larger dish. Originally SES, which owns Astra, specified the use of a 60cm dish and an LNB with a noise figure of 1.5dB in the central European area where the signal strength (e.i.r.p.) is 52dBW. Use of a 75cm dish was recommended in the "fringe" areas mentioned above, where the signal strength is 50dBW. Given these conditions it was predicted that CCIR grade 4 (or better) quality reception would be achieved with a clear sky, while acceptable performance would be obtained under 99.9 per cent of weather conditions. This however was a "link-budget" calculation: practical experience has taught us about the effects of bad weather and poor installation.

I decided to carry out some checks on dish performance by using various sizes with a standard set-up. All other

things being equal, an improvement in delivered signal strength should be obtained as dish diameter is increased. The tests were carried out using an Amstrad SRD400 receiver and three dishes provided by Lenson Heath, each of which was fitted with the same Northern Telecom LNB/polariser unit. Comparisons were made between 60cm mesh and 80cm solid dishes, some additional measurements being made using Lenson's new 98cm solid dish. Before any practical measurements were carried out, the relative gain of each dish was calculated from its signal-gathering area. This was then compared with the manufacturer's data. Table 1 lists the results of this exercise.

Performance Tests

Measurements were carried out on each of Astra 1A and 1B's channels, using the 60 and 80cm dishes, to establish the effect on the C/N level of using a larger dish. The results are listed in Table 2. The location was in South Wales and the measurements were made under clear sky conditions. Equipment conditions were as follows: LNB noise figure 1.3dB (quoted), meter receiver threshold 8dB (quoted).

Each Astra satellite has four transponder groups. Two use vertical and two horizontal polarisation. The four groups are "aimed" at different points in Continental Europe, i.e. they have different footprints/service areas. SES distinguishes the groups by referring to them as mode 1 horizontal, mode 1 vertical, mode 2 horizontal and mode 2 horizontal. Except for the Movie Channel, the Sky services allocated to the UK use mode 1 with vertical polarisation. Mode 1 is aimed to the west to give a footprint centred on Northern France/SE England. Hence the mode 1 signals should be the strongest ones.

Table 2 shows that the Sky channels 4, 8, 12 and 16 produce the highest C/N levels while the German channels 2, 6, 10 and 14 produce the lowest levels. This is largely because of the different group footprints. The D2-MAC channels 3, 7 and 11 have slightly better C/N ratios than expected, due to the MAC system's resilience to noise degradation. The Astra 1B satellite's transponder groups are not so clearly distinguishable in terms of measured C/N ratios, though again the vertical mode 1 signals are the strongest, particularly Documania via transponder 32. The choice of transponder 23 for UK Gold seems strange, as it produces one of the lowest C/N ratios. Overall these measurements seem typical of systems in this part of the world.

In considering the C/N ratio figures given in Table 2 we

Table 1: Dish size and relative gain.

Dish diameter (cm)	63*	80	98
Relative gain	1	1.61	2.42
Maker's quoted gain (dB)	36	38.5	41

*Lenson Heath's 60cm nominal diameter dish has an actual mean diameter of 63cm.

Table 2: C/N level measurements.

Channel/ group	Programme	C/N level (dB)	
		60cm dish	80cm dish
Astra 1A			
1 1H	Screensport	13.6	15.8
2 2V	RTL	13	14.8
3 2H	TV3	14.5	16.2
4 1V	Eurosport	15.1	16.9
5 1H	Lifestyle/JSTV	14	15.8
6 2V	SAT 1	12.5	14.4
7 2H	TV1000	14.5	15.9
8 1V	Sky One	14.9	16
9 1H	Teleclub	13.7	15.3
10 2V	3 Sat	12	14.2
11 2H	Filmnet	13.3	15.1
12 1V	Sky News	14.3	15.9
13 1H	RTL V	13.7	15.5
14 2V	Pro 7	13	14.6
15 2H	MTV	13.6	15.9
16 1V	Sky Movies Plus	14.7	16.4
Astra 1B			
17 1H	Premier	13.7	15.4
18 2V	Movie Channel	14.6	16
19 2H	ZDF	14.6	15.9
20 1V	Sky Sport	13.5	15.1
21 1H	DSF	14.1	15.7
22 2V	MTV	14.4	16
23 2H	UK Gold	12.6	13.9
24 1V	TCC/JSTV	14.1	15.9
25 1H	N3	14.2	15.3
26 2V	Sky Gold/TV Asia	13.6	15.4
27 2H	TV3	15.1	16.7
28 1V	CNN International	14.3	15.6
29 1H	NTV	13.8	15.4
30 2V	Cinemanía	14.8	16.6
31 2H	TV3	12.3	14.9
32 1V	Documanía	15	16.7

For measurement conditions see main text.

should perhaps mention that for good quality reception a C/N ratio of about 13dB is desirable. Less than 13dB usually means degraded performance in terms of a worse S/N ratio and sparklies. With the equipment used it was not possible to measure accurately below 11dB.

Similar results were obtained when the Amstrad receiver was used with an older "blue cap" LNB (noise figure 1.8dB) except that on all channels the measured C/N levels were approximately 1dB lower. Received picture quality was acceptable, though it was sometimes impossible to eliminate sparklies completely with the UK Gold and German channels when using a 60cm dish. Again this is typical of installations in this area.

Better results were obtained when the 98cm dish was tested, an improvement of 3dB in the C/N ratio being recorded in comparison with the 60cm dish. This would provide a good increase in the performance margin under adverse weather conditions. Unfortunately this size of dish is not specified for Astra reception, though it could form the basis of a motorised system. This takes us into the realms of

planning permission of course.

As a separate test, mostly to satisfy my own curiosity, the same checks were made using an older 60cm solid aluminium dish. No measurable performance differences were noted in comparison with the results obtained using the 60cm mesh-type dish. Lenson Heath points out that the gain of a mesh dish should be similar to that of a solid one provided the holes are not too large. Of greater importance apparently is the shape of the holes: poorly designed perforations can trap water and snow, attenuating the signal when the weather turns bad. The choice of a solid or mesh dish is largely a cosmetic one.

Conclusions

What conclusions can we draw from these tests? It seems that SES's original calculations for the expected signal strength and dish and receiver characteristics were correct. When one gets close to the boundary of the 52dBW footprint however signal degradation increases. Although this boundary defines the area in which the use of a 60cm dish is recommended, better results are obtained using an 80cm dish. This is definitely the case where the customer wishes to receive German programmes without interference. More important perhaps is the improved margin against interference under bad weather conditions provided by a larger dish.

Another advantage of a larger dish is its reduced beamwidth, which means that it will be less likely to pick up interference from satellites adjacent to the one with which it is aligned. I have already come across a 60cm Astra system that, because of slightly incorrect azimuth alignment, was receiving signals from the Eutelsat craft at 16° as well. This problem can only worsen with time, as more satellites are placed in orbit and dish alignments move.

Acknowledgement

My thanks to Lenson Heath for the loan of dishes and the provision of technical data. In a later article I'll describe the installation of a polar mount designed for use with their 80 and 98cm dishes.

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Letters

CHEAP WASHERS

During the course of my daily round I've noticed an increasing number of self-installed aerial brackets. Although they are fitted well enough the screw holes are too big for most woodscrews and leave little enough landing for Rawl-bolts unless a washer is used. The thing that drew my attention was the number of cases where a two-pence piece with a hole drilled through the centre was being used in place of a washer. This intrigued me so much that I asked the price of a two-pence sized washer at my local hardware shop. The answer? Ten pence each!

Now don't get me wrong. I don't think that anyone can expect to buy anything for less than ten pence today, and if you think about it most of our use of the odd penny is because VAT brings the price to £XX.99 or something similar. But isn't it a sign of the ravages of inflation when five coins of the realm can be used as washers for the price of one of the real thing! I should perhaps add that I think it's against the law to deface British currency. Punishment is probably death by hanging or the rack. I believe it's quite an old law.

*John Hopkins, The TV Workshop,
Felixstowe, Suffolk.*

BRASS DRIVE BUSH

My thanks to W. Wilcock (February) and S.J. Caine (March) for their comments about the Sharp brass drive bush. If only to ensure that I haven't mislead anyone on the subject of the method of fitting I must comment further. In my original note (December 1992) I said that the brass item should be fitted using a hot soldering iron. Clearly this would be no good with the Sharp part. The one to which I was referring has a tapered fit however and is made to be heated for fitting to the shaft. I hope I didn't give the impression that I was actually soldering the thing on. The taper-fit bush is available from VAS Electronics, Gleneagles Avenue, Leicester (0533 664 850).

*Chris Watton,
Boston, Lincs.*

NICADS AND CAMCORNERS

I read John Kendall's letter (March) with some sympathy. The problem with the palmcorder is that the layman thinks, when it shuts down, that the 6V battery has been properly discharged. It hasn't. The memory effect will then affect the charge-discharge cycle and in no time at all the battery has become useless for its purpose. It can recover from this effect, with careful treatment, but the layman will have gone off to buy another battery – at some cost!

A nicad battery delivers only 1.2V per cell. Thus a battery of five is needed for 6V. Ideally they should be discharged until each cell reaches 0.9V, the end-of-charge voltage for a 6V unit being 4.5V. This is far below the point at which the camcorder shuts down. Possibly cost and size are the reasons for using a 6V battery, but if the end result is such an unsatisfactory charge life surely, as Mr. Kendall suggests, a 7.2V unit with some regulation in the machine would be a better option?

Discharging the battery until it is flat is not a good idea. Some cells may reach 0V before others. These will then

begin to charge in the reverse direction, which makes life even more difficult. I've made a discharger for my 12V nicads. It senses when the terminal voltage has fallen to 9V then shuts off. By doing it this way I've managed to keep in service for over six years the batteries I use. Varta produced a very good guide for nicad users at one time: it might be worth trying to obtain one.

Many people comment about the short life of nicads used in radio receivers and personal stereo equipment. These items were designed to be used with zinc-carbon or alkaline batteries whose cell voltage is 1.5V. When a nicad battery with only 1.2V per cell is used the end-point voltage for the load is reached that much sooner!

*Graeme M. Yeung,
Nottingham.*

NICAM ON A SHOESTRING

I read with interest Keith Wevill's article in the February issue, having myself built a near identical system about ten months ago using components obtained from the same sources. I bypassed the TDA8421 tone control chip with some regret as it has such obvious potential, but I'd no way of obtaining data on the device or the I2C bus system. My solution was simply to take the audio signals from CS56/7 to 10kΩ log. potentiometers and, after removing diodes DS81/2, take the sliders of the potentiometers to RW37/CW28 and RW34/CW25 via 22μF capacitors.

The video signal required was obtained from the excellent signals panel used in the Philips G11 chassis. Since this requires some 40V to tune across the bands it fitted well with the 36V the Nicam panel needs. A further advantage of this signals panel is that it has a stand-alone audio demodulator and output section that also operates at 36V. This can be used for initial tuning, or as a separate mono output.

I wired up the G11 unit first to ensure that it operated satisfactorily, then carried out modifications to the Nicam panel as described by K. Wevill. The Nicam signal was taken from the video detector to the Nicam panel. In my case a d.c. bias was already present at the panel's video input so no problems were expected and none were found. Since I didn't intend to use the video signal for viewing I deliberately tweaked the vision i.f. to enhance the Nicam signal level.

The sound quality is excellent without any additional tone control and fully justifies reports on the system.

*I.C. Rohsler,
Harborne, Birmingham.*

COWBOYS SHOOT BACK

I read with particular interest Ed Rowland's article (February) on cowboys since by his definition I would be one of them though I've had twenty five years experience of repairing TVs and VCRs as well as the design and manufacture of various electronic products. But I'm not a member of any guild. I've moved away from full-time repair work now but do undertake the odd job in any spare time I am lucky enough to have.

While the cases mentioned by Ed Rowland are horrific, I can quote quite a number of instances of gross over charging and what amounts almost to fraud by 'respectable' dealers. An acquaintance of mine recently took a six-year old Hitachi VCR to one firm and was told that the trouble was caused by defective heads, which cost £97 plus fitting, and that the machine was therefore a write off. When my acquaintance asked for it back he was told rather aggressively that there was no point and that it would be disposed

of for him. He rather stupidly agreed to this.

Now you and I know that a set of replacement heads for such a machine can be obtained for between £10 and £20. I wouldn't mind betting that the dealer concerned whacked in such a set and either put the machine out on rental or sold it off. Such cases are not rare in this part of the world. I recently fitted a motor supplied by the customer to a record deck. Total time taken was less than five minutes. The quote from another firm was £45 plus VAT.

I'm sure that most dealers are from time to time guilty of making up losses incurred in sorting out the real pig that we've all had occasionally. My point is that there seems to be an increasing trend for certain dealers to do this all the time. The same trend can be observed with other retail businesses. My wife recently took a ring to a well-known firm of High Street jewellers for a small replacement opal to be fitted. The manager quoted £150 – we had the job done for £8 by another more honest but much smaller jeweller.

Maybe if the repair business cleaned up its act and charged an honest rate for each job, based on the amount of time spent doing it, instead of working out the cost on the "how much can I get from this client" basis, the cowboys would be out of business because the public would learn to trust local dealers. I've just had a set in from someone who lives forty miles away: he simply doesn't like being ripped off the minute he walks through the door of a 'respectable' dealer.

*L.J. Pitts, B.Sc.(Hons.), FIAP, LRSC,
South Brent, Devon.*

I feel that I must take issue over Ed Rowland's Cowboys article (February). It seems to suggest that anyone who offers a repair service without certain paperwork or qualifications is a crook. A comparatively few bad experiences are cited, leaving the reader to infer that this is the inevitable penalty for not paying the full price asked by those who have the paperwork. Qualified people are not immune from dishonest practices however.

Be honest about the fact that many cowboys, almost certainly a majority, are capable of doing just as good a job as those with qualifications. Many of them will honourably admit defeat if they cannot cope.

It's natural for those who have undergone formal training to feel hard done by when they find that others can do a lot of their work as a result of informal learning and self-taught skills. One shouldn't deny the right to those members of the public who want, or can only afford, to take a cheaper and often worthwhile risk in getting their servicing done. I know that there are safety issues here, but Ed Rowland didn't specifically mention these. Clearly any servicing involves risks. Electronic work is not alone in this respect, and there will always be a minority of bad cowboys. But this is what free competition and choice is all about.

And for heaven's sake don't encourage the Eurocrats to get their ham-fisted fingers on any more of our activities. This would only make life more difficult for us all, including those who feel that they are fully qualified.

What's needed is a way of punishing those who behave badly rather than more restrictive practices.

*Martin J. Loach,
Abingdon, Oxon.*

I'd like to point out that not all cowboys are the small fry, as suggested in Ed Rowland's article (February). About two years ago I was working at a training establishment in Liverpool. Trainees from our and other departments were allowed to bring in TV sets, VCRs etc. to be repaired where

possible. The majority of sets were old ones (Philips G8s etc.), many intended for use with little Johnny's computer games.

One morning however a three year old set made by a large European manufacturer was brought in. Its owner told us that the local approved dealer, who advertised and sold just this one brand and had sold him the set, had said that the tube was duff. A replacement, with fitting etc., would cost around £150, with a small discount for cash. He could have the latest all singing and dancing model however for a good discount with trade in. There was an argument and the disgruntled set owner withdrew. We were his second opinion.

The type of tube involved is renowned for premature failure. Its display was sad to say the least – very dark and muddy. The red appeared to be missing, but on closer observation seemed to be fading in and out cyclically. A check showed that the tube base voltages were all more or less correct. By now most of you will have guessed that the tube was o.k. Disconnecting the degaussing plug and carrying out a manual degauss restored a perfect picture. The degaussing thermistor was the offending item of course and was replaced. The old one sounded like Mick Jagger's maracas, and showed perfectly for our students what the inside of a cooked thermistor capsule looks like. From set switch on to repair completion took about an hour, including discussion of the fault with the trainees initiating the sequence of steps in the fault-finding process. The happy owner bought everyone a pint.

His annoyance with the dealer was understandable. Further questioning brought out the information that during his visit to the dealer the set was at no time out of his sight (he was actually taken into the workshop) and that the set was never opened, diagnosis being based on off-air signal reception. How many other basic rules were ignored?

How many other people are taken in by these methods? Joe Public expects an accredited dealer to be a little more honest than the Snoddies of this world, but there are nevertheless such obvious rackets.

About a week later the set's owner came back to see us. He'd returned to the shop and confronted the engineer, who had a 'manager' badge on his coat. Once again he was offered a discount to buy a new set. He left after telling the 'manager' that he would never shop there again.

*P. Perkins,
Wirral, Merseyside.*

FIXING GRUNDIGS

Excellent technical advice on Grundig products can now be obtained from a very helpful gentleman, Allan Dyson of Tameside Technical Services. He's an ex-Grundig TLO whose advice is available to the trade at a very reasonable charge.

Our own problem started when a service manual for the VS520 VCR couldn't be obtained from Willow Vale, who told us that they had been trying to obtain it from Grundig for months. I had paid my membership to TTS: my phone call to Allan Dyson resulted in a tuner/i.f. fault being traced to component level – with a complimentary service manual being thrown in!

With Grundig phone lines that are permanently busy, or "we don't give technical advice to non-approved service departments", I can certainly recommend Allan Dyson's service. He can be reached on 061 367 9400. This is what technical advice should be like.

*Brian Davidson, Davidson Bros.,
Greenock, Renfrewshire.*

Modern TV Receiver Techniques

Part 4

Eugene Trundle

There was a time when TV receiver audio circuits could be dealt with in a few paragraphs. While this is still true with simple, basic TV sets, there have been tremendous changes in audio systems at both ends of the broadcasting chain over the last few years. We'll start with the simplest arrangement and work up from there.

Mono FM System

The monaural sound signal is transmitted on its own frequency-modulated r.f. carrier, with $\pm 50\text{kHz}$ maximum deviation, at a level 10dB below that of the vision carrier. With system I the sound carrier frequency is spaced 6MHz above the vision carrier: with the European systems B/G the spacing is 5.5MHz above the vision carrier. As before, we'll stick to system I for our examples.

The sound carrier beats with the local oscillator in the tuner to produce an i.f. output at 33.5MHz. There are two alternative ways in which this signal can be processed. It can either be filtered out then amplified and demodulated, or passed via the vision i.f. amplifier to the vision demodulator where it will beat with the vision carrier to produce a 6MHz difference signal, with the f.m. intact, which can then be selected, amplified and demodulated. The latter system, called the intercarrier system, has been in use for many years. It has several advantages: tuning errors and drift have no effect on the carrier frequency, which is governed solely by the very accurately maintained vision-sound spacing at the transmitter; the sound carrier benefits from the gain provided by the vision i.f. amplifier; and the sound circuit is simple.

Typical Circuit

Fig. 1 shows a typical simple TV sound system of this type. The input from the vision demodulator is first passed through a ceramic filter which is resonant at 6MHz, its bandwidth being about 200kHz. This is wide enough to embrace the $\pm 50\text{kHz}$ f.m. sound deviation while rejecting the luminance and chroma signals. In some receivers two ceramic filters are used, connected in series. The sound carrier enters the chip at pin 1, after which it's passed through several stages of amplification with limiting – the limiting clips off any amplitude modulation caused by the vision signal, the a.m. rejection with normal input levels being about 55dB.

The clipping action produces a squarewave output. As this contains many harmonics of the baseband frequency the signal is next passed through a low-pass filter. This restores the carrier waveshape to something like a sine wave for application to the f.m. demodulator, which is of the quadrature synchronous type. Again, as described last month, the action is based on the sample-and-hold principle. The sampling gate is opened for an instant during each carrier cycle. An unmodulated carrier will be passing through zero when the gate is opened, so there will be no output. As the phase/timing of the signal advances and retreats, the sampling action generates an output that's proportional to the frequency deviation.

A reference carrier is required to produce the gating action. This is generated by the high-Q tuned circuit L1/C5 whose flywheel effect averages the carrier frequency, thus providing a constant-phase reference feed for the demodulator. In current practice a ceramic filter is used for this purpose instead of a discrete LC circuit.

Next comes a voltage-controlled amplifier (VCA) whose gain depends on the resistance between pin 6 of the i.c. and chassis. An alternative way of arranging for this volume control action is to apply a variable d.c. control voltage to pin 6, the volume level then being proportional to the applied voltage. Where control is done by sending serial data along a bus line the chip must incorporate a circuit to decode the data and set the gain of an amplifier stage. Back to the simple circuit shown in Fig. 1 however.

The Audio Amplifier

The demodulated audio signal has to be de-emphasised. An RC network performs this operation, the capacitor being connected to pin 12 of the chip while the 10k Ω resistor is within the chip. The signal is now ready for application to the driver and output stages which in a simple system are generally, as shown here, within the same chip. The output stage usually consists of a push-pull pair of transistors operated under class B conditions, the d.c. mid-point voltage being isolated from the loudspeaker by coupling capacitor C10.

The value of the resistors connected to pin 7 of the chip determine, as part of a negative feedback loop, the a.c. gain of the output stage, the capacitors connected to pin 8 setting the amplifier's upper frequency limit. R5 and C12 form a Boucherot cell which suppresses any tendency for h.f. oscil-

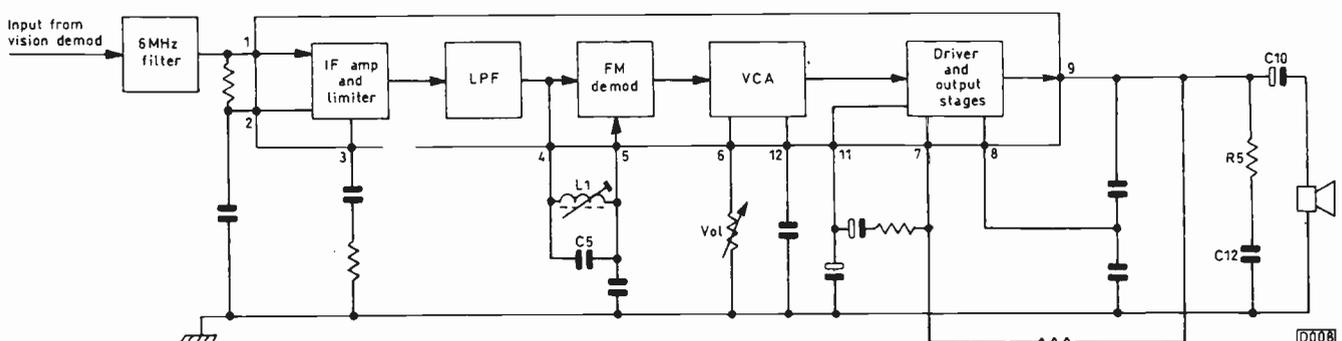


Fig. 1: Typical intercarrier sound/audio amplifier chip arrangement.

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lation, due to the inductive load (the loudspeaker and its wiring), to occur in the output stage – similar arrangements are used in field output stages.

A small chip of the type taken as an example here will provide an audio output power of about 3W average, depending on the supply voltage and the heatsink arrangement used. This type of i.c., or a small power amplifier chip fed from a separate intercarrier sound amplifier/demodulator i.c., easily caters for the needs of a portable set or an economy large-screen receiver using a single loudspeaker.

Although for purposes of illustration we've shown a dedicated sound channel chip, in modern sets the intercarrier sound and audio preamplifier stages are likely to be incorporated in a more complex chip that performs many other functions.

Stereo Sound

There are several possible sources of stereo sound in a TV receiver: a built-in Nicam decoder; external sound-with-picture sources such as a satellite TV receiver, a hi-fi VCR or a Laserdisc player; and, in some countries, a built-in analogue stereo sound decoder. Incorporating a stereo sound system calls for difficult choices by the setmaker in terms of loudspeaker arrangements and operating power. The power drain introduced by a reasonably high-energy stereo audio system may be at least equal to that of the line output stage. With a class B output stage it fluctuates in sympathy with the sound: if a constant-current system is chosen there's little problem with regulation but a lot of heat has to be dissipated. For outputs up to about 5 + 5W a single dual-channel power output chip is generally used; for higher powers there is usually a separate audio output chip in each channel.

Since low-frequency sounds are not very directional some sets have a single, centrally-mounted woofer that's fed with the L and R signals and a pair of side-mounted boxes that take L and R feeds respectively and produce just the medium- and high-frequency sounds. Fig. 2 shows such an arrangement, devised by Sony. The centrally-mounted 13cm woofer has separate 7Ω coils for the L and R audio signals, which are fed to them via low-pass LC filters. The side-boxes each contain a 7.5 x 13cm mid-range unit, a 5cm dome tweeter and a first-order crossover network. In conventional stereo TV sets much ingenuity is used by manufacturers to overcome the acoustic problems associated with small loudspeakers in plastic cabinets. Bang and Olufsen, always aware of sound quality, have in some models used a pair of rear speaker-loading horns inside the TV set's cabinet, sticking up on each side of the c.r.t.

No matter how well a TV set's sound system is designed, there's no doubt that taking separate audio feeds from the set – or VCR – to a hi-fi system with widely-spaced loudspeaker enclosures is better for stereo.

Spacial Effects

Because a stereo receiver has two sound channels with closely-mounted speakers and may well work with a monaural signal for much of the time, several 'ambience' techniques have been devised to enhance the sound. They are also sometimes used in audio equipment.

The first of these is the 'stereo-wide' system, which gives the subjective effect of increased L and R sound separation. It's done electrically, by emphasising the difference between the L and R audio signals. The simplest and most common way of doing this is to inject into each audio channel an anti-phase (polarity-reversed) signal from the

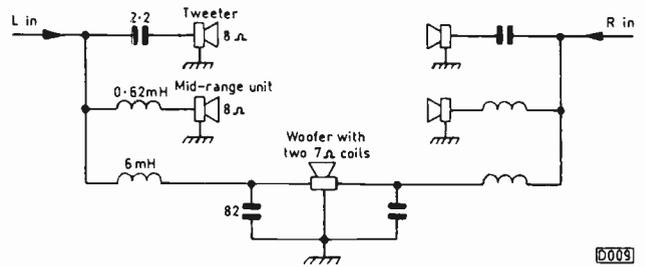


Fig. 2: 3-D loudspeaker system with a common base unit.

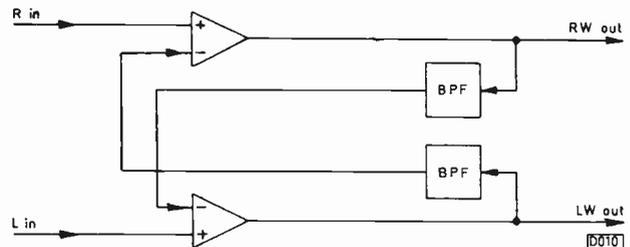


Fig. 3: A stereo-wide arrangement.

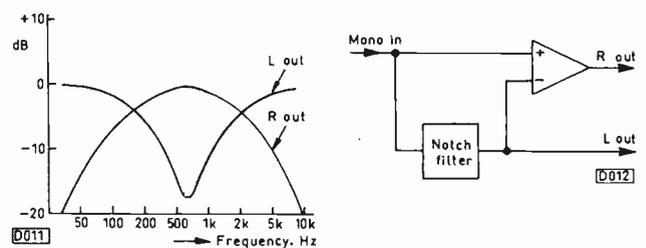


Fig. 4: Response curves for one form of pseudo-stereo system.

Fig. 5: Way of obtaining the response curves shown in Fig. 4.

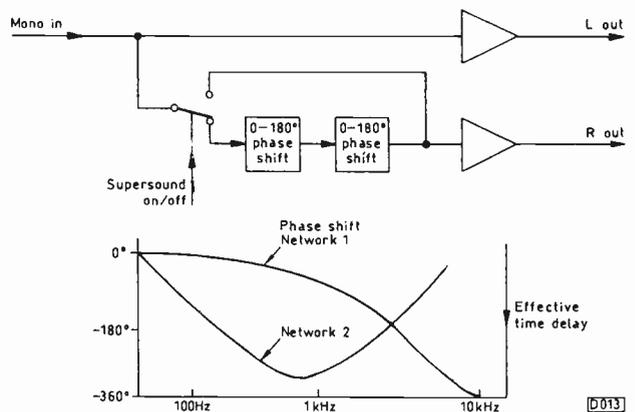


Fig. 6: Ferguson's Supersound system, in which the signals in the R channel are subjected to a frequency-dependent time delay.

other channel, generally via filters that pass only the mid- and high-frequency components of the audio signals. Fig. 3 shows the arrangement. Thus the greater the difference between the L and R sounds, the greater the differential emphasis. This arrangement is sometimes called spatial sound – the terms are often used indiscriminately.

With a monaural sound source and a pair of correctly-phased speakers at each side of the set the sound appears to come from a point between them – the picture tube screen. It's possible to process the monaural signal electrically to

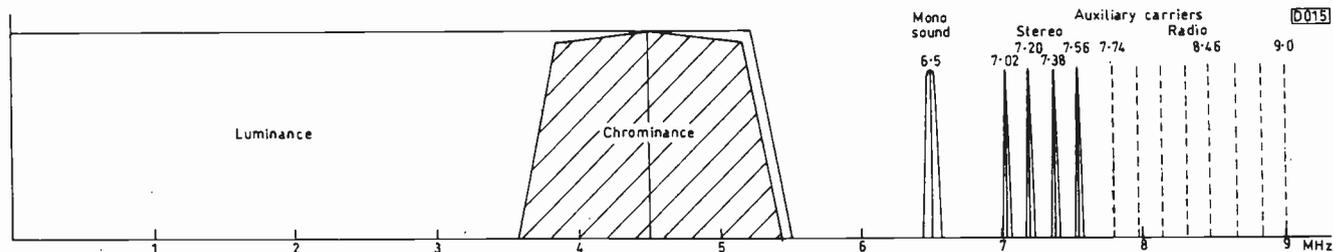


Fig. 8: Baseband Astra channel spectrum. In addition to the primary and four stereo carriers there may be up to eight further carriers, typically used for radio programmes. The spacing of the four stereo carriers is 180kHz.

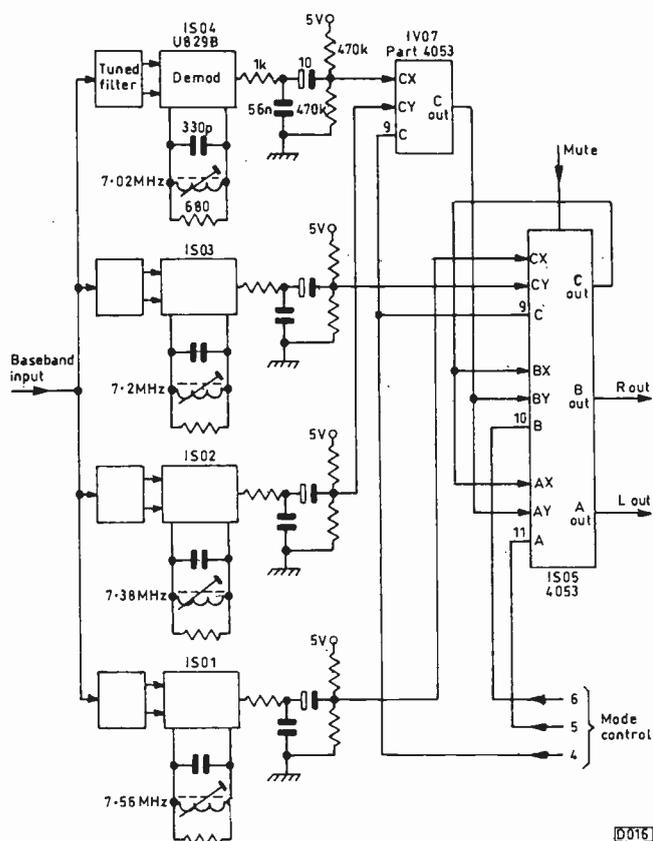


Fig. 9: Audio demodulator arrangement used in the Ferguson SRA4 satellite TV receiver. The four channels are identical.

a poorer signal-to-noise ratio a noise-reduction system is used – with Astra transmissions the Wegener Panda 1 type is employed. The term Panda is derived from ‘processed narrow-deviation audio’. It’s a form of adaptive pre-emphasis. The dynamic range of the audio signal is compressed before transmission so that, in relative terms, high-level signals are attenuated and low-level ones are boosted, the amount of compression also being frequency-dependent. The opposite has to be done to the baseband audio signal in the receiver so that its dynamic range is restored. In the process the noise component is suppressed.

The system has much in common with the companding principle used in hi-fi VCRs and with Dolby noise-reduction techniques. It’s implemented by i.c. VCAs whose control voltages are derived from the signal itself via filters. Without noise reduction the signal-to-noise ratio of a narrow-band satellite TV sound channel is about 50dB; the Wegener Panda 1 system provides an improvement of about 18dB, increasing the subjective signal-to-noise ratio towards 70dB, which is very good for an analogue transmission.

Table 1 shows the uses to which the auxiliary sound carriers are put, for stereo and multi-lingual sound, with Astra transmissions. Fig. 9 shows the simple multi-channel sound selection system used in one satellite TV receiver, in which each carrier is selected by an LC tuned circuit and fed to its own f.m. demodulator. The four demodulators work all the time, the switching chips IV07 and IS05 selecting the ones required in accordance with the control signals applied to pins 9, 10 and 11.

Sound Carrier Conversion

An alternative to using four parallel sets of filters and demodulators is to employ a superhet system to convert the wanted carriers to fixed frequencies that can be handled by a pair of fixed-tuned filters and demodulators. This technique has the advantage of being versatile: it will work with any pair of carrier frequencies, including the piggy-back radio stations (see Fig. 8) that many transponders carry on carrier frequencies between 7.74 and 9MHz, while in sophisticated systems the required channel can be user-programmed per transponder and stored in memory.

There are several variations on the sound-superhet technique. A common one is shown in block diagram form in Fig. 10. Two fixed-frequency oscillators run at 17.72 and 18.08MHz. The output from one or the other is selected and fed to one of the gates of a dual-gate f.e.t. mixer, where it beats with the incoming signal to produce i.f.s at 10.52MHz (R channel) and 10.7MHz (L channel). With the output from the 17.72MHz oscillator in use the R sound comes from the 7.2MHz carrier ($17.72 - 7.2 = 10.52\text{MHz}$) while the L sound comes from the 7.02MHz carrier ($17.72 - 7.02 = 10.7\text{MHz}$). When the system control switches over to select the output from the 18.08MHz oscillator the R and L sound signals come from the 7.56MHz and 7.38MHz carriers respectively.

Table 1: Astra sound carrier arrangements.

Mode	7.02MHz	7.2MHz	7.38MHz	7.56MHz
1	Language 1 L	Language 1 R	Language 2 L	Language 2 R
2	Language 1 L	Language 1 R	Lang. 2 mono	Lang. 3 mono
3	Lang. 1 mono	Lang. 2 mono	Lang. 3 mono	Lang. 4 mono

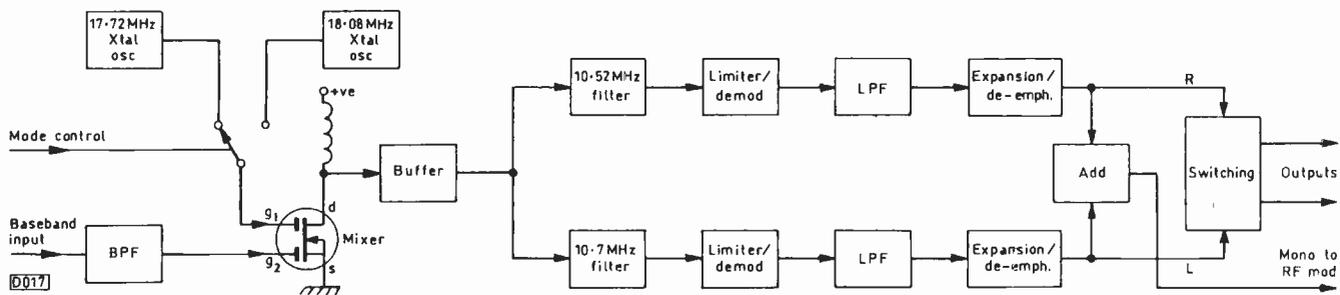


Fig 10: Superhet sound carrier selection system. The wanted carriers are shifted to 10.52 and 10.7MHz. Not all receivers have true Wegener Panda 1 expanders: the system is a licensed one and alternatives, which are known as soundalikes, may be used.

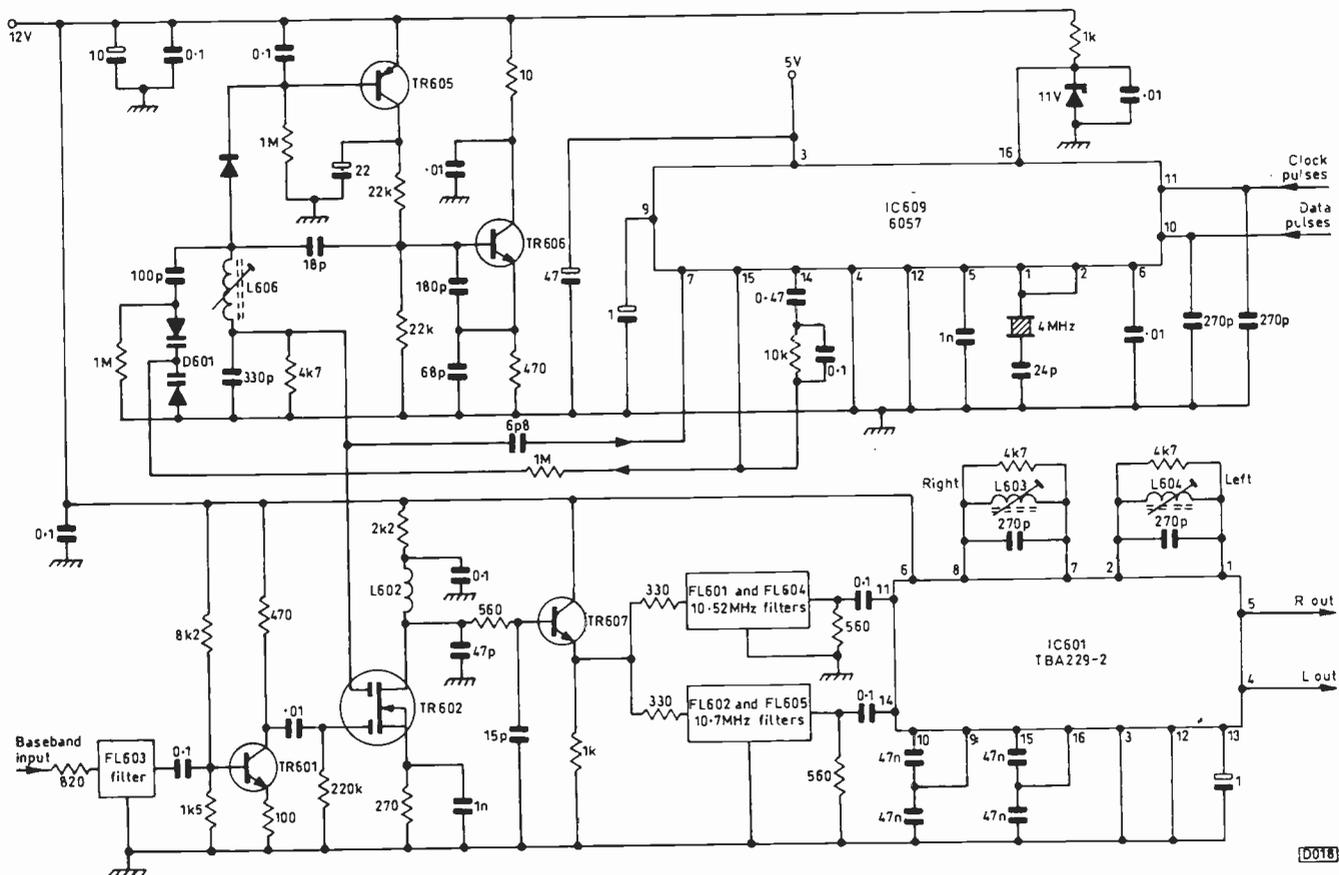


Fig. 11: Frequency-synthesis satellite sound tuning system, with effectively continuous coverage over 5-9MHz. The R and L outputs from IC601 in this Tatung design go to a dual Wegener Panda expander chip.

Instead of having fixed oscillators it's possible to use a variable or programmable oscillator: adjusting its frequency will tune, rather like a radio receiver, through the band of sound carriers associated with each satellite broadcasting channel. Fig. 11 shows one possible circuit. Tr606 is the local oscillator whose frequency is controlled by IC609 which contains a programmable divider and a 4MHz reference oscillator. These form a frequency-synthesis tuning system which is controlled by the receiver's microcomputer system control chip. The oscillator's output is fed to gate two of mixer transistor Tr602, whose other gate receives the whole spectrum of sound carriers from bandpass filter FL603 - this has a bandwidth of 5-9MHz.

The mixer's output contains all the sound carriers, converted to difference frequencies in the range 8-13MHz. Those centred on 10.52 and 10.7MHz are selected by ceramic filters FL601/4 and FL602/5 respectively and applied to pins 11 and 14 of the dual f.m. demodulator chip IC601. By programming IC601 any pair of sound carriers 180kHz apart (as in Table 1) can be brought into line with

the filters and demodulators. In this particular design the sound is tunable in 10kHz steps from 5MHz to 9MHz, and any required point can be stored in memory. These tuning/control systems will be described in detail later in this series.

The L and R outputs from pins 4 and 5 of IC601 are passed to de-emphasis circuits that can be switched between simple linear (50µsec) or Wegener-expander operation.

Earlier in this series we looked at the principle of the double-superhet. In the type of satellite receiver we've just considered the sound carriers undergo four frequency changes: in the LNB, at the indoor tuner, at the vision demodulator and at the sound carrier frequency changer.

Next Month

Having covered analogue TV sound systems, in the next instalment we'll examine digital TV sound broadcasting - the Nicam and MAC/packet systems now used with many terrestrial and satellite TV transmissions.

VCR Clinic

Reports from Eugene Trundle, Nick Beer, Chris Avis, Graham Richards, Brian Storm, Alfred Damp, Chris Watton, Ed Rowland, J.R. Cutts, Michael Dranfield and John Edwards

GoldStar GHV1240I

This machine produced an unstable E-E picture, with poor sync, white crushing and bright psychedelic colours. The cause, as is usually the case, was the 1 μ F a.g.c. reservoir/decoupling capacitor, in this case C715. It was open-circuit. **E.T.**

Akai VS23

This machine has a rather complex power supply, with a mains transformer, chopper circuits and voltage doublers. One of the more obscure faults that arises in this area is partial failure of C6 (220 μ F, 10V). The symptoms are wavy horizontal bars (like r.f. interference) across the picture and on-screen captions and intermittent colour in the E-E and playback modes.

It's worth noting that if the audio/preamplifier PCB behind the drum isn't earthed the syscon shuts the deck down within a few seconds in all modes. Beware of this!**E.T.**

Tatung TVR6111

We do a lot of Tatung servicing and have on several occasions come across the following fault: the reel drive intermittently fails to engage when fast forward or rewind is selected. If you get this symptom, check that lever trigger 260 is free to slide along brake plate 261. If it's stiff, the metal stop for the brake plate (formed from the deck plate) needs to be bent very slightly to the right as you view the underside of the deck from the front. The numbers quoted above are taken from the exploded deck diagram in the service manual. This machine also appears under the Amstrad banner. **E.T.**

JVC HRD150/Ferguson 3V45

The play symbol, a dotted triangle, was lit up the whole time the machine was switched on, whether or not the play mode was engaged. It was caused by leakage between pins 4 and 5 of the fluorescent display PCB. Someone must have managed to spill liquid through the cassette loading slot! Thorough scrubbing with surgical spirit removed the conductive deposit in this very high-impedance circuit. **E.T.**

Sharp VC381

Misalignment is becoming a common problem with older VCRs. Realignment usually provides a lasting cure, making repairs justifiable. This particular example suffered from intermittent playback chroma. When the colour was present there was patterning on it. The cure was to reset the carrier peak adjustment slightly. In the record mode there was no picture because the dark clip was misadjusted. **N.B.**

Granada VHSHX3/Hitachi VT8700

This old timer had been bought for £50 at a sale. There are still plenty of them about! The customer said that it

wouldn't play. On test there was no vision in the E-E mode – that's right, there were dry-joints in the i.f. can. It was the first time in years I've had that one. Next the supply guide post was missing, then the loading belt and the spool tyres were duff. After sorting that lot out and setting the machine up I found that it worked very well. An interesting point was that it had a large safety test label on the side from the previous day – presumably all electrical items in the sale had been tested. **N.B.**

Mitsubishi HS330

The complaint with this machine was that the sound would vibrate when the machine had warmed up. Having tested the machine for ages and heard no "vibration" I questioned the customer to find out whether she meant wow and flutter, which is not uncommon with this model. Not so. It seemed to be a buzz. So I had a poke around and had success – a buzz appeared on the playback sound. Its cause was traced to a dirty connection between the copper-coloured spring metal that earths the top of the cassette housing and the regulator heatsink. A clean and retension cured the problem. **N.B.**

Ferguson 3V54/55/57

Here's a trap for the unwary, like me. The VCR owner's house mains supply earth leakage trip had operated for some reason. When it was reset, the VCR was stuck in the aux mode. Embarrassment prevents a description of our efforts to restore sanity to the confused microcontroller chip and ourselves until a wiser colleague advised us to press the recessed "ch set" button. **C.A.**

Hinari VXL5

Two non-working, ex-rental machines we'd purchased had the same fault – when play was selected the tape laced, the drum ran very fast then the tape unlaced. The cause of the trouble was that the 6V supply to the drum feedback amplifier IC104 was very low as C145 (100 μ F, 10V) was short-circuit. We used a replacement rated at 16V. **C.A.**

Ferguson 3V54/55

We purchased a quantity of 3V54 non-remote control machines for reconditioning as the preferred 3V55 remote control version wasn't available at the time. It surprised us to find that infra-red receivers were fitted, though the machines would respond only to manual operation. When we traced the signal path from the IR receiver's output we came to a link, which had been cut, next to connector CN402 on the small eject-tracking PCB PC1614/1626. When the broken link is replaced the 3V54 becomes a fully remote-controlled 3V55! **C.A.**

Hitachi VT64

Playback was all right but when record was selected the drum and capstan failed to rotate though the record indicator

lit and the tape laced up briefly before unlacing again. We found that the record/play switching voltage double-diode block D626 was open-circuit on the record side. By coincidence we found a similar faulty device recently in the sound section of an older Hitachi machine. In both cases a couple of good old 1N4148 diodes wired in back-to-back proved to be a suitable replacement. C.A.

Sentra VX8100HQ/Samsung VI710

For no erase replace transistor Q0501. It's a 2SD261 and no other transistor will work in this position! The cause of its failure is the erase head going open-circuit intermittently because of the plug/socket arrangement. Remove this and solder the lead on directly. How many more types of VCR will need this modification? G.R.

Hinari VXL8

The problem, because of mains-borne transients, was no E-E operation, no channel changing, cannot program etc. with just the letter E in the display. Unsolder the back-up capacitor for thirty seconds then reconnect it. Switch on and the microcontroller chip should recover from its crash. We've had this more than once and the routine has worked each time! G.R.

GoldStar GHV1248I

The E-E pictures were pulling, with ragged edges, more so on some channels than others. Attenuating the input signal (via the aerial lead) established that it was an i.f./a.g.c. type fault – in fact the symptoms were identical to those you get with some CUC series Grundig TV sets. Replacing C715 (1 μ F, 63V) put matters right. We assume that it provides a.g.c. smoothing but as we don't have the manual we can't be sure. G.R.

Alba VCR6000X/Sentra VX8400

As mentioned by Nick Beer in the January Clinic these machines very often suffer from tuning drift. Decoupling capacitors C133/4/5 for the VT line are prone to being leaky. In addition hardwiring the VT line to cure leakage will indeed provide a cure. But the reason for this tuning drift isn't leakage between the print tracks: it's caused by leakage on the component legs themselves! – around C134. The problem is caused by the quantity of glue that's put around the components in this area of the PCB during manufacture (top upper left-hand side with the board hinged up). I suspect that this glue absorbs moisture and then slowly becomes conductive. Thus rather than hardwiring it's easier and quicker to remove this glue and replace C134 (0.1 μ F). The μ 574 33V regulator on this board can also be the reason for tuning drift. G.R.

Panasonic NVJ42

Although this machine would accept a cassette it was difficult to get the cassette back and the mechanism spooled backwards and forwards a great deal, rarely performing any function correctly. Checks soon showed that the solenoid which engages the mechanism was operating erratically. Instead of a satisfyingly solid clunk when the operation buttons were pressed only an anaemic click was heard. The solenoid drive system has two parts, a kick and a hold circuit. D603 in the kick section was open-circuit, a replacement restoring normal operation. B.S.

Panasonic NVF55

I seem to get more than my fair share of search-tuning faults. This machine would search but wouldn't lock on to stations. Checks on the sync low, a.f.c. defeat and a.f.c. feeds showed that there was nothing amiss to and from the demodulator pack, so out came this plug-in pack, revealing a surface-mounted diode (D6701, type MA151WK) with one end missing. A replacement cured the problem. B.S.

Ferguson FV31R

This machine had a nasty habit of breaking its back-tension arm as the deck mechanics mistimed themselves, no matter how carefully the instructions in the manual were followed. We noticed that when the machine set off in play the drum motor didn't rotate. This turned out to be a vital clue. The drum stood still because the 5V supply to pin 2 of chip IM02 was missing. From a look at the circuit diagram this appears to be totally unrelated. The PCB layout holds the clue: the link that supplies 5V to IM02 also supplies the pull-up resistor RT67 in the mode-sensing circuit, the cause of the trouble being a dry-joint on this link. With the dry-joint resoldered and the deck mechanics realigned yet again everything worked correctly. All that was left to do was to fit a new back-tension arm. A.D.

Ferguson 3V44/JVC HRD140

The drum and the capstan were both running slowly. A check on the servo reference signal, using a frequency counter, showed that it was running at only 2.5MHz. The cure was to replace the 4.433MHz crystal in the chroma circuit. A.D.

Matsui VX3000

The complaint was of loss of tuning overnight. On the bench however no channels could be tuned in. R6045 (33k Ω) was open-circuit. A.D.

Akai VS22

The problem with this machine was a bad hum bar on the E-E pictures. We found that C4 (47 μ F, 25V) on the power supply PCB was leaky. A.D.

Hitachi VTM722

The E-E audio was low and distorted while playback of a prerecorded tape produced only a cyclic chirping sound. We found that the always 9V supply to IC401 was low at only 4.9V because zener diode ZD854 on the power board was short-circuit. A.D.

Toshiba V83

The capstan motor was clearly running too fast. A check on the drive voltage showed that it was high at about 10-11V instead of 6.7V. Checks around the servo chip IC501 showed that although the voltage at pin 14 (capstan a.p.c.) was correct at 3.3V the voltage at pin 15 was only 0.9V instead of 3.3V. Scope checks at pins 19 and 20 (CTL in and out) showed that the control pulses were of correct amplitude though the frequency was of course high because of the excessive tape speed. The tracking input at pin 28 varied the length of the waveform, so all seemed to be correct here.

The next check was on the FG pulses at TP518. The waveform here had gaps in it and varied a little in amplitude. Unfortunately I ignored this, putting the irregularity down to the motor's increased and wowing speed. Wrong decision! So after replacing IC501 and finding that the fault remained as before I had a closer look at the FG pulses. When I dismantled the capstan assembly I found that the coil which forms the stator of the pulse generator was dry-jointed at the point where the enamelled copper wire is connected to the terminal.

C.W.

Amstrad VCR4600

This machine was dead with the 2A fuse F603 open-circuit. I checked the rectifiers in the main power supply and as they all read o.k. a new fuse was fitted. It blew only a few seconds after switching the machine on again. The cause of the fault turned out to be C836 (3.3µF, 35V) which is in one of the voltage regulator circuits on the main servo/system control panel.

C.W.

Logik VR950/Samsung VI611

This machine came to us with the infra-red sensor broken and the loading arms flopping about all over the place. The owner said that she'd tried to remove a jammed cassette and had damaged it in the process. What in fact appeared to have happened was that the nylon gear sector – it's the fan-shaped bit on the loading mechanism – had split where the steel pin is located, allowing the pin to slip out. Hence the looseness of the loading arms. A spot of Superglue was all that was required to repair the infra-red assembly. A new gear sector and pin – they are separate items – had to be ordered from Mastercare.

Imagine our surprise when, a few days later, the postman delivered two packages from Mastercare, one a box containing the gear sector, the other a jiffy bag containing the pin! Anyway fitting the parts and removing a thick ring of oxide from the capstan restored normal operation.

E.R.

Saisho VR1200HQ/Matsui VX820/Hinari VXL35

Failure of Q02, type 2SD1207, is common with these machines. We find that a TIP41C with a heatsink is a reliable replacement.

J.R.C.

Hitachi VT150

This machine is almost the same as the VT130 but has long play. The problem was a tape stuck inside, no functions and no eject. Whilst checking around we found that the M54649L loading motor and cassette lift motor control chip IC902 was very hot. As both motors ran when powered from a separate d.c. supply we replaced IC902. Unfortunately this made no difference. Voltage checks then showed that the 12V supply at pin 9 was very low at 0.5V. It's worth noting that this chip has two 12V supplies, one at pin 7 for the internal logic and one at pin 9 for the high-current motor drive.

Tracing back from pin 9 brought us to the power supply where IC851 had 18V at its input but no 12V output. Although the power supply panel looks the same as that in the VT130 the regulator chip is different – type STK5476. This is a 12-pin device with only pins 1-10 used. We didn't have one in stock though we did have the STK5471 as used in the VT130. When we removed the STK5476 we

found that the heatsink was drilled with two sets of holes. The smaller 10-pin STK5471 was quickly fitted to the heatsink, restoring full operation. Could the STK5476 have been fitted because of a shortage of the other type of regulator?

M.Dr.

Hitachi VT7000

This two-part tuner-timer/VCR came in with the symptoms of a dirty head. Cleaning this appeared to cure the fault but when a recording was made and played back nothing but snow and sound had been recorded. After borrowing a service manual we found that the record 9V supply at pin 8 of the TA4190 chip IC205 was very low at only 1V in the record mode. The source of this supply was traced to a small relay, RL402, on the bottom PCB. There was 9V at the input to this relay but no output. As we couldn't find a relay with the same pin connections amongst our scrap panels we decided to try cleaning the contacts of the old one. We used an Electrolube contact cleaning strip that's specially made for this type of job. It provided a complete cure and after a long soak test the machine was pronounced fit again.

M.Dr.

Toshiba V71

As a new reel motor failed to restore reel operation we started to make checks in the drive circuit. The conditions at the fast forward and rewind selection pins of the TA7267P motor drive chip IC603 were correct but there was no motor supply at pin 3. Replacing this i.c. cured the problem.

For reference purposes note that in the rewind mode pin 7 is at 12V, pin 6 drops from 12V to 5V then returns to 12V, pin 5 changes from zero to 0.7V, pin 4 is the chassis pin, pin 3 changes from zero to 5V for a couple of seconds then rises to 10V, pin 2 changes from 5V to zero and pin 1 stays at 5V. In the fast forward mode the voltages are the same except that pin 2 remains at 5V and pin 1 changes from 5V to zero. It's not uncommon for the reel motor or IC603 to fail, so the above readings may be of help in deciding which item to blame if you don't have the manual.

J.E.

Akai VS105

Everything worked correctly except eject, the problem here being that the cassette came out flush with the front panel and couldn't be gripped. All the mechanical functions are set in motion by a motor which drives the main rotary cam beneath the deck via a plastic toothed belt and worm pulley. The carriage up/down lever is driven by a groove in the rotary cam. It was not travelling far enough to push the carriage all the way up, i.e. to eject. When the metal plate that covers the rotary cam was removed we saw that there was a split across half the width of the cam. Replacing the cam and retiming the mechanism cured the problem. Only the eject mode was affected because the other modes used the good portion of the cam.

J.E.

Ferguson 3V44/JVC HRD140

This machine wouldn't accept a cassette. As the power supply circuit protectors were intact we turned our attention to the carriage assembly. The cassette could be loaded manually, after which all functions such as fast forward, rewind and play worked normally and the cassette was ejected correctly. We found that the cause of the problem was the leaf switch at the right-hand side of the carriage assembly. All was well after fitting a replacement.

J.E.

CD Player Casebook

Reports from Nick Beer,
Mike Leach and Savio Da Costa

Toshiba SL55

In the February casebook I mentioned an SM55 that refused to play some discs because the lens was dirty. It seems to be a problem with these machines – I've had others since. Despite the large metal cover over the mechanism the lens gets badly affected by dirt. **N.B.**

JVC XLE300

With consumer electronic equipment becoming ever more complex we all too often overlook the obvious. This was just such a case, and I could have kicked myself for not realising sooner what was happening. The complaint was that the player sometimes wouldn't read a disc, though when it did the results were o.k. On test in the workshop it wouldn't read any discs at all. So we assumed that the laser assembly was faulty and fitted a replacement. As this seemed to cure the problem we set up the machine and left it on a test run. Just for good measure we tried a long-play disc as well. This too was o.k.

When the next disc was tried however the machine took an extremely long time to read the TOC – in fact it made several attempts before it played the disc. After taking out the new laser assembly and again checking the mechanics I eventually realised what was going on. When a disc that

lasted say an hour or more had been played the laser unit returned only very slowly to the beginning to read the next disc, which rotated very slowly. This in fact was the key to the problem. Fitting a new sled motor provided a complete cure. **M.L.**

Akai ACM370L

With most discs that were tried in it this midi system wouldn't play the first one or two tracks. The outer tracks played all right. As the machine always read the TOC we decided that the laser unit was o.k. After some soul-searching we resolved the problem: the PLL coil was marginally out of adjustment and wouldn't lock up at the beginning of the disc. Slight adjustment of the coil was all that was necessary. **M.L.**

Sharp DX650

This American (110V) machine came on when a new mains transformer from RS Components had been fitted to adjust for the different mains supply voltage. But when a disc was inserted CD showed in the display. The sled motor had seized – a drop of oil on the bearings freed it. After that the machine worked well. **S.DaC.**

VTR. Terry Martini, 6 Levant House, Mile End Road, London E1 4RB. 071 790 6807.

Wanted: Any Philips LaserVision discs (CLV or CAV) or any CD-Video (single or extended play) discs. B. Willis, 50 Sarum Crescent, Wokingham, Berks RG11 1XF. 0734 784 002.

Does anyone have a collection of *Television* from the first issue (April 1950) to 1977? Would be going to a very good home! Also maybe *Practical Wireless* from the first issue to 1970. Michael Dranfield, Dranfield and Harrop Colour TV-Video, 62 Fairfield Road, Buxton, Derbyshire SK17 7DW. 0298 71689 day, 0298 26094 home.

Wanted: Service information for the Lloyds LVC3000 VCR, made by NEC. S. Burns, 1 Harewood Drive, Ilford, Essex IG5 0PJ. 081 550 8222.

Wanted: LOPT for the Waltham Model 1401. Also a TDA1104, TDA1106 or MB1106 i.c. B. Battams, 23 Dudley Drive, South Ruislip, Middx HA4 6QN. 081 845 5123.

Wanted: Mains transformer for the JVC Model 7170GB and a LOPT for the Panasonic TC381GR. I.E. Finch, 6 Avon Court, Avondale Road, Luton LU1 1DT. 0582 487 533.

Wanted: Circuit diagram for the Bush Arena Model BC6130A (Rank Z718G chassis). Photocopy would do. D. Maciver, 46 Newhaven Main Street, Newhaven, Edinburgh EH6 4TD. 031 551 1616.

Can anyone supply service and operating manuals for the Houston Instruments EDMP-56E plotter? Stephen Shaw, PO Box 1404, Randfontein 1760 S. Africa.

HELP WANTED

Wanted: An e.h.t. transformer for the Tektronix type 545B scope, part no. 120-0308-00. Also an August 1986 copy of *Television*. W. Larman, Derimar, Horton Road, Stanwell Moor, Middx TW19 6BD.

Can anyone supply the correct circuit for the light gun that's used with the Binatone 01/4907 video game? Roger Burchett, 12 Ormonde Road, Hythe, Kent CT21 6DN. 0303 267 969.

Wanted: Circuit diagram or service manual for the LCM Electronics Ltd. telephone answering machine type P148F. F.C. Hughesdon, 19 Lower Road, Higher Denham, Uxbridge, Middx UB9 5EA. 0895 833 774.

Can anyone supply an AUX-box for the Luxor Model 6615 TV receiver, also a service manual? R. Burgess, 82 Bressey Grove, London E18 2HX. 081 989 6830.

Can anyone supply details of the modification to convert a Philips BSB receiver, Model STU902, for PAL reception? Peter Clarke, 28 Wentworth Gate, Linton Park, Wetherby, W. Yorks LS22 4XD. 0937 582 828.

Can anyone supply a battery or batteries for the Sony Model SLF1UB portable VCR – they are 12V types? R. Buckley, 25 Clarence Place, Morice Town, Plymouth PL2 1SF. 0752 560 660.

Wanted: Manuals for the following equipment – Sony VO1810 U-Matic VTR; Teac reel-to-reel X1000M; Sharp VC9300H VCR; Sony AV3420CE portable reel-to-reel

Inside the Ferguson IKC2 Chassis

J. LeJeune

It's some four years now since Ferguson started to use Thomson-designed TV chassis. We are becoming familiar with a certain family likeness between them, as was the case with the 'old' Ferguson-designed chassis. The IKC2 is obviously a descendant of the ICC5 with which it bears many similarities, including the infamous though quite reliable thyristor field output stage. So what's new?

For one thing there's a totally different discrete-component chopper power supply. This is partly due to the use of a different colour decoder chip, type TA8659CN, which also incorporates the sync circuitry and the field and line time-base generators – you will recall that in the ICC5 a TEA2029C chip produced the line, field and chopper drive waveforms. Other features of the TA8659CN include automatic switching between PAL/SECAM/NTSC operation and a sharpness control circuit. The chassis is used in models with 41 and 51cm tubes. Unfortunately the audio section is nothing to rave over and has given rise to some customer complaints – in early versions of Model 41P3 the audio is definitely odd!

This article explains the new features incorporated in the IKC2 chassis, notably the power supply, and aims to help with fault finding, covering some common failures and how to deal with complaints about audio performance.

The Power Supply

Fig. 1 shows the power supply circuit used in the IKC2 chassis. It's a conventional chopper arrangement, but has three modes of operation – start-up, standby and full power. The chopper transformer LP36 provides mains isolation, and feedback from the secondary to the primary side of the circuit is also transformer-coupled (LP42), just as in the ICC5.

At switch-on the power supply operates in its start-up mode. Transistors TP09 and TP12 form a relaxation oscillator that produces a sawtooth waveform at a frequency of approximately 15kHz. The ramp is generated by CP09 which charges via RP09 and RP03. DP13 clamps the waveform to chassis potential. It's then fed to the base of amplifier transistor TP13. To get the oscillator running, a start-up voltage is provided by half-wave rectification from the mains supply – one side of the bridge rectifier provides the rectification, the feed being via RP36. RP06 provides a feed for the amplifier and driver stages.

Once the chopper circuit gets going and the secondary supply voltages are established the start-up oscillator is disabled by the crowbar circuit consisting of TP02/3 and the associated components. It senses the rise in the voltage produced by the rectifier circuit DP30/CP30. When the voltage at the junction of potential divider RP02/7 is sufficient to turn on DP20, the crowbar transistors TP02/3 latch on, removing the supply to the start-up oscillator.

TP02 and TP03 are also used in the standby mode, when they operate in a slightly different manner. Because the line output stage is inoperative in this mode, the drain on the power supply is very light. As there are no line pulses to drive the regulation system, the power supply runs in a kind of self-oscillating condition. What happens is that the start-up oscillator delivers 'bursts' of 15kHz drive. When the voltage developed across CP30 rises sufficiently, TP02/3

shut down the oscillator. The whole power supply then stops and the voltage across CP30 falls. Thus the oscillator can run again. This 'squegging' action provides a rudimentary level of regulation on the primary side of the chopper transformer, maintaining the voltage levels sufficiently for the standby condition.

To switch the set to full power operation a remote control command produces a low output at pin 20 of the microcomputer control chip IR01 (see Fig. 2). TR16 and TR17 then switch on, raising the PO (Power On) line to 15V. This brings the TA8659CN chip IV01 into operation and the line drive appears. The control action is at pin 40 of IV01 – it rises to 9V in the on condition. The line output stage now starts to work and pulses from pin 9 of the output transformer are integrated to produce a sawtooth waveform at the base of transistor TP54, which drives TP13 via TP69 and LP42. TP13 receives negative-going pulses that cut it off.

Now for the regulating action in the chopper circuit. Transistor TP53 acts as a comparator. Its emitter is held at a constant 5.6V by the action of zener diode DP55 and diode DP54 – the combination of a zener diode and a silicon diode provides the correct temperature coefficient. TP53's base senses the h.t. voltage via the potential divider RP51/PP52/RP52, PP52 being used to set the h.t. voltage. Thus the voltage at the collector of TP53 and the emitter of TP54 varies as the h.t. voltage varies. This sets the point during the sawtooth waveform at the base of TP54 at which this transistor switches on. TP54 is in fact acting as a pulse-width modulator. Note that the h.t. is set at different levels for different tubes. In Model 41P3 the h.t. should be 107V; in Model A51F it should be 111V with an Hitachi tube and 113V with a Philips/Videocolour tube.

As TP54's on time varies, so the conduction period of the chopper transistor TP29 alters to stabilise the output voltages. The base of transistor TP13 is forward biased via RP13. Negative-going, width-modulated pulses are fed to its base via DP17 and DP16 to switch it off. When TP13 is on, TP16 is off and TP17 is on – these are the chopper driver transistors. When TP13 is switched off TP16 conducts and TP17 switches off. Current via CP24 then drives the chopper transistor TP29 into conduction. The voltage across CP24 is limited to 2.1V by the combined junction voltages of the three diodes DP24/26/27. When TP13 switches on again TP17 conducts, discharging CP24 and cutting off TP29.

The longer TP29's period of conduction, the greater the amount of energy stored in the core of the chopper transformer and the higher the voltages developed by the rectifier diodes when TP29 switches off to release this energy.

TP18 and TP19 form an excess-current trip. Excess current is sensed across resistors RP32 and RP34 which are in series with the chopper transistor. When TP18/19 latch on, the drive to TP16/17 is removed. The supply to the start-up oscillator is also removed because DP08/9 conduct. There is auto-reset at a rate determined by the time-constant of CP18 and RP26.

The Line Timebase

Apart from the fact that, as in the ICC5 chassis, the output transformer has a load winding for the field output

Fig. 1). This removes the line drive to TP54 with the result that the power supply operates in the standby mode. Note that TV02 (type BC548C) is incorrectly shown as a pnp device in the circuit diagrams in the service manuals.

The Field Timebase

The field timebase has unusual features throughout. Fig. 4 shows the circuit. Although the TA8659CN chip IV01 produces a field drive waveform at pin 31 this is used for sync purposes only. The field sawtooth waveform is generated across CF06, which is linked to the 180V line via the two 1.5M Ω resistors RF01/02. The ramp is negative-going however, CF06 being linearly discharged during the forward scan period via the pnp transistor TF08 which is driven at its base by the feedback capacitor CF02. IV01's field drive output is fed to the base of transistor TF25 which produces negative-going pulses at its collector to synchronise TF08. The negative-going field ramp is fed to the non-inverting input (pin 3) of operational amplifier IF01a. This is half of a TL082 dual junction f.e.t. operational-amplifier chip. The height control PF11 is part of the negative feedback network connected to IF01a's inverting input (pin 2).

The second operational amplifier IF01b is used as a pulse-width modulator. IF01a produces a negative-going output ramp at pin 1. This is applied to the non-inverting input of IF01b (pin 5). IF01b's inverting input (pin 6) is fed with a line-frequency sawtooth waveform (produced from integrated line flyback pulses). Pin 7 (output) of IF01b goes high whenever the voltage at pin 6 exceeds that at pin 5. The result at pin 7 is a series of line-frequency pulses whose width increases as the field ramp progresses – this is illustrated in Fig. 5. During teletext operation an additional 25Hz signal is applied to pin 6. This destroys the interlacing to remove vertical jitter.

The width-modulated line-frequency pulses are applied to the gate of the field output thyristor TF16 to switch it on. The field scan coils are connected in series with RF24/20/23, the winding between pins 5 and 6 of the line output transformer, and TF16/DF16 between the 13V supply and chassis. During the field flyback the thyristor is not triggered and DF16 rectifies the line-frequency pulses picked up by the winding on the transformer, charging CF25 to about 80V. This produces a voltage difference of about 65V across the scan coils, sufficient to produce a rapid flyback. When the thyristor is triggered on at the start of the field scan the pulse is of short duration. TF16 switches off when the next line pulse is produced by the transformer. Thus TF16 is on for only a brief period. It's switched on progressively earlier during each line, remaining on for a longer time. As a result the voltage across CF25 is reduced linearly to approximately 3V at the end of the field scan. This integrating action produces a linear field scan current.

Signal Processing

Colour decoding, sync processing and generation of timebase drive waveforms are carried out by the TA8659CN chip IV01, a Toshiba device with 64 pins. Though designed for multi-standard operation, UK sets are sold as PAL-I only models. Thus many of the pins are not used, being left open-circuit or returned to chassis via resistors. It has two crystal oscillators, one working at 4.43MHz for the colour decoding and the other at 503kHz (approximately 32 times line frequency) in the line sync phase-locked loop. Direct rather than count-down sync is used for the field drive in order to cater for non-standard signals.

The RGB output stages, of the class AB type, are on the

c.r.t. base panel which has red and green gain and cut-off controls for grey-scale setting.

Tuner/IF Section

The tuner and the i.f. circuitry are contained within a screened compartment, their separate modules being soldered into the main PCB. The tuner is a Thomson MTP-I-2011, which has a dual-gate MOSFET r.f. amplifier stage with reverse bias a.g.c. It incorporates the PLL tuning control system. An LA7550 chip (IS10) amplifies and demodulates the sound and vision signals. It incorporates a d.c. volume control system. I.F. bandpass filtering is provided by a single-ended input SAWF.

Audio Output

A TDA2030A chip provides the audio output. It's operated with 30V and -30V supplies. The circuitry is simple and easily understood, but the peculiar audio quality provided by some Model 41P3 receivers requires a bit of explanation. Early production sets have a 24 Ω speaker at the side of the cabinet. There's space for a similar unit at the opposite side, and one of the same type can be installed, wired in parallel with the existing speaker. An immediate improvement in sound quality will be noted. The sound is louder of course. Any worries about the TDA2030A overheating because of the doubled load current appear to be unfounded. Louder sound can also be obtained by reducing the value of RA07 in the feedback circuit from 5.6k Ω to 3.9k Ω , as in Model A51F. This increases the power available to around 5W.

The plastic moulded cabinets tend to rattle at high volume. Ferguson has available a small kit of damping pads to stop this – it's quite effective. Model A51F is the main suffered from this malady.

The Microcomputer Control Chip

Control of the receiver's functions is the responsibility of the TMP47C634N FERG 01 microcomputer chip IR01. These include on-screen displays, keyboard scanning and front panel display matrixing, the analogue controls and power on-off. Most of the operations are straightforward but the power control port, pin 20, is a useful one to know. Fig. 2 showed the circuitry and we've already seen that pin 20 goes low for power on, switching TR16 and TR17 on – TR16 is another transistor that's shown as a pnp instead of an npn device in the official circuit diagrams. There's a short delay in the application of drive to the line timebase as CV02 in the safety circuit (Fig. 3) has to charge. This prevents any wildly incorrect-frequency drive being applied to the line output stage, with the possibility of damage.

Teletext and externals

Models 41P3 and A51F are fitted with a scart interface and Fastext PCB. Demodulated video output signals are available at pin 19 of the scart socket while pin 20 accepts an analogue video input. In Model A51F front-panel Cinch connectors are paralleled with the scart socket. RGB input signals can be fed to the scart socket, after which they pass to a CD4066B switching chip that sends either external or teletext RGB signals to the display circuits. The two-chip Fastext decoder is controlled by IR01 via an I2C bus.

The scart/text modules vary between the 41P3 and the A51F, but only in minor details. Both have an on-board 5V regulator whose input is obtained from the chopper's 7V

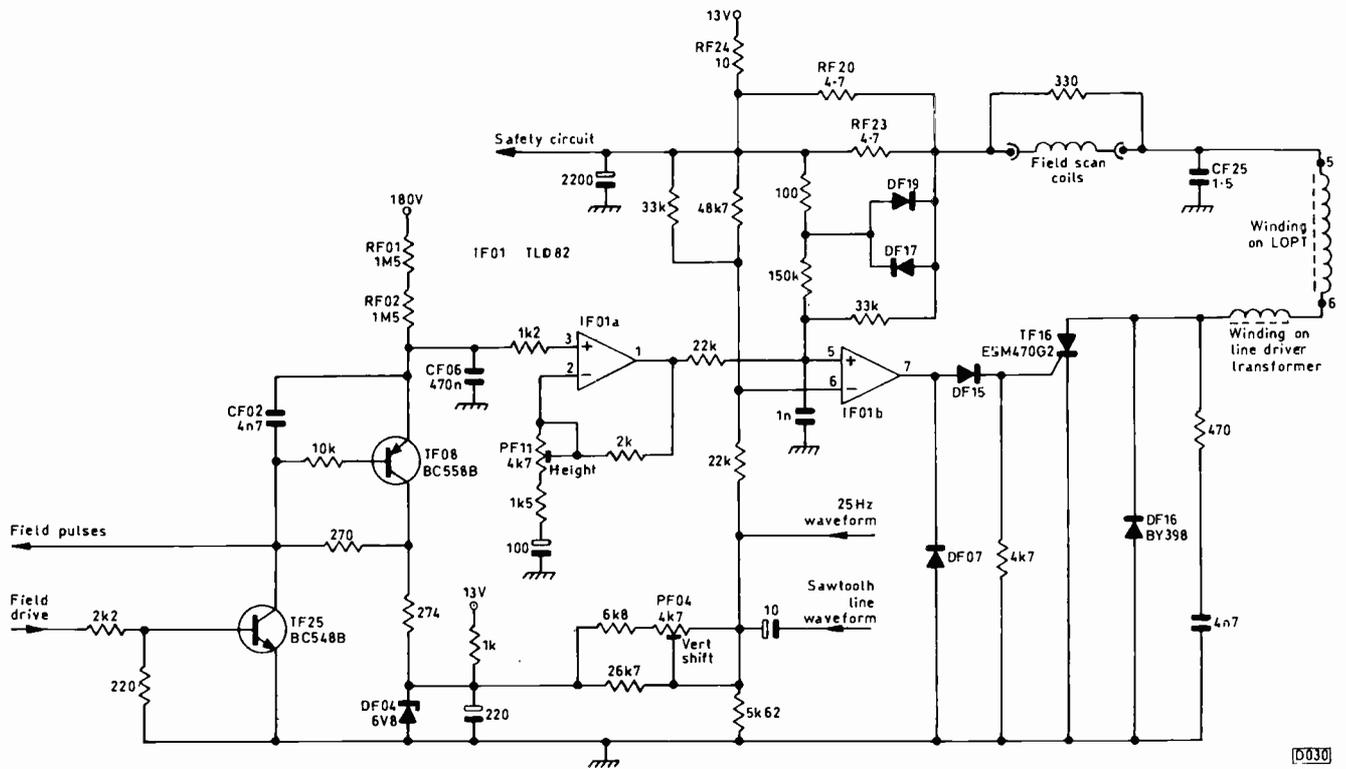


Fig. 4: The field timebase circuit.

output but requires, in addition, the presence of the line output stage derived 13V supply (V5) to enable it. A switch-on delay is included in the regulator circuit to prevent operation during the power-up sequence.

The scart interface handles composite PAL input and output signals, stereo audio input and output signals (there's only a mono output stage however) and RGB inputs. Pin 8 is for AV switching and pin 16 for RGB switching.

Servicing

While the chassis has a good reliability record the fact that it's tightly packed with components can cause difficulty when fault tracing and repairs have to be carried out. The copper side of the PCB is marked with the positions of the major components. This helps with location, but the circuit diagram is confusing in that lines which join don't always have a dot while use in a few places of the Continental habit of lumping wires into a 'loom' has infiltrated into publications that were once famed for their clarity and well thought-out design. Because of its low fault rate the chassis is not a familiar one to most engineers. This has made it, rather unfairly, unpopular.

Since many faults can cause the power supply to shut down it's possible to test the latter on its own in the standby

mode. Running it at full power is not possible because this requires line pulses to drive the regulation system. To test the power supply on its own in the standby mode, disconnect pin 20 of IR01. Note that in the standby mode the voltage outputs obtained from the power supply will be approximately 25 per cent low and not in their correct ratios.

Faults in the IKC2 chassis are generally confined to the line output stage and the power supply, as you'd expect. A common complaint with early production sets was of tripping off at high beam currents. This was remedied by a string of modifications. Whilst these cure the trouble they are not easy to implement in the ordinary dealer's service workshop. For the brave however here are the details:

Change TL19's heatsink to a new type, part no. 50855846. Connect an 8.2Ω, 10% 10W resistor and a 2,700pF, 20% 100V capacitor in parallel and mount them on the new heatsink using the clip assembly that comes with it. These components replace jumper wire J138 in the h.t. feed to the line output transformer, so remove the link and connect the RC combination in its place via flying leads. Change RP18 to 1kΩ, 5%; C54 to 220nF, 63V; RP55 to 220kΩ, 5% 0.16W; and RP26 to 3.3kΩ, 5% 0.25W. Add a 22kΩ, 5% 0.25W resistor (RP50) between the base and emitter of TP54. If tripping still occurs, the value of RP26 may be further reduced as follows: to 1.8kΩ with 14in. sets, 1.5kΩ with 15-17in. sets or 1.2kΩ with 20in. sets.

DP28 going short-circuit will prevent the power supply working because the chopper driver stage has no supply – a clue is that RP06 will be quite hot. The 180V rectifier DL11 going short-circuit and its associated resistor RL11 open-circuit will affect the pulse feed from the line output transformer to the power supply with the result that the set trips.

Finally, take care when desoldering components in this chassis: good-quality desoldering wick should be used.

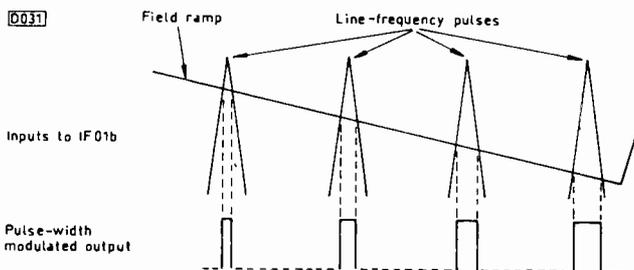


Fig. 5: Operation of the pulse-width modulator (IF01b).

A Day at the Thick End

Chris Watton

It was a cold, rainy dismal Monday morning. As I entered the shop at around 9.20 a.m. to start the week with the usual zest and vigour I saw a strange figure, an unshaven man with unruly hair, dirty shoes and a solemn look. It was fearsome at this time of the morning, but as the haze of cigarette smoke cleared and the view through my bloodshot eyes came into focus I realised that some oaf had left a mirror facing the shop door when we closed on Saturday.

Turmoil

The day was uneventful until 9.35. Then all hell broke loose and the phone, which I'm sure is connected to the shop's door bell since one doesn't go without the other, didn't stop until lunchtime. We're the only TV shop in a village about ten miles from the nearest town and I'm sure all our customers think that if it's got a plug, a length of wire or some batteries we must be able to repair it or, worse, tell them how to use it. The recent bout of electric fence generators proves the point. Must be the time for the sheep to eat all the bits that we don't when the cabbage harvest is over.

Every Monday starts the same way for us. First we sort out the jobs we forgot to do on Saturday, then we start on the repairs where loan sets have been put out.

Some Easy Ones

The first of these was simple, a 22in. manual control Philips K30 that was tripping. It still tripped after the tripler had been unhooked. Oh no, please don't be difficult this early in the morning. After a quick check on the line output transistor I started to smile again – it read about $2k\Omega$ between its emitter and collector. A new BU208 and a quick look for reasons why the old one should have failed soon revealed some dry-joints in this area, one on the flyback tuning capacitor. I'm sure that this was the cause of the transistor failure. Anyway the set was now working and displaying a good picture. So we put it on the soak test rack and lifted the next one on to the bench.

This was a Samsung CI1541ZG with a line across the screen. The field output stage in this chassis receives its supply from the line output stage. But not on this occasion as the 1.5Ω safety feed resistor R412 had failed. Replacement cured the fault and the set was left to run for the rest of the day to prove that no other fault had caused R412's death.

The Leslie Speaker System

After the first cup of tea and with two easy jobs under my belt I was ready for anything. I let myself in for a real treat, a Leslie speaker system. Now for those of you who haven't had the pleasure of acquaintance with this magnificent job here is what it is. An immense cabinet made from one-inch thick veneered plywood, measuring some 4ft 6in. by 3ft by 2ft and weighing about as much as a Philips G6 (remember those?), houses a 15in. woofer, two mid-range speakers and a tweeter, not forgetting the US-made solid-state amplifier in the bottom. There are also two motors that drive a rotating baffle for the woofer, and a pair of horns into which

the tweeter is directed. In principle these rotating devices make the sound come and go. Questionable I think, but the owner assures me that this is what makes an organ sound like an organ. The problem was that the mains fuse kept blowing. Its cause was in the power supply where four huge diodes form a bridge rectifier for the amplifier. Two of them were short-circuit.

A Satellite TV Job

Now for a very important job. The boss had been complaining about the spotty picture his satellite TV system produced. My recent visit proved that the dish alignment was o.k., so the LNB was condemned. Right again. Four jobs in a row. This can't last! The new LNB was fitted in record time and a check on all channels produced perfect results. Incidentally although the satellite TV system is an Amstrad SRX200 the LNB I fitted was a new type called Continental. It's a smaller unit and has screws rather than rivets to hold it together. The F connection is at the bottom instead of the face side. It produced much better quality than the standard unit, with much less background noise – and is about ten quid cheaper.

A Tripping Sony TV

The last job before lunch was an 18in. Sony set that tripped. I don't know much about these sets but some basic fault-finding procedures soon put me on the right road. As with all sets that are tripping we first have to find out whether the fault is in the power supply or elsewhere. The way I do this with most sets is to identify the output from the power supply to the line output stage, disconnect this and use a 60W bulb to replace the load. If the tripping stops, the h.t. voltage can be checked. If this is correct the cause of the fault is likely to be somewhere in the line output stage.

Back to the Sony set. I followed my own advice and the tripping stopped. As the h.t. was about right at 118V I assumed that the power supply was o.k. So I removed the bulb and for some reason the idea that there must be a short-circuit in the line output stage was in my head. After much checking of diodes and capacitors it occurred to me that the line output stage was perhaps open-circuit rather than short-circuit. To test this theory I again disconnected the power supply and ran it with a lamp as the load. It worked. Then I disconnected the lamp and the power supply started to trip. I reconnected the power supply and put my lamp on the case connection of the line output device, a gate-controlled switch (GCS). The power supply now worked. This seemed to make fault finding much easier. I came to the conclusion that there was no line drive. As the bench was a bit piled up and the scope wasn't to hand I had another brainwave. If I put the meter on to its frequency counter range and checked for line drive I should get a reading of around 15kHz. So I checked at the gate of the GCS and found that there was a 15kHz signal here. It was time to check the GCS, which was open-circuit. Well, all this had led me somewhat astray but maybe next time I'll remember that the power

supply won't run with an open-circuit load. And once again praise to the man who invented light bulbs.

After Lunch

Back from a healthy lunch – two cream buns, a bag of chips and a tin of pop followed by a very dry cigar – I now felt awful. But the first job that faced me was a set with which I'm more familiar than the one that preceded the refuelling session. It was a Finlux 9510 that was dead. My attention was drawn to the blackened d.c. fuse, so I checked the chopper transistor which was short-circuit. Experience has shown that when this device has failed the 270kΩ resistor Ru17 will be open-circuit. Replacing these two items brought the set back to life but there was no sync. Transistor Tb1 on the video output panel is the video inverter for the sync feed. It was open-circuit. Incidentally if you've not come across these sets before don't try to open the tuning flap – there isn't one. Many of these sets are marked around the on/off switch where people have tried to open the trim to adjust the set. It's all done via the remote control unit.

Things were really going well. I always start to worry when it's like this, knowing that some pitfall awaits. Would it be the Toshiba 140R4B that was next in line? It ran all right for long enough to make a cuppa and talk to colleagues about the state of the world. We soon put all the major unrest and catastrophes to rights. Then the Toshiba began to burp, producing a display that looked like a wineglass. Time for the pitfall I bet. When I removed the back the set ran for half a minute, burped a bit then ran again. Strange, I thought. Maybe a power supply fault of some sort. Time for some tapping on the panel. This made the funny noise come and go. There was a dry-joint on the line output transformer. This just shows that when you think it's going to be difficult it's easy, but when you think it's easy stop thinking.

VCRs

With about two hours to go to tea time I really had to set about some of the VCRs that were piling up. I mused over the job cards and picked an old favourite, an Hitachi VT11E. The job card said "won't rewind, chews tapes and stops whilst playing". Great! I popped in a dummy cassette and set it going. Sure enough the reel torque was poor, and the loading belts squealed as the arms reached the end of their travel. So I removed the case and opened the bottom panel, then connected the machine to a monitor and checked the recording and playback to make sure that the heads were o.k. They were, so the strip-down started.

I do this in two halves with these machines, as with most others. First the top: the head drum discharge brush, the pinch roller, the back-tension band, the reel idler and both reel discs, not forgetting where the height shims and washers etc. come from. I also remove the capstan oil seal at this time. With all these bits laid out, cleaning can commence. The reel shafts and the slant poles, tape guides and lower cylinder are all cleaned with alcohol. The reel discs are cleaned with methylated spirit, both inside the spindle holes and on the drive surfaces.

Part two is to tip the machine upside down then remove the capstan securing plate (two screws), take off the belts then remove the capstan – that's why I took off the oil seal before. Almost certainly the capstan shaft will be all brown and sticky. Finally the clutch/drive unit is removed (again two screws). Now there are bits everywhere.

My next step is to clean out the capstan bushes. Two pipe cleaners twisted together fit nicely. Soak them in meths and pull them through a few times. This removes all sorts of

muck. When the bushes are clean I insert a cotton bud, with only one end on it, from the tape side of the deck which is now nearest the bench. Push it in just far enough so that it won't fall out then run some oil into the bushes from the open end (God this is confusing!). It will have time to work its way into the bushes while other work is being carried out. I feel that it's essential to service the capstan shaft in this way as I'm sure that heavy running greatly contributes to capstan motor failure. At about £45 trade these items should be looked after. I also put a drop of oil on the bearing at the other end of the capstan motor itself, using a thin blade to get it under the drive pulley. Make sure that any surplus is removed before reassembly. At this point the drive pulley must be cleaned. The old belt gunge that sticks like glue can be taken off using an ink rubber or a fibre pencil.

Finally the clutch unit can be completely stripped, taking care to note the positions of all the securing split washers and which way round the various wheels should be. Clean all the surfaces with meths – not the felt in the clutch of course – then very lightly oil the three spindles. When the clutch unit is reassembled with a replacement belt it should run like new. The grooves in the drive end of the clutch can be cleaned easily when out of the unit, but don't be tempted to roughen the surface in an effort to improve the traction to the idler – it won't work. A toothbrush and meths or a fibre pencil are excellent for this purpose.

Reassembly should be easy – remember to wipe away any oil that may get on to the belts or reel drive components. Remove the cotton bud from the capstan bearing and start to put it all back together. First the clutch, then the capstan which is now very shiny, watching out for the drop of oil that will come from the bushes when the capstan is pushed home. Then fit the two new belts and the capstan securing plate. The last part to sort out here is the loading motor drive belts. One screw and take off one belt. Unplug the connector and the motor is out. Check whether the bearing of the intermediate drive pulley is dry, also the motor bearing – lubrication may be needed. Replace both belts, then refit the motor and connector. All is now finished at this end and the unit can now be turned the right way up.

Put the reel discs back on, with a tiny spot of oil on the spindles. Fit a new belt between the take-up disc and the dummy counter pulley. Replace the back-tension band and fit a new pinch roller. Clean the static discharge brush and refit it. Lastly, wipe the capstan shaft and replace the oil seal. With no more bits left on the bench and all the moving parts and the tape guides, heads and lower cylinder gleaming like new pins it's time to try the machine. The result? Perfection, as always. Well sometimes.

Final Chores

So much for all the good times I've had today. Now to start ringing customers with estimates and ordering spares. Colleagues have put job cards into my tray, requesting spares and asking me to ring Mr. and Mrs. So-and-so to tell them that their TV set is really too old to mend. As you know, not all of them take this too well. Some think that you're a robber while others think that a relative has just passed away. But on with the chores that only the dog's body gets left with.

Well, the customers have all been contacted, now for some fun. The recently purchased viewdata terminal awaits. Part numbers found, autodial on and away we go. Why does my terminal always say "?" – because the last time I used COPS I didn't press Q to leave the system, that's why. Sorry Willow Vale. Other orders are faxed. Now we eagerly await the parts. . .

Long-distance Television

Roger Bunney

January was one of the quietest months ever for DX-TV reception. At the present stage of the solar cycle F2 layer propagation is virtually non-existent. What little SpE reception was noted is recorded below. Very early in January and again early in February there was an improvement in tropospheric conditions, with associated high pressure and fog. Even meteor scatter propagation has been very poor. So to the brief SpE log:

5/1/93	DR (Denmark) ch. E2; +PTT (Switzerland) E2.
8/1/93	NRK (Norway) E3; TVE (Spain) E2.
16/1/93	SVT (Sweden) E2, 3; CIS (Russia) R1; TVE E3.
17/1/93	TVE E2, 3.
23/1/93	DR E3; NRK E2.
24/1/93	TVE E2.
30/1/93	+PTT E2; TVE E2.
31/1/93	TVE E2.

Iain Menzies (Aberdeen) reports two auroral events, a small one on the 5th and a more sustained evening one on the 25th. My thanks to Iain, Simon Hamer (Powys), David Oliver (Birmingham), David Glenday (Arbroath), Tim Anderson (St Leonards), Roger Fussell (Torpoint) and Peter Schubert (Rainham) for sending in reception reports.

50MHz Experiment

An interesting experiment in the 50MHz band is being carried out by two Californian amateurs. In the early hours of February 6-7th the moon was centred between Western Europe and the US West Coast, presenting an ideally placed reflector for aerials at the two locations. Signals were transmitted for two hours each day, on even minutes, the aim being to reflect signals from the States to Europe via the moon. Amateur station W6JKV fed 1.5kW to a 16 x 6 element aerial stack (20.5dBd gain) at 50.03MHz. Station

K6QXY fed similar power to a 4 x 11 element aerial (18.5dBd gain) at 50.007MHz. With the aerials aimed at the horizon an additional 3-6dB of ground gain was obtained. I hope to be able to report on the results in due course.

News Items

UK: Following the failure of the country-wide Channel 5 franchise allocation the ITC is considering a more localised system based on larger towns and cities. A consultative paper will be published in the summer. ITV network programming could be distributed in digital form from 1994 onwards, with NTL operating the service.

In its January 1993 bulletin the UK Six Metre Group summarises the current situation with 50MHz amateur operators throughout Europe. With the possible exception of Portugal (no information available) there are now operators in all European countries. Output powers range from 3W up to 500W (Denmark): restrictions vary from country to country depending on other Band I services, in particular TV transmitters.

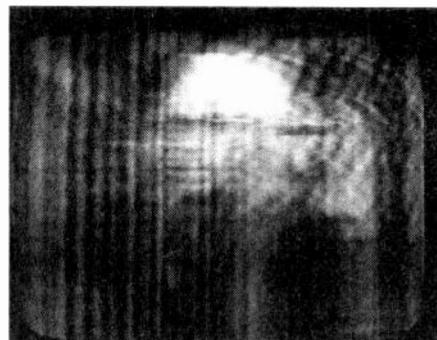
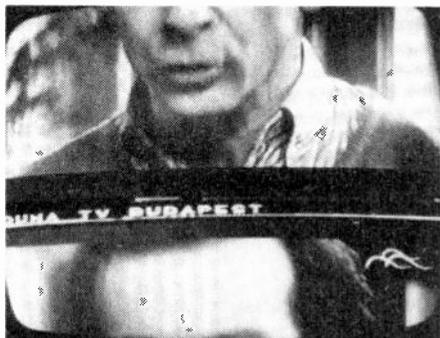
CIS: The Lithuanian OK1 relay over the LTV2 network has ended – a full-time LTV2 service is planned. It seems that the Swedish Kinnevik broadcaster (TV2/TV1000) may use the LTV2 system for a commercial service. A new OK1 transmitter is in operation at Kaliningrad, on ch. R4 with 5kW.

Belgium: Canal Plus is now being transmitted from Leglise on chs. E11 and E63. It's a 24-hour service.

Finland: The MTV service has now moved to the third network and hopes to achieve country-wide coverage within months. An interesting English-language f.m./TV/satellite bulletin called *FM-TV Busybody*, aimed at DXers throughout Europe, is being published by FMBB, Box 7, SF-05901, Hyvinkaa, Finland, from whom sample copies can be obtained. The 1993 subscription rate, for nine issues, is 110 FIM.

Turkey: Up to ten commercial TV stations are now transmitting, either on test or with programmes. The latest programme provider is Flash TV.

Greece: The authorities are about to award commercial broadcasting licences. There have been almost ninety applicants, some of which are already transmitting! Hellas 62, Sky TV, Channel Seven X, Kanali 29, Nea Teleorasis,



Left: A convenient station identification, the Duna TV field blanking pulse insert, received via Eutelsat II F3 at 16°E. Centre: SpE reception of RTT (Tunisia) ch. E4 at St. Leonards, East Sussex by Tim Anderson. Right: Multipath ch. E2 reception of a Koran reading from IRIB (Iran) in early 1992 by Ryn Muntjewerff in The Netherlands – classic F2 reception.

Antenna TV and Mega Channel are all in operation and hope for national network status. State broadcaster ERT is maintaining its three services.

India: The Metro Channel has been given permission to operate, initially in the four main population areas (Madras, Delhi, Bombay and Calcutta).

Satellite TV

Good news for sat-zappers: the EBU programme exchange network has moved from the vintage Eutelsat I F5 at 21.5°E to the modern Eutelsat II F4 at 7°E, with four transponders in use daily at much higher powers than previously. You will notice that the pictures, because of the use of sound-in-syncs, are unsteady. One method of picture stabilisation is to strip off the incoming sync pulses and insert locally-generated ones phased with the picture to obtain correct lock. At present sync inserter units do not appear to be available commercially, though PDS offered a video sync processor that did just this in the early days of satellite TV. If anyone has one of the latter units lying about unused, please let me know! Eutelsat I F2 at 3°E was fired up in late January with an uplink from an Austrian station: signals were seen for three days then ceased.

The EBU's French-based (Lyon) Euronews service started on January 1st, providing up to twenty hours of news material daily with sound subcarriers for various languages. Check at 11.575GHz (vertical) from Eutelsat II F1 (13°E). An Italian news service called Elefante TV is due to start at any time.

Starting this spring Marco Polo 2, now at 0.8°W and renamed Thor after being sold to Norwegian Telecom, will start carrying CNNI and Filmnet programming. Children's and sports channels will be added later in the year. Both CNNI and Filmnet will use Eurocrypt S, CNNI with D-MAC and Filmnet with D2-MAC. Keep a lookout at 11.785, 11.861, 11.938 and 12.015GHz.

Screensport has now been combined with Eurosport and may adopt scrambling. A French-language version, TV Sport, is to be transmitted via the Telecom 2 satellite. Red Hot Dutch, the scrambled hard porn channel that's been in the news recently, may adopt an addressable rotating line encryption standard instead of the present inverted video plus 100kHz sinewave. A further two German-based hard porn channels are promised by early summer. A UK version of the American Nickelodeon children's channel is due to be started by BSkyB this autumn via Astra 1C.

A new identification to watch out for is VTM – Vlaamse Televisie Maatschappij NV. This is a Belgian satellite news gathering operator that uses analogue or digitally compressed video plus voice, data or fax transmissions.

Hispasat, the Iberian satellite at 30 or 31°W (depending on which publication you read), is now in operation with various encrypted services at high levels plus the German Tele 5 channel dubbed into Spanish.

Glum faces in Australia over the loss of the Optus B2 satellite due to a launch malfunction. A replacement won't be ready until mid-1994. Optus B1 is now carrying some of the services previously carried by the elderly Aussat A2 satellite, with Aussat A3 taking over the others. The Thaicom 1 satellite, due for launch in November, will go into orbit at 101°E, carrying twelve C band transponders. It will provide a rival service to Star TV via AsiaSat 1. The Hindi-language ZEE TV service via AsiaSat 1 intends to start 24-hour operation by mid-summer and hopes to be able

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to use AsiaSat's northern beam to give coverage over the whole of Asia and the Middle East.

BBC World Service TV is now being transmitted terrestrially by the South African M Net service, which uses scrambling. Apparently it's possible to view BBC WSTV for free by subtle manipulation of the M Net decoder – one newspaper published details of the knob programming required.

According to Pat Hawker, writing in the February issue of *Radio Communication*, LNBs have been producing interference in the h.f. bands. The source of the interference was tracked down by an amateur using an OptoElectronics 2300 spectrum analyser. It seems that the problem is being caused by high-level operation of the local oscillator in many Ku band LNBs, which are not covered by EMC guidelines. It's possible that interference of this type could occur in Band 1.

Market Place

The third edition of *European Scrambling Systems – Circuits, Tactics and Techniques* by John McCormac has just been published. Also known as the "black book", it's a goldmine of information on the principles and practice of encryption, including how the various systems were defeated and how you can do this yourself! There are full details of each encryption standard, including Videocrypt. As the book is aimed at European readers in general Filmnet, RTL-4, Canal Plus-RA1 and so on are all covered in detail. I found the "dirty tricks" section particularly interesting. A concluding section mentions that the Eurocrypt smart card "is based on the Bull CP8 masked programmed

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15R0H	3.83	ZSC15790	0.26	ZSD716	1.11	BC148	0.12	BD232	0.28	BFR90A	0.61	CD4069	0.17	MS231L	0.55	SN29764AN	1.47	TA7233P	1.77	TDA1518Q	3.32	TC106M	0.60
15R5R	3.84	ZSC1675	0.09	ZSD718	1.45	BC148A	0.06	BD234	0.25	BFR91	0.53	CD4070	0.14	MS3216P	1.48	SN7474N	0.38	TA7240AP	0.08	TDA1670A	2.01	TC45	0.59
1705Z	3.20	ZSC1685	0.14	ZSD734	0.24	BC148B	0.04	BD237	0.30	BFR96	0.30	CD4070	0.14	MS3216P	1.48	SN76013AN	7.99	TA7240P	2.21	TDA1701	4.06	TL100	0.21
1705Z	3.20	ZSC1740	0.12	ZSD782	1.27	BC149	0.04	BD238	0.11	BFR92A	0.40	CD4070	0.14	MS3216P	1.48	SN76227N	1.07	TA7241	2.30	TDA1770	0.00	TP110	0.36
17088	2.38	ZSC1815	0.17	ZSD784	0.24	BC149C	0.04	BD238	0.29	BFR93	0.33	CD4070	0.14	MS3216P	1.48	SN76666N	1.26	TA7243P	0.00	TDA1870	2.64	TP112	0.00
17089	3.39	ZSC1815	0.14	ZSD787E	0.26	BC151	0.13	BD241	0.41	BFR95	0.34	CD4070	0.14	MS3216P	1.48	SN76705AN	1.70	TA7250	3.38	TDA1904	1.21	TP112H	0.39
17127	1.77	ZSC1826	0.72	ZSD837	0.90	BC159	0.06	BD243	0.39	BFR95	0.34	CD4070	0.14	MS3216P	1.48	SR2M	3.31	TA7267P	2.02	TDA1905	0.93	TP120	0.57
1M4001	0.04	ZSC1827	0.77	ZSD841	1.61	BC160	0.42	BD243A	0.43	BR100	0.17	DTA124EF	0.13	MS4648A	5.51	STA31M	2.38	TA7270	1.68	TDA1908A	1.14	TP121	0.42
1M4002	0.07	ZSC1845	0.20	ZSD856	0.87	BC161	0.27	BD243C	0.37	BR101	0.90	DTA144EF	0.17	MS4898AP	17.01	STA401	2.38	TA7270P	1.68	TDA1940	2.77	TP126	0.48
1M4003	0.05	ZSC1846	0.29	ZSD869	2.80	BC167	0.42	BD244A	0.34	BR103	0.39	ER1400	2.15	MS4898P	5.95	STA441C	3.62	TA7271P	1.90	TDA1950	1.06	TP132	0.46
1M4004	0.07	ZSC1923	0.14	ZSD870	2.80	BC171B	0.14	BD244C	0.42	BR303	1.22	HA11235	1.60	BR370	2.38	STK0029	5.08	TA7273	3.21	TDA2002	0.85	TP137	0.48
1M4005	0.06	ZSC1942	3.33	ZSD871	5.80	BC177	0.14	BD245C	0.72	BR444	1.02	HA11244	3.03	MB3731	2.04	STK0039	7.45	TA7274P	2.72	TDA2003V	1.27	TP295	0.83
1M4006	0.06	ZSC1959	0.11	ZSD882	0.34	BC178	0.11	BD246C	0.71	BRY56	0.43	HA1124A	0.73	MB3732	2.47	STK0040	7.40	TA7280	2.11	TDA2004	1.02	TP29C	0.30
1M4007	0.06	ZSC1969	2.15	ZSD882	0.43	BC182	0.06	BD278A	0.56	BSS38	0.23	HA11423	2.92	MC13002	0.00	STK0059	9.75	TA7281	0.00	TDA2005	1.27	TP29E	0.41
1M4148	0.04	ZSC1983	0.07	ZSD888B	2.97	BC182A	0.90	BD317	0.07	BT120	1.20	HA11440	2.02	MC13002P	0.05	STK025	9.66	TA7299	2.34	TDA2006	1.06	TP3055	0.77
1M4448	0.06	ZSC2001	0.14	ZSD904	5.35	BC182L	0.06	BD318	1.10	BT129	3.26	HA1166X	3.43	MC1310P	0.05	STK043	0.00	TA7313AP	0.62	TDA2009	2.29	TP30C	0.17
1M5061	0.23	ZSC2029	0.00	ZSD973	0.96	BC182LB	0.06	BD380	0.34	BT139600	0.95	HA11713	1.24	MC1327AP	1.62	STK062	5.08	TA7317P	0.93	TDA2020	3.72	TP31	0.00
1M5402	0.09	ZSC2073	0.51	74L500	0.21	BC183	0.06	BD433	0.06	BD433	0.97	HA11741	6.90	MC1330AP	1.26	STK062	8.88	TA7325P	0.45	TDA2030	0.00	TP31A	0.32
1M5404	0.12	ZSC2078	0.70	7805	0.24	BC184	0.09	BD434	0.34	BT151800	1.15	HA11745	5.10	MC1330AP	1.02	STK1131	7.79	TA7343AP	0.72	TDA2030H	0.61	TP31B	0.30
1M5406	0.12	ZSC2141	1.48	7805T022	0.00	BC184L	0.04	BD435	0.30	BU205	1.07	HA13001	1.74	MC1352P	1.45	STK1411	8.85	TA7358P	0.78	TDA2030V	0.93	TP31C	0.39
1M5408	0.12	ZSC2166	0.96	7808	0.30	BC184LC	0.10	BD436	0.32	BU208A	1.16	HA13108	2.36	MC1358P	1.59	STK1412	8.21	TA7358P	0.68	TDA2040	0.70	TP32A	0.37
1M5410	0.04	ZSC2168	0.85	7812	0.30	BC204	0.37	BD437	0.32	BU208B	1.07	HA13118	1.91	MC1493P	4.00	STK162M	9.51	TA7607AP	2.11	TDA2170	2.55	TP32C	0.38
1S15515	0.22	ZSC2184	0.25	7815	0.30	BC207B	0.23	BD438	0.17	BU226A	0.90	HA13119	2.03	MC145288CP	2.22	STK1711	10.50	TA7609P	1.95	TDA2210	1.68	TP32O	0.00
1S2076	0.29	ZSC2271	0.22	7818	0.41	BC212	0.06	BD441	0.41	BU406	0.65	HA13403	5.42	MDA2062	2.21	STK1811	12.85	TA7630P	0.00	TDA2525	0.00	TP33A	0.92
2M2219A	0.27	ZSC2274	0.22	7905	0.34	BC212B	0.06	BD442	0.29	BU406D1.02	4.10	HA1374A	4.10	MU2955	0.97	STK181A	12.46	TA7630P	1.87	TDA2525	4.76	TP33C	0.98
2M2222	0.21	ZSC2274	0.22	7912	0.43	BC212L	0.06	BD510	1.34	BU407	0.53	HA1377	1.60	MU802	2.29	STK432	5.54	TA7640AP	0.98	TDA2540	0.38	TP34	0.00
2M2905	0.17	ZSC2314	0.33	AA119	0.36	BC213	0.11	BD529	0.87	BU407D	0.97	HA1388	2.63	MU13005	0.02	STK432	1.70	TA7676P	4.25	TDA2541	0.72	TP34C	0.89
2M2926G	0.37	ZSC2335	1.11	AA123	0.13	BC214	0.00	BD530	1.10	BU426A	0.96	HA1389	2.52	MU2955	0.60	STK437	6.30	TA7680AP	4.52	TDA2560	2.55	TP41A	0.31
2M3053	0.36	ZSC2458	0.09	AA147	0.11	BC214L	0.09	BD535	0.43	BU426E	2.13	HA1392	1.61	MU3055	0.51	STK4392	6.31	TA7680AP	5.93	TDA2562	5.95	TP41B	0.38
2M3054	0.38	ZSC2482	0.34	AA141K	0.46	BC237	0.05	BD536	0.40	BU500	1.09	HA1397	2.63	MU340	0.40	STK441	10.28	TA7705P	1.68	TDA2577	4.81	TP41C	0.37
2M3055	0.59	ZSC2547E	0.24	AC176K	0.30	BC237A	0.08	BD675	0.38	BU508A	0.95	HA1398	2.33	MU327B	0.80	STK459	10.27	TA7769P	1.43	TDA2577A	4.25	TP42A	0.34
2M3442	0.75	ZSC2565	6.40	AC187	0.16	BC237B	0.05	BD677	0.32	BU508AF	1.27	HA1452	3.36	MU923	5.10	STK461	9.27	TA8205	3.65	TDA2578A	2.55	TP42C	0.37
2M3702	0.11	ZSC2570A	0.29	AC187K	0.33	BC238	0.11	BD707	0.51	BU508D	1.27	HE6028	10.36	MU1405VNF	11.00	STK483	11.10	TA8210H	4.66	TDA2579	0.90	TP42P	0.51
2M3704	0.14	ZSC2577	2.13	AC188	0.80	BC238B	0.05	BD839	0.51	BU508DF	0.95	HE6252	9.55	MU1435VX	14.35	STK5211	13.79	TA8215	3.81	TDA2581	10.15	TP79JA	1.17
2M3773	1.02	ZSC2632	2.45	AC188K	0.37	BC239	0.04	BD901	0.51	BU508E	1.16	HE7103	14.07	MU1435VXB	10.66	STK522	5.59	TA8891N	6.69	TDA2581Q	10.15	TP43	0.66
2M3819	0.34	ZSC2632	0.29	AD149	0.52	BC252B	0.07	BD902	0.51	BU526	1.41	IC82H	1.24	MU650	2.50	STK525	5.33	TA850	0.00	TDA2582	1.66	TP101P	1.38
2M3904	0.11	ZSC2655	0.25	AD161	0.82	BC300	0.48	BD911	0.65	BU536	1.00	KA2101	0.60	MPS462	0.23	STK526	5.06	TAG626	1.05	TDA2591	1.15	TP171CP	0.36
2M4444	2.68	ZSC2671	0.60	AD162	0.86	BC301	0.24	BD912	0.63	BU608	1.50	KBLO8	0.07	MPS456	0.12	STK531	3.02	TA8120	0.53	TDA2593	9.75	TP494	1.49
2M6292	0.62	ZSC2688	0.60	AD124	0.77	BC302	0.36	BDV658	1.16	BU705	1.63	KBLO8	0.09	MPS493	0.09	STK532	2.74	TA120AS	0.90	TDA2594	2.21	TMP47C432AP	1.29
2SA1015	0.19	ZSC2785	0.17	AF127	0.59	BC303	0.28	BDW84C	1.28	BU806	0.82	L200CV	1.13	MPSU10	0.00	STK533	4.28	TA120S	0.89	TDA2595	2.16		11.24
2SA1016	0.10	ZSC2791	5.44	AF139	0.29	BC307	0.06	BDW93C	0.50	BU806A	0.90	LA1201	0.56	MR854	0.14	STK537	5.28	TA120T	0.58	TDA2596	3.08	TMP47C434N	1.78
2SA1020	0.31	ZSC3150	1.44	AF239	0.43	BC307A	0.06	BDW94C	0.46	BU807	0.51	LA1230	1.45	MSMS840H	15.36	STK5421	2.60	TA120U	0.39	TDA2611A	0.64		16.58
2SA1020Y	0.30	ZSC3153	2.37	AF239	0.30	BC307B	0.06	BDX32	1.70	BU825A	1.59	LA1235	1.45	MYS240	0.53	STK5422	5.74	TA120U	0.68	TDA2611AQ	1.74	UC3844	1.78
2SA1095	7.44	ZSC3156	6.50	AA102	2.55	BC308	0.06	BDY20	2.13	BU908	1.17	LA3161	0.40	NE458	3.20	STK5451	5.27	TA395	0.68	TDA2640	3.98	UP81C	0.72
2SA1102	2.54	ZSC3182	3.25	AA145	0.20	BC308A	0.09	BF115	0.41	BU944	2.38	LA1410	0.37	NE555	0.21	STK5466	5.08	TA820	0.85	TDA2652	14.32	UPC1181H	6.80
2SA1143	0.17	ZSC3225	0.38	AA3821K	7.23	BC308C	0.06	BF179	0.31	BU111	0.68	LA4182	1.75	NE555N	0.37	STK5471	4.51	TA8450	1.97	TDA2653A	3.26	UPC1182H	5.95
2SA1175	0.51	ZSC3795	1.79	AA5625	1.34	BC327	0.10	BF184	0.47	BU111A	0.85			NE592	1.85	STK5476	5.00	TA840Q	0.77	TDA2680	5.10	UPC1185H	10.20
2SA1186	3.52	ZSC3800	0.12	AA5435	1.45	BC327B	0.17	BF185	0.29	BU111AF	0.85			NE546N	2.47	STK5481	5.61	TA8560C	0.68	TDA3190	1.27	UPC1188	3.83

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ZSA1265	1.95	ZSC458	0.00	AN5515	2.13	BC337	0.06	BF196	0.15	BU156A	0.57	LA4220	1.29	0A47	0.25	STK5962	2.65	TBA551	1.				

card. It appears that this card has now been pumped or stripped. Card Tricks of Switzerland will market alternative microcontroller cards from January. The conflict has moved into a new phase". This comprehensive book sells at £32 plus £2.50 UK postage.

The 1993/94 World Satellite Almanac by Mark Long is available at £69 plus £2.50 UK postage. It's the reference work for all that's happening in the satellite world, but of course things keep changing. So Mark Long's *The 1993-1994 World Satellite Annual* has been published as an official supplement at £41 plus £2.50 UK postage.

Truly excellent as these books are, the cost is perhaps rather high for those not professionally engaged in satellite telecommunications. Frank Baylin has broken through the price barrier with the *1993 World Satellite Yearly*. It provides a comprehensive reference work at a much lower cost, including data on all satellites at present in orbit or soon to arrive there, with detailed coverage of transmission techniques, encryption, digital compression/HDTV, satellite installation/reception problems and calculations, footprints etc. The book has 440 A4 format pages and is available at £38 plus £2.50 UK postage.

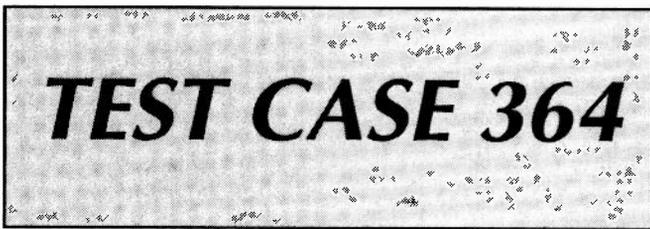
Retail orders for the above books should be sent to Swift Television Publications, 17 Pittsfield, Cricklade, Swindon, Wilts SN6 6AN – telephone number 0793 750 620. J. Vincent Technical Books, 24 River Gardens, Purley, Reading RG8 8BX (0734 414 468) is the official wholesale distributor in the UK.

Tim Anderson is marketing two computer discs in either Amiga or IBM PC compatible 3.5in. form. The first, called

DXWATCH, contains two programs, *DXWATCH* and *IDWATCH*. *DXWATCH* itself is a database of worldwide Band I TV offsets plus small files with Band III and u.h.f. offsets. The program allows you to create your own files so that you could, for example, create files for each channel, each continent or whatever you like. *IDWATCH* is intended to help with picture source identification by referring to key words. As we all know test patterns are rare nowadays, so that signal identification is an increasing problem. This program contains station identifications and words that often occur on pictures, such as news and weather – the entries for The Netherlands for example include PTT NED, NOS, NOZEMA, Nieuws, Pauze etc. Users can add to these entries, building up a comprehensive database. This disc costs £8 including UK postage.

The second disc, *AMISCAN Version 2.0*, is a database for anyone interested in frequencies above 25MHz – scanner users for example. There are well over a thousand entries that can be searched, sorted, listed, edited and printed. Each entry contains frequency, channel number, mode, service, location, comments etc. Entries can be added or expanded for updating. Information on the disc includes worldwide 10m f.m. repeaters, many of the low v.h.f. signals heard during F2 and SpE openings, amateur radio beacons, European air-band frequencies, many TV offsets and much more. Cost is £7.50 including UK postage.

These discs can be ordered from Tim Anderson at 2 Bury Road, St. Leonards-on-Sea, East Sussex TN37 6QX. I found them easy to use and if I can cope anyone should be able to!



The workshop never seems to run at full bore in late winter. Thus anyone who brings in a repair at this time of the year is likely to get very quick service from our team of highly-trained technical sleuths. On this bright and chilly morning they were engaged on such mundane tasks as filing service manuals and carrying out repairs to stock machines. Service Manager was casting a jaundiced eye over last month's accounts – gloomy reading indeed.

A car drew up in the yard. Its driver picked up a VCR from the passenger's seat and brought it into reception. As soon as it was booked in we had it hooked up on the bench and running. But not running very fast: the cassette loading operation was painfully slow, the cassette just about making it into the machine and down on to the spool turntables. Time to get the service manual out. The machine was an Hitachi VT430.

In this deck the front-loading operation is powered by the capstan motor which drives it, along with the tape reels, via a belt and a conglomeration of plastic cogs and pinions. So the first step was to replace the belt. This didn't have the slightest effect on the cassette loading and unloading operations, which were still performed very slowly. Real Technician, who had won the fight for the machine when it came it, decided to see how the capstan motor coped with its other tasks. Before doing so he discovered that tape lacing took place at normal speed – it's done by the loading motor, quite separately from the capstan department – while the drum quickly ran up to 1,500 r.p.m. So none of

the other motors on the deck were afflicted. Back to the capstan.

In the play modes the tape ran very slowly and at an uneven speed. As a result the reproduced sound was slurred and had a heavy wow. In the search modes the tape moved hardly any faster than the normal play speed. Sometimes, when cue or review was selected, it would come to a complete standstill and the deck would then shut down. Similarly if pause was selected during play or record and then released the capstan would often fail to restart, the result again being deck shutdown. Fast forward and rewind were sluggish, with every sign that a three-hour cassette would take ten to fifteen minutes to transfer all the tape from one spool to the other.

Well, that seemed to be enough evidence, the finger of suspicion pointing at the capstan drive system. Real Technician again removed the reel-drive belt, then checked for any tightness in the reel-drive department, here called the clutch base assembly. Everything ran freely, and the reel brakes were seen to be coming off all right. What a pity that, with the belt still off, another similar test wasn't carried out! With the drive belt back in place the machine was once more set to play while further tests were made.

RT first had a look at the capstan motor's supply voltage. The A16V line was at almost 19V, but a look at the circuit diagram showed that it comes from an unregulated 18V supply, so that was o.k. The 5V line was correct. The drive circuitry could have been in trouble but RT next found, the machine having run for fifteen minutes or so now, that the capstan motor's rotor and the on-board drive chip IC1601 were running quite hot. This was the clincher. He decided to replace the motor assembly. Was this a wise move, and would it have cured the trouble? Give some thought to this before turning to page 442 to discover the answers!

Repairing LED Clock Radios

Part 2

Ian Rees

In Part 1 last month we dealt with the clock and display sections. For space reasons Table 1 was held over and is included this time. It shows the control and supply pin connections for common clock chips. Now to the radio side of things.

Quick identification of the stages of an unfamiliar radio can be difficult. There's a colour code for the small coils used in radios of Far Eastern origin however and this can be a helpful guide to circuit layout. Details are as follows:

Circuit	A.M.	V.H.F.
Oscillator	Red	—
First i.f.	White	Orange
Second/third i.f.	White	Green
Fourth i.f.	—	Pink
Detector	Black	Blue

The tuned section of an m.w./l.w. ferrite rod aerial is colour coded plain/blue or black, the coupling coil green/red.

VHF Radios

As you would expect these days, single-chip radios are the norm. The only exception is the v.h.f. front end, which is basically the same as that used in other transistor designs. The chips are standard types, but the pin connections vary from one chip to another. Sometimes a separate audio chip is used.

Fig. 7 shows a typical v.h.f. radio section up to the audio output point. Q1 is an earthed-base r.f. amplifier which is followed by a self-oscillating mixer stage, Q2, which is again used in the earthed-base mode. The voltages shown are typical.

Weak reception is most likely to be caused by transistor Q1 being dead or dying. A quick test is to touch Q2's emitter lead with the end of a short length of wire used as an aerial. If this results in a louder signal than when Q1's

emitter is similarly touched, replace Q1. Short-wave reception but no v.h.f. signals when the same wire is touched on Q2's collector lead suggests that this transistor may be faulty. Dry-joints on L2, L3 and L4 are common because they are pulled about at the factory when being set. The enamelled wire adds to the difficulty of soldering the leads, which are easily broken loose by movement. Note the wax mess in this area, used to dampen microphony and hold components in place. Small movement of components in the oscillator circuit will result in a large amount of detuning and should thus be avoided.

As elsewhere the ceramic capacitors used to decouple various points are never above suspicion. Loss of any supply should lead to checks on the relevant ones. Next in line are the relevant electrolytics. The LM1868 chip in the circuit shown receives its supply at pin 19. A decoupled 4V output is provided at pin 16 – this is an unusual arrangement that's difficult to spot without a circuit diagram. The demodulated audio output appears at pin 17.

AM Section

Fig. 8 shows the first couple of stages of a typical a.m. radio section. Once again a completely dead front end can be caused by failure of Q1, but remember that leakage in the 20nF base coupling capacitor will upset the biasing. Open-circuit coupling windings will be the result if the rod aerial is able to move. Litz wire becomes very brittle when solder is allowed to run up from its joints. If a winding is open-circuit, check farther back towards the coil: it's often possible to use a short fly-lead to remake the connection.

The value of the 5,000pF feedback capacitor in the emitter circuit sometimes has to be increased to 10nF or more to maintain oscillation in the l.w. band. This component can also cause low sensitivity – another cause of this is disconnection of the unmarked lead from the aerial rod's tuned winding to the gang.

The practice of decoupling to the positive side of the supply instead of to chassis can mislead if not expected. If

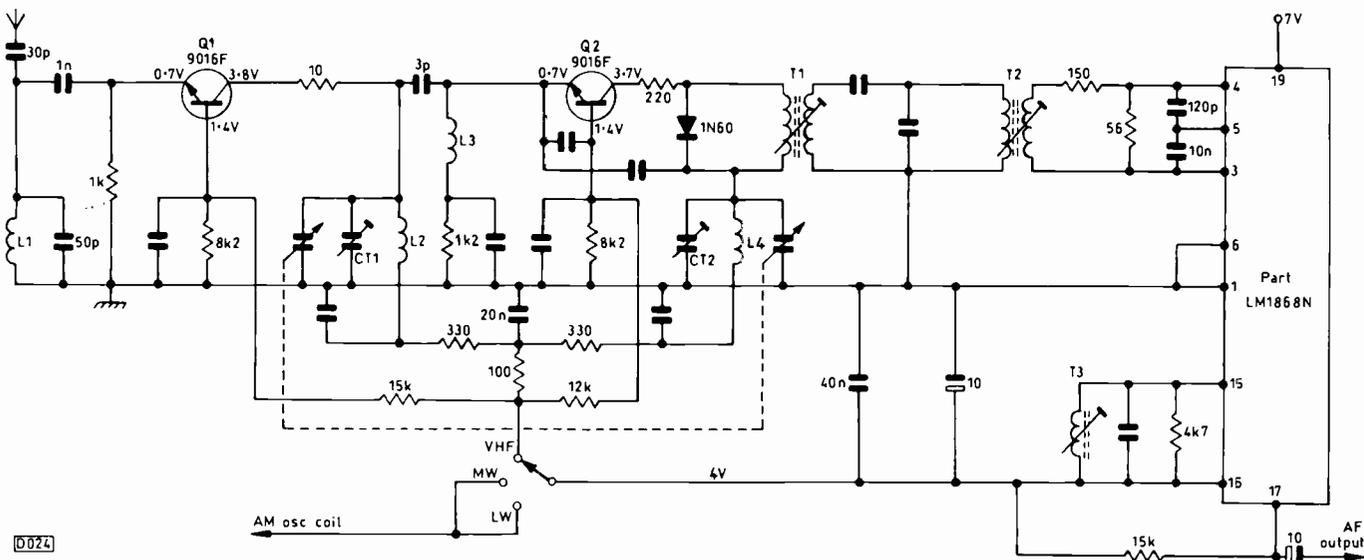


Fig. 7: Typical v.h.f. radio receiver circuitry.

Table 1: Pin connections for common clock chips.

IC	Hours Set	Mins Set	Alarm Set1	Alarm Set 2	Snooze Out	Snooze Set	Alarm Off	Alarm Out	50Hz In	Vss	Vdd
TMS1941	34	33	31	--	25	24	26	27	36	28	29
TMS1944	34	33	31	--	25	24	26	27	36	28	29
TMS1951	34	33	31	--	25	24	26	27	36	28	29
TMS1952	34	33	31	--	25	24	26	27	36	28	29
TMS3450	22	21	19	--	17	24	23	17	25	26	20
LM8361	36	33	31	--	27	26	32	27	35	28	29
LM8363	35	34	32	38	--	25	*	26	36	24	30
LM8560	22	21	--	--	17	24	23	17	25	26	20
MM5387	34	33	31	--	27	24	30	27	35	37	29
MM5402	34	33	31	--	27	24	30	27	35	23	28

*With the LM8363 pin 27 is alarm 1 off, pin 29 alarm 2 off.

TMS1941/1944/1951/1952 common collector; TMS3450/LM8560 duplex type.

LM8361/MM5387/MM5402 require separate oscillator.

LM8363 X2 alarm.

the 20nF capacitor that decouples the emitter of Q2 is leaky the supply will be connected across the 330Ω emitter resistor, giving the impression that Q2 is short-circuit. There will be no output from this stage if the transistor's base bias decoupling capacitors are faulty – the 20nF ceramic connected to the positive rail and the 10μF electrolytic connected to chassis. The unmarked capacitor that tunes the i.f. transformer's primary winding is within the screening can. Check this at the transformer's pins before removing the can. The very act of removing the can may clear the fault if there are dry-jointed connections here. Instability is once again usually caused by a faulty ceramic decoupling capacitor.

Failure of individual i.f. transistors is not uncommon. Check the operating conditions after replacement.

Fig. 9 brings us up-to-date with an a.m. circuit in i.c. form. The LM1868 is typical of a host of other chips that provide both a.m. and f.m. reception. As with the clock chip, it gives very little trouble. Don't consider replacing it until all other possibilities have been exhausted.

If there's no a.m. reception connect a scope to pin 8 to check whether the local oscillator is running. Turning the gang will confirm that tuning is taking place. A sinewave at around 70mV peak-to-peak should be expected here.

No l.w. or m.w. oscillation is often due to a faulty oscillator coil. Loss of l.w. only is most likely to be caused by a short in trimmer CT4 or the 120pF capacitor in parallel with it.

If the oscillator is o.k. try touching pin 7. This should produce a lot of noise but probably no stations. Leakage in the 20nF capacitor that couples the input to this pin will stop reception.

The wavechange switches are often not very good and may bridge internally as the contacts wipe backwards and forwards. Repair is possible if they are opened carefully but replacement is better. Note that the switch bodies may be used as links for the PCB print. If they are loose, whole sections of circuit can be affected. I add wire links to avoid this type of problem.

Tuning

If you do a lot of radio work you'll probably have made yourself a wand to check the ferrite rod's coil setting. It consists of a piece of ferrite rod an inch or so long with a length of wire soldered into a loop of about one inch diam-

eter at one end. For convenience, tape this loop to the rod. In use, the non-loop end of the rod is brought up to the end of the set's aerial assembly. As it approaches, any improvement in a.m. reception would indicate that the aerial coil needs to be moved farther towards the centre of the rod aerial. By bringing the shorted loop around, any reception increase shows that the coil needs to be moved towards the end of the rod. Do this with the l.w. and m.w. coils separately. When no further improvement is possible, lock the coils with wax. This adjustment is done in conjunction with the aerial padders CT1 and CT2.

Before moving a wax-locked coil it's best to soften the wax with a soldering iron or hairdryer.

If the tuning gang operates intermittently when turned or is very noisy, tighten the four small nuts that hold it together – one at each corner. To gain access you might have to crack open the gang's casing. Aerosol switch cleaner can be sprayed into a noisy gang to clean the rotor's contacts. Don't use anything that might dissolve the insulation, and leave to evaporate. Check the v.h.f. and a.m. padder alignment after the repair.

Alignment is best carried out with a suitable a.m./f.m. generator and an output meter connected across the loudspeaker. Manufacturers use a wobulator to align the f.m. circuits, but good results can be obtained using conventional peaking. If an f.m. generator is not available the discriminator or quadrature coils can be set up using an a.m. signal, tuning for a null.

Breakthrough between m.w. and l.w. experienced in some parts of the country can sometimes be reduced by reversing the connections to one of the aerial coils on the ferrite rod.

Muting

The circuit shown in Fig. 9 incorporates an audio muting arrangement. Muting is done by feeding a d.c. signal from the clock's alarm output to the base of transistor Q1. The alarm tone is fed in at a point after the slider of the volume control so that the control doesn't affect the alarm. No audio output can be caused by Q1 being defective. Anything that results in Q1 being off when the alarm tone is present will mean that an audio output is also heard. In other circuits muting is done by feeding a voltage to the i.c. Faults in this circuit can cause clock ticking – a symptom similar to that described when we dealt with the power supply. With

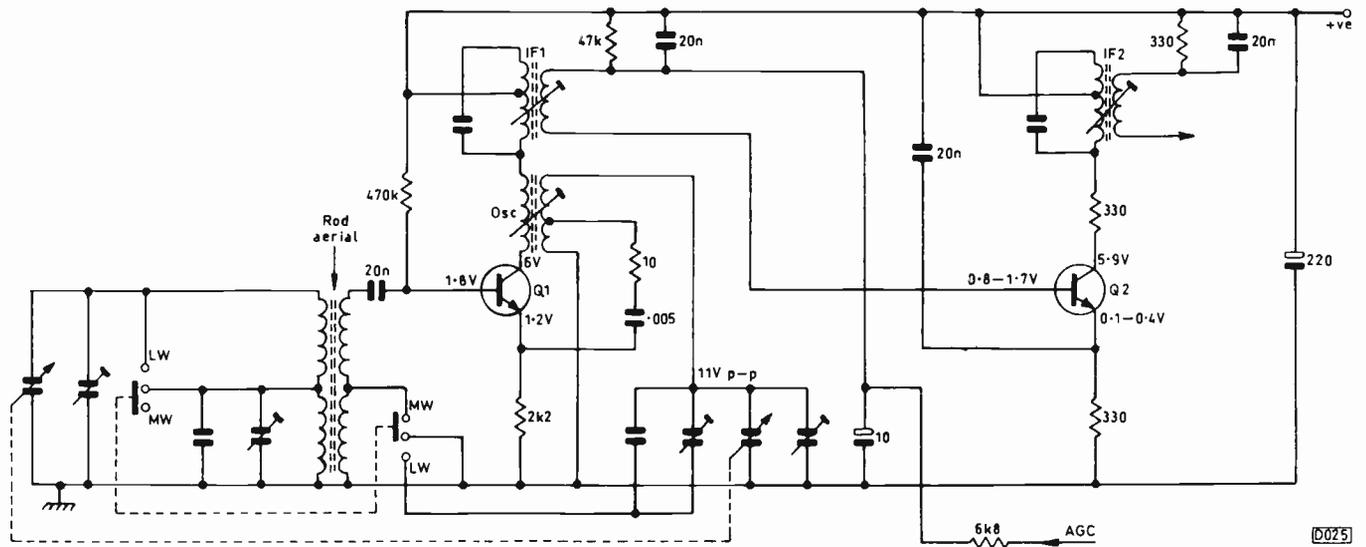


Fig. 8: Circuitry used in the first couple of stages of a typical a.m. radio receiver.

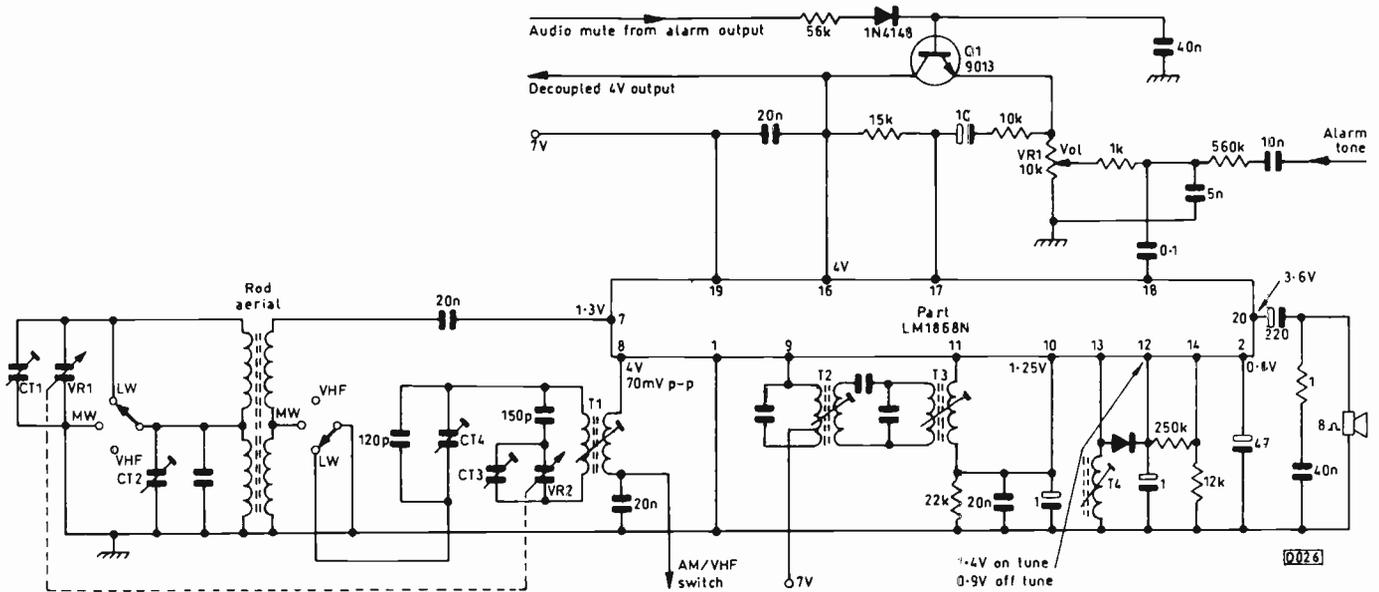


Fig. 9: A.M. receiver circuitry in chip form.

cheaper models the audio and tone occur together, the user being expected to turn the volume to minimum to kill the audio output. A variation on this is to use a switch on the volume control to turn the audio off and on.

Audio Problems

Where the audio signal enters the chip from the volume control but little or nothing is heard check the electrolytic capacitor connected to pin 2 (Fig. 9). With any i.c. that's used in the audio department the associated electrolytic capacitors can be bridged or better replaced during fault tracing. No or uncontrollable volume occurs when the tags of the volume control break loose from the print or their own rivets. Loss of the volume control's chassis connection will result in some chips muting themselves even when the wet finger test is applied directly at the audio input. Spray may cure a noisy volume control. With edge-type controls I prefer to retension the wiper as well.

The small loudspeakers used are prone to failure. The magnet becomes unstuck or goes off centre, the speech coil leads fracture or the coil goes open-circuit. Speaker replacement is the only cure. Rattle is sometimes caused by case resonance, a loose item on the cone or the speaker being

incorrectly fixed. A speech coil that scrapes against the polepieces produces a static-type interference on loud sounds.

What sounds like speaker distortion is often caused by r.f. oscillation in the audio section. Try connecting an 0.1µF capacitor across the loudspeaker to see whether this provides a cure. With some sets this symptom arises only after the warm-up period. Scoping the output to the speaker will show that an r.f. envelope is present. The problem seems to arise quite often when a TBA820 chip is replaced with its KA equivalent.

Problems can arise when a PCB is mounted closely behind a speaker and the manufacturer has fitted a piece of insulation to the back of the speaker. Another problem is that solder spikes can short to the speaker tags or case when the set is reassembled.

Pointer Drives

Finally a few words on station pointer drives – dealing with these has as long as I can remember been one of the most hated jobs in radio servicing. These marvels of string have given many an engineer a hard time. I still have nightmares about a Rigonda valve radiogram drive system that

became unstrung when my then young son spun the dial when the gang was disconnected. Steel cords took hours to work out and refit.

Fortunately the systems used with clock radios are usually simpler. Many have a push-pull arrangement with flexible plastic rods, or a simple direct drive with a calibrated knob.

The old problems remain where the drive-cord method is used. The worst fault is likely to be when a pulley snaps off its fixing. A new shaft can be made by drilling and replacement, with a suitable bolt melted in.

If a cord diagram is not available and complete restringing is required I prefer to have the gang either open or closed. Starting with the spring under tension (assuming that it's on the drum) I head off around the pulleys, bearing in mind the direction in which the cord has to move in relation to the pointer. About three turns around the drive shaft is enough – take care that adjacent turns don't overlap each

other when the shaft is turned in the reverse direction, with the characteristic ping and shudder of pointer. Note also that the direction of the turns should coincide with the pointer movement. End up finally back at the drum. Leave pointer fitting to the last – this will enable the last bit of slack to be taken up. Put a spot of glue or varnish on the pointer and all knots to lock them in place. Nylon drive cord in all sizes can be obtained from a boat chandler – it's sold for sail repair.

An easy way to raise the tuning drive drum without unstringing the cord is to release its centre screw. Gently swing the drum upwards, giving it a couple of twists against the lay of the cord. It can then be taped to the PCB, out of the way. Provided you've not moved the gang or the drum it can be refitted in the reverse order.

Some radios have an arrangement with which the drum can be disengaged from the drive. This makes life simpler, provided that care is taken about their relative positions during reassembly.

Teletopics

NIMBUS DEVELOPS LONG-PLAY CD

Nimbus Technology and Engineering of Monmouth has developed a double-density CD with twice the playing time of a conventional disc. The system, known as CD2X, is based on the use of a special mastering lathe developed by Nimbus and Dr. Jonathan Halliday. Its longer playing time has been made possible by reducing the pit size, track pitch (from 1.6 microns to 1.2 microns) and reading speed (by a factor of 1.4). Despite these changes the new discs can be read by a conventional red laser. Nimbus says that CD2X discs can be played by some of today's CD decks, though with some of the newer ones the optical system will need to be tweaked to focus on the smaller pits.

CD2X is seen primarily as a replacement for VHS and the LaserDisc. Nimbus has developed a small video adaptor box that plugs into a CD player's digital output socket. It contains a video expansion chip, type CL450, developed by C-Cube Microsystems. This is used to decode the MPEG-compressed video signal from the disc. Nimbus says that some players may have the chip built into them.

The new discs will play around two and a quarter hours' of video with f.m. quality sound. Picture quality is claimed to be better than that of VHS. The playing time can be reduced to 75 minutes, offering wide-screen, broadcast-quality pictures. An additional bit will have to be added to the sub-code to tell the player that the disc is an LP one (today's machines recognise playing times only up to 99 minutes, 59 seconds).

Nimbus is confident that CD2X will be accepted by video companies but doesn't expect music companies to market LP audio discs. CD2X could also be used to store more Photo CD pictures, and can be used as a CD-ROM to store up to 1.2Gbytes of data. The new system doesn't provide interactive operation and is therefore not seen as a rival to CD-I. CD2X discs could be on sale within a year. Nimbus has also developed quadruple-density discs, known as CD4X, but these require the use of a blue laser and are more expensive to produce.

HDTV

The MAC system as a way of achieving the goal of HDTV in Europe has to all intents and purposes been aban-

done, though a formal decision to drop MAC cannot be taken until the next meeting of EC telecoms ministers in May. The new EC industry commissioner Martin Bangemann has said that Europe will have to follow the US lead when it decides on a digital HDTV standard later this year. Mr. Bangemann sees no point in starting a further global TV standards battle. There has been a further delay in the USA however, where a decision has been postponed for five months or so while the FCC carries out a further series of tests on the four remaining contenders for selection as the HDTV standard.

Meanwhile the partners in VADIS (Video-Audio Digital Interface System), a pan-European digital TV project, have agreed to expand its aims to include digital HDTV. The VADIS project has developed compression systems that reduce the data rate for a standard digital picture source from 216Mbits/sec to around 4-8Mbits/sec with little reduction in quality. The compression system will make it possible to offer digital audio-visual services from a variety of sources, including telecommunications networks and satellite, terrestrial and cable TV channels. The work is being co-ordinated with the second phase of the international coding standards being developed by the ISO/IEC, known as MPEG. When applied to HDTV pictures the compression techniques will reduce the data rate from 1,152Mbits/sec to around 12-25Mbits/sec. The new work involves the development of a multi-layer picture compression scheme that's matched to European requirements. VADIS members include the BBC, BT, National Transcommunications (NTL), Philips and Thomson.

SATELLITE TV

SES, which operates the Astra satellite system, has decided that its fourth and fifth satellites, due to be launched in 1994 and 1995 respectively, will incorporate digital TV capacity. This will enable Astra to offer a 180 TV channel system from 1995. SES believes that the arrival of digital TV is much nearer than some suppose. It considers that the next two years will be the testing time, and that digital TV decoders could be made available as early as next year.

The latest *Financial Times* Satellite Monitor, conducted by Continental Research, estimates that some 65,000 satellite TV systems were installed in the UK in January. This compares with 70,000 in January 1992. Continental Research estimates that 17,000 were upgrades, replacements or renewals after a break in subscription. It forecasts that by 2000 some 9.5 million homes in the UK will be equipped

for satellite TV reception.

A new range of multi-function integrated receiver-decoders designed and developed by the Pace Micro Technology research and development team is being launched at Cable and Satellite '93. They include the DMAC/D2MAC/PAL MRD950 with integrated Eurocrypt M and S decoding facilities, 120-programme capacity, concise on-screen multi-language graphics, dual LNB inputs, a comprehensive parental lock facility and automatic 16:9 widescreen format selection. The top-of-the-range MRD960 has the added convenience of a dual card reader for increased ease of use.

NEXT GENERATION VCRs

Japanese consumer electronics companies led by Matsushita and Sony are holding talks with the aim of reaching agreement on a new standard for the next generation of VCRs, which will use digital techniques for video storage. The use of digital techniques offers the prospect of virtually perfect pictures no matter how many copies are made. It's hoped that foreign manufacturers will support the standard, facilitating the introduction of digital video technology in the consumer market.

SUCCESSOR TO FM

The trade and industry secretary Michael Heseltine has launched a 'national forum' to promote digital audio broadcasting (DAB). The forum will involve broadcasters, equipment manufacturers, retailers and the providers of services. DAB is expected to replace f.m. broadcasting over a 15-25 year period starting with the first commercial DAB services in 1995. A preliminary technical specification, developed under the European collaborative research programme Eureka, has been submitted to the European Telecommunications Standards Institute. Those participating in the project include the BBC, Philips and Thomson.

DOLBY NEWS

According to Dolby its SR.D six-channel digital stereo sound system is now on fifteen major titles, including Malcolm X, The Bodyguard and Dracula. The new system is compatible with equipment that uses Dolby's older stereo, four-channel and mono sound systems. Yorkshire TV's programme Bad Influence, broadcast on January 28th, was this company's first production to use Dolby Surround sound. Dolby Laboratories has moved to Wootton Bassett, Wiltshire SN4 8QJ (0793 842 100).

BUSINESS NEWS

JVC is to close one of its German manufacturing plants in order to reduce mounting losses. In announcing a 27 per cent pre-tax profits fall in the quarter to the end of December, after discounting the effect of an extraordinary gain in 1991 (otherwise the profits fall amounts to 62 per cent), Sony says that VCRs and camcorders suffered the largest fall in sales, of nearly twelve per cent. Audio sales fell by six per cent while TV sales rose by ten per cent on the strength of worldwide demand for computer displays. The surprise announcement by Matsushita that its president Akio Tanii has resigned has shocked the Japanese business community.

Philips is to increase co-operation with Grundig, its 31.6 per cent owned, loss-making affiliate, in an effort to boost both companies' consumer electronics activities. According to Philips "drastic cost reductions can be achieved only if

NEXT MONTH IN TELEVISION

CAMERA FAULT RECORDER

The causes of intermittent faults are particularly difficult to find, especially when the TV set goes to standby or the VCR to the stop mode almost immediately, removing the fault condition. One approach is to use a camera and VCR to record the operation of the faulty equipment, enabling you to get an action replay of the transient fault event. Eugene Trundle explains the technique, describes the system he uses and provides some case histories. Test equipment can be included in the recordings to provide clues.

PHILIPS' DOUBLE-SCAN TECHNIQUE

Flicker has always been a problem with a 50Hz field rate. Doubling the rate to 100Hz eliminates it. George Wilding describes the techniques used in the Philips FL1.2 chassis to provide 100Hz scanning.

"IT'S ONLY THE ON/OFF SWITCH"

Steve Cannon on some recent 'power supply' faults.

NICAM AND MAC AUDIO

The next instalment in our Modern TV Receiver Techniques series outlines the operation of the digital sound transmission systems now in use and describes the way in which the signals are demodulated and decoded to recover the original analogue sound.

MOTORISING A FIXED DISH

Ian Martin on installing a polar mount for reception across the satellite arc.

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both companies avoid duplication of efforts, especially in development and manufacturing". Philips has an agreement, dating from 1984, to finance Grundig's losses.

VIDEO NEWS

JVC has launched a budget camcorder, Model GRM3, at £599: features include a x8 zoom lens, video light and wired remote control. Nokia has just released three new VCRs: two of them have a built-in VideoPlus timer system. The Grundig GV201 at £360 includes text programming with

Startext and an automatic cassette identification and play time indication system (ATTS).

Sharp has launched an LCD projection TV system, Model XV710P, at £1,800. It can handle PAL, SECAM and NTSC signals and can project an image with a diagonal size up to 100in. Sockets are provided for S video, composite video etc. It uses a newly-developed metal-halide lamp which costs about £180 and has a maximum useful life of around 4,000 hours. For the brightest and clearest picture a 60in. polarising screen (Model XUPP60S) is available at about £1,290.

Simple ESR Meter for Electrolytics

Ray Porter, M.Sc., C.Eng., M.I.E.E.

In an article in the January issue I described the way in which the effective series resistance (ESR) of an aluminium electrolytic capacitor can increase so that it no longer acts as a low-impedance component. This explains why a fault is often cleared by replacing an electrolytic capacitor even though its value, when checked with a capacitance meter, is close to that marked on it. In view of this I decided to design a simple meter to measure the ESR of electrolytic capacitors. Its range suits the ESR values of PCB-mounted electrolytics. By checking against standard values (see Fig. 3) you can reject lossy capacitors.

The tester makes use of an operational amplifier as a negative-resistance oscillator. Since the operation of negative-resistance operational-amplifier circuits doesn't seem to be well known a short explanation of the relevant theory is provided later.

Circuit Description

The circuit produces a negative resistance to cancel the ESR of the capacitor being tested so that there is continuous series resonance with a fixed inductor. Fig. 1 shows the circuit diagram of the meter. The negative resistance is produced by IC1b; Cx is the capacitor under test and L1 the fixed inductor. VR1 enables the negative resistance to be adjusted. Rotate it until oscillation stops: the ESR value can then be read from a scale fixed to VR1.

When there is no negative resistance present L1 and Cx

form a series resonant circuit that's damped by L1's resistance and Cx's ESR. This circuit will ring when energised by an impulse. IC1a is used as an oscillator to produce a squarewave output at a frequency of a few Hz. This output is differentiated to produce the spikes (impulses) that energise the resonant circuit. When the capacitor's ESR and the resistance of R1 are cancelled by the negative resistance the ringing becomes a continuous oscillation. LED D1 is then on. When the oscillation is stopped by reducing the value of the negative resistance the LED goes off.

If a short-circuit capacitor is connected to the tester the LED comes on with full brightness. When the resonant circuit is oscillating the LED is illuminated on only the positive-going half cycles: it therefore glows at half brightness.

IC1d provides a half-supply voltage reference for IC1b. S1 varies IC1b's gain, changing the negative resistance to provide 0-1, 0-10 and 0-100Ω ESR ranges.

Construction

The circuit was built on a piece of stripboard which, with a PP3 battery, fits easily into an ABS box. L1 was wound around the four pillars on the inside of the box's lid - see Fig. 2. It consists of 42 turns of 30 s.w.g. enamelled copper wire. This results in a coil with a resistance of 3.2Ω and an inductance of 90μH. A different wire gauge could be used, but its resistance plus that of R1 must equal 10Ω.

With the coil as specified above a 1,000μF capacitor in

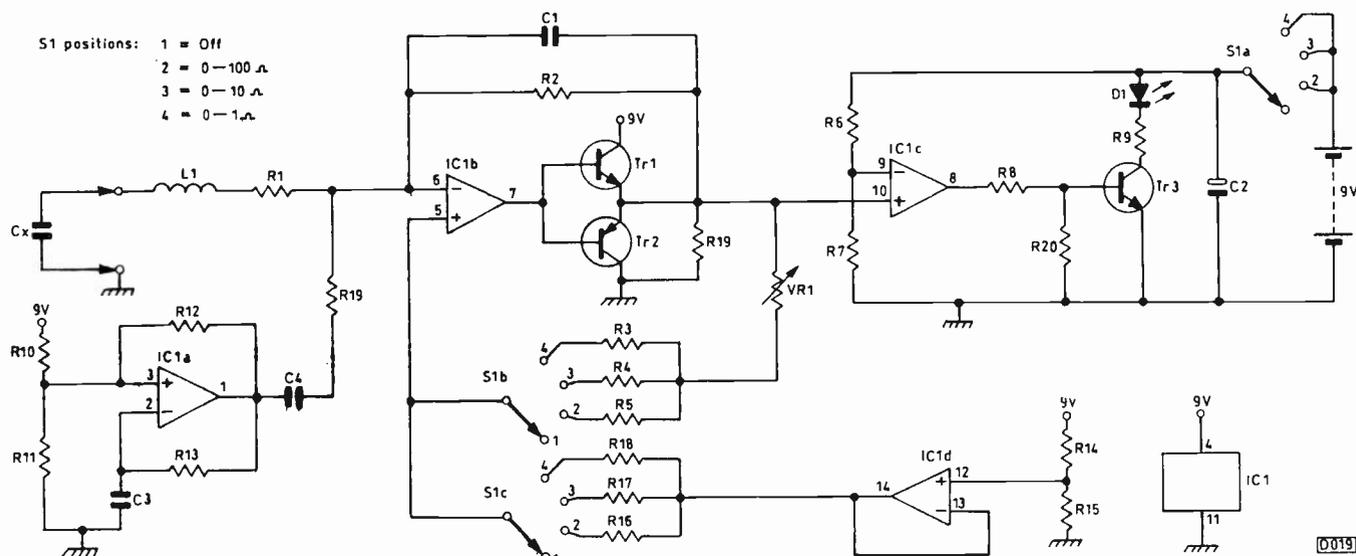


Fig. 1: Circuit diagram of the ESR meter.

position Cx produces oscillations at 70Hz. A 1μF capacitor increases the frequency to 10kHz. When testing the circuit I connected a crystal earpiece via a 100nF capacitor to R19 to check for oscillation. The clicks of a square wave can be heard when VR1 is set far away from the position that stops oscillation. As the critical setting of VR1 is approached the pure sound of a low-amplitude sinewave is audible.

Calibration

Start by using a known good 1,000μF capacitor with a voltage rating of at least 25V in position Cx. Adjust VR1 until the LED goes off. Mark the scale 0.1Ω. Now add known-value resistors in series with Cx and adjust VR1 until the LED just goes off. Mark the scale with the new total resistance value. You may find it convenient to use increments of 0.1Ω on the 1Ω range and suitably larger increments on the other two ranges.

Interpreting the Results

Fig. 3 shows typical ESR values, based on manufacturers' data and allowing for the fact that ESR measured at 10kHz is usually one third of that measured at 1kHz. The ESR values with 10V normal grade capacitors can be seen to be four times those with low-ESR 63V types. Thus when a low-ESR type has deteriorated to the point where its ESR is the same as that of a normal electrolytic its internal heating will have quadrupled!

If you find that the measured ESR value is more than twice that shown in Fig. 3 the capacitor is past its best. ESR values for capacitors with voltage ratings other than those specified in Fig. 3 will be between the relevant lines on the graph.

Negative Resistance with an Op Amp

When a voltage increase is applied to a negative resistance there's a current decrease, i.e. $I = -V/R$.

Two operational-amplifier configurations exhibit negative input resistance. They are shown in Figs. 4 and 5. The one to use depends on the source resistance of the circuit to which it's connected. This is because the circuits use negative and positive feedback simultaneously, the source being part of the feedback potential dividers. If the proportion of

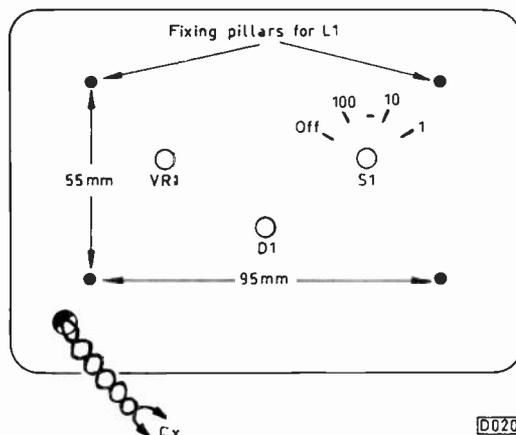


Fig. 2: Front panel layout.

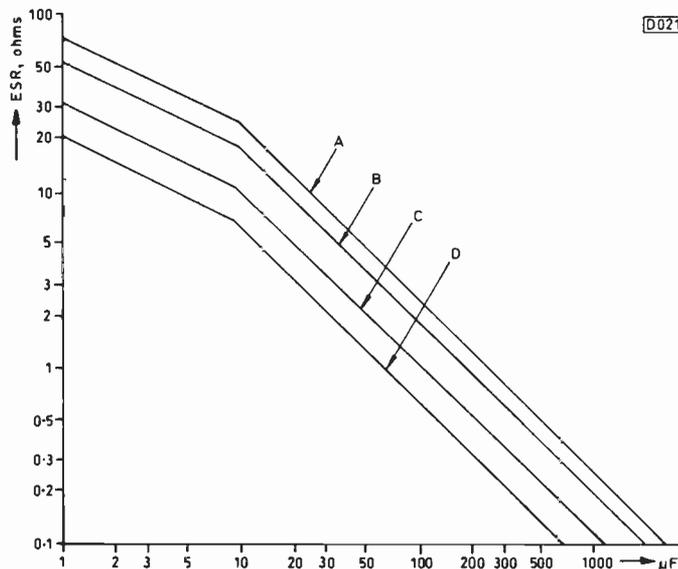


Fig. 3: Typical ESR values, A 10V normal grade, B 25V normal or 10V low-ESR grade, C 100V normal or 25V low-ESR grade, D 63V low-ESR grade.

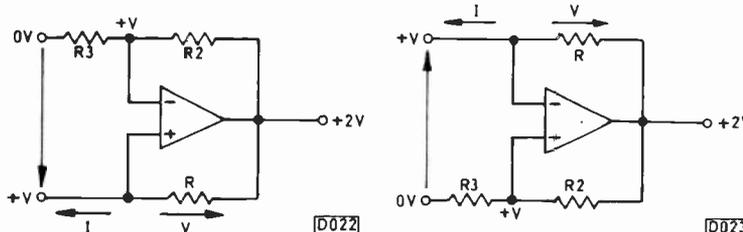


Fig. 4 (left): Negative-resistance op-amp circuit when the source resistance is less than R.

Fig. 5 (right): Negative-resistance op-amp circuit when the source resistance is greater than R.

the output fed back to the non-inverting (+) input in Fig. 4 is too large or the stage gain in Fig. 5 is too great unwanted oscillation will occur and the circuit won't function as a negative resistance.

Conventional current notation is used in the following explanation. In Fig. 4 the values of R2 and R3 are equal. Thus when +V is applied to the input the output rises to +2V. The voltage across R is then V and its direction is such that I must flow out of the input. So the circuit's input resistance is $V/I = -R$, which means that the input resistance is of magnitude equal to R but negative in value.

The same analysis can be applied to the circuit shown in Fig. 5. Remember that these circuits will be stable only when the source resistance is as shown, and that operation as described is possible only when the operational amplifier's normal voltage and current ratings are not exceeded.

Components list

R1	6.8Ω	R8	47k	R15	150k
R2	1k	R9	560Ω	R16	1.1k
R3	1M	R10	120k	R17	2k
R4	100k	R11	120k	R18	11k
R5	10k	R12	33k	R19	10k
R6	270k	R13	2.2M	R20	10k
R7	470k	R14	150k	All	0.25W 5%

VR1 100k

C1 2.2nF C2 220μF, 15V C3 0.1μF
C4 10nF

IC1 TL084CN Tr1 BC547 Tr2 BC557
Tr3 BC547 D1 Red LED

L1 14m of 30g enamelled wire – see text

S1 3-pole 4-way switch

ABS box, stripboard

Panasonic NVMS2B

This camcorder would play back a tape quite normally if the record tab was removed but a virgin tape would be greeted with high-pitched whistling that drowned out the sound track. In these machines the tab switch enables Q6003, which then feeds 9V to various places including the 2SB1219 transistor Q4005 that produces the delayed 9V record voltage. The problem was that Q4005 was passing about 2.5V to the record circuits even when no switching voltage was applied to it. A replacement cured the fault – it's a surface-mounted device. **B.S.**

Panasonic NVMC5

This rather elderly camcorder came in with a request for an estimate for head replacement and a service. Despite the machine's apparent age the mechanism was clean and sparkling, with no signs of wear and tear. When our test 'C' cassette was played back however we found that the output from one head was missing. As I suspected, replacement heads produced no improvement. So attention was turned to the head amplifier pack and the flexible connector from the drum to the pack. Removing and resoldering the connecting pins cured the fault completely. **B.S.**

Panasonic NVMC20

This camcorder was accused of bloody-mindedness: it would sometimes refuse a tape, just ejecting it then leaving the cassette door open! It performed beautifully on test of course, showing no inclination at all to misbehave. After a call to Panasonic a nice man called Phil assured me that a replacement mode switch would cure the problem. It's part no. VES0416 and did the trick. **B.S.**

Sony CCDF340E

The symptoms were no sound and intermittent VTR functions. Neither fault was difficult to cure. The no sound fault was cured by replacing the microphone preamplifier chip IC585. A damaged flexi board was the cause of the intermittent VTR functions (how do they get damaged?). **D.C.W.**

Ferguson FC28

The fault report said "won't always switch on and, when working, won't always switch off". I thought that this was probably a mechacon reset problem but inspection revealed nothing more than a faulty power switch (SW617). Note that with these machines the response to a selected mode, e.g. power on/off, play etc. is not always instant – a sort of "soft" response to commands is often evident (or is it me?). **D.C.W.**

JVC GR65E

No autofocus was the problem with this one. The motor assembly proved to be at fault, with a jammed gearbox. The initial drive from the motor is via a belt that's connected to a reduction gear (a sealed unit). It was this item that had failed, possibly because the slipping clutch assembly, which

is the final part of the autofocus drive to the lens assembly, was locked tight and was unable to slip when required. Manual focus adjustment probably caused the gearbox failure. **D.C.W.**

Sony CCDF450E

I suppose we all get caught out sometimes by diving in too deeply. The symptom with this machine was intermittent playback functions, including fast-forward/rewind search. Recording was o.k. After some abortive in-depth investigations I discovered that the power switch (camera/player) made intermittently poor contact in the play mode. A replacement put matters right. **D.C.W.**

Panasonic NVMS1

Sound recording via the microphone was o.k. when listened to using the headphones but there was no output from the A/V out connector (the picture was o.k.). Playback sound was also available only via the headphone socket. The cause of the trouble was that the 2SD1328 audio mute transistor Q4013 was short-circuit emitter-to-base. Note that it's mounted at the opposite end of the main PCB to most of the audio circuitry. **D.C.W.**

JVC GRA30E

Two of these came in at the same time from the same source with the same fault – no functions, with the emergency mode indication E01 in the viewfinder. This means that the 8V supply is missing. Amongst other uses it appears as the r.f. unit supply at the AV output socket. The cause of the trouble was a faulty AV lead, which had been tried with both cameras. Unfortunately there's no fuse in this line to protect the main d.c.-d.c. converter. So two converters had to be replaced, which was a costly exercise. In view of the fact that it's an easily produced fault it is surprising that better protection wasn't incorporated. **D.C.W.**

Sony CCDV88E

This machine would shut down intermittently in the play mode and just sit there looking at you. Careful inspection at the instant of failure revealed that just before the shut down occurred the capstan motor's speed rapidly increased. We decided to investigate the capstan FG circuit and found a dry-joint at pin 16 of IC503, the capstan FG waveform shaper. **D.C.W.**

Fugix M890

This machine is a clone of the Sony CCDTR75E. The problem was an intermittent trigger button – the sub-trigger button worked all right. Unfortunately the trigger button switch is available only as part of the complete control assembly, which includes wide/telephoto toggle, play, record, pause etc. and all the operation keys. A replacement is costly, especially when only one key function has failed. **D.C.W.**

TV Fault Finding

Reports from Philip Blundell, AMIEE, Richard Newman, Paul Hardy, Chris Watton, John Edwards, Michael Dranfield, Brian Storm, Steve Cannon, Alfred Damp, and Geoff Fardon

Philips K40 Chassis

This set had no sound or vision – there was just a blank raster. Tracing back through the signal path with a signal generator I obtained activity when injecting a signal at the output of the TDA2541 i.f. chip but none when applying the signal to its inputs. The voltages at the input pins were different: they should both be at 5.2V but pin 16 was low, with a 1.5k Ω leak to chassis. The other input (pin 1) didn't have this leak. Disconnecting pin 16 proved that there was internal leakage via the chip so a replacement was fitted – to no effect! What else that could cause a low resistance from pin 16 to chassis was connected to the chip? Nothing seemed to be likely until I looked in the SGS data book and found that pins 2 and 15 have decoupling capacitors connected to them. The one connected to pin 15, C2115 (22nF), was leaky. **P.B.**

Philips CP90 Chassis

When checking this chassis for dry-joints one place where you might not think to look is in the i.f./sync can. Dry-joints can occur in this can, especially around the TDA2579 chip. **P.B.**

Philips NC3 Chassis

There was a blank raster though sound was present and the on-screen display worked. A check on the waveforms around the TDA3565 colour decoder chip showed that the sandcastle pulses were present and a video signal went in, but nothing came out. Voltage checks then showed that the brightness control pin was high – 2.5V instead of 0.6V at the maximum brightness setting. A new TDA3565 was required. **P.B.**

Philips 2A Chassis

The power supply was dead. Checks showed that there was 0.6V at the base of the BUT11AF chopper transistor and over 300V at its collector, but the circuit wouldn't oscillate. As there were no shorts across the secondary windings of the chopper transformer attention was turned to the snubber network connected to the primary winding. D6663 (1N5062) was found to be leaky – 150 Ω both ways. **P.B.**

Philips G110 Chassis

When the power supply in this chassis breaks down Philips supplies a complete repair kit. You must replace all the parts supplied. I recently had one of these sets come in from another dealer who said that although he'd fitted the power supply kit the set would shut down after an hour or so, just as though it had been switched off. Sure enough the set did exactly as he said. When I checked the 140V supply I found that there was virtually no voltage here while the supply from the mains bridge rectifier was down to about 20V (instead of 280V). Two of the bridge rectifier diodes were going open-circuit when warm. I replaced all four and had no further problems after that. When I spoke to the dealer he

said that he hadn't bothered to change the diodes, although they are part of the kit, because they had measured all right. A lot of frustration could have been avoided if he had heeded the manufacturer's instruction to change all the parts in the kit. **R.N.**

Questar CTR14

This set was dead. I'd seen it about a year before for a similar fault and had had to replace R652 (390k Ω) which had been open-circuit. It again had to be replaced, but this time the STK7348 went short-circuit at switch on, taking with it R651 (27 Ω , 2W), R653 (1.5 Ω , 2W) and C655. Everything was fine when these items had been replaced. **P.H.**

Contec KT8135

There was no luminance. The cause was a poor plug and socket connection for the luminance drive on the c.r.t. base panel. **P.H.**

Hitachi C14P218 (G7P Mk 2 Chassis)

This 14in. portable was stuck in standby. A check at the collector of the BUT11AF chopper transistor Q903 produced a reading of some 300V, so obviously the mains bridge rectifier diodes etc. were o.k. Two series-connected 82k Ω resistors, R902 and R903, provide a start-up bias for Q903. They are at the front, right-hand corner of the chassis and were both open-circuit.

Another fault you get with these sets is that the screen goes very bright then the set trips. The cause is that a capacitor near the line output transformer becomes dry-jointed because a part of the cabinet back pushes against it, eventually forcing it from the panel. The capacitor concerned is C711 (47 μ F), which is the reservoir capacitor for the h.t. supply to the RGB output transistors. I cut the offending portion off the inside of the cabinet back – it doesn't seem to have any purpose. **C.W.**

Matsui MB10

"Dead on mains" the report said and a quick check with the bench 12V power supply proved that the set was otherwise o.k. So off with the back and into the chopper power supply on the left-hand side. The primary supply was present but there was no oscillation. I noticed a capacitor on the print side of the panel: it was not shown in the circuit diagram and was connected between the h.t. line and the collector of the chopper transistor. A check showed that it was short-circuit, thus preventing any current flowing in the chopper transformer's primary winding. A replacement restored mains operation – it's a 4,700pF capacitor with a voltage rating of 2kV. **C.W.**

Toshiba T211T4BA

When I switched this set on it seemed to work all right but as soon as I changed channel it began to search tune down-

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	AN253P £1.80	HA3434 £2.75	LA1307 £5.40	ME4220P £4.50	SL4710P £2.20	STR1085 £3.60	TA7807 £3.50	TD15112 £2.70	TDAS391 £3.00	UPC15134A £2.00
	AN3281K £0.75	HA343 £1.20	LA1398 £3.50	MM1035 £5.75	SL480 £3.30	STR125 £5.50	TA7807AP £2.50	TD15151A £2.50	TDAS651AQ £5.50	UPC1520CA £2.48
	AN3822 £7.50	BA3505F £2.75	HA1406 £2.00	MM1036N £3.70	SL490 £3.00	STR40090 £8.50	TA7809P £2.70	TD1520 £3.95	TDAS653 £4.00	UPC339C £0.70
	AN5015 £3.50	BA3704 £2.75	HA1457 £2.10	MM1112CN £3.30	SLR018 £3.00	STR4211 £6.50	TA7814 £2.50	TD1522 £1.50	TDAS654 £2.80	UPD4011 £1.75
	AN5033 £5.00	BA4210 £2.50	HA4219 £2.70	ML1360 £5.00	SLR178 £4.20	STR440 £5.00	TA7828P £2.40	TD1670A £3.00	TDAS710 £2.90	UPD4066 £1.95
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	AN6332 £4.00	BA6109 £1.80	L7905 £0.80	ML6402G £1.00	STK2029 £8.50	TA4193 £3.00	TA7888AP £5.50	TD2005 £1.70	TDAA600-2 £2.60	2SA942 £0.35
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	AN6344 £0.50	BA6154 £2.50	L7915 £0.80	MM749CN 8 PIN £1.25	STK2250 £9.20	TA4301 £5.50	TA7909 £2.50	TD2006S £1.95	TDAA610 £2.50	2SB1016 £1.50
	AN6346 £4.50	BA6208 £2.75	L7918 £0.80	MM749N £2.00	STK3041 £5.70	TA4345 £3.40	TA7938 £2.50	TD2007 £3.50	TDAA501 £2.00	2SB872 £0.40
	AN6346 £4.50	BA6208 £2.75	L7924 £0.80	MM749N £2.00	MM4567N £2.50	STK4030 £3.00	TA7939 £3.00	TD2010P £1.10	TDAA750 £5.50	2SB872 £0.40
	AN6359 £0.50	BA6219 £1.95	ML1480 £2.60	M104 £7.00	MM4568N £2.50	STK4121 £0.80	TA7912 £1.20	TD2030H £2.00	TDAT600P £2.40	2SB879 £0.55
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	AN6884 £2.75	BA6304 £1.70	ML3220 £1.00	MS1014L £1.95	MPF45148C £5.00	STK435 £3.00	TA7222 £2.25	TD2510 £4.20	TEA1039 £2.00	2SC2230 £0.50
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	AN7116 £1.20	BA718 £1.80	ML3700 £2.50	MS1383 £4.25	SAA1005 £2.50	STK441 £10.50	TA7232P £1.50	TD2532 £3.00	TL011CP £2.00	2SC2331 £0.26
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VIDEO HEADS Continued

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ASK FOR VIDEO HEADS NOT LISTED

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wards. If the down button at the front of the set was pressed the search would stop for a short time then start again. A new 47C232AN4984 tuning chip (ICA11) cured the trouble. C.W.

Finlux 3029 (3000 Chassis)

This monster set suffered from what could be described as "line spacing": the top quarter of the picture was o.k., but towards the bottom of the screen every other line appeared to be blanked out. A fault in the field output stage seemed likely so several components in this area, including the field output chip, were replaced. All to no avail until we came to CK8 (0.1 μ F, 63V). Replacing this cured the problem. It's a small, white square-shaped capacitor positioned beneath the field output chip's heatsink. J.E.

Hitachi CPT2188 (Salora K Chassis)

This set was dead. There was a distorted waveform at the base of the line output transistor and an almost identical waveform at its collector – a check showed that its base-collector resistance was only 85 Ω . We didn't have the original type (2SD1577) in stock so we decided to try a BU508A instead. The 2SD1577 has an insulated body, so its heatsink is soldered to chassis. The BU508A was therefore mounted on the heatsink using a conventional mica insulator, spacer and bolt system. A long test run showed that the transistor ran cool. J.E.

Tashiko 20F862

When this set was switched on the standby indicator flickered briefly but the set otherwise remained dead. The cause of the fault turned out to be C701 (47 μ F, 450V). For good measure we replaced C506 (47 μ F, 450V) as well. J.E.

Salora K Chassis

For tripping out when changing channel, also the field output chip IC501 having a very short life, check choke L601 in the line output stage. In the set we had in L601 looked as if it had got very hot and clearly had shorted turns. M.Dr

Hitachi CPT2656

This set wore a Finlandia badge but we were able to match it up with one of our Hitachi service manuals. Over a period of eight months it has been back to the workshop on several occasions, but each time it failed to display any fault during a soak test. The customer's complaint was that the bottom part of the picture was missing. Despite replacing many components in the field output stage the set kept on coming back. It was difficult to know what to do as we'd not seen the fault. On its latest visit however the fault put in an appearance: after about an hour the bottom of the picture began to cramp up while the top widened out. By feeding a crosshatch pattern signal to the set we could see that the actual symptom was change in linearity. A slight touch on preset RTB573 (470 Ω) cured the fault. So a replacement linearity potentiometer was fitted and the set was handed back to the customer with confidence. M.Dr.

Panasonic TX21T1 (Alpha 2 Chassis)

The complaint was about an intermittent whistling noise when the set was first switched on. Sure enough a high-

pitched whistle came from the set when I switched it on, stopping as soon as I touched it and then not to return until next day. In fact any attempt to touch the set cured the fault until next day. Many days later the cause of the fault was traced to a dry-joint on the line output transformer's over-winding – the point that provides sync between the line output stage and the chopper power supply. B.S.

Ferguson TX10 Chassis

We don't get many TX10s in these days. This one gave us some real grief however. It had been in for almost a fortnight, running on soak test, and the fault complained about was just beginning to put in an appearance. At switch on first thing in the morning there was field bounce. For only five minutes mind, then it would work perfectly for the rest of the day. Even switching it off and leaving it for a good few hours didn't seem to make any difference: the set would fault only between 9 and 9.15 a.m. We'd tried freezer of course, but this didn't give us any definite clues. Then one morning the fault showed up for a lot longer than usual and also developed further: there was intermittent field rolling and the line sync jittered. Well it was now or never, so on to the bench it came.

We replaced the TDA2578A timebase generator chip IC742 as this was the obvious thing to do. It didn't help, but at least the fault was still present. As both the line and field sync were affected I suspected that the cause of the fault was around the input to the sync separator. A scope check was made on the video waveform at pin 5 of the TDA2578A chip and at first glance it looked fine. This point is biased by R759 and R753, which are close-tolerance components and have given us trouble before. But replacements made no difference. Upon closer examination of the video waveform the line sync pulses did seem to be rather thin, if you know what I mean, so maybe there was a fault earlier in the video processing. This seemed a bit of a long shot. I couldn't compare waveforms, and the one we had wasn't far removed from the oscillogram shown in the manual. But to prove a point I found a signals panel and transplanted it into the set. Sync lock was now perfect and, looking at the scope, the pulses had certainly put on weight. The original panel was refitted and scope checks showed that the video waveform was faulty right back to the i.f. panel. When this was swapped over the fault had cleared. Now the set was on rental, so I contemplated leaving it with the good panel installed. But as there was only half an hour till lunch time I thought that I might as well continue. I'd been at it all morning, and might as well get some satisfaction by tracing the cause of the problem to component level – and anyway I wasn't going to cheat!

I thought it was only going to be the i.f. chip. How wrong can you be? Replacing it made no difference, but use of freezer and the heat gun now made the fault come and go. Its cause was finally traced to the electrolytic capacitor C35 (1 μ F) in the a.g.c. feed to the SL1432 i.f. preamplifier chip. A replacement sent me off to lunch with a beaming smile. S.C.

Panasonic TC21R1 (Alpha 2 Chassis)

The reported fault was no picture. E.H.T. was present but there was no raster. When the first anode voltage was increased I saw that the cause of the symptoms was field collapse. A new field output chip made no difference and its supply was intact. Now the first thing to suspect with a faulty Panasonic set, once the obvious items have been ruled

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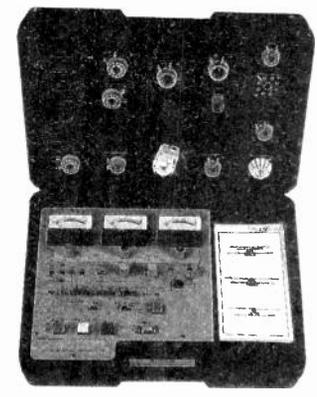
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out, is a defective 10nF ceramic capacitor. I looked at the circuit diagram and the first one I came across was C403, which is connected to pin 2 of the TDA2579 timebase generator chip. A check showed that it read just over 100Ω in circuit. When a new one had been fitted we had full field scanning. If I had a pound for every 10nF ceramic capacitor I've replaced I'd be laughing. S.C.

Philips 2A Chassis

This set ticked quite noticeably in standby. Everything else was perfect, but the ticking wouldn't go. I was convinced that the cause of the trouble was in the power supply, and after a long and finally rewarding search the culprit turned out to be C2690. It's a 1μF, 100V non-polarised capacitor that's connected between the earthy side of the chopper driver transistors and the non-isolated chassis. S.C.

Mitsubishi CT21M1BM

The red LED was illuminated but apart from that the set wouldn't come on at all. I removed the back with some trepidation, being rather a novice when it comes to Mitsubishi sets. Fortunately the power supply looked to be reasonable and conventional. After checking the output voltages it seemed that the cause of the problem was absence of the 12V supply. This comes from a 12V regulator, and I soon found that there was an input to this device but no output. The standby control line acts on this regulator, and I thought I'd try my luck here.

This line leaves the power supply and goes directly to the POW pin of the microcontroller chip IC701. After probing around in this area with the meter I found that the set would kick up. Dry-joint time, it seemed. The legs of crystals are usually a favourite, whether it be a remote control unit, a Nicam panel or a microcontroller chip. Sure enough both legs of the 4MHz crystal CF701, which is connected to pins 28 and 29 of IC701, were dry-jointed. Resoldering them provided a speedy cure, thankfully. S.C.

Toshiba 2512DBT

The reported fault was of whistling Nicam reception. In fact Nicam reception was pretty dire, with crackling and popping in addition to a permanent high-pitched whistle. As expected, the f.m. sound was perfect. By chance I noticed that moving the scan coil flylead or the Nicam signal leads aggravated or alleviated the problem. It transpired that the line scan current was interfering with the digital data signal going to the Nicam panel. Redressing both sets of leads completely solved the problem. S.C.

Grundig CUC2410 Chassis

This set was dead: the power supply would try to start, but with little success. After a cold check on all relevant resistors and fitting a new TDA4600 chopper control chip we eventually traced the cause of the fault to C633 (100μF, 25V) which was open-circuit. A.D.

Matsui 2890/Saisho CM2880TX

There was field collapse, the white line being very bright indeed. Had this additional factor registered with us time wouldn't have been wasted looking for a fault in the field output stage. The cause of the fault was in the video output supply, where D406 was short-circuit and the series safety resistor R440 was open-circuit. A.D.

Hitachi G8Q Chassis

There was an intermittent start-up fault with this set. When cold it would sometimes come on only in standby. But if the mains switch was held the set would eventually come on correctly. The cause of the fault was traced to the start-up thermistor TH902. A.D.

Amstrad TVR2

Several of these sets have come in either dead or intermittently dead. In just about every case the cause has been that C1507 (1μF, 50V) was either leaky or open-circuit.

An exception came in the other day. Although the job ticket said that the set was dead it wasn't the 1μF capacitor. The cause of the problem was that the mains relay wasn't being energised because there was no 5V output from the power supply. In fact the fault had nothing to do with the TV side of the combination: a fuse in the VCR section had blown. A.D.

Supra STV1401R

This colour portable was dead. There was 350V at the input to the STR5412 regulator chip IC104 but no output at pins 2 and 4. Replacing this item restored normal operation. G.F.

Saisho CT142RX

There was an intermittent fault with this set. The picture would go very dark, with very prominent colour. It was as though the luminance delay line was open-circuit. Additional symptoms were a three-inch vertical band, predominantly red, and faint flyback lines.

We found that the tube base panel was very sensitive to being touched. The cause of the trouble was poor joints on three of the pins of the ribbon cable that goes to connector plug/socket CD803. G.F.

Hinari TVA1

After the initial start-up this set was very intermittent/temperamental about coming out of standby. Just about everything in the power supply seemed to be sensitive to heating/freezing, including the relay. The fault cleared when a new STR5412 chip was fitted. G.F.

Matsui CTV2055

There was an over-bright picture with flyback lines. When the first anode and brightness settings were reduced there was shading from the left-hand side of the screen. We found that the h.t. supply to the RGB output stages was low at only 113V instead of 190V. The reservoir capacitor C120 (4.7μF, 350V) was open-circuit. Incidentally this set is a Fidelity clone. G.F.

Bush 2020

This set suffered from an intermittent fault. There would sometimes be a blank screen, but on occasions this would have a thin red line across it, as if there was field collapse. The fault was so intermittent that it could take anything from minutes to weeks for it to recur. We found that touching the board almost anywhere when the set was warm would produce the fault, which was thus very difficult to localise. Eventually we found a bad joint on C307, which is partially hidden by a plastic support strut. G.F.

AN3215K	£4.50	AN7163	£2.95	LA3210	£0.95	MB3730	£2.20	SK5337	£7.25	TA727A/AP	£2.50	TEA1017	£2.75	2N3055	£0.60
AN3310K	£4.50	AN7166	£3.70	LA3370	£2.50	MB3731	£2.75	SK5338	£4.50	TA7280P	£2.95	TEA1039	£2.20	2N3773	£1.50
AN3312K	£2.95	AN7168	£2.75	LA3375	£2.50	MB8841	£5.75	SK5421	£8.50	TA7281P	£2.75	TEA1042	£3.75	2N3819	£0.30
AN3320K	£4.95	AN7169	£2.95	LA3376	£2.20			SK5422	£6.50	TA7299P	£2.95	TEA1060	£2.20		
AN3331K	£5.75	AN7171K	£4.75	LA4108	£2.20			SK5451	£5.30	TA7317P	£1.50	TEA1061	£2.20		
AN3792	£2.95	AN7172K	£2.95	LA4137	£1.95	SAA1124	£2.50	SK5471	£5.60	TA7307AP	£2.20	TEA2018A	£1.95	2SA7669	£0.95
AN3821K	£2.95	AN7173K	£3.50	LA4145	£1.70	SAAS030	£2.50	SK5481	£9.95	TA7609P	£2.70	TEA2018A	£1.95	2SA1106	£2.75
AN3822K	£2.95	AN7178	£2.50	LA4160	£2.20	SAAS042	£8.00	SK5482	£5.95	TA7611AP	£2.20	UPC575C	£1.00	2SA1111	£0.95
AN3830K	£2.50	AN7310	£1.20	LA4162	£2.50	SAA301A	£3.95	SK5730	£4.25	TA7628P	£1.95	UPC1025H	£1.30	2SA1186	£0.95
AN5010	£2.50	AN7420	£1.95	LA4170	£1.75	STA401A	£4.50	SK6732	£1.75	TA7640AP	£1.30	UPC118EH	£3.75	2SA1285	£2.40
AN5011	£2.50	BA5408	£2.20	LA4182	£1.95	STA441C	£2.75	SK7308	£5.30			UPC1191V	£1.20	2SA1294	£3.95
AN5033	£2.95	BA5410	£2.95	LA4183	£2.20	STK0029	£4.75	SK7348	£4.95			UPC1192C	£1.80	2SA1302	£3.25
AN5135K	£3.25	BA6209	£1.95	LA4190	£1.75	STK0049	£4.75	SK7404	£6.95			UPC1237H	£1.20	2SA1306	£0.95
AN5150	£2.50	BA6229	£2.20	LA4260	£2.30	STK0433	£5.25	SK8050	£9.50			UPC1263C	£1.30	2SA1307	£1.10
AN5151N	£2.50	BA6239A	£2.20	LA4261	£2.30	STK435	£5.50	SK8250	£9.95			UPC1277H	£2.50	2SA1516	£2.50
AN5256	£1.75	BA7005	£1.80	LA4265	£2.30	STK437	£7.50	SK8250P	£12.50			UPC1279H	£2.50		
AN5410	£3.95	BA7004	£2.00	LA4280	£2.95	STK443	£8.95	STR450	£8.95			UPC1318A	£2.75	2SB856	£0.50
AN5435	£2.20	BA7512AL	£1.95	LA4282	£2.50	STK459	£7.50	STR454	£8.75			UPC1318B	£2.75	2SB856	£0.50
AN5510	£2.75	HA1339A	£3.50	LA4428	£2.50	STK459	£7.50	STR456A	£8.75	DA11010A	£1.40	UPC1318C	£2.75	2SB856	£0.50
AN5515	£2.20	HA1339	£2.95	LA4445	£2.20	STK463	£9.50	STR457	£8.75	DA1510	£1.40	UPC1318D	£2.75	2SB856	£0.50
AN5521	£2.20	HA1377	£2.20	LA4446	£2.20	STK465	£9.95	STR459	£9.70	DA15180	£2.95	UPC1318E	£2.95	2SB856	£0.50
AN5560	£2.20	HA1388	£2.95	LA4460	£1.80	STK1050II	£7.25	STR1209	£8.20	DA1522	£1.95	UPC1318F	£1.20	2SB856	£0.50
AN5610N	£4.95	HA1392	£2.95	LA4461	£1.80	STK1060	£7.95	STR1209E	£8.20	DA1770A	£2.95	UPC1387C	£1.95	2SB875	£1.80
AN5615	£2.50	HA1398	£2.20	LA4465	£2.30	STK1070II	£7.95	STR2005	£9.95	DA1770B	£2.95	UPC1387D	£1.95	2SB875	£1.80
AN5620X	£4.95	HA1394	£2.50	LA4466	£2.30	STK2028	£7.50	STR2012	£6.20	DA20003	£0.95	UPC1391H	£1.50	2SB883	£2.95
AN5622	£3.20	HA1396	£3.75	LA4475	£2.50	STK2029	£6.50	STR2013	£6.20	DA20004	£0.95	UPC1403CA	£3.20	2SB883	£2.95
AN5635N	£3.75	HA1398	£2.50	LA4476	£2.50	STK2038II	£9.50	STR3105	£4.75	DA20025	£1.95	UPC1403CA	£3.20	2SB883	£2.95
AN5700	£1.75	HA1211	£2.30	LA4498	£2.95	STK2048II	£9.75	STR3115	£9.95	DA2005M	£2.50	BD131	£0.35	2SB1105	£1.20
AN5750	£2.20	HA11219	£1.75	LA4500	£2.50	STK2125	£6.75	STR3125	£5.50	DA2005S	£2.50	BD135	£0.25	2SC1405A	£4.50
AN5790	£2.95	HA11223W	£1.50	LA4505	£2.80	STK2128	£6.95	STR4211	£4.50	DA2005T	£2.50	BD136	£0.25	2SC1405A	£4.50
AN5836	£2.20	HA11226	£4.50	LA4508	£2.50	STK2155	£9.50	STR5015	£6.20	DA20200	£1.50	BD137	£0.25	2SC1415A	£2.60
AN5900	£2.20	HA11244	£2.85	LA4700	£3.50	STK2230	£6.50	STR5412	£9.20	DA20203	£1.50	BD146	£0.25	2SC1573	£0.50
AN6250	£1.50	HA11255	£1.50	LA5327	£1.85	STK2240	£9.50	STR6020	£6.20	DA25440	£1.70	BD139	£0.25	2SC1827	£1.00
AN6256	£1.50	HA11261	£2.50	LA5327	£1.85	STK2250	£9.50	STR6020	£6.20	DA2577	£3.25	BD140	£0.25	2SC1969	£1.75
AN6270	£3.50	HA11256	£4.75	LA7032	£2.95	STK3041	£6.50	STR1006E	£6.70	DA2578A	£2.50	BD244C	£0.50	2SC1969	£1.75
AN6310	£5.50	HA11714	£4.75	LA7033	£2.75	STK3041	£6.50	STR11006	£6.20	DA2579	£2.50	BD244C	£0.50	2SC1985	£0.95
AN6320	£2.95	HA11724	£8.00	LA7035	£4.95	STK3044	£5.75	STR20005	£5.50	DA2579B	£2.50	BD607	£0.95	2SC2073	£1.20
AN6326N	£3.50	HA11747A	£5.50	LA7042	£2.75	STK3062	£6.75	STR20012	£5.20	DA2600	£6.00	BD608	£0.95	2SC2166	£1.00
AN6327	£3.50	HA11747ANT	£7.50	LA7223	£2.75	STK3082II	£6.95	STR30125	£4.75	DA2611A	£1.30	BD711	£0.85	2SC2335	£1.20
AN6332	£4.75	HA11781N	£3.50	LA7224	£2.95	STK3102II	£5.75	STR40090	£6.75	DA2653A	£4.50	BD712	£0.85	2SC2542	£1.80
AN6337	£3.95	HA11781NT	£3.95	LA7520	£3.25	STK3152II	£5.50	STR4090	£6.20	DA3501	£4.50	BD912	£0.95	2SC2570	£0.50
AN6340	£3.75	HA11788	£4.50	LA7755	£3.20	STK3152II	£5.50	STR41090	£6.20	DA3501A	£4.50	BD912	£0.95	2SC2580	£2.80
AN6342N	£2.50	HA11827N	£8.50	LA7800	£1.50	STK4025	£6.50	STR44115	£8.20	DA3510	£4.50	BD939	£0.50	2SC2792	£4.95
AN6344	£4.75	HA11870N	£5.25	LA7801	£1.50	STK4121II	£5.95	STR50020	£6.20	DA3560	£3.90	BD940	£0.50	2SC2837	£2.95
AN6348N	£3.75	HA12047	£3.50	LA7808	£2.75	STK4122II	£5.95	STR50103	£4.50	DA3561A	£3.95	BD731A	£0.60	2SC3026	£5.50
AN6350	£3.50	HA12047	£3.50	LA7808	£2.75	STK4131II	£6.75	STR50150	£5.70	DA3562A	£4.50	BD732	£0.60	2SC3026	£5.50
AN6356	£3.85	HA13001	£1.90	LA7910	£1.75	STK4132II	£6.75	STR5015A	£5.70	DA3563A	£4.95	BD761A	£0.75	2SC4236	£5.50
AN6357N	£4.50	HA13007	£4.50			STK4141II	£7.50	STR50213	£6.20	DA3730	£4.75	BT152-600R	£1.50	2SD288	£0.80
AN6359N	£5.50	HA13108	£2.95	LA8103	£1.50	STK4141V	£7.95	STR50401	£5.20	DA4271	£4.75	BT152-600R	£1.50	2SD401A	£1.20
AN6360	£2.60	HA13117	£2.75	LA8105	£1.50	STK4142II	£7.30	STR50401	£5.20	DA4427	£2.95	BT152-600R	£1.50	2SD401A	£1.20
AN6362	£4.50	HA13119	£2.50	LA8160	£2.20	STK4151II	£7.50	STR50941	£6.20	DA4437	£3.90	BU238A	£2.75	2SD526	£0.80
AN6363	£3.50	HA13128	£3.50	LA8164	£2.50	STK4152II	£7.85			DA4440	£3.95	BU238A	£2.75	2SD526	£0.80
AN6367K	£5.50	HA13128	£3.50	LA8164	£2.50	STK4161II	£7.95			DA4450	£3.95	BU260A	£1.30	2SD669	£1.25
AN6387	£5.50	HA13403V	£3.50	LC4066B	£2.95	STK4161V	£7.95			DA4500	£3.95	BU260A	£1.30	2SD678	£0.65
AN6394	£5.20	KA2206	£1.75	LC4066B	£2.95	STK4172II	£8.95			DA4510	£4.50	BU406	£0.95	2SD811	£2.85
AN6571K	£4.95	KA2210	£2.40	LC7137	£4.50	STK4181II	£9.95	TA7193P	£4.00	DA4600	£2.50	BU407	£0.70	2SD871	£4.90
AN6575	£4.50	KA2213	£1.30	LC7815	£2.95	STK4191II	£9.50	TA7205AP	£1.00	DA4600-2D	£2.50	BU408	£0.95	2SD880	£0.60
AN6577	£4.50	KA2214	£1.50	LC7818	£2.95	STK4192II	£9.50	TA7217AP	£1.60	DA4600-3D	£2.50	BU426A	£0.80	2SD988	£2.85
AN6587	£3.50	LA1130	£2.50	MS218L	£1.95	STK4332	£4.50	TA7222AP	£1.30	DA4600-3D	£2.50	BU426E	£0.70	2SD1346	£1.40
AN7105	£2.50	LA1170	£1.75	MS218P	£0.95	STK4332V	£5.90	TA7229P	£1.25	DA4600-4D	£2.50	BU500	£1.50	2SD1148	£1.90
AN7106K	£2.50	LA1185	£1.60	MS1102L	£2.95	STK4803	£8.50	TA7232P	£1.95	DA4660P	£2.95	BU508A	£1.00	2SD1207	£0.90
AN7143	£2.50	LA1240	£1.95	MS1104L	£3.20	STK4833	£9.50	TA7233P	£2.50	DA7000T	£2.80	BU508D	£1.00	2SD1276	£1.20
AN7147	£2.50	LA1260	£2.95	MS1358P	£1.75	STK4843	£9.95	TA7240AP	£2.95	DA7250	£4.95	BU508V	£1.20	2SD1397	£2.80
AN7148	£2.50	LA1266	£2.95	MS1393AP	£4.50	STK4853	£9.50	TA7241AP	£2.95	DA7255	£4.95	BUT11	£1.20	2SD1438	£1.50
AN7149	£2.50	LA1265	£1.50	MS1397AP	£3.50	STK5315	£6.75	TA7243P	£2.95			BUT11AF	£1.20	2SD1492	£2.95
AN7158N	£3.95	LA2400	£1.50	MS4937	£5.75	STK5324	£5.75	TA7250P	£2.95	TEA1002	£2.85	TIF4C	£0.35	2SD427	£3.30
AN7161N	£3.50	LA3101	£1.75	MS4544L	£2.75	STK5325	£6.75	TA7251BP	£2.95	TEA1009	£2.85	TIF4C	£0.35	2SD439	£2.20
AN7161NFP	£3.50	LA3160	£0.95	MB3712	£1.50	STK5332	£3.50	TA7270P	£2.50	TEA1014	£2.20	ZTX650	£0.30	2SD1887	£3.75

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The Universal Transistor

Gene Turnbull

Even though conventional transistors have largely been ousted by integrated circuits there are more types – though fewer of each – in use than ever before. To reduce stock-holdings, by both manufacturers and the service industry, research is being carried out by a Korean company, Taegu Semiconductor Inc., on a single device to replace all those in current use.

The most promising prototype has been given the development number UR1, and the aim is that it should be a workable substitute for both npn and pnp transistors in applications ranging from switch-mode power supplies to s.h.f. front-ends, taking in timebase, audio and logic switching roles. The device currently being tested has two bases, one for pnp configuration and the second for npn operation. The unused base is connected to the collector for an hFE (gain) of 40 and to the emitter for an hFE of 200, thus covering the tolerance spread of most transistors. Other characteristics of the device are V_{cbo} 1,400V, I_c 5A and f_r (typical) 14GHz.

Production transistors will be supplied with optional mounting kits, one of which adapts the device for surface mounting where this is required. Another one consists of a TO3 bracket, for use in place of BU208 and similar power transistors. A heatsink is required for high-power applications like these, but not for use in place of devices such as BC171s or BFQ33s. It has been calculated that high-power applications will account for less than half of the universal transistors used so, like the mounting kit, the heatsink will be marketed as an optional extra.

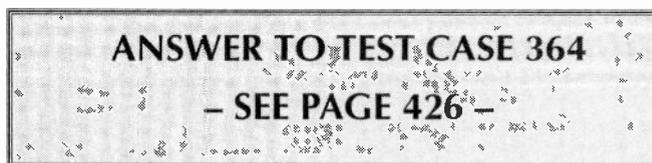
Price is of paramount importance with this type of product. If world sales reach the expected level, it's hoped that a trade price of £1.49 (UK equivalent) can be achieved. At this level Taegu Semiconductor expects to attract orders from all the major setmakers as well as service and repair shops in Europe, the Far East and America. A spokesman for the company claimed that the saving in stockholding, data books and equivalents lists would run to millions of dollars annually in the USA alone.

Taegu has several similar projects on hand in its research laboratories. One is a range of semiconductor-based replacement modules for thermionic valves, using high-voltage power f.e.t. technology. Each package will be similar in shape and size to the valve it replaces, with identical plug-in base connections. KT66 and 6V6G types are expected to find a large market amongst valve amplifier enthusiasts, who will be able to get the "valve-sound" characteristic they like without the risk of breakage or the need to pay for cathode heating power in an increasingly energy-conscious world. Other advantages of solid-valve technology are greater reliability, lower price and ready availability from Korea. Many conventional valve types are scarce and diffi-

cult to obtain now. The EF86, a low-noise audio preamplifier, is a typical example. Its solid-state equivalent, the SEF86, will use spin-off technology from the UR1 universal replacement transistor described above.

Also under development, but not yet available even in prototype form, is a universal integrated circuit. For economic and logistic reasons, it's unlikely that this will be designed as a replacement for all i.c.s – it's too difficult to price a chip that can act as either a simple quad-inverter or a VCR system-control microcomputer. If and when the device becomes available, it's most likely to be in the form of a 4-bit programmable microcontroller with a minimum of 100 pins. Not all applications will require use of all these pins, nor all four bits, especially as the CPUs used in domestic electronic gear generally work with serial control bus lines like the I2C. Here the spare pins are used to configure the i.c. as required, for control of a washing machine, a VHS VCR, an edit controller or a remote control gun for example. One of the most difficult aspects of the design of an i.c. like this is the arrangement of the lead-out pins and assigning it a type number.

Apart from the i.c. device, for which no production date has been quoted, the products are expected to come on stream at the beginning of the second quarter of next year. Distribution in the UK and Europe is likely to be in the hands of a Scandinavian company, Lufkirpa, that will set up a network of agents and wholesalers.



Two questions were posed at the end of this month's puzzle. Their answers are no, it wouldn't have been a wise move to replace the troublesome Hitachi VT430 VCR's capstan motor, and yes a replacement motor would have cured the problem!

How can we reconcile these two answers? Well, no sooner had Real Technician got the capstan motor out of the machine and gone to the component storage racks to look for a replacement than coffee break time came around and Television Ted, who also knows a thing or three about video machines, joined RT for a breather. On hearing about the faulty motor Ted asked to see the body before it was committed to the dustbin. When he turned the rotor he found that it was as stiff as a rusty winch!

When the motor's rotor and stator were separated the upper bearing surfaces were found to be covered with a dry, black substance that looked like hardened grease. A fibre pencil and a rag soaked in solvent were used to remove it from the shaft, while a solvent-saturated cotton bud on a stick was used to clean it off the sleeve. The bottom bearing seemed to be unaffected but was similarly cleaned. Both bearings were given a tiny dose of lubricant.

When the serviced motor was refitted the machine's performance was transformed. All functions worked properly and the motor ran cool.

Why is it that some VCR makes and models suffer from this problem while others are completely free of it, though all of them have a barrier ring just above the upper bearing to prevent the ingress of dirt?

Published on the third Wednesday of each month by Reed Business Publishing Ltd, Quadrant House, The Quadrant, Sutton, Surrey SM2 5AS. Filmsetting by Marlin Graphics, 2-4 Powerscroft Road, Sidcup, Kent DA14 5DT. Printed in England by BPCC Magazines Division, Carlisle Web Offset, Cumbria. Distributed by IPC Marketforce, Kings Reach Tower, Stamford Street, London SE1 9LS (071 261 5000). Sole Agents for Australia and New Zealand – Gordon and Gotch (Asia) Ltd., South Africa – Central News Agency Ltd. "Television" is sold subject to the following conditions, namely that it shall not, without the written consent of the Publishers first having been given, be lent, resold, hired out or otherwise disposed of by way of Trade at more than the recommended selling price shown on the cover, excluding Eire where the selling price is subject to currency exchange fluctuations and VAT, and that it shall not be lent, resold, hired or otherwise disposed of in a mutilated condition or in any unauthorised cover by way of Trade or affixed to or as part of any publication or advertising, literary or pictorial matter whatsoever. ISSN 0032-647X.



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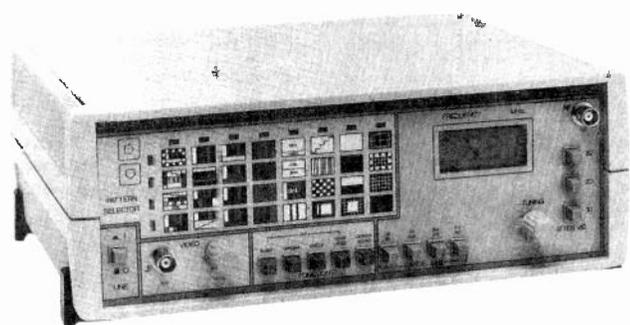
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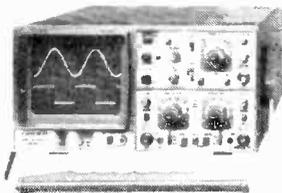
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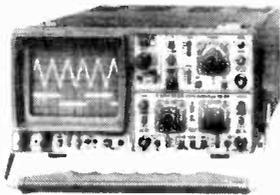
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- Triggering: DC - 80MHz
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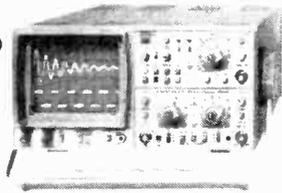
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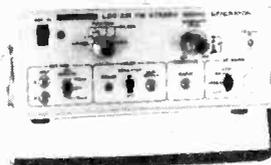
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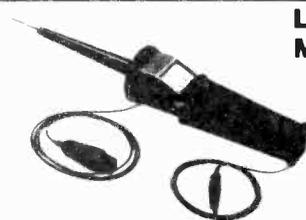


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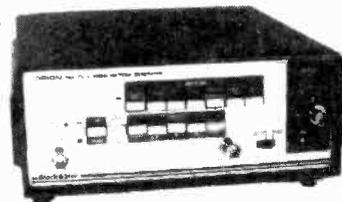
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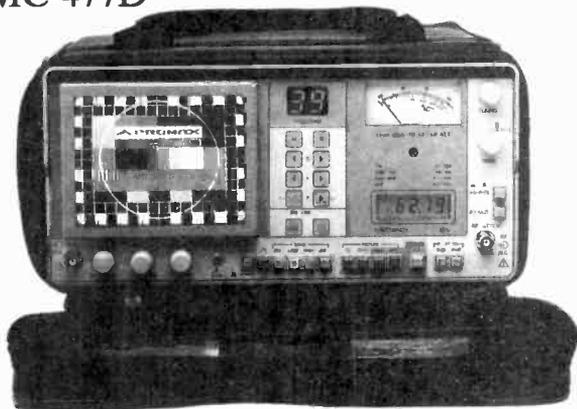
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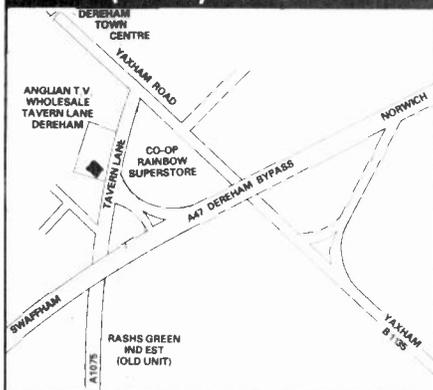
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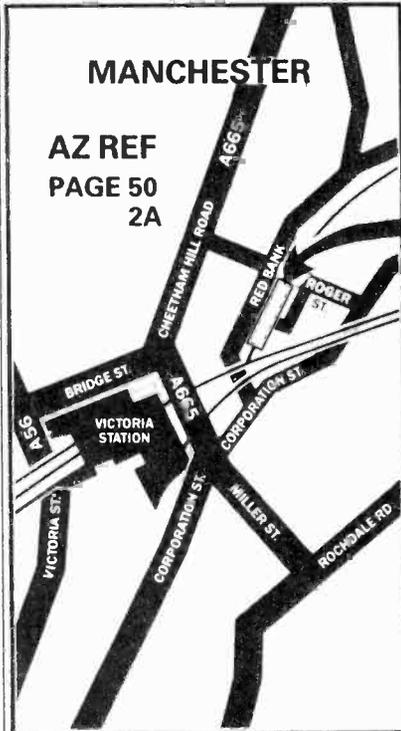
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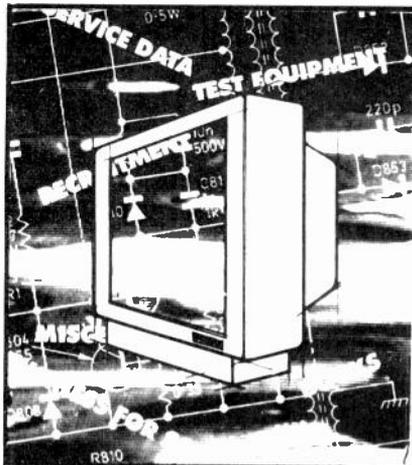
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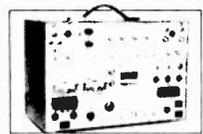
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SMALL SATELLITE TUNERS (950 to 1750 MHz), L.F. frequency 4000MH £9.00 each VHF/UHF S.BAND TUNER £3.00 NEW PLASTIC CASE 32 C.H. SAT-RECEIVER (no hand set) £35 (Post £5) NEW METAL CASE SAT-RECEIVER, 32 C.H. WITH DOB.BY & CHANNEL C (no hand set) £35 (Post £5) DAM MAINS CHASSIS AMSTRAD MONITOR C £5.00 UNIVERSAL TRIPLER, NEW TYPE £4.00 VIDEO LEADS 80p AMSTRAD Line O.P. Transistors with Diode 2SD453 £1.00 BL208A £1.00 VIDEO LAMPS, Long Lead £1.00 HITACHI & GEC FRAME, Thick Film £2.40 FIDELITY SPLIT DIODE FCC2215AE.....£20 FCC2015BE.....£10 FCC2215BE.....£10 K30 FRONT PANEL TEL-TEX TYPE £5.00 NEW G11 LINE OP PANEL £8.00 PHILIPS YEARS AHEAD THE CREDIT CARD CALCULATOR Solar Powered £3.75 NEW PHILIPS SBC 1R33 Solar & Battery Powered Calculator £8.00 THORN PANEL TX9 REC. & REMOTE PANELS with Mains Trans £5.00 TX10 REC. & REMOTE PANELS with Mains Trans £5.00 TX100 FRONT PANEL £3.00 TX10 TUBE BASE ON PANEL £3.00 TX91F £2.00 THORN PANEL No.515-353, 548.02, 565-01, 509/102, 515/173, 509/161 £5.00 THORN TX STEREO SOUND O.P. PANEL (I.C. TA727P) £1.00 THORN VIDEO AERIAL AMP 01 M4-597401 £6.00 ULTRASONIC TRANSDUCER 15p IN LINE 12-35 VOLT SUPPRESSOR 4,000 MRD 20p		CAMCORDER SANYO NP22 6v 1300mah Rechargeable Battery Pack £6.00		PB500 Panic and Button Transmitter 180MHz £1.00 G11 CAP 250V, 470M £1.35 NOT WORKING NEW PROFESSIONAL SATELLITE NO HAND SET METAL CASE WITH METER, DOLBY CHANNEL C WITH POLARIZER SUPPLY £20 £5 post SEND FOR DATA AND PHOTO			
TX100 REMOTE PANEL No.56413IC M293B/and SAA5012 £10 etc		Philips Stereo Headphones No. SBC 3140 £4.00 144MHz Changed Over Relay Aerial 50p THICK FILM HITACHI HM9205A £4.00 TX 85 FERGUSON BATTERY MAINS CONVERTOR £5 each TX9-TX100 FRONT PANEL £5 WITH REMOTE £10 NON REMOTE 8 push button £10		Gas Soldering Irons Variety Nickel Cadmium Batteries from Telephone Type to Sub-C.50p per cell Mainly in packs of 6 to 8 New Type £10.00 THORN FRAME IC TX100 etc IC TDA 3652 IS OBSOLETE REPLACEMENT TDA 3654 £2.00			
NICAM UNIT — Ferguson made for ICC5 Chassis — home market and export — has circuit diagram and can be converted to most sets — £15.		PHILIPS UNIVERSAL BATTERY TESTER 5BC 1695 £5.00 BATTERY CONVERTER FOR TA185 FERGUSON TX85 £8.00 ONE I.C. K35 Decoder £10.00 PHILIPS Desk Calculator £7.00 REGULATED PWR. SUP. 500MA 1.5V-12VDC switched + & - £5.00 ITT Tuner & IF Can HF-module 2 UK £10.00 KT3-K30 IF £5.00 STR5481 £5.00		SALORA 19" RACK MOUNT SAT RECEIVER with Variable Tuning £30.00 Post £5 00 STEREO SOLAR RADIO VHF AND MW £10.00 COST £25 PHILIPS METER ANALOG £9 G11 470 MFD 250v £1.35 CASSETTE SCART MAINS Socket, Print LEADS 30p Type 20p TELEPHONE EXT. LEAD 3 Metre 30p LEAD SCART TO D PLUG 50p BRIDGES RECTIFIER Mixed BR-31 to 34 2 Amp to 5 Amp 8 for £1.00 NEW LUXOR SATELLITE ANTENNA POWER DRIVER £15.00 T6070V TX9 Transistor £1.00 1 METRE SCART LEAD £1.00 VIDEO SCART TO SCART ALL PIN, LONG LEAD £3.00 ALL PINS TX90 TX925 TX100 Mains Switch with Stand-by and Lead 50p each TDA 3562A 10 off each £1.50 UHF Modulator MPM8010 30p			
LARGE Foacs Pots. Fits Pye, GEC, ITT, Decca 75p BSB SAT/REC HALF COMPLETED. CHASSIS, TUNER AND MOD £5 + Post £3 GLASS BEADS Diodes 20K/1.2A 50 for £1.00 G11 LOPT Panel £4.00 G11 Tip Switch £20.00 G11 IF Panel £3.00 G11 Decoder Panel £2.00 G8 Push Button Unit £2.00 G8 Con/Panel New Back Type £4.00		PHILIPS NEW TYPE U/V HANDSET £10 MIXED TOSHIBA HAND SETS FIVE FOR £12 EACH 10 off £1.00 MDA2062		DECODER C-CAM PHILIPS MADE for K40 CHASSIS IC No. TDA 3590 Colour Monitor £5.00 RGB CONVERTER £20.00 TV - Video - Hi-Fi Video in: R.G.B. out in black metal case with black knobs 56420A 20A/600V THYRISTOR £1.75 LCD VIDEO AMSTRAD HANDSET for models 1900 £8 each ITT BG2032-642A TRIPLER £5.00 ITT/NOKIA RF IF MODULE £20 COAX PLUG TO PHONO LEADS £1 SCART TO SCART LEAD £1 TV GAMES AERIAL VIDEO COMBINER SWITCH £1.50 MIXED 20 BRIDGE RECTIFIERS (1 Amp to 5 Amp) £1.50			
LATEST VIDEO For Latest Philips, GEC, Pye and Hitachi. Front panel with memory chip and push button and pots and LEDs £6.00 NEW		Have you got Acid Rain in your garden? PH METER Video Power Supply for Amstrad. Last year mods. Mains Transformer for Amstrad Video £5.00 25p (£1 post) DAMAGED AMSTRAD 1640 Colour Monitor Chassis £6 + post £3.		FERGUSON CHASSIS IKC 2712 £20 IKC-2000 £20 IKC-2705 PALSECAM/NTSC £20 TX89 £20 TX98 £20 GEC HITACHI DECODER PANEL TBA810AS, TBA120, HA1215A, UPL1365 £10 SCART TO SCART LEADS TX90 REMOTE PANEL IC TMS1000 AND M293 £12 5 Mixed VIDEO MOTORS £5.00 SATELLITE TUNER UNIT 2427611 with Base Band, Video Out £15.00 TX10 8 way button unit £8.00 24v 0.24v 3amp MAINS TRANSFORMER £3.00 10 MIXED FERGUSON CIRCUIT DIAGRAMS £5.00 MSH1FC109 £7.77			
2433752 2432984 2432871 2432301 2435016 2433952 2434393 2432211 T9088A D5T83B243 TFB3069D K41, O.P.T K35 L.O.P.T K40 2433452 2432904		SPLIT-DIODE 2433752 £15 TX100 Green Spot £15.00 TX100 Yellow Spot L.O.P.T £10.00 TX90 White Spot L.O.P.T £15.00 Split Diode 110° £12.50 Onion 65-3M GEC 78-9793-6 TX9 Transistor 2432101-2 £5 2434141 EACH 2434492 £10 2435066 2434493		36761 TFB4023AD £10.00 2692120/10 37051 CTK Lopt 36212 33651 36072 36362 36482 36761 36831 36832 36833 3692179 3692279 TX85 2435701 2434393 2435016 2435014 £10 TRANSFORMERS 2435701 £10 2435012 £10 FERGUSON 47003481 £10 AMSTRAD LPTS £10 TFB3069D EQU TFB4009AN			
24327655 AT207671T AT208115 RCO ST CT3325 OT2041 FB16SKA Onon CVC 820 207651 2432461 2433451		SHARP MSH1FC109 £10 EACH 0004-235 002-01 FIT MOST SETS New Thorn Hand Set Type u/v (£10) VIDEO MOTOR for VT568 type £8.00 VC621D8 AMP TUNER IF for VT568 Hitachi & GEC £9.00		BRIDGE RECTIFIERS 10 FOR £1.00 4 Amp for Video Power Supply			
SATELLITE TUNER 950MHz-1750MHz £5.00 TTT PANEL CMC 301 CMC 113 CMC 302 CMC 115 CMC £5.00 303 CMC 904 VIDEO LEADS 4 for £1 SEL ITT IFB254F/2 Front Panel £15.00 DECCA — GEC — ITT 6 push button £5.00		BURGLAR ALARM £2.00 with siren 9 VOLT RELAYS 35p 5V-12V-24V-48V Large and Small 25 Way Plug and Socket with Case £1.50		KIKUSYI 20 MHz OSCILLOSCOPE (5020) £200 40 MHz OSCILLOSCOPE (5042) £250 60 MHz OSCILLOSCOPE (7060A) £1000 12V/1 AMP POWER SUPPLY WITH MAINS PLUG £4 PHILIPS HALOGEN LIGHT, NEW, NO ON/OFF SWITCH, NO HANDLE WITH CORD, BLACK IN COLOUR £5 PHILIPS HAND SET G11 TEXT IN RED HAND SET £15.00 G11 HAND SET ULTRASONIC £10 PHILIPS RC5 EASY CONTROL £10 TRV3 Amstrad Cassette Mechanisms. New with 2 motors and sound head. £15 TVR3 Power Supply. £5. Amstrad Television Tuner UHF. Small, Fits most Amstrads. £6.			
SENDZ SEE BACK PAGE		PHILIPS SBC 522 RGB1 GENERATOR £90 PHILIPS SBS 850 ANALG MULTIMETER £11.50 PHILIPS SBS 521 RF SIG GENERATOR £90.00 FERGUSON TX110 — IK2 and IK7 MANUAL £1 each		FERGUSON ICC5 STEREO O.P. PANEL ICs TDA4805 TDA8421 TBA1204 £10		NICAM MkII KIT MODULE £20.00 with data Burglar Alarm Has time delay to set £2 Mains Transformer £4.00 240v in 110V to 120v out 1 amp post £3	

SENDZ COMPONENTS

TO ORDER SEE BACK PAGE

LA11440	£1.00	Voltage Regulators	30p	CMC 302 Panel with TC mains switch etc	£5.00	GRUNDIG TRIPLER BG-2032-642-3002 £5
TAA7750 HA 411485 UPC1373 M58657P M491BB1 M50441/550 M58658P	50p £1.00 50p £1.00 £3.00 £1.00 £1.00	+5V/UA78P05SC -8V/79M08c +6V/78M08c LM 317T LM 337 LM 342/18 LM 340T 5 0 +12V/LM 340T12 +18V/MC78M18 +24V/78M24 MC 7724cp MC 7824	30p 30p 30p 30p 30p 50p 20p 30p 30p	Turntable Satellite Modulator Sound 5.5MHz MPM 100UT Sound 6.0MHz MPM 1040	£1 £1 £1	
Receiver TX100 Panel I.C. No. SAB3035 -MAB8440P D066 -SAA1060 -PCF8571P		Power Supply for Sinclair Spectrum +2	£5.00	Safe Block	£5.00	TOSHIBA REMOTE CT9123 £4
20 off £2.00 High Voltage Condenser IN5 to 8NZ 1500V to 2KV	£2	Bush Thyristor RCA 76122 Transformer 240v/20v-500Ma Chassis type Transformer 240v/12 Volts 500ma CVC 20 tube base Tube base Rank & G11	£1.00 75p 75p £2.00 £1.20	FEROX RF Filter Clamp for CoAx Cable	Cost	TV GAMES COMBINER SWITCH £1
TX9 C CAM Decoder	£5.00	BRIDGES	30p 30p 30p 15p 15p 20p 30p	Ferguson TX85 TX86 Switch Mod Transformer TX98	£2.00 £2.00 £2.00 £2.00	AMSTRAD SANKYO CAPSTAN MOTOR 6,000 £3
4 Types Fidelity front panels with i.c. & parts	£2.00 each	KBL 005 KBL 02 KBP 04 W02 W004 W005 800V Bridges 2 1/2 Amp	30p 30p 30p 15p 15p 20p 30p	ICCS Ferguson Switch Mod Trans 3112-338-32642	£4.00	AMSTRAD LOADING MOTOR 6,000 £1
BB 103 BB 105A x12 BB 105B x12 BB 105G x12 BB121a	10p £1.00 £1.00 £1.00 10p	K30 Drawer Ass with pots cable forme	£1.00	ICCS L.O.P.T. DST 88B243 DST 85B243 Thorn Mixed	£10.00 each £10.00	HAND SETS FOR 6000 SERIES AMSTRAD FOREIGN ORIGON £4 WITH LED
1A/1600V DG3P EQV -BY228 2 amp bridge rec. wire end SKE4G202 Eqv. BYX71/600 500ns	10p 10 for £1.00 15p 15p	Modulator for Ferguson Sat Receiver 5.5Meg or 6Meg	£1.75	Ferguson Hand Set ICCS Mod IK2000	£8.00 £8.00	TOSHIBA REMOTE CT9233 £3
3 Way regulated adaptor 240V 6V/ 7.59V/30mA Rank Toshiba preb unit 0354 4 Push button unit preb 6 Push button VHF/UHF for v/cap. GEC - Decca type 7 Push button for CVC5 IIT KT3 1/2 Push button unit KT3 (Export) 12 P B u 6 Push button Unit Thorn 6 Push button GRC 6 Push button PYE 731 1 hearing aid unit Rank Z718 4 P/B Unit MECH1 7 Button Unit GEC with Lamps 697 Push Button Unit Z916B panel T513AP panel	£3.50 £9.50 £1.00 £7.00 £8.00 £2.00 £1.00 £6.00 £6.00 £3.00 £4.00 £7.00 £6.00 £5.00 £5.00	Radio Telescopic Aerial	£1.00	Special Price RC4001 KT3 and Teletex TX10 Hand Set Text TX9 with Text TX9 & TX10 button print TX10 Focus Pots	£13.00 £14.00 £12.50 £12.50 £2.00 £5.50	TOSHIBA TV TUNER. IF ENV 57836 G2F £3
TT14 GEC TEX-DECODER 13 IC Panel with cable form	£9.50	De-solder pump + 2 nozzles Philips	£4.00	Mains Stand By Switch with Coil	£1.00	PHILIPS K35 ETC 12 WAY SWITCH WITH KNOBS 50p
PHILIPS Decoder SAA IC 5020-5030 S940B-5050 K40 Text Panel	£8.00	Flat Red LED and Green	5p	PHILIPS UNIVERSAL HAND SET £12.00 RC5 KT3 - K45 - £10.00		60.40 SOLDER 500G £3.75
ICCS TUBE BASE ON PALEL ICCS DECODER PANEL	£5.00 £15.00	K30 Thermistor 232266298009	75p	TEXT-TYPE Replace 1 Hand Set for Philips KT3-K30, K4 etc	£12.50	AMSTRAD 4.600 FOREIGN ORIGIN HAND SET £3
K35 Decoder K35 Sound OP Thick Film Daughter Kit3 33122-127-43891	£8.00 £4.00 £3.00	De-solder Pump	£2.50	THORN HAND SETS 9000 - 9600 - TX9 - TX10 - TX100 Text and Non-Text	£10.00	AMSTRAD VIDEO FRONTS WITH FLAP LONG CHASSIS ALL MODELS MADE IN 1991 TO 1992 AND DECCA PRO LINE £4
12 CH. K30 Tex Rec Front Panel with I.C.	£5.00	Gas Soldering Iron	£12.00	PHILIPS RCS171 (HAND SET)	£12.00	AMSTRAD - LONG CHASSIS AND SHORT CHASSIS POWER SUPPLY £4 MODELS 1991 TO 1992
Plug in K4 Focus Pot K40	£1.00	Hill Meter Leads, S/Rubber and Probes	£4.00	K35-K4 HAND SET Repaired for £5.00		DOUBLE DECKER SWITCH MODE £8 POWER SUPPLY
Fidelity Tube Base with transistor & focus pot	£1.50	85-4538-3 Tatung GEC 8 Button Unit Print Type 1990 to 1992	£5.00	SANYO MAGMTRON Type 2M218H	£10	DOUBLE DECKER CHASSIS. ALL PANELS £5 each panel
TX10 Tube Base on Panel	£3.00	Philips Handset IC SAA3010P MAB8461/WO63	£3.00 £3.00 £3.00	Microwave Oven Condenser 1.5 MFD 2KW	£3	AMSTRAD LONG CHASSIS DISPLAY PANEL 1992 TO 1993 £4
PHILIPS HAND SET K35-K4-K40, etc	£10	MAB 8420P-C031 MAB 8400B-6 MAB 8440P-D070 MAB 8440P-D033 MAB 8440P-D056 MAB 8441P-T001 MAB 8441P-T132	£3.00 £3.00 £3.00 £3.00 £3.00 £2.00	10 Panels Ferguson Mixed from TX9 to ICC5	£20	AMSTRAD TUNER UE33-B01 £3 IF £2
THORN CASSETTE HOUSING PAS26805U	£18.00	M58484P	£2.00	TV Aerial Ring Type	40p	PHILIPS INFRA RED RECEIVER IN-CAN 1990 50p
LITHIUM BATTERY BR-23 Volts	20p	FERGUSON ICs Ferg-TX982 TMP47C 634N 2685 ST6391B1/B2 ICC7	£3.00 £3.00 £4.00	TX100 Remote Hand Sets	£6	
TUNER. SAT 2000 KHC	£8	CMC 301 front panel CMC 303 front panel	£5.00 £5.00	Philips Video Remote Hand Set Works most sets. No L.C.D. Display	£6	
MIXED FUSES 1/4 AND 20mm and Black Print Type 100 off £2		International Rectifier EHT Diodes G770/IV34 6KV 6A/600V Stud Diodes 6A/1000V Stud Diodes	3 for 8p £3.00 10p	ITT-Nokia Tuner IF RF-IF-Module 5829 02 58	£6	
		6A/1000V Stud Diodes	20p	SEL-ITT HF-Module 2 UK 5828-04-10	£6	
		6A/1000V Stud Diodes	20p	01 M4-412-001-RU1 8 Way Pre sets for TX10-TX100	£3	
				01 V6-251-002 Text Panel ICC5 Ferguson	£10	
				Sharp Tuner and IF 1810587 PAL1 UK	£3	
				Tuner IF UE30-BO 3 Amstrad	£3	

DIODES		Voltage Regulators		SENDZ COMPONENTS		ML926		TBA1440C		TDA3565	
Bridge KBF-08	40p	+5V UA78P05SC	30p	CV 8617	10p	BD646	50p	TBA1440C	£1.00	TDA3565	£3.00
BY 26	10p	+8V 79M08	30p	Y 716	10p	BD939	30p	TBA200Q	£2.00	TDA2575A	£1.00
BY 127	10p	+6V 78M06	30p	Y 729	30p	BD948	30p	TBA200Q	£2.00	TDA2577A	£2.00
BY 133	10p	LM 317T	30p	Y 730	30p	BD131A	30p	TBA200Q	£2.00	TDA2578A	£2.00
BY 134	10p	LM 337	30p	Y 827-6A/1KV	20p	BDV68	30p	TBA200Q	£2.00	TDA2581	£2.00
BY 176	25p	LM 342L8	30p	Y 860	30p	BDV65	30p	TBA200Q	£2.00	TDA2591	£1.00
BY 179	25p	LM 340T 5.0	30p	Y 933	30p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 184	25p	+12V LM 340T12	50p	Y 969	30p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 187	10p	+18V MC78M18	50p	Y 997	30p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 190	40p	+24V 78M24	30p	Min 12 volt Relays	75p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 196	30p	MC 7724p	40p	R 1038	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 198	10p	MC 7824	40p	R 1039	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 204/4	8p		30p	R 2009	80p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 206	8p		30p	R 20106	£1.00	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 208/800	8p		30p	R 2029	50p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 210/400	5p		30p	R 2210	30p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 210/800	5p		30p	R 2257	60p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 223	10p		30p	R 2305	50p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 224/600-4.8A/600p	50p		30p	R 2306	40p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 226	15p		30p	R 2322-2323	pair 80p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 227	15p		30p	R 2325	15p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 228/1500p	15p		30p	R 2396	50p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
Flat BY229/black	15p		30p	R 2461	80p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 229 Rcd	30p		30p	R 2030	50p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 229/400	30p		30p	R 2433=BD124	30p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 229/800	30p		30p	R 2540	£2.00	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 237	30p		30p	R 2737	40p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 254	10p		30p	R 2738=TP141	40p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 255	30p		30p	R 2739=TP141	40p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 298	10p		30p	R 3129=TP147	40p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 299	10p		30p	BYW 56.2A/1000V G11	8p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 306	10p		30p	BYW 205/0	15p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 406	10p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 527	20p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 407a	10p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 448	10p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 100/200-5 amp	10p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 527	10p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY 602	10p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BY V 26C	10p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
F347	5p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
GP20	5p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
GRP81G (TX10)	10p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
XK 3102	50p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BYV 2K200	20p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
Bridge TX10/800/3 amps	40p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
KBF3542 Bridge	£1.50		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
Bridge Rec. D35B10	40p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BYT17800	12p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
Hitachi sets etc.			30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
STR454	£2.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
STR620	£6.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
S 200A/F line o.p.	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
2SC941	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 105/04	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 108	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 124	50p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 126	50p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 180a	65p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 204	60p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 205	75p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 206	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 207	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 208	80p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 208A	75p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 208D	90p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 222	50p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 326	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 407	60p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 500D	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 508A	90p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 508AF	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 508D	80p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 705	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 806A	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BU 807	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BUK 454/600	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BUK 824	50p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BUK 84	50p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BUW 84	60p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BYW 20/08-9	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BYW 95	10p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BUX 39/25A-150V	£1.00		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BUX 84	10p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
BYV 9	20p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
T.C. 106a	30p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
TIC 116m	30p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
TIC 116m Y 1003	30p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
TIC 126N	30p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
TIC 126S	30p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
TIC 226E	30p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
TIC 226m	30p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
TIC 236m	30p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
IAG 226/600	30p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
TKCV 106D	30p		30p	BYW 90A	10p	BDV68	30p	TBA200Q	£2.00	TDA2593	£3.00
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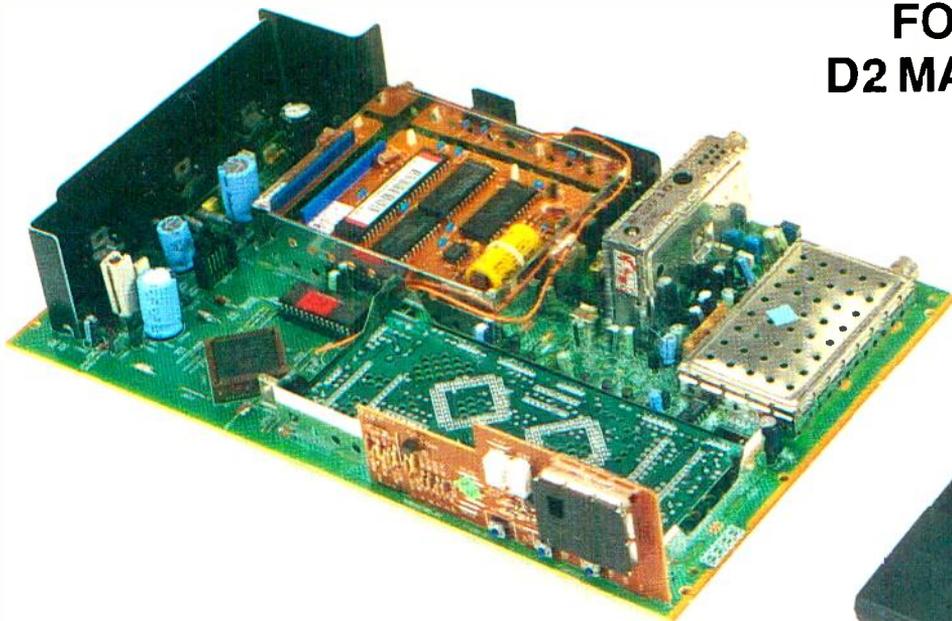
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